

Robotic Fundamentals: Serial and Parallel Robot Kinematics

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ABSTRACT

This report contains details, results and analysis for a series of simulations created to investigate the kinematics of serial and parallel robots. For the serial robot, the forward and inverse kinematics are derived and used to simulate a drawing task with both linear and arcing motion. The reachable workspace is derived. A bug2 algorithm is implemented for obstacle avoidance. For the parallel robot, the inverse kinematics and workspace are derived and displayed. Investigation into avoiding failure due to singularities is made. Simulations are created in MatLab, the original code can be found in the appendices of this report, or at the Author's GitHub repository: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots

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I. INTRODUCTION

Forward and inverse kinematics provide the ability to control and position robots in real space. Simulation allows testing well as quickly viewing the results of changes to code, without risk of damaging expensive equipment.

The serial robot simulated in this project is the LynxMotion ALD5 Robot Arm (*lynxmotion* n.d.). This robot has five degrees of freedom (DoF), counting the final rotating prismatic joint which does not affect the spatial position of the robot's end effector. The parallel robot simulated is in the style of a surgery robot.

This report details the methodology used to create each simulation, before presenting results, discussion and methods to avoid singularities. Conclusions are made including suggested further work. The appendices contain the full original code for each MatLab script created (Finlo Heath 2022).

II. SERIAL ROBOT: INVESTIGATIONS & METHODOLOGY

A. Forward Kinematics

Forward kinematics (FK) aims to derive the spatial position of each joint and the end effector of the robot, given the link lengths and joint angles. This project uses the Distal Denavit Hartenberg (DH) approach to FK (Wang et al. 2014). This requires creation of a diagram of the robot to fill the values in a "DH Table" as shown in FIG. 1. This method is more robust than the modified proximal method, as it does not require imaginary axes in the case that two joints have no physical distance between them.

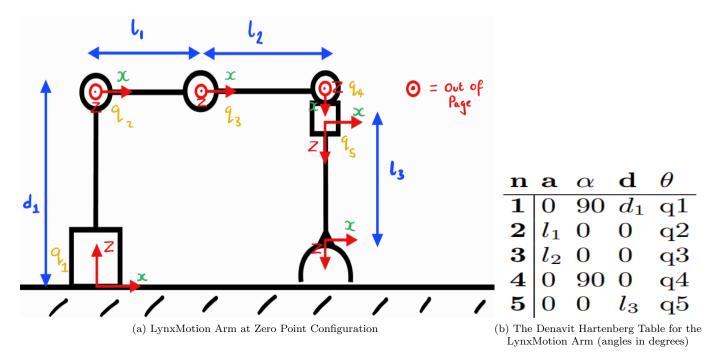


FIG. 1. (a) LynxMotion robot arm annotated with the z-axis of rotation at each joint in the x-z plane of the base. The robot is drawn in it's zero point configuration, meaning that each angle q1-5=0. From this Diagram, table (b) is generated and substituted into the transformation matrix given in FIG. 2 to generate the transformation matrices between each consecutive joint.

Each row of the DH table is applied to the distal transformation matrix shown in FIG. 2, providing the transformation from one joint of the robot to the next. Multiplying in sequence, one can find the full transformation from the base of the robot to end effector, including both the rotation matrix and spatial translation; discernible within the transformation matrix as shown in FIG. 2 (b). In Appendix A, the transformation matrices are given in lines 25 - 53, with the DH table provided above in comment lines 14 - 20. Matrix multiplication - from right to left - is used to get the full transformation from base to end effector on line 62.

To acquire full robot arm motion, one must take the spatial translation component from not only the full base to end effector transformation matrix (lines 109 - 143) but also each of the preceding composite transformation matrices (lines 164 - 240). The spatial position of each joint is plotted at each angle value to give the overall change in motion of the whole arm.

$$\begin{bmatrix} c\theta_n & -c\alpha_n s\theta_n & s\alpha_n s\theta_n & a_n c\theta_n \\ s\theta_n & c\alpha_n c\theta_n & -s\alpha_n c\theta_n & a_n s\theta_n \\ 0 & s\alpha_n & c\alpha_n & d_n \\ 0 & 0 & 1 \end{bmatrix}$$
(a) The Distal Transformation Matrix (b) Rotation and Translation Components of a Transformation Matrix

FIG. 2. (a) shows the generic distal transformation. Each element is substituted for the value in a given row of the DH table (FIG. 1 (b))to find the transformation between two joints connected by a link (Wang et al. 2014). (b) distinguishes the rotation and translation components of a transformation matrix.

1. Testing

Edge cases allow testing that the FK work correctly. Providing each angle value as zero should output the robot arm in the zero point configuration displayed in FIG. 1 (a). Another useful reference position is q1, q3, q5 = 0 and $q2, q4 = \pi/2$, which should place the robot in the straight upward orientation with spatial translation:

$$\begin{pmatrix} 0 \\ 0 \\ d1 + l1 + l2 + l3 \end{pmatrix}$$

A more concrete way of checking that both FK and inverse kinematics (IK) are working is to pick a desired end effector position, run the IK code to output the joint angles, then run these through the FK to check that this code returns the original end effector position.

B. WorkSpace

The WorkSpace of the robot is the full set of coordinates reachable by its end effector (Szep et al. 2009). The dexterous workspace is the subset of these coordinates which the robot can reach in all possible orientations. In Appendix A Lines 275 - 322, the reachable workspace is plotted. Using the full range of motion for each joint, a series of loops plot each point. Any points where the z coordinate is less than zero are skipped, preventing the end effector from moving below the ground surface.

C. Inverse Kinematics

IK takes an input of the end effector's orientation and position, outputting the five joint angles (q1-q5). This can be done entirely using trigonometric analysis of the robot; this is illustrated in FIG. 3.

q1 is derived using FIG. 3 (a). q5 has no bearing on the spatial position of the robot, only the rotary orientation of the end effector. Hence it is given as in input.

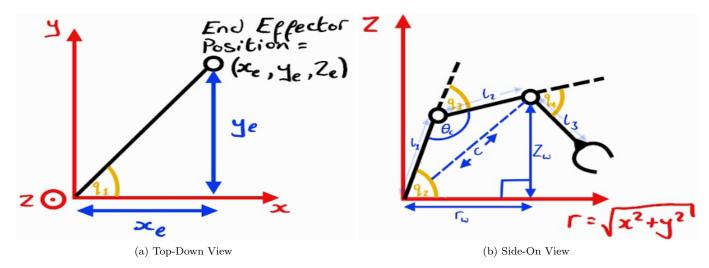


FIG. 3. The top down view allows one to find q1, the side on view allows for one to directly find q2 and q3. q4 is then found using the equation for ψ .

The remaining angles, q2, q3, q4 are derived by modelling the mid section of the robot as a three joint planar robot and using trigonometric identities, displayed in FIG. 3 (b). With a few exceptions, there are multiple orientations the robot can have to reach a given position. This orientation is defined by

$$\psi = q2 + q3 + q4$$

For this reason, as shown in Appendix B lines 26-27, the full range of possible values for ψ are used. Imaginary results are filtered out and a list of all real sets of possible angles are printed.

D. Task Completion

The chosen task was for the robot to draw (move to) the eight corners of a cuboid in 3D space. Completing the task is done using the following approach:

- 1. The points that the robot must move to are provided in a list.
- 2. IK are run to acquire the joint angles for the robot at each of these points
- 3. FK are run to acquire the position of each joint at these angles
- 4. The full robot orientation is plotted at each required point.

E. Trajectories and Obstacle Avoidance

Appendices D, E & F provide MatLab files for the three paths. The robot was modelled as operating at 10Hz, with a 1 second travel time between each point, meaning the trajectories display ten intermittent points between each corner of the cuboid. While a real robot must operate at far higher frequencies, this was deemed sufficient for this simulation.

1. Linear Motion

Linear motion means the robot end effector moves in a straight line. This was achieved by adding an extra step between steps 1 and 2 in section II D. straight lines are defined by equations of the form y = mx + c. A function was created which takes consecutive points in the list of those the robot must move to, returning the line gradient and

constant.

Ten points are sampled along the line between each of the original points to create a new robot trajectory array. Inverse and forward kinematics are run in sequence as before and the robot motion is displayed in a figure.

2. Free Motion

Free motion means the robot does not have to obey a specific path between each point. To achieve this, the first two steps of the method in section IID are followed. Consecutive sets of angles output by the IK are samples for ten intermittent points. FK are run on this expanded set of angles and the output is displayed, showing arcing as opposed to linear motion between points.

3. Obstacle Avoidance

The free motion trajectory was used as the starting point for the obstacle avoidance. As well as defining the points the robot must move to, the obstacle is defined as well. The chosen obstacle is a small cuboid in the path of the robot's trajectory. The inverse and forward kinematics are run, to find the full path of the robot with no diversion.

A function was created which samples the trajectory of the robot and discerns where it first impacts and leaves the obstacle. The function returns a path for the robot to move from its impact point, over the surface of the obstacle, to the point at which it leaves the obstacle, emulating the bug 2 algorithm (Yufka and Parlaktuna 2009). This new path is inserted in place of the previous path.

III. PARALLEL ROBOT: INVESTIGATIONS & METHODOLOGY

A parallel robot operates with multiple arms at different positions on the base, rather than a single base to end effector chain. The parallel robot in this study operates in the horizontal (x - y) plane. It has three identical arms each comprised of two joints attaching to a separate corner of the triangular end effector and base.

A. Inverse Kinematics

IK were solved by modelling the robot as three identical serial robot arms with different bases and at different angles to the end effector. This allows one to solve the IK for a planar three DoF arm and apply this to each of the arms in sequence. For each arm, the position of it's base is taken as the origin in that arm's frame, and the position of the end effector is shifted to it's coordinate in that arm's frame.

The angle of the arm to the end effector is the third joint angle, q3 and is fixed based on the end effector angle, a. For the first arm, $q3 = a + \frac{\pi}{6}$ as this is the angle from the x-axis to the centre of the end effector. The end effector is an equilateral triangle, hence $\frac{\pi}{6}$ is the angle between it's edge and the vector to it's centre point. For the second arm, this angle is the same except offset by an additional $\frac{2\pi}{3}$. The third is offset by $\frac{4\pi}{3}$. This occurs as the angle is always measured from the x-axis and the arms are set $\frac{2\pi}{3}$ apart on the end effector.

Once the relative end effector position and angle of the arm to the end effector is found, a function outputs the possible values for the first and second joint angles. These form an "elbow" joint which can each have two values for a given position. This function can be viewed in Appendix G lines 343 - 360.

B. WorkSpace

The file created in section III A was adjusted to take a large range of end effector positions. All imaginary results are removed, all real results are plotted to show the workspace for a given end effector orientation. Greater end effector angles require more taut links resulting in a smaller workspace.

IV. SERIAL ROBOT: RESULTS, ANALYSIS AND DISCUSSION

Across all simulations, link lengths of the robot are set to 0.1m.

A. Forward Kinematics

The full analytical solution for the FK of the LynxMotion robot arm is a large 4×4 transformation provided at the start of Appendix A. One can be sure it is correct as it provides the expected results when given edge case angles. Two examples of this are shown in FIG. 4.

$$egin{bmatrix} 1 & 0 & 0 & 2 \ 0 & -1 & 0 & 0 \ 0 & 0 & -1 & 0 \ 0 & 0 & 1 \end{bmatrix} egin{bmatrix} -1 & 0 & 0 & 0 \ 0 & -1 & 0 & 0 \ 0 & 0 & 1 & 4 \ 0 & 0 & 0 & 1 \end{bmatrix} \ _{q_1=q_2=q_3=q_4=q_5=0}^{(a)\ T_e\ for} & q_1=0, q_2=90, q_3=0, q_4=90, q_5=0 \end{pmatrix}$$

FIG. 4. (a) shows the specified T_e matrix for the zero point of the robot, matching the configuration shown in FIG. 1 (a); z axis translation cancels out, leaving only translation along the x axis. (b) shows the specified T_e matrix when the robot angles are set for it's max height; all four links point translation along the z axis.

Testing this with a series of positions, the following figure is generated:

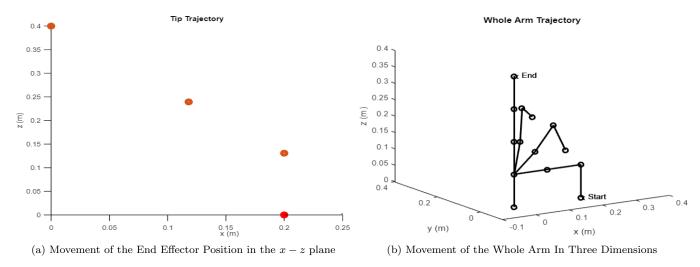


FIG. 5. (a) shows the motion of the end effector only and in the x-z plane. (b) shows the same motion for the whole arm from a three dimensional viewpoint.

FIG. 5 shows the robot beginning at the configuration given by the matrix shown in FIG. 4 (a) and ending at the configuration given by the matrix in FIG. 4 (b)

B. WorkSpace

FIG. 6 Shows the comprehensive workspace of the LynxMotion arm, operating on a flat surface. The workspace is hemispherical since the robot cannot pass through the ground. For the main figure, FIG. 6 (a), each joint is incremented in steps of 15 degrees, steps of 30 degrees are used for (b) and (c); the 15 degree plot was too computationally intense for perspective changes. The true workspace is a continuous area enclosing the points shown in the figure.

Workspace

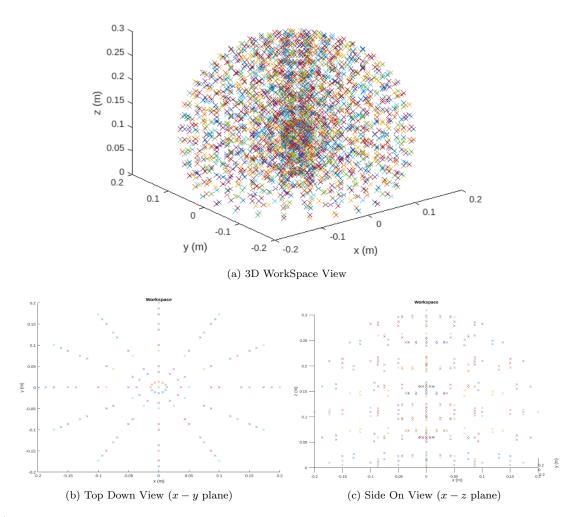


FIG. 6. (a) displays the three dimensional figure showing the workspace of the LynxMotion arm on a flat surface with all link lengths equal to 0.1m. (b) and (c) show a top down and x-z planar view respectively.

C. Inverse Kinematics

The inverse kinematic output consists of five joint angles acquired from an input of the end effector spatial position and orientation. The position is given by coordinates x, y, z. The orientation is given by end effector rotation of μ and angle to the horizontal plane, ψ .

The following values for each joint angle were derived:

$$q1 = \arctan(\frac{y}{x})$$

$$q2 = \arctan(\frac{z_w}{r_w}) + \arctan(\frac{l_2 sin(q3)}{l_1 + l_2 cos(q3)})$$

$$q3 = \arctan(\pm \frac{\sqrt{1 - D^2}}{D})$$

q3 is found first of q2, q3 & q4, the value of D, $z_w \& r_w$ are derived in Appendix B lines 70 - 78. As there can be two values of q3 for each orientation, it follows that there can be two values of q2 and q4. After finding values for q2 and q3, one can find possible q4 values for each valid ψ value by rearranging the ψ equation for q4,

$$q4 = \psi - q2 - q3$$

$$q5 = \mu$$

Example results for four end effector positions are given below, including the two edge cases we have looked at in section IV A:

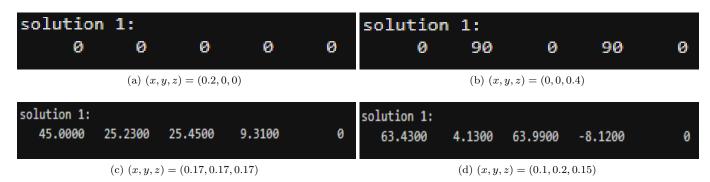


FIG. 7. Output of the Inverse Kinematics file shown in Appendix B. The sub-captions display the input coordinates, the joint angles are output in order q1-5. The final angle is always zero as $\mu=q5=0$ is chosen.

We can see that FIG. 7 (a) and (b) return the input angles given in FIG. 4, and extensive testing corroborates that the forward and kinematics output the inverse kinematic input and vice versa. For each figure in FIG. 7, with the exception of (b) which can be reached in only one orientation, the program outputs multiple possible solutions.

D. Task Completion

The task of plotting the points of a cuboid was successfully carried out by the arm, as shown in FIG. 8. This is also confirmed by the printed output of the file. A check is done to see if the desired points array is identical to the array output for the arm to follow. As long as the desired points are within the workspace, the arm is always successful.

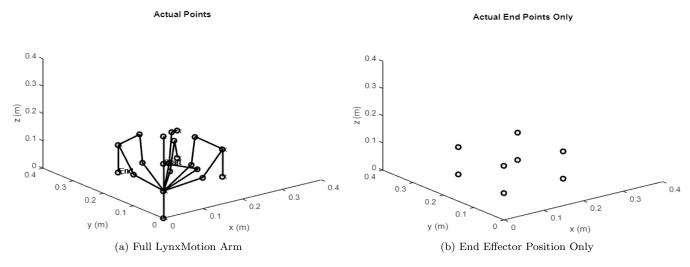


FIG. 8. This figure displays the arm outputting each vertex of a cuboid as required by the set task. (a) shows the full arm, while (b) confirms the endpoint position only.

E. Trajectories and Object Avoidance

When running the MatLab files, each of the trajectory plots are animated, showing robot motion. The task remains identical, but now the robot's path between each cuboid vertex is plotted.

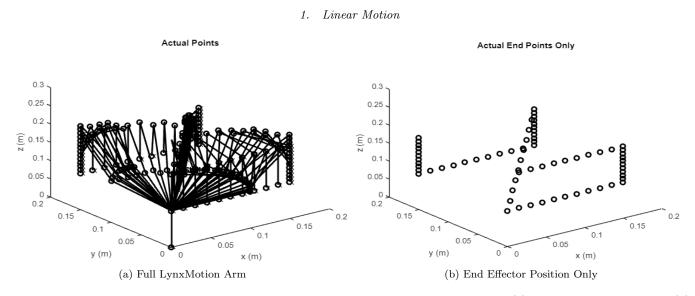


FIG. 9. The robot simulated moving in a linear path between each required vertex point. (a) shows the full arm, while (b) confirms the endpoint position only. The robot begins at (x, y, z) = (0.0, 0.0, 0.2) and finishes at (x, y, z) = (0.0, 0.15, 0.2).

Linear motion is simple to achieve in two dimensions but more complex in three. To speed up the program, the equation function filters to check for lines which pass along each axis first as the gradient and constant are more quickly discerned. This is shown in Appendix D lines 404 - 445.

2. Free Motion

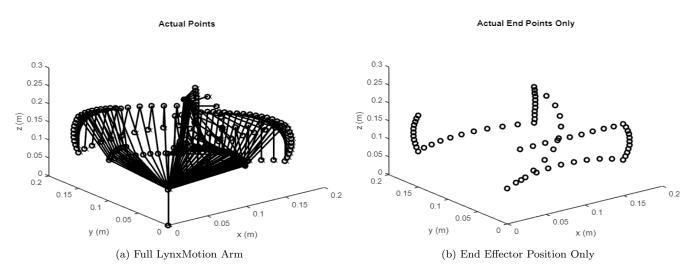


FIG. 10. The robot simulated moving in an arcing path between each required vertex point. (a) shows the full arm, while (b) confirms the endpoint position only. The robot begins at (x, y, z) = (0.0, 0.0, 0.2) and finishes at (x, y, z) = (0.0, 0.15, 0.2).

The arcing effect is created with the increment of each joint angle equally as the arm moves between two points.

3. Obstacle Avoidance

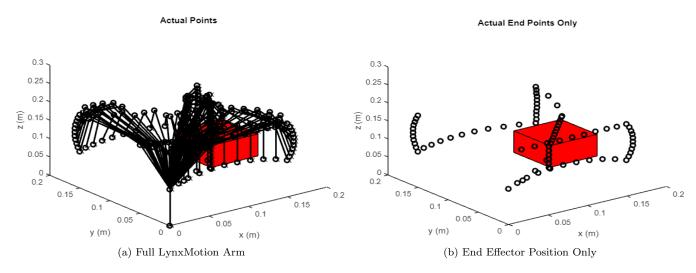


FIG. 11. Free motion of the robot, with bug2 obstacle avoidance implemented. (a) shows the full arm, while (b) confirms the endpoint position only. The robot begins at (x, y, z) = (0.0, 0.0, 0.2) and finishes at (x, y, z) = (0.0, 0.15, 0.2), diverting it's path to move around the red cube.

The red cuboid interrupts the arc of the robot. Once it reaches the obstacle, the robot alters it's path and traverses the obstacle surface. The solution is general, the obstacle position may be moved and the robot will still traverse

across it. While inefficient, it is necessary to re-run the entire inverse and forward kinematics once the end effector path across the obstacle has been determined. Without this, the joint positions of the robot would not change while it traversed the obstacle - the link lengths would not be constant and the simulation would be inaccurate.

V. PARALLEL ROBOT: RESULTS, ANALYSIS AND DISCUSSION

The parallel robot end effector is shown in dark blue. The three arms are cyan and the base is red. This simulation is completely general. FIG. 12 shows the two opposite configurations, six more can be made as combinations of these two. The end effector remains in the same position despite the differing arm angles.

A. Inverse Kinematics

Readers can test other inverse kinematic solutions by running the file given in Appendix G. The end effector is drawn by connecting the positions of the third joint on each of the arms. Since this always results in an equilateral triangle of side length $\sqrt{3} \times 0.17$ - the defined shape of the end effector - one can be sure the result is correct. If the user requests an end effector position which is outside the workspace for the given angle, the error message, "Chosen Position is outside of robot workspace.", is provided.

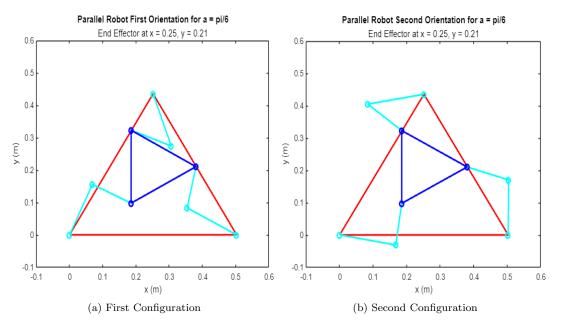


FIG. 12. Two configurations outputting the same end effector position. The two configurations each use the alternating "elbow" possible with the arm links, there are eight different configurations possible overall.

B. WorkSpace

In FIG. 13 we see that the end effector angle, a, has a significant effect on it's workspace. The convex hull enclosing the points would suggest a circular workspace for a = 0, however the plotted points show that the end effector cannot reach segments of the circle toward the corners of the base triangle. This is because the arms opposite to these corners reach their full extension at these points. For $a = \frac{\pi}{6}$, the workspace shifts in the direction of the angle, increasing on the right side of the robot but decreasing it on the left.

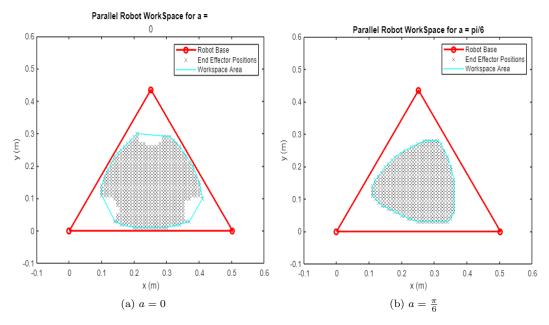


FIG. 13. The full workspace for the parallel robot with the end effector angles a = 0 and $a = \frac{\pi}{6}$ to the horizontal (x-axis). The workspace is further reduced as the angle is increased.

VI. PART THREE: INVESTIGATION OF METHODS TO AVOID ISSUES WHEN OPERATING THE ROBOT CLOSE TO A WORKSPACE SINGULARITY

Robots can reach singularities during real world operation. A singularity is defined as a point in the workspace at which the robot cannot operate as intended due to a mechanical limitation causing the loss of one or more DoF (Zhao et al. 2021). For example, in FIG. 5 (b), the end point of the arm is positioned straight up, along the z-axis. In this orientation, it can no longer move along the z-axis without moving in the x-y plane too; a DoF has been lost. This is a boundary singularity. This is why many modern robots, such as Boston Dynamics' Atlas, move exclusively with bent legs (Griffin et al. 2018). In simulation, we can solve this issue by adding angular constraints to each of the joints as shown in FIG. 14. This method reduces the overall workspace of the robot, but it ensures the LynxMotion arm avoids the only full extension singularity in its workspace.

```
% Define our set of angles for each joint
       q1_set = [ 0 20 40 45 ]'*pi/180 ; % base can spin full 360 degrees
2
       q2\_set = [ 0 30 60 90]'*pi/180 ; % first p joint can move 0 to 180
3
       q3\_set = [ 0 10 20 30 ]'*pi/180 ; % second p joint can move -180 to 180
4
       q4\_set = [ 0 -10 -20 -30]'*pi/180 ; % third p joint can move -180 to 180
       q5\_set = [ 0 90 180 30 ]'*pi/180 ; % claw can spin full 360 degrees
6
7
       % Robot hits straight arm singularity only if q2 = q4 = 90 and q3 = 0,
8
       % as d1 link must always point straight up.
9
10
       for i = 1:length(q2_set)
11
         if q2_set(i) == 90 && q4_set(i) == 90 && q3_set == 0
12
           q2\_set(i) = 95
13
           q4\_set(i) = 85
14
           q2\_set(i) = 5
15
         end
16
17
```

FIG. 14. Example code to prevent full extension (boundary) singularities in the LynxMotion robot arm.

A second singularity type is the internal singularity, where joint axes of the robot line up perfectly, meaning the links of the robot attempt to occupy the same spatial position. This can cause serious damage to the robot and danger to humans operating it. For this a more robust solution is needed. Singularities occur when the determinant of the Jacobian matrix is equal to zero, det(J(q)) = 0, meaning it's inverse does not exist (Zhao et al. 2021). This is because the Jacobian matrix converts the joint angular velocity (\dot{q}) to end effector velocity (v_e) , and singularities occur when infinitesimal changes in the end effector velocity cause large changes in joint velocity,

$$v_e = J(q)\dot{q}$$

These singularities can be avoided by checking the planned route of the robot against the Jacobian first, and throwing an error before the code is executed if at any point Det(J) = 0, an example is given in FIG. 15. The code in FIG.s 14 & 15 are developed from the Appendix A simulation.

```
% Check each end effector point to ensure it is not at a singularity. Throw an error if it is.
       % End effector position and orientation is defined by T.e transformation matrix.
2
3
       % Use matlab's native jacobian computation.
4
       Jacobian_of_arm = jacobian([T_e], [q1, q2, q3, q4, q5])
5
       % Calculate the general determinant
       Det_J = det(Jacobian_of_arm)
7
       % check each value of T_e_specified to see if Det(Jacobian_of_arm) == 0
9
       for i = 1:length(q1_set(i)
10
         Det_J_Specified = subs(yt_element,[d1 11 12 13 q1 q2 q3 q4 q5], [d1_set 11_set 12_set 13_set ...
11
             q1_set(i) q2_set(i) q3_set(i) q4_set(i) q5_set(i)])
12
         % If it is, stop the simulation and throw an error message.
13
         if Det_J_Specified == 0
14
           error('One of your robot orientation angle sets (position %s) results in a singularity! ...
15
               Please change it and try again.', i)
         end
16
       end
17
```

FIG. 15. Example code to prevent both internal and boundary singularities in the LynxMotion robot arm.

VII. CONCLUSIONS & FURTHER WORK

The simulations created for this project are each successful and written as general solutions. This allows the input parameters to be changed to simulate all possible solutions for each input being provided.

Improvements could be made in efficiency and robustness. Addressing the former, Appendix F is over 800 lines long as both the inverse and forward kinematics are run twice. One could simplify this code by converting the forward and inverse kinematics sections to a function which need be written only once.

Regarding robustness, the linear motion simulation is successful for a wide range of possible inputs, but fails at certain edge cases. The straight line equation is derived as z = mr + c. m and c are gradient and z-axis intercept, $r = \sqrt{x^2 + y^2}$ is the magnitude of movement in the horizontal plane. This method is limited by the fact that it cannot distinguish direction in the horizontal plane. This limitation could be removed by checking the sign of the change in x and y coordinates and using conditional statements to discern the direction. This would be added in Appendix D, in the else statement at line 433.

The parallel robot simulations are both efficient and accurate, making these the most production ready in their current state. Overall, the set of simulations created for this project provide useful and accurate insight into the operation of the LynxMotion arm and parallel surgery robot. They allow for testing of new operations with zero risk to real hardware and demonstrate all possible solutions for a user to achieve a given robot configuration; a valuable tool for engineers working with robots of this type.

Appendix A: Serial Robot Forward Kinematics

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_FK_LynxMotionArm.m

FINN_FK_LynxMotionArm.m

The general solution of the end effector forward kinematics transformation matrix (T_e) is given here. It is a 4×4 matrix where each row is contained within a set of square brackets and separated by a line break. Each column is separated by a comma and a new line. The full file prints this result.

```
T_e =
    1
   2
    3 [\sin(q1) * \sin(q5) + \cos(q5) * (\cos(q4) * (\cos(q1) * \cos(q2) * \cos(q3) -
   4 \cos(q1) * \sin(q2) * \sin(q3)) - \sin(q4) * (\cos(q1) * \cos(q2) * \sin(q3) +
                    cos(q1)*cos(q3)*sin(q2))),
    6 \cos(q5)*\sin(q1) - \sin(q5)*(\cos(q4)*
                   (\cos(q1) * \cos(q2) * \cos(q3) - \cos(q1) * \sin(q2) * \sin(q3)) - \sin(q4) *
    s (\cos(q1) \cdot \cos(q2) \cdot \sin(q3) + \cos(q1) \cdot \cos(q3) \cdot \sin(q2))),
   9 \cos(q4) \star (\cos(q1) \star \cos(q2) \star \sin(q3) + \cos(q1) \star \cos(q3) \star \sin(q2)) + \sin(q4) \star
                        (\cos(q1) * \cos(q2) * \cos(q3) - \cos(q1) * \sin(q2) * \sin(q3)),
11 13*(\cos(q4)*(\cos(q1)*\cos(q2)*\sin(q3) + \cos(q1)*\cos(q3)*\sin(q2)) + \sin(q4)*
12 \quad (\cos{(q1)} \star \cos{(q2)} \star \cos{(q3)} - \cos{(q1)} \star \sin{(q2)} \star \sin{(q3)})) + 11 \star \cos{(q1)} \star \cos{(q2)} + 11 \star \cos{(q3)} + 11 \star \cos{(q3)
13 12*\cos(q1)*\cos(q2)*\cos(q3) - 12*\cos(q1)*\sin(q2)*\sin(q3)]
14
15
                         [-\cos(q1)*\sin(q5) - \cos(q5)*(\cos(q4)*(\sin(q1)*\sin(q2)*\sin(q3) -
16 \cos(q^2) * \cos(q^3) * \sin(q^1) + \sin(q^4) * (\cos(q^2) * \sin(q^4) * \sin(q^3) + \sin(q^4) * \cos(q^2) * \sin(q^4) * \sin(q^4) * \sin(q^4) * \cos(q^4) * \sin(q^4) * \sin(q^4) * \cos(q^4) * \sin(q^4) * \cos(q^4) * \sin(q^4) * \sin(q^4) * \cos(q^4) * \sin(q^4) * \sin(q^4) * \sin(q^4) * \cos(q^4) * \sin(q^4) * \sin(q^4)
17 cos(q3)*sin(q1)*sin(q2))),
\sin(q5)*(\cos(q4)*(\sin(q1)*\sin(q2)*\sin(q3) -
\cos(q^2) \cdot \cos(q^3) \cdot \sin(q^1) + \sin(q^4) \cdot (\cos(q^2) \cdot \sin(q^4) \cdot \sin(q^3) + \sin(q^4) \cdot 
20 \cos(q3) * \sin(q1) * \sin(q2))) - \cos(q1) * \cos(q5),
\cos(q4) * (\cos(q2) * \sin(q1) * \sin(q3) + \cos(q3) * \sin(q1) * \sin(q2)) - \sin(q4) * \cos(q4) * \cos(
(\sin(q1) * \sin(q2) * \sin(q3) - \cos(q2) * \cos(q3) * \sin(q1)),
23 \quad 13*(\cos{(q4)}*(\cos{(q2)}*\sin{(q1)}*\sin{(q3)} \ + \ \cos{(q3)}*\sin{(q1)}*\sin{(q2)}) \ - \ \sin{(q4)}*\cos{(q4)}*\cos{(q4)}
                         (\sin(q1)*\sin(q2)*\sin(q3) - \cos(q2)*\cos(q3)*\sin(q1))) + 11*\cos(q2)*\sin(q1) + 11*\cos(q2)*\sin(q1)
24
25
                       12*\cos(q2)*\cos(q3)*\sin(q1) - 12*\sin(q1)*\sin(q2)*\sin(q3)
26
                 [\cos{(q5)}*(\cos{(q4)}*(\cos{(q2)}*\sin{(q3)} + \cos{(q3)}*\sin{(q2)}) + \sin{(q4)}*(\cos{(q2)}*\cos{(q3)} - \sin{(q2)}*\sin{(q3)})),
                      -\sin(q5)*(\cos(q4)*(\cos(q2)*\sin(q3) + \cos(q3)*\sin(q2)) + \sin(q4)*(\cos(q2)*\cos(q3) - \sin(q2)*\sin(q3)))
                      \sin(q4) * (\cos(q2) * \sin(q3) + \cos(q3) * \sin(q2)) - \cos(q4) * (\cos(q2) * \cos(q3) - \sin(q2) * \sin(q3)),
                   d1 + 11*\sin(q2) - 13*(\cos(q4)*(\cos(q2)*\cos(q3) - \sin(q2)*\sin(q3)) - \sin(q4)* 
                         (\cos(q^2)*\sin(q^3) + \cos(q^3)*\sin(q^2))) + 12*\cos(q^2)*\sin(q^3) + 12*\cos(q^3)*\sin(q^2)]
31
32
                      [ 0, 0, 0, 1 ]
33
```

The full forward kinematics file is given here:

```
%% lynxmotion arm has 5 dof!
  % NOTE: Defined angles start from x = 0, rotating +ve or -ve direction, about the z
3 % axis always!!
4 %#ok<*NOPTS> do not pester me about semi colons
_{5} %#ok<*SAGROW> do not pester me about lists
  % click line numbers to enforce a pause at that line during run.
7 % remember, cos(x) is radians, cosd(x) would be degrees.
8 % remember, arrays count from 1 not 0 in matlab.
9 % clear the output
10 clear all %#ok<*CLALL>
11 close all
12 clc
13
  %% DH TABLE
14
15
  % a
         alpha
                 d
                     theta
                 dl ql
  e 0
         90
16
                 0 q2
17 % 11
        Ω
18 % 12
                 0 q3
         0
19 % 0
         90
                 Ω
                     q4
```

```
0
20 % 0
                13 q5
21 %% Set our variables
22 syms d1 l1 l2 l3; % length variables
23 syms q1 q2 q3 q4 q5; % angle variables
24 %% Show our 5 tranformation matrices
25 T_01 = [
26 [\cos(q1), 0, \sin(q1), 0]
   [sin(q1), 0, -cos(q1), 0]
27
         0, 1,
                   0. d11
28
   Γ
29
          0, 0,
                       0, 111;
30
31
   T_12 = [
   [\cos(q2), -\sin(q2), 0, 11*\cos(q2)]
32
   [\sin(q2), \cos(q2), 0, 11*\sin(q2)]
33
         0,
                    0, 1,
                                    0]
   Γ
          Ο,
                    0, 0,
                                    1]];
35
   [
36
37 \quad T_23 = [
   [\cos(q3), -\sin(q3), 0, 12*\cos(q3)]
38
   [\sin(q3), \cos(q3), 0, 12*\sin(q3)]
         0,
                    0, 1,
40
  ſ
          Ο,
                    0, 0,
                                    1]];
41
42
43 \quad T_34 = [
44 [\cos(q4), 0, \sin(q4),
                                    01
   [\sin(q4), 0, -\cos(q4),
                                    0]
45
46
         0, 1,
                       0,
                                    0]
          0, 0,
                                    111;
47
   Γ
                       0,
48
49
  T_45 = [
   [\cos(q5), -\sin(q5), 0,
50
   [\sin(q5), \cos(q5), 0,
51
                   0, 1, 13]
         0,
52
   ſ
          Ο,
                    0, 0, 1]];
55 %% Multiply them in the required order (right to left)
  % You can show or comment out the components.
57
58 % uncomment to see step by step multiplication of T matrices.
59 % T_34*T_45
60
  % T_23*T_34*T_45;
61 % T_12*T_23*T_34*T_45;
T_e = T_01 * T_12 * T_23 * T_34 * T_45;
64 % Show our final transformation matrix
65
66
67 % now get a specified result, for example:
   T_eSpecified = subs(T_e, [q1, q2, q3, q4, q5, 11, 12, 13, d1], ...
69
       [0*(pi/180), 90*(pi/180), 0*(pi/180), 0*(pi/180), 0*(pi/180), 1, 1, 1, 1])
71 %% The following code simulates the forward kinematics of a the lynxmotion
72 % arm using my forward kinematics calculated above.
73 % Figure 2 shows its movement from start to end
  % position, Figure 1 shows the location of its end effector at points of
75 % its trajectory and Figure 3 shows the maximum potential workspace of the
76 % arm's end effector.
77
78 disp('The following code simulates the forward kinematics of a simple 2DOF')
   disp('serial manipulator. Figure 2 shows ts movement from start to end position,')
80 disp('Figure 1 shows the location of its end effector at points of its trajectory')
81 disp('and Figure 3 shows the maximum potential workspace of its end effector')
82
83 %% A series of joint angles
84 % The following variables are defined in the form of column-vectors with
85 % 4 rows each. Each row represents a different position (angle) of the joint.
86 % e.g. inititally we hae 60 degrees for q1 and -30 for q2.
87 % USING _set TO MARK WHEN WE HAVE DEFINED OUR SYMBOLIC VARIABLES.
88 	ext{ q1\_set} = [ 0 20 40 45 ]'*pi/180 ; % base can spin full 360 degrees
```

```
89 \quad q2\_set = [ 0 \ 30 \ 60 \ 90]'*pi/180 ; % first p joint can move 0 to 180
90 q3_set = [ 0 10 20 30 ]'*pi/180 ; % second p joint can move -180 to 180
   q4\_set = [0 -10 -20 -30]'*pi/180; % third p joint can move -180 to 180
   q5\_set = [ 0 90 180 30 ]'*pi/180 ; % claw can spin full 360 degrees
92
94
   %% Links Lengths
95
   d1_set = 0.1; % example lengths, start with all as 10cm
   11\_set = 0.1;
   12\_set = 0.1;
99 13_set = 0.1 ;
100
101 %% Trigonometric abbreviations
102 % not required at the moment but see orginal uwe script if you want to add
103 % them.
104
105
106
   %% Tip position
   % These equations are taken from our general T_e matrix above.
107
109 % CHECK: I think these are going to be the x,y,z translation values from
   \mbox{\%} T_E and ignore the rot values for orientation of the end effector.
111 xt-element = T-e(1,4); % the x transformation is the 4th element of the 1st row of our general ...
        transformation matrix, T_e.
112 yt_element = T_e(2,4); % the y transformation is the 4th element of the 2nd row of our general ...
        transformation matrix, T_e.
   zt.element = T.e(3,4); % the z transformation is the 4th element of the 3rd row of our general ...
        transformation matrix, T.e.
114
115 % to add the angles and lengths, we will use a quick loop.
116 % lengths are just one value, but angles have an array, so we'll loop
   % through the angle arrays.
118 xt = [];
119 for i = 1:length(q1\_set)
        xt_value = subs(xt_element,[d1 11 12 13 q1 q2 q3 q4 q5], [d1_set 11_set 12_set 13_set ...
120
            q1_set(i) q2_set(i) q3_set(i) q4_set(i) q5_set(i)]); % substitute in the set values.
        xt(i,1) = xt_value;
121
   end
122
123
124
125
   % repeat for y
126
127 yt = [];
128 for i = 1:length(q1_set)
        yt_value = subs(yt_element,[d1 11 12 13 q1 q2 q3 q4 q5], [d1_set 11_set 12_set 13_set ...
129
            q1_set(i) q2_set(i) q3_set(i) q4_set(i) q5_set(i)]); % substitute in the set values.
        yt(i,1) = yt_value;
130
    end
131
132
133
134
135 % repeat for z
136 zt = [];
137 for i = 1:length(q1_set)
        zt_value = subs(zt_element,[d1 11 12 13 q1 q2 q3 q4 q5], [d1_set 11_set 12_set 13_set ...
138
            q1\_set(i) q2\_set(i) q3\_set(i) q4\_set(i) q5\_set(i)]); % substitute in the set values.
        zt(i,1) = zt_value;
139
   end
140
141
   % pt is a 4 by 3 double as required for the formatting below.
142
   pt = [xt yt zt];
143
144
146 %% Plot the trajectory of the end-effector
147
   figure (1)
    %line below just dictates where the image appears on the screen in matlab
149 %desktop
set(1, 'position', [680 558 560 420])
151
152
```

```
153
 154 % IN 3D...
 155 plot3(pt(1,1), pt(1,2), pt(1,3), 'ro')
                                                                                      % plot the first position of the robot's end effector
 156 hold on
 157 plot3(pt(2:4,1),pt(2:4,2),pt(2:4,3), 'o')
                                                                                             % plot the 3 following positions of the robot's ...
               end effector
       title('Tip Trajectory'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
 158
 159
 160
 161
       %% Plot the robotic arm, in 4 different positions
 162 % this currently just moves q1, the base. Do we want to rotate more than
 163
       % one joint? We defo don't want to rotate just the base.
 164 figure (2)
 165 %line below just dictates where the image appears on the screen in matlab
 166 %desktop
 set(2, 'position',[116 190 560 420])
 168
       %base is at origin
 169
 170 \text{ base} = 0 ;
 171
 172
       % next joint given by T01 translations (movement from base to joint 1)
 173
 174 % need to make into a 4 by 3 array.
 175 Tj1_x = zeros(4,1); % x translation is zero
 176 Tj1_y = zeros(4,1); % y translation is zero
       Tj1_z = subs(zeros(4,1), 0, d1_set); % z translation is d1
 177
 _{179} % next joint given by T-01T-12 translations - movement from base to joint 2
 180 % make our general elements for each array
 181 movement = T_01 * T_12;
 182 xt_element = movement(1,4);
       yt_element = movement(2,4);
 184  zt_element = movement(3,4);
 185 % fill the joint 2 4x1 arrays
 186 \text{ Tj2}_{-x} = [];
       Tj2_y = [];
 187
       Tj2_z = [];
 188
       for i = 1:length(g1_set)
 189
              xt_value = subs(xt_element, [11 d1 q1 q2], [11_set d1_set q1_set(i) q2_set(i)]);
 190
               yt\_value = subs(yt\_element, [11 d1 q1 q2], [11\_set d1\_set q1\_set(i) q2\_set(i)]);
 191
               zt_value = subs(zt_element, [11 d1 q1 q2], [11_set d1_set q1_set(i) q2_set(i)]) ;
 192
               Tj2_x(i,1) = xt_value;
 193
               Tj2_y(i,1) = yt_value;
 194
               Tj2_z(i,1) = zt_value;
 195
 196 end
 197
        % above worked, now continue for the rest.
 198
199
 200 % next joint given by T-01T-12T-23 translations - movement from base to joint 3
201 % make our general elements for each array
 _{202} movement = _{T_01*T_12*T_23};
 203 xt_element = movement(1,4);
204 yt_element = movement(2,4);
205  zt_element = movement(3,4) ;
 206 % fill the joint 2 4x1 arrays
 207 \text{ Tj3-x} = [];
208 \text{ Tj3-y} = [];
209 \text{ Tj3_z} = [];
210 for i = 1:length(q1_set)
               xt_value = subs(xt_element,[d1 11 12 q1 q2 q3], [d1_set 11_set 12_set q1_set(i) q2_set(i) ...
211
                       q3_set(i)]) ;
               yt_value = subs(yt_element,[d1 11 12 q1 q2 q3], [d1_set 11_set 12_set q1_set(i) q2_set(i) ...
212
                      a3_set(i)1) ;
               \verb| zt_value = subs(zt_element, [d1 11 12 q1 q2 q3], [d1_set l1_set l2_set q1_set(i) q2_set(i) \dots | (d1_set l2_set l2_set l2_set) | (d1_set l2_set l2
213
                      q3_set(i)]) ;
214
               Tj3_x(i,1) = xt_value;
               Tj3_y(i,1) = yt_value;
215
               Tj3_z(i,1) = zt_value;
216
217
       end
218
```

```
219
220 % next joint given by T_01T_12T_23T_34 translations - movement from base to joint 4
    % note there's no translation in this joint so no change from above.
222 % make our general elements for each array
223 movement = T_01*T_12*T_23*T_34;
224 xt_element = movement(1,4);
225  yt_element = movement(2,4);
226
    zt_element = movement(3,4);
227 % fill the joint 2 4x1 arrays
228 \quad T \dot{j} 4 x = [] ;
229 \quad Tj4_y = [];
230
    Tj4_z = [];
    for i = 1:length(q1_set)
231
        xt_value = subs(xt_element,[d1 11 12 13 q1 q2 q3 q4], [d1_set 11_set 12_set 13_set q1_set(i) ...
232
             q2_set(i) q3_set(i) q4_set(i)]) ;
        yt_value = subs(yt_element,[d1 11 12 13 q1 q2 q3 q4], [d1_set 11_set 12_set 13_set q1_set(i) ...
233
            q2_set(i) q3_set(i) q4_set(i)]);
        zt_value = subs(zt_element,[d1 11 12 13 q1 q2 q3 q4], [d1_set 11_set 12_set 13_set q1_set(i) ...
234
            q2_set(i) q3_set(i) q4_set(i)]);
235
        Tj4_x(i,1) = xt_value;
        Tj4_y(i,1) = yt_value;
236
237
        Tj4_z(i,1) = zt_value;
238
    end
239
240
    % We already calculated our end effector positions - that's the pt array.
241
242
243
244
245
        % generate the graph. Note: only 4 joints will be visible as there is
246
        % no spatial distinction between joins three and 4.
247
    for i = 1:4 % zeros is the base position, doesn't change.
248
249
        xx = [base; Tj1_x(i); Tj2_x(i); Tj3_x(i); Tj4_x(i); pt(i,1)];
250
        yy = [base; Tj1_y(i); Tj2_y(i); Tj3_y(i); Tj4_y(i); pt(i,2)];
        zz = [base; Tj1_z(i); Tj2_z(i); Tj3_z(i); Tj4_z(i); pt(i,3)];
251
252
        pause(1) % pause long enough that we see the first position
253
        plot3(xx,yy,zz,'ko-','Linewidth',2)
254
255
        axis equal
        hold on
256
257
        % label axes, start point, end point.
258
        xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)')
259
        \texttt{text}(\texttt{pt}(1,1),\texttt{pt}(1,2),\texttt{pt}(1,3), \ 'x') \ ; \ \texttt{text}(\texttt{pt}(1,1) \ + \ 0.002,\texttt{pt}(1,2) \ + \ 0.002,\texttt{pt}(1,3) \ + \ \dots
260
             0.002, 'ptStart');
        \text{text}(\text{pt}(4,1),\text{pt}(4,2),\text{pt}(4,3), 'x'); \text{text}(\text{pt}(4,1) + 0.002,\text{pt}(4,2) + 0.002,\text{pt}(4,3) + ...
261
            0.002, 'ptEnd');
        axis([ -0.1 0.4 -0.1 0.4 0 0.4 ])
262
        hold off % CHANGE TO HOLD ON TO SEE ALL LINES AT ONCE.
263
264
        pause (2)
265
    end
266
    267
    %% Workspace - once working, set to finer increments to get workspace plot.
268
269
    % Here we must extend the range of the set angles to encompass all possible
270
271
    % angles.
272
    % SETTING ARRAYS: start:interval:end. x = 1:2:7 -> x = [1,3,5,7]
273
    % to be able to plot, keep intervals consistant.
275 q1_set = (0:30:360)*pi/180; % base angle can go 0 to 360, using intervals of 5 atm.
q2\_set = (-90:30:90)*pi/180; % joint has range -90 to 90
q3\_set = (-180:30:180)*pi/180; % joint has range -180 to 180
q4\_set = (-180:30:180)*pi/180; % joint has range -180 to 180
279 q5_set = 0; % rot of end effector has range 0 to 360 but this doesn't
280 % affect workspace.
{\tt 281}\, % we don't care about q5 as workspace is about how far the robot
282 % can reach, the final orientation of the end effector doesn't matter
283 % therefore, set q5 as a constant.
```

```
284
    %% Angles Full Range of motion
285
    % Not realistic but worth knowing
286
287
^{288} % ql_set = 0:30:360 ; % base angle can go 0 to 360, using intervals of 5 atm.
289 % q2_set = -90:30:90 ; % joint has range -90 to 90
    % q3\_set = -180:30:180 ; % joint has range -180 to 180
290
    % q4\_set = -180:30:180 ; % joint has range -180 to 180
292 % q5_set = 0; % rot of end effector has range 0 to 360 but this doesn't
293 %% Plot the workspace of the robot
294 figure (3)
295
    %line below just dictates where the image appears on the screen in matlab
296
    %desktop
    set(3, 'position', [1243 190 560 420])
297
298
299
    for i = 1:length(q1_set)
300
                                 % for q1
         for j = 1:length(q2\_set) % for q2
301
             for k = 1: length(q3\_set) % for q3
302
303
                 for l = 1:length(q4\_set) % for q4
                     % define our x y z values for the given q 1-4 values
304
                     xwork = subs(xt_element,[d1 11 12 13 q1 q2 q3 q4 q5], [d1_set 11_set 12_set 13_set ...
305
                          q1\_set(1,i) q2\_set(1,j) q3\_set(1,k) q4\_set(1,1) q5\_set]); % substitute in the ...
                          set values.
306
                     ywork = subs(yt_element,[d1 11 12 13 q1 q2 q3 q4 q5], [d1_set 11_set 12_set 13_set ...
                         q1\_set(1,i) q2\_set(1,j) q3\_set(1,k) q4\_set(1,l) q5\_set]); % we still want our ...
                          end effector positions
                     {\tt zwork = subs(zt\_element,[d1 \ 11 \ 12 \ 13 \ q1 \ q2 \ q3 \ q4 \ q5], \ [d1\_set \ 11\_set \ 12\_set \ 13\_set \ \dots]}
307
                          q1.set(1,i) q2.set(1,j) q3.set(1,k) q4.set(1,l) q5.set]); % given by subbing ...
                          into the element eqns.
                     % plot this point!
308
                     if zwork < 0 \mid | abs(q2\_set(1,j) + q3\_set(1,k) + q4\_set(1,l)) > 2*pi % skip ...
309
                          plotting this point if the z value is less than zero, e.g arm goes into the \dots
                          table. or if psi greater than 360
                        continue
310
                     end
311
312
                       disp("position set: " + num2str(i) + ", point: " + num2str(j) + num2str(k) + ...
         num2str(1))
                       disp("x:" + double(xwork) + ", y:" + double(ywork) + ", z:" + double(zwork) + ...
313
         ", psi: " + round((q2_set(1,j) + q3_set(1,k) + q4_set(1,l)),2,"decimals") + ", mu: " + ...
         q5_set *180/pi)
                     plot3(xwork, ywork, zwork, 'x');
314
                     hold on
315
                 end
316
             end
317
318
             % this can take some time, so display current percentage
319
             % done while you wait.
320
             percent_done = (i*j*k*1)/(length(q1_set)*length(q2_set)*length(q3_set)*length(q4_set))*100
321
    end
322
324 title('Workspace'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
```

Appendix B: Serial Robot Inverse Kinematics

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_IK_LynxMotionArm.m

FINN_IK_LynxMotionArm.m

```
\% Inverse Kinematics Calculator for LynxMotion {\tt Arm}
2 % key is to maintain list order across lists of each angle.
3 clear all %#ok<*CLALL> %#ok<*SAGROW>
4 close all
5 clc
   %% Links Length
s d1 = 0.1;
9 11 = 0.1 ;
10 	 12 = 0.1 ;
11 	 13 = 0.1 ;
13 %% Desired position of end-effector - SET ME
14
15 % Cartesian Coords for x,y,z values.
16 \text{ px} = 0.17;
17 py = 0.17;
18 pz = 0.17;
_{\rm 20}\, % mu and psi angles for orientation
21 mu = 0; % mu is rotation of end effector relative to "wrist"
23 % list of all possible psi values. they will be narrowed down later to only
24 % real values. technically could go negative angle but it just ends up
^{25} % repeating. e.g +90 is same as -270 degrees logically.
26 psi = 0:pi/6:2*pi; % RADIANS
27 psi = psi - pi/2; % angular correction to line up with zero point of FK.
29 % psi is angle between end effector and negative-z-axis, based on FK.
30 % psi = q2 + q3 + q4
31 % End effector desired position and orientation given by array End.Effector
32 End_Effector = [ px py pz ]';
33 % disp('Desired position =')
34 % disp("x,y,z")
35 % disp(End_Effector)
36 % disp("mu")
37 % disp(mu)
38 if norm(End_Effector) > 11+12+13+d1 % workspace is above ground
       error('desired position is out of the workspace')
40 end
41
42
44 % For details on calculations, view notes in ReadMe.
45 % We must find values for the 5 joint angles below.
46 sym q1 ; % single value
q2 = []; % potentially many values
48 q3 = []; % potentially many values
q4 = []; % potentially many values
50 sym q5; % single value
52 %% Simple angles to find:
54 % Find q1
q1 = atan2(py,px);
56 % Find q5
57 	 q5 = mu ;
59 %% Define extra variables to help us find q2,3,4
```

```
60
61 % define (r,z) plane
   r = sqrt(px^2 + py^2); % r is hypotenues in x-y plane.
63
64 % For each value of psi, there is a value of rw, zw and D
65 	ext{ r_w} = (1:length(psi));
z_w = (1:length(psi));
D = (1:length(psi))
68 for i = 1:length(psi)
    % define position of wrist in (r,z) plane
        r_w(i) = r - 13*cos(psi(i)); %r_w and z_w will be real as cos or sin of a real number is a ...
70
            real number
71
        z_{-w}(i) = pz - d1 - 13*sin(psi(i));
72
73
       % define D - a placeholder variable for a large combination we derived in
74
75
        % notes
76
       D(i) = - (r_w(i)^2 + z_w(i)^2 - 11^2 - 12^2) / (2*11*12);
77
       D(i) = round(D(i), 7); % rounding D avoids fake imaginary numbers due to rounding
                        % errors.
79
80
   %% MAKE LISTS FOR EACH ANGLE AND ENSURE ALL THE SAME LENGTH. IF ONE OF THE ANGLES IN A SET OF 5 IS ...
81
        IMAGINARY, REMOVE THAT INDEX FOR EVERY ANGLE. SHOULD START WITH MANY BUT REDUCE TO ONLY A FEW.
    %% get only real values
83
84 psi_real = [] ;
s_5 r_w_real = [];
z_w_real = [];
87  D_real = [] ;
   for i = 1:length(psi)
88
        if imag(sqrt(1-D(i)^2)) == 0 % for real values, append to real lists.
            psi\_real(end + 1) = round(psi(i), 7); % round each list to get zeros rather than e^-10 or ...
90
91
            r_w=real(end + 1) = round(r_w(i), 7);
            z_w_real(end + 1) = round(z_w(i), 7);
92
            D_real(end + 1) = round(D(i), 7);
93
        end
94
   end
95
96
97
   % we can see these four lists MUST have same length.
   % disp(psi_real)
99 % disp(D_real)
100 % disp(z_w_real)
101 % disp(r_w_real)
102
103 %% Find q3 possibilities
104 % there are two posibilities for each value of D depending on
105 for i = 1:length(D_real)
106
        q3(end+1) = atan2( sqrt(1-D_real(i)^2), -D_real(i)) ;
107
108
        q3(end+1) = atan2(-sqrt(1-D_real(i)^2), -D_real(i));
   end
109
110
111 % disp("q3")
      disp(q3)
113 %% Explaining list order.
114 % matlab indexes from 1 not 0.
115 % if D has 3 values, we can see q3 will have 6, where
116 % D(1) corresponds to q3(1 & 2)
117 % D(2) corresponds to q3(3 & 4)
118 % D(3) corresponds to q3(5 & 6)
119 % we can see D(i) corresponds to values
120 % q3(2*i -1) and q3(2*i)
121 % we need to ensure this is *consistant* across all q lists below.
122 %% Find q2
123
124 % two options based on q3
125 for i = 1:length(D_real)
       % for each r_w,z_w value, find first q2 value using first q3 value
```

```
q2(end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(l2*sin(q3(2*i)), l1+l2*cos(q3(2*i)));
127
        % add +1 to
128
129
        q2 (end+1) = atan2(z_w.real(i), r_w.real(i)) + atan2(12*sin(q3(2*i-1)), 11+12*cos(q3(2*i-1)));
130 end
131 % disp("q2")
132 % disp(q2)
133 %% Find q4
134
    % two options based on two sets of q2,q3
135
136
    % use psi = q2 + q3 + q4
   % +pi/2 is the geometry correction for zero point of q4
137
    for i = 1:length(D_real) % round to remove zero discrepancies.
138
        q4(end+1) = psi\_real(i) - q2(2*i -1) - q3(2*i -1) + pi/2;
139
        q4(end+1) = psi\_real(i) - q2(2*i) - q3(2*i) + pi/2;
140
141
142
143
144 % disp("q4")
145 % disp(q4)
146 %% Remove duplicate values
    % make a matrix out of the lists where one row is one solution
147
149 % we know matrix will have initial size: no. of items in q2, 3 or 4 \times 5
150 % angles
151 Solution_Matrix = zeros(length(q2), 5);
for i = 1: length(q2)
        Solution_Matrix(i,1) = q1;
        Solution_Matrix(i,2) = q2(i);
154
        Solution_Matrix(i,3) = q3(i);
155
156
        Solution_Matrix(i,4) = q4(i);
157
        Solution_Matrix(i,5) = q5;
158
   end
    % disp(Solution_Matrix)
159
160 % remove duplicate rows
161 Unique_Solutions = unique(Solution_Matrix, "rows", "stable");
    % stable prevents order being changed.
162
163
164
    %% we also know, q4 can't be more than 360 degrees. filter these out.
165
valid_Solutions = [];
167
    for i = 1:size(Unique_Solutions,1)
        if abs(Unique_Solutions(i,4)) < 2*pi
168
            valid_Solutions = [valid_Solutions; Unique_Solutions(i,:)];
169
170
171
    end
    %% Display Solutions
172
173
    for i = 1:size(valid_Solutions,1) % for no. of rows aka no. of solutions
174
175
        disp("solution " + num2str(i) + ": ")
176
177
        disp(round(valid_Solutions(i,:)*180/pi,2,"decimals"))
178
179 end
```

Appendix C: Serial Robot Task Completion

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_TASK_LynxMotionArm.m

FINN_TASK_LynxMotionArm.m

```
%% LvnxMotion Arm Task
   % This file uses inverse and forward kinematics to plan and show a task for
   % the lynxmotion arm in matlab.
5 % the chosen task is to draw the vertices of a cuboid in 3d space.
7
   % ***Task Steps***
   % 1. define x,y,z positions for 5 or more points that would make a cuboid
9 % in 3d space.
10 % 2. use IK to find the q1-5 angle values for the arm at a each point.
_{11} % 3. use FK to plot the arm trajectory in 3d space and save the end
   % effector points to display the smiley face.
13 clear all %#ok<*CLALL> %#ok<*SAGROW>
14 close all
15 clc
16
   %% 1. define x,y,z positions that make a smiley face in 3d space.
17
18
19
20 % TASK: plot a cuboid in 3D space.
21 points_to_plot = [[0.0 0.0 0.2]; [0.0 0.0 0.1]; [0.15 0.0 0.2]; [0.15 0.0 0.1]; [0.15 0.15 0.15 0.1]; ...
        [0.15 0.15 0.2]; [0.0 0.15 0.2]; [0.0 0.15 0.1]];
^{22} % check the plotted points.
23 figure (1)
^{24}
   for i = 1:size(points_to_plot,1)
25
       \verb|plot3(points_to_plot(i,1), points_to_plot(i,2), points_to_plot(i,3), 'ko-', 'Linewidth', 2)| \\
26
           plot the first position of the robot's end effector
       hold on
27
28 end
29
   axis([ 0 0.4 0 0.4 0 0.4 ])
   title('Desired Points'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
30
31
33
   \% 2. use IK to find the q1-5 angle values for the arm at a each point.
34
35 % Inverse Kinematics Calculator for LynxMotion Arm
36 % key is to maintain list order across lists of each angle.
37 % Links Length
38 d1 = 0.1;
39 	 11 = 0.1 ;
40 	 12 = 0.1 ;
41 13 = 0.1;
43 % Run through the list of point
   IK_OUTPUT = zeros(size(points_to_plot,1),5); % holding array for output q angles.
   for j = 1:size(points_to_plot,1)
45
       % Cartesian Coords for x,y,z values.
46
47
       px = points_to_plot(j,1);
48
       py = points_to_plot(j,2) ;
       pz = points_to_plot(j,3);
49
50
51 % mu and psi angles for orientation
52 mu = 0; % mu is rotation of end effector relative to "wrist"
53
54 % list of all possible psi values. they will be narrowed down later to only
55 % real values. technically could go negative angle but it just ends up
56 % repeating. e.g +90 is same as -270 degrees logically.
57 \text{ psi} = (0:pi/20:2*pi);
```

```
58 for i = 1: length(psi)
59
       psi(i) = psi(i) - pi/2;
    end
60
61
63 % psi is angle between end effector and negative-z-axis, based on FK.
64 % psi = q2 + q3 + q4
   % End effector desired position and orientation given by array End Effector
66 End_Effector = [ px py pz ]';
67 % disp('Desired position =')
68 % disp("x,y,z")
69
   % disp(End_Effector)
70 % disp("mu")
71 % disp(mu)
72 if norm(End_Effector) > 11+12+13+d1 % workspace is above ground
       error('desired position is out of the workspace')
73
74
75
76
78 % For details on calculations, view notes in ReadMe.
   % We must find values for the 5 joint angles below.
80 sym q1 ; % single value
81 q2 = []; % potentially many values
q3 = []; % potentially many values
83 q4 = []; % potentially many values
84 sym q5; % single value
85
86 %% Simple angles to find:
87
88 % Find q1
q1 = atan2(py,px);
90 % Find q5
91 	 q5 = mu ;
93 %% Define extra variables to help us find q2,3,4
94
95 % define (r,z) plane
96 r = sqrt(px^2 + py^2); % r is hypotenues in x-y plane.
97
98 % For each value of psi, there is a value of rw, zw and D
99 r_w = (1:length(psi));
z_w = (1:length(psi));
D = (1:length(psi));
102 for i = 1:length(psi)
103
    % define position of wrist in (r,z) plane
       r_w(i) = r - 13*cos(psi(i)); %r_w and z_w will be real as cos or sin of a real number is a ...
104
           real number
105
       z_w(i) = pz - d1 - 13*sin(psi(i));
106
107
108
       % define D - a placeholder variable for a large combination we derived in
       % notes
109
110
       D(i) = - (r_w(i)^2 + z_w(i)^2 - 11^2 - 12^2) / (2*11*12);
111
       D(i) = round(D(i), 7); rounding D avoids fake imaginary numbers due to rounding
112
                       % errors.
113
114 end
115 %% get only real values
116
117 psi_real = [] ;
118 r_w_real = [] ;
119 z_w_real = [] ;
120 D_real = [] ;
    for i = 1:length(psi)
121
        if imag(sqrt(1-D(i)^2)) == 0 % for real values, append to real lists.
122
           psi\_real(end + 1) = psi(i);%round(psi(i),7); % round each list to get zeros rather than ...
123
               e^-10 or something.
124
           r_{w}=(end + 1) = r_{w}(i); round(r_{w}(i), 7) ;
           z_{w}=(end + 1) = z_{w}(i); round(z_{w}(i), 7);
125
```

```
D_{real}(end + 1) = D(i); % round(D(i), 7);
126
127
        end
128
    end
129
    % we can see these four lists MUST have same length.
130
131 % disp(psi_real)
    % disp(D_real)
132
133
       disp(z_w_real)
134 % disp(r_w_real)
135
136 %% Find q3 possibilities
137
    % there are two posibilities for each value of D depending on
   for i = 1:length(D_real)
138
139
        q3(end+1) = atan2(sqrt(1-D_real(i)^2), -D_real(i));
140
        q3(end+1) = atan2(-sqrt(1-D_real(i)^2), -D_real(i));
141
142
    end
143
    % disp("q3")
144
145 % disp(q3)
146 %% Explaining list order.
    % matlab indexes from 1 not 0.
148 % if D has 3 values, we can see q3 will have 6, where
149 % D(1) corresponds to q3(1 & 2)
150 % D(2) corresponds to q3(3 & 4)
151 % D(3) corresponds to q3(5 & 6)
   % we can see D(i) corresponds to values
33 % q3(2*i -1) and q3(2*i)
154 % we need to ensure this is \starconsistant\star across all q lists below.
155 %% Find q2
156
    % two options based on q3
157
    for i = 1:length(D_real)
158
        % for each r_w,z_w value, find first q2 value using first q3 value.
160
        % Switching order here corrects angles... why?
        q2(end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(l2*sin(q3(2*i)), l1+l2*cos(q3(2*i)));
161
162
        % add +1 to
        q2 (end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(12*sin(q3(2*i-1)), 11+12*cos(q3(2*i-1)));
163
164 end
    % disp("q2")
165
166
    % disp(q2)
167
    %% Find q4
168
169 % two options based on two sets of q2,q3
170 % use psi = q2 + q3 + q4
    for i = 1:length(D_real)
171
        q4 (end+1) = psi_real(i) - q2(2*i -1) - q3(2*i -1) + pi/2;
172
        q4(end+1) = psi\_real(i) - q2(2*i) - q3(2*i) + pi/2;
173
174 end
175
    % disp("q4")
176
177 % disp(q4)
178 %% Remove duplicate values
179 % make a matrix out of the lists where one row is one solution
180
   % we know matrix will have initial size: no. of items in q2,3 or 4 \times 5
181
182 % angles
183 Solution_Matrix = zeros(length(q2), 5);
184 for i = 1:length(q2)
        Solution_Matrix(i,1) = q1;
185
        Solution_Matrix(i,2) = q2(i)
186
        Solution_Matrix(i,3) = q3(i);
187
        Solution_Matrix(i,4) = q4(i);
188
        Solution_Matrix(i,5) = q5;
189
190 end
191
    % disp(Solution_Matrix)
192 % remove duplicate rows
193 Unique_Solutions = unique(Solution_Matrix, "rows", "stable");
194
    % stable prevents order being changed.
195
```

```
196
    %% we also know, q4 can't be more than 360 degrees. filter these out.
197
    valid_Solutions = [] ;
198
    for i = 1:size(Unique_Solutions,1)
199
        if abs(Unique_Solutions(i,4)) < 2*pi</pre>
201
            valid_Solutions = [valid_Solutions; Unique_Solutions(i,:)];
202
203
    end
204
205
    % stable prevents order being changed.
         for i = 1:5
206
             IK_OUTPUT(j,i) = valid_Solutions(1,i);
207
208
209
210 end
    disp("Using IK: Array of q1-5 values:")
211
    disp(IK_OUTPUT)
212
213
214
215
    %% 3. use FK to plot the arm trajectory in 3d space
216
    syms q1 q2 q3 q4 q5; % angle variables
217
218
219 % Show our 5 tranformation matrices
220 T_01 =[
    [\cos(q1), 0, \sin(q1), 0]
221
    [\sin(q1), 0, -\cos(q1), 0]
           0, 1,
                        0, d1]
223
            0, 0,
                         0, 1]];
224
225
226 T_12 = [
    [\cos(q2), -\sin(q2), 0, 11*\cos(q2)]
227
    [\sin(q2), \cos(q2), 0, 11*\sin(q2)]
228
          0,
                   0, 1,
                                     0]
           0,
                      0, 0,
                                      1]];
230
    [
231
232 \quad T_23 = [
233 [\cos(q3), -\sin(q3), 0, 12*\cos(q3)]
    [\sin(q3), \cos(q3), 0, 12*\sin(q3)]
234
           0,
                      0, 1,
                                      0.1
235
    [
236
           Ο,
                      0, 0,
                                      1]];
237
238 T_34 = [
239 [cos(q4), 0, sin(q4),
                                      0]
    [\sin(q4), 0, -\cos(q4),
                                      01
240
                         Ο,
           0, 1,
                                      0]
241
           0, 0,
                         0.
                                      1]];
242
243
244 \quad T_{4}5 = [
[\cos(q5), -\sin(q5), 0, 0]
    [\sin(q5), \cos(q5), 0,
                             0]
246
                     0, 1, 13]
247
    ſ
          0,
                      0, 0, 1]];
           0,
248
249
250 % Get overall forward kinematics
    T_{e} = T_{01}*T_{12}*T_{23}*T_{34}*T_{45};
251
252
253
    % extract the x,y,z elements of these
    xt_element = T_e(1,4); % the x transformation is the 4th element of the 1st row of our general ...
254
        transformation matrix, T-e.
    yt-element = T-e(2,4); % the y transformation is the 4th element of the 2nd row of our general ...
        transformation matrix, T_e.
   zt_element = T_e(3,4); % the z transformation is the 4th element of the 3rd row of our general ...
        transformation matrix, T_e.
257
258 % Define all our angles in their own arrays
259 q1_set = [] ;
q2\_set = [];
261 q3_set = [] ;
262 q4_set = [];
```

```
263 	ext{ q5\_set} = [] ;
    for i = 1:size(IK_OUTPUT,1) % i in range number of rows
264
         % number of columns always 5 for q1-5
265
         q1\_set(i) = IK\_OUTPUT(i,1);
266
        q2\_set(i) = IK\_OUTPUT(i,2);
267
268
        q3\_set(i) = IK\_OUTPUT(i,3);
        q4\_set(i) = IK\_OUTPUT(i,4);
269
         q5\_set(i) = IK\_OUTPUT(i,5);
270
    end
271
272
273
274
275
    % Now simply plot using our FK
276
277
    % define variable for number of points
278
    NoP = size(IK_OUTPUT,1); % same as number of sets of q values.
279
280
    %base is at origin
281
_{282} base = 0 ;
283
284
    % next joint given by T01 translations (movement from base to joint 1)
285
286 % need to make into a 4 by 3 array.
287 Tj1_x = zeros(NoP,1) ; % x translation is zero
    Tj1_y = zeros(NoP,1) ; % y translation is zero
288
    Tj1_z = subs(zeros(NoP,1), 0, d1); % z translation is d1
290
    % next joint given by T_01T_12 translations - movement from base to joint 2
291
292 % make our general elements for each array
293 movement = T_01 * T_12;
    xt_element = movement(1,4);
295 yt_element = movement(2,4);
296 zt_element = movement(3,4);
297 % fill the joint 2 4x1 arrays
298 Tj2_x = [] ;
    Tj2_y = []
299
300 \text{ Tj2_z} = [];
    for i = 1:length(q1_set)
301
        xt\_value = subs(xt\_element, [ q1 q2], [q1\_set(i) q2\_set(i)]) ;
302
        yt\_value = subs(yt\_element, [ q1 q2], [q1\_set(i) q2\_set(i)]) ;
303
        zt\_value = subs(zt\_element, [ q1 q2], [q1\_set(i) q2\_set(i)]) ;
304
        Tj2_x(i,1) = xt_value;
305
        Tj2-y(i,1) = yt\_value;
306
        Tj2_z(i,1) = zt_value;
307
308
309
    % above worked, now continue for the rest.
310
311
312 % next joint given by T_01T_12T_23 translations - movement from base to joint 3
    % make our general elements for each array
314 movement = T_01*T_12*T_23;
315 xt_element = movement(1,4);
316  yt_element = movement(2,4) ;
317  zt_element = movement(3,4);
    % fill the joint 2 4x1 arrays
319 \quad T j 3_x = [];
320 \text{ Tj3-y} = [];
321 \quad Tj3_z = [];
    for i = 1:length(q1_set)
322
         xt\_value = subs(xt\_element, [q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
323
         yt_value = subs(yt_element,[q1 q2 q3], [q1_set(i) q2_set(i) q3_set(i)]);
324
         zt\_value = subs(zt\_element, [q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
325
326
        Tj3_x(i,1) = xt_value;
        Tj3_y(i,1) = yt_value;
327
328
        Tj3_z(i,1) = zt_value;
329
    end
330
331
332 % next joint given by T_01T_12T_23T_34 translations - movement from base to joint 4
```

```
333 % note there's no translation in this joint so no change from above.
334 % make our general elements for each array
335 movement = T_01*T_12*T_23*T_34;
336 xt_element = movement(1,4);
337 yt_element = movement(2,4);
338  zt_element = movement(3,4) ;
339 % fill the joint 2 4x1 arrays
340 \text{ Tj4}_x = [];
341 \quad Tj4_y = [];
342 \quad T j 4_z = [];
343
    for i = 1:length(g1_set)
344
         \texttt{xt\_value} = \texttt{subs}(\texttt{xt\_element}, \texttt{[q1 q2 q3 q4]}, \texttt{ [q1\_set(i) q2\_set(i) q3\_set(i) q4\_set(i)])} ; \\
        yt_value = subs(yt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
345
        zt_value = subs(zt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
346
        Tj4_x(i,1) = xt_value;
347
        Tj4_y(i,1) = yt_value;
348
        Tj4_z(i,1) = zt_value;
349
350
    end
351
352
    % final joint given by T_01T_12T_23T_34T_45 translations - movement from base to joint 4
    % note there's no translation in this joint so no change from above.
353
    % make our general elements for each array
355 movement = T_01*T_12*T_23*T_34*T_45;
356 xt_element = movement(1,4);
357 yt_element = movement(2,4);
358  zt_element = movement(3,4);
    % fill the joint 2 4x1 arrays
360 EE = [] ; % End Effector Positions list
    for i = 1:length(q1_set)
361
362
        xt_value = subs(xt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
         yt\_value = subs(yt\_element, [q1 q2 q3 q4], [q1\_set(i) q2\_set(i) q3\_set(i) q4\_set(i)]); \\
363
         zt_value = subs(zt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
364
        EE(i,1) = xt_value ; % x values in column 1
365
366
        EE(i,2) = yt_value ; % y values in column 2
367
        EE(i,3) = zt\_value ; % z values in column 3
    end
368
369
    % Check if end effector positions match points to plot.
370
371 disp("EE values (should match points to plot): ")
372 disp(EE)
373
    disp("do they match? 0 = no, 1 = yes: ")
    isequal(round(points_to_plot,2,"decimals"),round(EE,2,"decimals"))
374
375
376
    figure (2)
377
         % generate the graph. Note: only 4 joints will be visible as there is
378
         \mbox{\%} no spatial distinction between joints three and 4.
379
    for i = 1:NoP % zeros is the base position, doesn't change.
380
         xx = [base; Tj1_x(i); Tj2_x(i); Tj3_x(i); Tj4_x(i); EE(i,1)];
381
        yy = [base; Tj1_y(i); Tj2_y(i); Tj3_y(i); Tj4_y(i); EE(i,2)];
382
         zz = [base; Tj1_z(i); Tj2_z(i); Tj3_z(i); Tj4_z(i); EE(i,3)];
383
384
        axis([ 0 0.4 0 0.4 0 0.4 ])
        plot3(xx,yy,zz,'ko-','Linewidth',2)
385
386
        hold on % CHANGE TO HOLD ON TO SEE ALL LINES AT ONCE.
        pause(2)
387
388
         % label axes, start point, end point.
389
390
        text(EE(1,1) + 0.002,EE(1,2) + 0.002,EE(1,3) + 0.002,'Start');
        text(EE(end,1) + 0.002,EE(end,2) + 0.002,EE(end,3) + 0.002,'End');
391
392
        % label end effector points
393
         text (EE(i,1), EE(i,2), EE(i,3), 'x')
394
395
    \label{linear_title} \mbox{title('Actual Points') ; xlabel('x (m)') ; ylabel('y (m)') ; zlabel('z (m)');}
396
397
398
    figure (3) % end points only
399
    for i = 1:NoP
400
        plot3(EE(i,1),EE(i,2),EE(i,3),'ko-','Linewidth',2)
401
402
```

```
403 end
404 title('Actual End Points Only'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
405 axis([ 0 0.4 0 0.4 0 0.4 ])
```

Appendix D: Serial Robot Linear Trajectories

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_TASK_LIN_TRAJECTORIES_LynxMotionArm.m

$FINN_TASK_LIN_TRAJECTORIES_LynxMotionArm.m$

```
1 %% linear motion (straight lines)
 2 clear all %#ok<*CLALL> %#ok<*SAGROW>
 3 close all
 4 clc
 5 % link lengths
  6 d1 = 0.1;
       11 = 0.1;
 8 	 12 = 0.1 ;
 9 	 13 = 0.1 ;
11 % assuming 10 HZ robot, performing each line in 1 second
       %% TRYING LINEAR FIRST
13 %1. get start, end point and line eqn between.
14 %2. sample function for 10 points between each start and end point
15 %3. apply IK and FK
16
      %% 1 & 2 -> find eqn for each line and add 10 points to the trajectory.
17
18 % function at bottom to do this.
19
20 points_per_line = 10 ;
21 points_to_plot = [[0.0 0.0 0.2]; [0.15 0.0 0.2]; [0.15 0.0 0.1]; [0.0 0.0 0.1]; [0.15 0.15 0.2]; ...
                 [0.15 0.15 0.1]; [0.0 0.15 0.1]; [0.0 0.15 0.2]];
22 trajectories = zeros((size(points_to_plot,1) - 1)*points_per_line, 3);
24 % Use our function to get the gradient and constant, filter for lines along
      % each axis.
25
      for i = 1:(size(points_to_plot,1) - 1)
26
                [grad, const, r_dir, r] = ...
27
                         find\_line\_eqn (points\_to\_plot (i,1), points\_to\_plot (i+1,1), points\_to\_plot (i,2), points\_to\_plot (i+1,2), points\_to\_plot (i
28
                for j = 1:points_per_line
29
                         if r_dir == 10
30
                                 if i == 1 && j == 1
                                          trajectories(((i-1)*10+j),3) = points_to_plot(i,3) + ...
32
                                                    (points_to_plot(i+1,3)-points_to_plot(i,3))*(j/points_per_line)
                                          continue
33
                                 end
34
                                 trajectories(((i-1)*10+j),1) = trajectories(((i-1)*10+j-1),1);
35
                                 \label{eq:trajectories} \texttt{trajectories(((i-1)*10+j),2)} = \texttt{trajectories(((i-1)*10+j-1),2);}
36
                                  trajectories(((i-1)*10+j),3) = points_to_plot(i,3) + ...
37
                                           (points_to_plot(i+1,3)-points_to_plot(i,3))*(j/points_per_line) ;
38
39
                        end
                        x = points\_to\_plot(i,1) + r*cos(r\_dir) * (j/points\_per\_line);
40
41
                         y = points_to_plot(i,2) + r*sin(r_dir) * (j/points_per_line);
                        r_{temp} = sqrt(x^2 + y^2);
42
                        z = grad*r_temp + const;
43
44
                        trajectories(((i-1)*10+j),1) = x;
45
                         trajectories(( (i-1)*10+j) ,2) = y;
                         trajectories(((i-1)*10+j),3) = z;
46
47
48
                end
49 end
      disp(trajectories)
50
51
52
54 %% 3
```

```
for j = 1:size(trajectories,1)
       px = trajectories(j, 1);
56
        py = trajectories(j,2);
57
       pz = trajectories(j,3);
58
59
60
        % mu and psi angles for orientation
        mu = 0; % mu is rotation of end effector relative to "wrist"
61
62
        psi = (0:pi/20:2*pi);
        for i = 1: length(psi)
63
           psi(i) = psi(i) - pi/2;
64
        end
65
        End_Effector = [ px py pz ]';
66
        if norm(End_Effector) > 11+12+13+d1 % workspace is above ground
67
            error('desired position is out of the workspace')
68
69
70
71
        72
        % For details on calculations, view notes in ReadMe.
73
74
        % We must find values for the 5 joint angles below.
        sym q1 ; % single value
75
        q2 = [] ; % potentially many values
76
        q3 = [] ; % potentially many values
77
        q4 = []; % potentially many values
78
        sym q5; % single value
79
80
81
        %% Simple angles to find:
82
        % Find q1
83
84
        q1 = atan2(py,px);
        % Find q5
85
        q5 = mu;
86
87
        %% Define extra variables to help us find q2,3,4
89
        % define (r,z) plane
90
91
        r = sqrt(px^2 + py^2); % r is hypotenues in x-y plane.
92
        % For each value of psi, there is a value of rw, zw and D
93
94
        r_w = (1:length(psi));
        z_w = (1:length(psi));
95
        D = (1:length(psi));
96
        for i = 1:length(psi)
97
        % define position of wrist in (r,z) plane
           r_w(i) = r - 13*cos(psi(i)); %r_w and z_w will be real as cos or sin of a real number is ...
99
                a real number
100
            z_w(i) = pz - d1 - 13*sin(psi(i));
101
102
            % define D - a placeholder variable for a large combination we derived in
103
            % notes
104
105
            D(i) = - (r_w(i)^2 + z_w(i)^2 - 11^2 - 12^2) / (2*11*12);
106
107
           D(i) = round(D(i), 7); * rounding D avoids fake imaginary numbers due to rounding
                            % errors.
108
109
        %% get only real values
110
111
112
        psi_real = [];
        r_w_real = [];
113
114
        z_w_real = [];
        D_real = [] ;
115
        for i = 1:length(psi)
           if imag(sqrt(1-D(i)^2)) == 0 % for real values, append to real lists.
117
                psi_real(end + 1) = psi(i);%round(psi(i),7); % round each list to get zeros rather ...
118
                    than e^-10 or something.
                r_{w_real(end + 1)} = r_{w_i(i)} * round(r_{w_i(i)}, 7) ;
119
                z_w_{eq} = z_w(i); %round(z_w(i), 7);
120
121
                D_{real(end + 1) = D(i); %round(D(i), 7);
122
```

```
123
        end
124
125
        % we can see these four lists MUST have same length.
        % disp(psi_real)
126
        % disp(D_real)
127
        % disp(z_w_real)
128
        % disp(r_w_real)
129
130
        %% Find q3 possibilities
131
132
        % there are two posibilities for each value of D depending on
        for i = 1:length(D_real)
133
134
             q3(end+1) = atan2(sqrt(1-D_real(i)^2), -D_real(i));
135
             q3(end+1) = atan2(-sqrt(1-D_real(i)^2), -D_real(i));
136
        end
137
138
         % disp("q3")
139
        % disp(q3)
140
        %% Explaining list order.
141
142
        % matlab indexes from 1 not 0.
        % if D has 3 values, we can see q3 will have 6, where
143
        % D(1) corresponds to q3(1 & 2)
144
        % D(2) corresponds to q3(3 & 4)
145
        % D(3) corresponds to q3(5 & 6)
146
147
        % we can see D(i) corresponds to values
        % q3(2*i -1) and q3(2*i)
148
149
         % we need to ensure this is *consistant* across all q lists below.
        %% Find q2
150
151
        \mbox{\%} two options based on q3
152
153
         for i = 1:length(D_real)
154
             % for each r_w,z_w value, find first q2 value using first q3 value.
             % Switching order here corrects angles... why?
155
             q2 (end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(12*sin(q3(2*i)), 11+12*cos(q3(2*i)));
157
             % add +1 to
             q2 (end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(l2*sin(q3(2*i-1)), ...
158
                 11+12*cos(q3(2*i-1)));
159
        end
        % disp("q2")
160
         % disp(q2)
161
162
         %% Find q4
163
        % two options based on two sets of q2,q3
164
        % use psi = q2 + q3 + q4
165
         for i = 1:length(D_real)
166
             q4 (end+1) = psi_real(i) - q2(2*i -1) - q3(2*i -1) +pi/2;

q4 (end+1) = psi_real(i) - q2(2*i) - q3(2*i) +pi/2;
167
168
169
170
        % disp("q4")
171
        % disp(q4)
172
        %% Remove duplicate values
173
         % make a matrix out of the lists where one row is one solution
174
175
        % we know matrix will have initial size: no. of items in q2,3 or 4 \times 5
176
177
        % angles
        Solution_Matrix = zeros(length(q2), 5);
178
179
        for i = 1: length(q2)
180
             Solution_Matrix(i,1) = q1;
             Solution_Matrix(i, 2) = q2(i);
181
             Solution_Matrix(i,3) = q3(i);
182
             Solution_Matrix(i,4) = q4(i);
183
             Solution_Matrix(i,5) = q5;
        end
185
         % disp(Solution_Matrix)
186
187
        % remove duplicate rows
        Unique_Solutions = unique(Solution_Matrix, "rows", "stable") ;
188
         % stable prevents order being changed.
189
190
191
```

```
\% we also know, q4 can't be more than 360 degrees. filter these out.
192
        valid_Solutions = [] ;
193
194
        for i = 1:size(Unique_Solutions,1)
            if abs(Unique_Solutions(i,4)) < 2*pi
195
                 valid_Solutions = [valid_Solutions; Unique_Solutions(i,:)];
196
197
        end
198
199
        % stable prevents order being changed.
            for i = 1:5
200
201
                 IK_OUTPUT(j,i) = valid_Solutions(1,i);
202
203
            end
204
    disp("Using IK: Array of q1-5 values:")
205
    %disp(IK_OUTPUT);
206
207
208
209
    %% 3. use FK to plot the arm trajectory in 3d space
210
211
    syms q1 q2 q3 q4 q5; % angle variables
212
    % Show our 5 tranformation matrices
213
    T_01 = [
214
215 [cos(q1), 0, sin(q1), 0]
216 [sin(q1), 0, -\cos(q1), 0]
           0, 1,
                         0, d1]
217
    ſ
218
           0, 0,
                         0, 1]];
219
    T_12 = [
220
[\cos(q2), -\sin(q2), 0, 11*\cos(q2)]
222
    [\sin(q2), \cos(q2), 0, 11*\sin(q2)]
223
           0,
                     0, 1,
                                      01
           0,
                      0, 0,
                                      111;
224
    Γ
225
226 \quad T_{-}23 = [
    [\cos(q3), -\sin(q3), 0, 12*\cos(q3)]
227
228
    [\sin(q3), \cos(q3), 0, 12*\sin(q3)]
          0,
                     0, 1,
                                     01
229
    Γ
                      0, 0,
230
                                      1]];
231
232
    T_34 = [
    [\cos(q4), 0, \sin(q4),
233
    [\sin(q4), 0, -\cos(q4),
                                      0]
234
          0, 1,
                       0,
                                      0]
           0, 0,
                         0,
                                      111:
236
    [
237
    T_45 = [
238
   [\cos(q5), -\sin(q5), 0, 0]
239
   [\sin(q5), \cos(q5), 0, 0]
           0,
                      0, 1, 13]
241
    Γ
242
           Ο,
                      0, 0,
                            1]];
243
244 % Get overall forward kinematics
T_e = T_01*T_12*T_23*T_34*T_45;
246
247
    % extract the x,y,z elements of these
    xt-element = T-e(1,4); % the x transformation is the 4th element of the 1st row of our general ...
248
        transformation matrix, T_e.
    yt-element = T_-e(2,4); % the y transformation is the 4th element of the 2nd row of our general ...
249
        transformation matrix, T_e.
    zt_element = T_e(3,4); % the z transformation is the 4th element of the 3rd row of our general ...
        transformation matrix, T_e.
252 % Define all our angles in their own arrays
253 q1_set = [] ;
254 q2_set = [] ;
255 q3_set = [] ;
|_{256} q4_set = [];
q5_{set} = [];
258 for i = 1:size(IK_OUTPUT, 1) % i in range number of rows
```

```
% number of columns always 5 for q1-5
259
        gl\_set(i) = IK\_OUTPUT(i,1);
260
        q2\_set(i) = IK\_OUTPUT(i,2);
261
        q3\_set(i) = IK\_OUTPUT(i,3);
262
        q4\_set(i) = IK\_OUTPUT(i,4);
263
264
        q5\_set(i) = IK\_OUTPUT(i,5);
265
    end
266
267
268
    %Now simply plot using our FK
269
270
271
    % define variable for number of points
272
    NoP = size(IK_OUTPUT,1); % same as number of sets of q values.
273
274
275
    %base is at origin
    base = 0;
276
277
278
    % next joint given by T01 translations (movement from base to joint 1)
279
    % need to make into a 4 by 3 array.
281 Tjl_x = zeros(NoP,1) ; % x translation is zero
282 Tj1_y = zeros(NoP,1) ; % y translation is zero
283 Tj1_z = subs(zeros(NoP,1), 0, d1); % z translation is d1
284
285
    % next joint given by T_-01T_-12 translations - movement from base to joint 2
   % make our general elements for each array
286
287 movement = T_01 * T_12;
288 xt_element = movement(1,4);
289 yt_element = movement(2,4);
    zt_element = movement(3,4);
291 % fill the joint 2 4x1 arrays
292 \quad Tj2_x = [];
293 \text{ Tj2-y} = [];
    Tj2_z = [];
294
    for i = 1:length(q1_set)
295
296
        xt_value = subs(xt_element, [ q1 q2], [q1_set(i) q2_set(i)]) ;
        yt_value = subs(yt_element, [ q1 q2], [q1_set(i) q2_set(i)]) ;
297
298
        zt\_value = subs(zt\_element, [ q1 q2], [q1\_set(i) q2\_set(i)]) ;
        Tj2_x(i,1) = xt_value;
299
        Tj2_y(i,1) = yt_value;
300
        Tj2_z(i,1) = zt_value;
301
302 end
    % above worked, now continue for the rest.
303
304
305
306 % next joint given by T_01T_12T_23 translations - movement from base to joint 3
307 % make our general elements for each array
308 movement = T_01*T_12*T_23;
   xt_element = movement(1,4);
310 vt_element = movement(2,4);
311  zt_element = movement(3,4);
312 % fill the joint 2 4x1 arrays
313 Tj3_x = [] ;
    Tj3_y = [];
314
    Tj3_z = [];
315
316
    for i = 1:length(q1_set)
        xt\_value = subs(xt\_element,[q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
317
        yt\_value = subs(yt\_element,[q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
318
        zt\_value = subs(zt\_element, [q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
319
        Tj3_x(i,1) = xt_value;
320
        Tj3_y(i,1) = yt_value;
        Tj3_z(i,1) = zt_value;
322
323
    end
324
325
326 % next joint given by T_01T_12T_23T_34 translations - movement from base to joint 4
327 % note there's no translation in this joint so no change from above.
328 % make our general elements for each array
```

```
329 movement = T_01*T_12*T_23*T_34;
330 xt_element = movement(1,4);
    yt_element = movement(2,4);
332  zt_element = movement(3,4);
333 % fill the joint 2 4x1 arrays
334 \text{ Tj4}_{-x} = [];
    Tj4_y = [];
335
    Tj4_z = [];
336
    for i = 1:length(q1_set)
337
        xt_value = subs(xt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
338
339
        yt\_value = subs(yt\_element, [q1 q2 q3 q4], [q1\_set(i) q2\_set(i) q3\_set(i) q4\_set(i)]);
          \texttt{zt\_value} = \texttt{subs}(\texttt{zt\_element}, [\texttt{q1} \ \texttt{q2} \ \texttt{q3} \ \texttt{q4}], \ [\texttt{q1\_set(i)} \ \texttt{q2\_set(i)} \ \texttt{q3\_set(i)} \ \texttt{q4\_set(i)}]) \ \textbf{\texttt{;}} 
340
341
        Tj4_x(i,1) = xt_value;
        Tj4-y(i,1) = yt\_value;
342
        Tj4_z(i,1) = zt_value;
343
    end
344
345
    \% final joint given by T_01T_12T_23T_34T_45 translations - movement from base to joint 4
346
    % note there's no translation in this joint so no change from above.
347
   % make our general elements for each array
349 movement = T_01*T_12*T_23*T_34*T_45;
    xt_element = movement(1,4);
351
    yt_element = movement(2,4);
352  zt_element = movement(3,4);
353 % fill the joint 2 4x1 arrays
    EE = [] ; % End Effector Positions list
354
    for i = 1:length(q1_set)
355
        xt_value = subs(xt_element, [q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
356
357
        yt_value = subs(yt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
358
         zt_value = subs(zt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
        EE(i,1) = xt\_value ; % x values in column 1
359
         EE(i,2) = yt_value ; % y values in column 2
360
        EE(i,3) = zt_value ; % z values in column 3
361
362
363
    % Check if end effector positions match points to plot.
364
    disp("EE values (should match points to plot): ")
365
    disp(EE)
366
    disp("do they match? 0 = no, 1 = yes: ")
367
    isequal(round(trajectories, 4, "decimals"), round(EE, 4, "decimals"))
368
369
370
    figure (2)
371
         % generate the graph. Note: only 4 joints will be visible as there is
372
        % no spatial distinction between joints three and 4.
373
374
    for i = 1:NoP % zeros is the base position, doesn't change.
        xx = [base; Tj1_x(i); Tj2_x(i); Tj3_x(i); Tj4_x(i); EE(i,1)];
375
        yy = [base; Tj1_y(i); Tj2_y(i); Tj3_y(i); Tj4_y(i); EE(i,2)];
376
         zz = [base; Tj1_z(i); Tj2_z(i); Tj3_z(i); Tj4_z(i); EE(i,3)];
377
        axis([ 0 0.2 0 0.2 0 0.3 ])
378
        plot3(xx,yy,zz,'ko-','Linewidth',2)
379
380
        hold on % CHANGE TO HOLD ON TO SEE ALL LINES AT ONCE.
        pause (0.3)
381
382
        % label axes, start point, end point.
383
        text(EE(1,1) + 0.002, EE(1,2) + 0.002, EE(1,3) + 0.002, 'Start');
384
        text(EE(end,1) + 0.002, EE(end,2) + 0.002, EE(end,3) + 0.002, 'End');
385
386
387
        % label end effector points
        text(EE(i,1),EE(i,2),EE(i,3), 'x')
388
389
    title('Actual Points'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
390
391
392
    figure (3) % end points only
393
    for i = 1:NoP
394
        plot3(EE(i,1),EE(i,2),EE(i,3),'ko-','Linewidth',2)
395
396
         hold on
397
    end
    title('Actual End Points Only'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
```

```
399 axis([ 0 0.2 0 0.2 0 0.3 ])
400
401
402
404 %% Function to find gradient and constant of line equation
    function [grad, const, r_dir, r] = find_line_eqn(x1, x2, y1, y2, z1, z2)
405
406
        % find which vector r = in x, y plane magnitude and direction
407
408
        % r dir is angle from x axis along r, at the point of x1,y1 in the x,y
        % plane.
409
410
        % check for lines along each axis first
411
        % line along z
412
        if (x2 - x1) == 0 && (y2 - y1) == 0
413
            grad = "null" ;
414
            const = "null" ;
415
            r\_dir = 10 ; % max value of atan2 is < pi/2 therefore < 10
416
            r2 = 0;
417
418
            r1 = 0 ;
            r = 0;
419
420
            return
        % line along y
421
        elseif (x2 - x1) == 0
422
423
            r1 = y1;
            r2 = y2;
424
            r = r2 - r1;
425
            r_dir = pi/2;
426
        % line along x
427
        elseif (y2 - y1) == 0
428
            r1 = x1;
429
            r2 = x2;
430
            r = r2 - r1 ;
431
            r_dir = 0;
        else
433
            r1 = sqrt(x1^2 + y1^2);
434
435
            r2 = sqrt(x2^2 + y2^2);
            r = sqrt((y2-y1)^2 + (x2-x1)^2);
436
            r_dir = atan2(y2-y1, x2-x1);
437
            if r_dir < 0
438
439
                r_dir = pi - r_dir;
            end
440
        end
441
        grad = (z2-z1)/(r) ;
443
444
        const = (z1*r2 - z2*r1) / (r) ;
445 end
```

Appendix E: Serial Robot Free Trajectories

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_TASK_FREE_TRAJECTORIES_LynxMotionArm.m

$FINN_TASK_FREE_TRAJECTORIES_LynxMotionArm.m$

```
1 %% Free Trajectories (Arcing motion)
2
3 clear all %#ok<*CLALL> %#ok<*SAGROW>
4 close all
5 clc
6 % link lengths
7 d1 = 0.1;
s 11 = 0.1 ;
9 	 12 = 0.1 ;
10 	 13 = 0.1 ;
11
  % assuming 10 HZ robot, performing each line in 1 second
13 %% FREE MOTION
14 %1. do IK to find angles to reach each point
15 %2. sample angle intervals to show trajectories
16 %3. get expanded angles list
17 %4. run FK.
18
19 %% Define points to plot
20 points_to_plot = [[0.0 0.0 0.2]; [0.15 0.0 0.2]; [0.15 0.0 0.1]; [0.0 0.0 0.1]; [0.15 0.15 0.2]; ...
       [0.15 0.15 0.1]; [0.0 0.15 0.1]; [0.0 0.15 0.2]];
22 %% Run IK
23 for j = 1:size(points_to_plot,1)
^{24}
      px = points_to_plot(j,1);
       py = points_to_plot(j,2);
25
       pz = points_to_plot(j,3) ;
26
27
       \mbox{\ensuremath{\$}} mu and psi angles for orientation
       mu = 0; % mu is rotation of end effector relative to "wrist"
29
30
       psi = (0:pi/20:2*pi);
       for i = 1: length(psi)
31
           psi(i) = psi(i) - pi/2;
32
       End_Effector = [ px py pz ]';
34
       if norm(End_Effector) > 11+12+13+d1 % workspace is above ground
35
           error('desired position is out of the workspace')
36
37
38
39
       40
       % For details on calculations, view notes in ReadMe.
41
       % We must find values for the 5 joint angles below.
42
43
       sym q1 ; % single value
       q2 = [] ; % potentially many values
44
45
       q3 = [] ; % potentially many values
       q4 = []; % potentially many values
46
       sym q5 ; % single value
47
48
       %% Simple angles to find:
49
50
       % Find q1
51
       q1 = atan2(py,px);
       % Find q5
53
       q5 = mu;
54
55
       %% Define extra variables to help us find q2,3,4
56
57
       % define (r,z) plane
58
```

```
r = sqrt(px^2 + py^2); % r is hypotenues in x-y plane.
59
60
        % For each value of psi, there is a value of rw, zw and D
61
        r_w = (1:length(psi));
62
        z_w = (1:length(psi));
63
        D = (1:length(psi));
64
        for i = 1:length(psi)
65
66
        % define position of wrist in (r,z) plane
            r_w(i) = r - 13*cos(psi(i)); %r_w and z_w will be real as cos or sin of a real number is ...
67
                a real number
68
            z_w(i) = pz - d1 - 13*sin(psi(i));
69
70
            % define D - a placeholder variable for a large combination we derived in
71
72
            % notes
73
            D(i) = - (r_w(i)^2 + z_w(i)^2 - 11^2 - 12^2) / (2*11*12);
74
            D(i) = round(D(i), 7) ;% rounding D avoids fake imaginary numbers due to rounding
75
                            % errors.
76
77
        end
        %% get only real values
78
79
80
        psi_real = [] ;
        r_w_real = [];
81
82
        z_w_real = [];
        D_real = [] ;
83
        for i = 1:length(psi)
84
           if imag(sqrt(1-D(i)^2)) == 0 % for real values, append to real lists.
85
                psi_real(end + 1) = psi(i);%round(psi(i),7); % round each list to get zeros rather ...
86
                    than e^{-10} or something.
                r_w_real(end + 1) = r_w(i); %round(r_w(i), 7);
87
                z_{w}=(end + 1) = z_{w}(i); round(z_{w}(i), 7) ;
88
                D_{real(end + 1) = D(i); round(D(i), 7);
89
90
            end
91
        end
92
93
        % we can see these four lists MUST have same length.
        % disp(psi_real)
94
        % disp(D_real)
95
        % disp(z_w_real)
96
97
        % disp(r_w_real)
98
        %% Find q3 possibilities
99
        % there are two posibilities for each value of D depending on
100
        for i = 1:length(D_real)
101
102
            q3(end+1) = atan2( sqrt(1-D_real(i)^2), -D_real(i)) ;
103
            q3(end+1) = atan2(-sqrt(1-D_real(i)^2), -D_real(i));
104
105
        end
106
        % disp("q3")
107
108
        % disp(q3)
        %% Explaining list order.
109
110
        % matlab indexes from 1 not 0.
        % if D has 3 values, we can see q3 will have 6, where
111
        % D(1) corresponds to q3(1 \& 2)
112
        % D(2) corresponds to q3(3 & 4)
113
114
        % D(3) corresponds to q3(5 \& 6)
115
        % we can see D(i) corresponds to values
        % q3(2*i -1) and q3(2*i)
116
117
        % we need to ensure this is *consistant* across all q lists below.
        %% Find q2
118
119
        % two options based on q3
120
        for i = 1:length(D_real)
121
122
            % for each r_w,z_w value, find first q2 value using first q3 value.
            % Switching order here corrects angles... why?
123
            124
            % add +1 to
125
126
            q2 (end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(l2*sin(q3(2*i-1)), ...
```

```
11+12*cos(q3(2*i-1)));
127
        end
128
        % disp("q2")
        % disp(q2)
129
        %% Find q4
130
131
        % two options based on two sets of q2,q3
132
133
        % use psi = q2 + q3 + q4
        for i = 1:length(D_real)
134
135
             q4(end+1) = psi\_real(i) - q2(2*i -1) - q3(2*i -1) + pi/2;
             q4 (end+1) = psi\_real(i) - q2(2*i) - q3(2*i) +pi/2;
136
137
138
        % disp("q4")
139
        % disp(q4)
140
        %% Remove duplicate values
141
142
        % make a matrix out of the lists where one row is one solution
143
        % we know matrix will have initial size: no. of items in q2,3 or 4 \times 5
144
145
        % angles
        Solution_Matrix = zeros(length(q2), 5);
146
        for i = 1:length(q2)
147
             Solution_Matrix(i,1) = q1;
148
             Solution_Matrix(i,2) = q2(i);
149
150
             Solution_Matrix(i,3) = q3(i);
             Solution_Matrix(i,4) = q4(i);
151
152
             Solution_Matrix(i,5) = q5;
153
        end
        % disp(Solution_Matrix)
154
155
        % remove duplicate rows
156
        Unique_Solutions = unique(Solution_Matrix, "rows", "stable") ;
157
        % stable prevents order being changed.
158
159
        \% we also know, q4 can't be more than 360 degrees. filter these out.
160
        valid_Solutions = [];
161
162
        for i = 1:size(Unique_Solutions,1)
             if abs(Unique_Solutions(i,4)) < 2*pi</pre>
163
                 valid_Solutions = [valid_Solutions; Unique_Solutions(i,:)];
164
165
            end
166
        % stable prevents order being changed.
167
             for i = 1:5
168
                 IK_OUTPUT(j,i) = valid_Solutions(1,i);
169
170
171
172
    end
    disp("Using IK: Array of g1-5 values:")
173
    disp(IK_OUTPUT);
175
176
177
    %% Expand angles to include motion between points
178
179 % define points per line and new list
180 points_per_line = 10 ;
    expanded_angles = zeros((size(points_to_plot,1) - 1)*points_per_line, 5);
181
182
183
    % populate new list
184
    for i = 1:(size(points_to_plot,1) - 1)
        for j = 1:points_per_line
185
            expanded_angles(((i-1)*10+j),1) = IK_OUTPUT(i,1) + (IK_OUTPUT(i+1,1) - IK_OUTPUT(i,1)) ...
186
                * j/points_per_line ;%q3
            expanded_angles(((i-1)*10+j),2) = IK_OUTPUT(i,2) + (IK_OUTPUT(i+1,2) - IK_OUTPUT(i,2)) ...
187
                * j/points_per_line ;%q3
             \texttt{expanded\_angles(((i-1)*10+j),3)} = \texttt{IK\_OUTPUT(i,3)} + (\texttt{IK\_OUTPUT(i+1,3)} - \texttt{IK\_OUTPUT(i,3)}) \dots 
188
                * j/points_per_line ;%q3
            \texttt{expanded\_angles(((i-1)*10+j),4)} = \texttt{IK\_OUTPUT(i,4)} + (\texttt{IK\_OUTPUT(i+1,4)} - \texttt{IK\_OUTPUT(i,4)}) \dots
189
                * j/points_per_line ;%q3
            \texttt{expanded\_angles(((i-1)*10+j),5)} = \texttt{IK\_OUTPUT(i,5)} + (\texttt{IK\_OUTPUT(i+1,5)} - \texttt{IK\_OUTPUT(i,5)}) \dots
190
                * j/points_per_line ;%q3
```

```
191
192
        end
193
    end
    disp(" Array of Expanded Angles: ")
194
195 disp(expanded_angles)
196 %% 3. use FK to plot the arm trajectory in 3d space
    syms q1 q2 q3 q4 q5; % angle variables
197
198
    % Show our 5 tranformation matrices
199
200
    T_{-}01 = [
    [\cos(q1), 0, \sin(q1), 0]
201
    [\sin(q1), 0, -\cos(q1), 0]
202
           0, 1,
203
                        0. d11
           0, 0,
                         0, 1]];
204
205
    T_12 = [
206
    [\cos(q2), -\sin(q2), 0, 11*\cos(q2)]
207
    [\sin(q2), \cos(q2), 0, 11*\sin(q2)]
208
          0,
                     0, 1,
209
210
           0,
                      0, 0,
                                      1]];
211
    T_23 = [
212
    [\cos(q3), -\sin(q3), 0, 12*\cos(q3)]
213
214 [\sin(q3), \cos(q3), 0, 12*\sin(q3)]
215 [
          0,
                     0, 1,
                                      01
           0,
                      0, 0,
                                      1]];
216
    [
217
    T_34 = [
218
    [\cos(q4), 0, \sin(q4),
219
                                      0]
    [\sin(q4), 0, -\cos(q4),
220
221
    Γ
           0, 1,
                         0,
                                      01
222
           0, 0,
                         Ο,
                                      1]];
223
224 \quad T_45 = [
225 [cos(q5), -sin(q5), 0,
                             0]
    [\sin(q5), \cos(q5), 0,
226
                            13]
227
           0,
                      0, 1,
                      0, 0, 1]];
228
           0,
229
    % Get overall forward kinematics
230
231
    T_e = T_01*T_12*T_23*T_34*T_45;
232
    % extract the x,y,z elements of these
233
xt-element = T-e(1,4); % the x transformation is the 4th element of the 1st row of our general ...
        transformation matrix, T_e.
    yt_element = T_e(2,4); % the y transformation is the 4th element of the 2nd row of our general ...
235
        transformation matrix, T_e.
    zt-element = T_{-e}(3,4); % the z transformation is the 4th element of the 3rd row of our general ...
236
        transformation matrix, T_e.
237
    % Define all our angles in their own arrays
239 q1_set = [] ;
q2_{set} = [];
q_{3} = [];
242 q4_set = [] ;
    q5\_set = [];
243
    for i = 1:size(expanded_angles,1) % i in range number of rows
244
245
        % number of columns always 5 for q1-5
246
        q1_set(i) = expanded_angles(i,1);
        q2_set(i) = expanded_angles(i,2);
247
        q3_set(i) = expanded_angles(i,3);
248
        q4_set(i) = expanded_angles(i,4);
249
        q5_set(i) = expanded_angles(i,5);
250
    end
251
252
253
254
    %Now simply plot using our FK
256
257
```

```
258 % define variable for number of points
259
    NoP = size(expanded_angles,1); % same as number of sets of q values.
260
261
    %base is at origin
_{262} base = 0 ;
263
264
265
    % next joint given by T01 translations (movement from base to joint 1)
266 % need to make into a 4 by 3 array.
267 Tj1_x = zeros(NoP,1) ; % x translation is zero
268 Tj1_y = zeros(NoP,1) ; % y translation is zero
269
    Tj1_z = subs(zeros(NoP,1), 0, d1); % z translation is d1
270
271 % next joint given by T_01T_12 translations - movement from base to joint 2
272 % make our general elements for each array
273 movement = T_01*T_12;
274 xt_element = movement(1,4);
275 yt_element = movement(2,4);
276  zt_element = movement(3,4);
277 % fill the joint 2 4x1 arrays
|_{278} Tj2_x = [];
    Tj2_y = [];
279
280 \text{ Tj}2_z = [];
for i = 1:length(q1_set)
282
        xt\_value = subs(xt\_element, [ q1 q2], [q1\_set(i) q2\_set(i)]) ;
        yt\_value = subs(yt\_element, [ q1 q2], [q1\_set(i) q2\_set(i)]) ;
283
284
        zt_value = subs(zt_element, [ q1 q2], [q1_set(i) q2_set(i)]);
        Tj2_x(i,1) = xt_value;
285
        Tj2_y(i,1) = yt_value;
286
287
        Tj2_z(i,1) = zt_value;
    end
288
    % above worked, now continue for the rest.
289
290
291
292 % next joint given by T-01T-12T-23 translations - movement from base to joint 3
293 % make our general elements for each array
294 movement = T_01*T_12*T_23;
295 xt_element = movement(1,4);
296  yt_element = movement(2,4);
297  zt_element = movement(3,4) ;
    % fill the joint 2 4x1 arrays
298
299 \text{ Tj3}_x = [];
300 \text{ Tj3_y} = [];
301 \text{ Tj3_z} = [];
302 for i = 1:length(q1_set)
        xt\_value = subs(xt\_element, [q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
303
        yt_value = subs(yt_element,[q1 q2 q3], [q1_set(i) q2_set(i) q3_set(i)]);
304
        zt_value = subs(zt_element,[q1 q2 q3], [q1_set(i) q2_set(i) q3_set(i)]);
305
        Tj3_x(i,1) = xt_value;
306
        Tj3_y(i,1) = yt_value;
307
        Tj3_z(i,1) = zt_value;
308
309
    end
310
311
312 % next joint given by T_01T_12T_23T_34 translations - movement from base to joint 4
    % note there's no translation in this joint so no change from above.
314 % make our general elements for each array
315 movement = T_01*T_12*T_23*T_34;
316  xt_element = movement(1,4);
317 yt_element = movement(2,4);
    zt_element = movement(3,4);
319 % fill the joint 2 4x1 arrays
320 \text{ Tj4}_x = [];
321 \quad Tj4_y = [];
    Tj4_z = [];
322
    for i = 1:length(q1_set)
323
        xt_value = subs(xt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
324
        yt_value = subs(yt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
325
326
        zt_value = subs(zt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
327
        Tj4_x(i,1) = xt_value;
```

```
328
        Tj4_y(i,1) = yt_value;
        Tj4_z(i,1) = zt_value;
329
    end
330
331
332 % final joint given by T_01T_12T_23T_34T_45 translations - movement from base to joint 4
333 % note there's no translation in this joint so no change from above.
334 % make our general elements for each array
335 movement = T_01*T_12*T_23*T_34*T_45;
336 xt_element = movement(1,4);
337 yt_element = movement(2,4);
338  zt_element = movement(3,4);
339
    % fill the joint 2 4x1 arrays
340 EE = [] ; % End Effector Positions list
    for i = 1:length(q1_set)
341
        xt_value = subs(xt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
342
         yt\_value = subs(yt\_element, [q1 \ q2 \ q3 \ q4], \ [q1\_set(i) \ q2\_set(i) \ q3\_set(i) \ q4\_set(i)]) \ ; \\
343
         zt_value = subs(zt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
344
        EE(i,1) = xt\_value ; % x values in column 1
345
        EE(i,2) = yt_value ; % y values in column 2
346
347
        EE(i,3) = zt\_value ; % z values in column 3
    end
348
349
    \ensuremath{\mbox{\$}} Check if end effector positions match points to plot.
350
351 % disp("EE values (should match points to plot): ")
352 % disp(EE)
    % disp("do they match? 0 = no, 1 = yes: ")
353
    % isequal(round(points_to_plot, 4, "decimals"), round(EE, 4, "decimals"))
355
    figure (2)
356
357
         % generate the graph. Note: only 4 joints will be visible as there is
358
         % no spatial distinction between joints three and 4.
359
    for i = 1:NoP % zeros is the base position, doesn't change.
360
361
         xx = [base; Tj1_x(i); Tj2_x(i); Tj3_x(i); Tj4_x(i); EE(i,1)];
362
        yy = [base; Tj1_y(i); Tj2_y(i); Tj3_y(i); Tj4_y(i); EE(i,2)];
         zz = [base; Tj1_z(i); Tj2_z(i); Tj3_z(i); Tj4_z(i); EE(i,3)];
363
364
         axis([ 0 0.2 0 0.2 0 0.3 ])
        plot3(xx,yy,zz,'ko-','Linewidth',2)
365
        hold on % CHANGE TO HOLD ON TO SEE ALL LINES AT ONCE.
366
        pause (0.3)
367
368
        % label axes, start point, end point.
369
        text(EE(1,1) + 0.002, EE(1,2) + 0.002, EE(1,3) + 0.002, 'Start');
370
        text(EE(end,1) + 0.002,EE(end,2) + 0.002,EE(end,3) + 0.002,'End');
371
372
373
         % label end effector points
        \text{text}(\text{EE}(i,1), \text{EE}(i,2), \text{EE}(i,3), 'x')
374
375
    title('Actual Points'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
376
377
378
379
    figure (3) % end points only
    for i = 1:NoP
380
381
        plot3(EE(i,1), EE(i,2), EE(i,3), 'ko-', 'Linewidth',2)
        hold on
382
383
384 title('Actual End Points Only'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
385 axis([ 0 0.2 0 0.2 0 0.3 ])
```

Appendix F: Serial Robot Obstacle Avoidance

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_TASK_OBSTACLE.m

FINN_TASK_OBSTACLE.m

```
%% Bug 2 Obstacle Avoidance
2 % linear motion (straight lines)
3 clear all %#ok<*CLALL> %#ok<*SAGROW>
4 close all
5 clc
6 % link lengths
  d1 = 0.1;
s 11 = 0.1 ;
9 	 12 = 0.1 ;
10 	 13 = 0.1 ;
11
  % assuming 10 HZ robot, performing each line in 1 second
{f 13} % Using free motion rather than linear so as to track curved objects as
14 % well as straight line ones.
16 %% Object avoidance
  % this file works in the following steps
18 % 1. object boundaries defined, currently a cube directly in the object
19 % path. Object task is still to plot the corners of a larger cube as in the
20 % previous free motion task.
   % 2. Ik and Fk are performed for the task, the end effector positions are
  % then sampled to see where they first impact and leave the object.
23 % 3. The end effector path is corrected using the obstacle avoidance function at the end
^{24} % to the bug 2 algorithm moving along the edge of the object.
{\bf 25}~\% 4. IK and FK are re run with the new final path to ensure correct q1-5
26 % values and maintain link lengths.
  % 5. Robot motion is plotted to show it still hits the desired points and
28 % avoids the object.
29
30
31 %% Define the object
32
33 % object is a smaller cuboid, detail x,y,z dimensions
34 % i = initial, f = final
35 \text{ ob_x_i} = 0.06;
36 \text{ ob}_x_f = 0.12;
37
38 \text{ ob_y_i} = 0.01;
39 \text{ ob-y-f} = 0.07;
40
41 ob_z_i = 0.12;
42 \text{ ob_z_f} = 0.18;
43
44 % Define whole object using an array
45 % define points per line for each axis and object array
46 points_per_line = 10;
47  object = zeros(points_per_line+1,3) ;
48
49 % populate object array
50
   for i = 1:(points_per_line + 1)
       object(i,1) = ob_x_i + (i-1)*(ob_x_f - ob_x_i)/points_per_line;
51
       object(i,2) = ob_y_i + (i-1)*(ob_y_f - ob_y_i)/points_per_line;
52
       object(i,3) = ob_z_i + (i-1)*(ob_z_f - ob_z_i)/points_per_line;
54 end
55 % disp(object)
  %% Define points to plot
57 points_to_plot = [[0.0 0.0 0.2]; [0.15 0.0 0.2]; [0.15 0.0 0.1]; [0.0 0.0 0.1]; [0.15 0.15 0.2]; ...
        [0.15 \ 0.15 \ 0.1]; [0.0 \ 0.15 \ 0.1]; [0.0 \ 0.15 \ 0.2]];
58
```

```
59
    %% Run IK
60
    for j = 1:size(points_to_plot,1)
61
        px = points_to_plot(j,1);
62
        py = points_to_plot(j,2);
63
64
        pz = points_to_plot(j,3);
65
66
        % mu and psi angles for orientation
        mu = 0; % mu is rotation of end effector relative to "wrist"
67
        psi = (0:pi/20:2*pi);
68
        for i = 1: length(psi)
69
            psi(i) = psi(i) - pi/2;
70
71
        End_Effector = [ px py pz ]';
72
        if norm(End_Effector) > 11+12+13+d1 % workspace is above ground
73
           error('desired position is out of the workspace')
74
75
76
77
78
        %% %%%%%%%%%%% Inverse Kinematics of LynxMotion Arm %%%%%%%%%%%%%%%%%%%%%
        % For details on calculations, view notes in ReadMe.
79
        % We must find values for the 5 joint angles below.
80
81
        sym q1 ; % single value
        q2 = [] ; % potentially many values
82
83
        q3 = []; % potentially many values
        q4 = []; % potentially many values
84
85
        sym q5; % single value
86
        %% Simple angles to find:
87
88
        % Find q1
89
        q1 = atan2(py,px);
90
        % Find q5
91
        q5 = mu;
93
        %% Define extra variables to help us find q2,3,4
94
95
        % define (r.z) plane
96
        r = sqrt(px^2 + py^2); % r is hypotenues in x-y plane.
97
98
99
        % For each value of psi, there is a value of rw, zw and D
100
        r_w = (1:length(psi));
        z_w = (1:length(psi));
101
        D = (1:length(psi));
102
        for i = 1:length(psi)
103
104
        % define position of wrist in (r,z) plane
            r_w(i) = r - 13*cos(psi(i)); %r_w and z_w will be real as cos or sin of a real number is ...
105
                a real number
106
            z_w(i) = pz - d1 - 13*sin(psi(i));
107
108
109
            % define D - a placeholder variable for a large combination we derived in
            % notes
110
111
            D(i) = - (r_w(i)^2 + z_w(i)^2 - 11^2 - 12^2) / (2*11*12);
112
            D(i) = round(D(i), 7) ;% rounding D avoids fake imaginary numbers due to rounding
113
114
                             % errors.
115
        %% get only real values
116
117
        psi_real = [] ;
118
        r_w_real = [];
119
        z_w_real = [];
120
        D_real = [] ;
121
        for i = 1:length(psi)
122
            if imag(sqrt(1-D(i)^2)) == 0 % for real values, append to real lists.
123
                psi\_real(end + 1) = psi(i); round(psi(i), 7); round each list to get zeros rather ...
124
                    than e^-10 or something.
125
                r_w_real(end + 1) = r_w(i); round(r_w(i), 7);
126
                z_{w}=(end + 1) = z_{w}(i); round(z_{w}(i), 7) ;
```

```
D_{real(end + 1) = D(i); round(D(i), 7);
127
                            end
 128
 129
                    end
 130
                   % we can see these four lists MUST have same length.
 131
 132
                   % disp(psi_real)
                   % disp(D_real)
 133
 134
                   % disp(z_w_real)
                   % disp(r_w_real)
 135
136
                   %% Find q3 possibilities
 137
 138
                    % there are two posibilities for each value of D depending on
                   for i = 1:length(D_real)
 139
 140
                             q3(end+1) = atan2(sqrt(1-D_real(i)^2), -D_real(i));
 141
                             q3(end+1) = atan2(-sqrt(1-D_real(i)^2), -D_real(i));
 142
 143
 144
                    % disp("q3")
 145
 146
                    % disp(q3)
                    %% Explaining list order.
 147
                   % matlab indexes from 1 not 0.
 148
                   % if D has 3 values, we can see q3 will have 6, where
 149
                   % D(1) corresponds to q3(1 \& 2)
 150
 151
                   % D(2) corresponds to q3(3 & 4)
                   % D(3) corresponds to q3(5 & 6)
 152
 153
                    % we can see D(i) corresponds to values
                   % q3(2*i -1) and q3(2*i)
 154
                   % we need to ensure this is *consistant* across all q lists below.
 155
 156
                   %% Find q2
 157
                    % two options based on q3
 158
                   for i = 1:length(D_real)
 159
 160
                             % for each r_w,z_w value, find first q2 value using first q3 value.
 161
                             % Switching order here corrects angles... why?
                              q2 \, (\texttt{end} + 1) \, = \, \texttt{atan2} \, (\texttt{z\_w\_real} \, (\texttt{i}) \, , \, \texttt{r\_w\_real} \, (\texttt{i})) \, + \, \texttt{atan2} \, (\texttt{12} \, \times \, \texttt{sin} \, (\texttt{q3} \, (2 \, \times \, \texttt{i})) \, ) \, , \, \, \texttt{11} + \texttt{12} \, \times \, \texttt{cos} \, (\texttt{q3} \, (2 \, \times \, \texttt{i})) \, ) \, ) \, ; \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, ) \, , \, \rangle \, , \, ) \, , \, \rangle \, , 
 162
 163
                             % add +1 to
                            q2 (end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(l2*sin(q3(2*i-1)), ...
 164
                                       11+12*cos(q3(2*i-1)));
 165
                   end
                    % disp("q2")
 166
                   % disp(q2)
 167
                    %% Find q4
 168
 169
                   % two options based on two sets of q2,q3
 170
                    % use psi = q2 + q3 + q4
 171
                    for i = 1:length(D_real)
 172
                             q4(end+1) = psi\_real(i) - q2(2*i-1) - q3(2*i-1) + pi/2;
 173
 174
                             q4(end+1) = psi\_real(i) - q2(2*i) - q3(2*i) + pi/2;
                   end
 175
 176
 177
                    % disp("q4")
 178
 179
                    % disp(q4)
                   %% Remove duplicate values
 180
                    % make a matrix out of the lists where one row is one solution
 181
 182
 183
                   % we know matrix will have initial size: no. of items in q2,3 or 4 x 5
 184
                   % angles
                    Solution_Matrix = zeros(length(q2), 5);
 185
                   for i = 1: length(q2)
 186
                             Solution_Matrix(i,1) = q1;
 187
                             Solution_Matrix(i,2) = q2(i);
 188
                             Solution_Matrix(i,3) = q3(i);
 189
                             Solution_Matrix(i,4) = q4(i);
 190
 191
                             Solution_Matrix(i,5) = q5;
 192
                   end
                    % disp(Solution_Matrix)
 193
 194
                   % remove duplicate rows
                   Unique_Solutions = unique(Solution_Matrix, "rows", "stable") ;
195
```

```
196
         % stable prevents order being changed.
197
198
         %% we also know, q4 can't be more than 360 degrees. filter these out.
199
         valid_Solutions = [] ;
200
201
         for i = 1:size(Unique_Solutions,1)
             if abs(Unique_Solutions(i,4)) < 2*pi</pre>
202
203
                  valid_Solutions = [valid_Solutions; Unique_Solutions(i,:)];
             end
204
205
         % stable prevents order being changed.
206
207
             for i = 1:5
                  IK_OUTPUT(j,i) = valid_Solutions(1,i) ;
208
209
210
    end
211
    % disp("Using IK: Array of q1-5 values:")
212
    % disp(IK_OUTPUT);
213
214
215
    %% Expand angles to include motion between points
216
217
218
    % define points per line and new list
219 points_per_line = 10;
220
    expanded_angles = zeros((size(points_to_plot,1) - 1)*points_per_line, 5);
221
222
    % populate new list
    for i = 1:(size(points_to_plot,1) - 1)
223
224
         for j = 1:points_per_line
            \texttt{expanded\_angles(((i-1)*10+j),1)} = \texttt{IK\_OUTPUT(i,1)} + (\texttt{IK\_OUTPUT(i+1,1)} - \texttt{IK\_OUTPUT(i,1)}) \dots
225
                 * j/points_per_line ;%q3
            expanded_angles(((i-1)*10+j),2) = IK_OUTPUT(i,2) + (IK_OUTPUT(i+1,2) - IK_OUTPUT(i,2)) ...
226
                 * j/points_per_line ;%q3
227
            expanded_angles(((i-1)*10+j),3) = IK_OUTPUT(i,3) + (IK_OUTPUT(i+1,3) - IK_OUTPUT(i,3)) ...
                 * j/points_per_line ;%q3
            \texttt{expanded\_angles(((i-1)*10+j),4)} = \texttt{IK\_OUTPUT(i,4)} + (\texttt{IK\_OUTPUT(i+1,4)} - \texttt{IK\_OUTPUT(i,4)}) \dots
228
                 * j/points_per_line ;%q3
             \texttt{expanded\_angles(((i-1)*10+j),5)} = \texttt{IK\_OUTPUT(i,5)} + (\texttt{IK\_OUTPUT(i+1,5)} - \texttt{IK\_OUTPUT(i,5)}) \dots 
229
                 * j/points_per_line ;%q3
230
231
         end
232
    end
    % disp(expanded_angles)
233
    \$\$ 3. use FK to plot the arm trajectory in 3d space and save the end effector points to display ...
         the smiley face.
    %IK_OUTPUT = [[45 30 30 30 0]*pi/180]
235
    syms q1 q2 q3 q4 q5; % angle variables
236
237
    % Show our 5 tranformation matrices
238
    T_01 = [
239
    [\cos(q1), 0, \sin(q1),
240
241
    [\sin(q1), 0, -\cos(q1), 0]
           0, 1,
                         0, d1]
242
    [
243
            0, 0,
                          0, 1]];
    [
244
    T_12 = [
245
    [\cos(q2), -\sin(q2), 0, 11*\cos(q2)]
246
    [\sin(q2), \cos(q2), 0, 11*\sin(q2)]
247
248
    Γ
           0,
                       0, 1,
                                        0.1
            0,
                       0, 0,
                                        111;
249
    ſ
250
    T_{23} = [
251
   [\cos(q3), -\sin(q3), 0, 12*\cos(q3)]
253 [sin(q3), cos(q3), 0, 12*sin(q3)]
           Ο,
                       0, 1,
254
    ſ
255
            0,
                       0, 0,
                                        1]];
256
257 \quad T_34 = [
                                        0.1
258 [cos(q4), 0, sin(q4),
259 [sin(q4), 0, -cos(q4),
```

```
0, 1,
260
                          0,
                                        0.1
                          0,
261
            0.0.
                                        111:
262
263 T 45 = [
    [\cos(q5), -\sin(q5), 0, 0]
265
    [\sin(q5), \cos(q5), 0, 0]
                       0, 1, 13]
0, 0, 1]];
           Ο,
266
267
            0,
268
269
    % Get overall forward kinematics
T_{e} = T_{01} * T_{12} * T_{23} * T_{34} * T_{45};
271
272 % extract the x,y,z elements of these
273 xt-element = T-e(1,4); % the x transformation is the 4th element of the 1st row of our general ...
         transformation matrix, T_e.
yt_element = T_e(2,4); % the y transformation is the 4th element of the 2nd row of our general \dots
         transformation matrix, T_e.
    zt-element = T_-e(3,4); % the z transformation is the 4th element of the 3rd row of our general ...
275
         transformation matrix, T_e.
276
    % Define all our angles in their own arrays
277
278
    q1\_set = [];
q2-set = [];
q_{3}=[];
q4_set = [];
q5_set = [];
    for i = 1:size(expanded_angles,1) % i in range number of rows
         % number of columns always 5 for q1-5
284
         q1_set(i) = expanded_angles(i,1);
285
286
         q2\_set(i) = expanded\_angles(i,2);
         q3_set(i) = expanded_angles(i,3);
287
         q4_set(i) = expanded_angles(i,4);
288
         q5_set(i) = expanded_angles(i,5);
289
290
291
    % final joint given by T_01T_12T_23T_34T_45 translations - movement from base to joint 4
292
    % note there's no translation in this joint so no change from above.
294 % make our general elements for each array
295 movement = T_01*T_12*T_23*T_34*T_45;
296 xt_element = movement(1,4);
297
    yt_element = movement(2,4);
    zt_element = movement(3,4);
298
299 % fill the joint 2 4x1 arrays
300 EE = [] ; % End Effector Positions list
    for i = 1:length(q1_set)
301
          \texttt{xt\_value} = \texttt{subs}(\texttt{xt\_element}, \texttt{[q1 q2 q3 q4]}, \texttt{ [q1\_set(i) q2\_set(i) q3\_set(i) q4\_set(i)])}; 
302
         yt_value = subs(yt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
303
          \texttt{zt\_value} = \texttt{subs}(\texttt{zt\_element}, [\texttt{q1} \ \texttt{q2} \ \texttt{q3} \ \texttt{q4}], \ [\texttt{q1\_set(i)} \ \texttt{q2\_set(i)} \ \texttt{q3\_set(i)} \ \texttt{q4\_set(i)}]) \ \textbf{;} 
304
         EE(i,1) = xt_value ; % x values in column 1
305
         EE(i,2) = yt\_value ; % y values in column 2
306
         EE(i,3) = zt_value ; % z values in column 3
307
308
    end
309
310 % Check if end effector positions match points to plot.
    % disp("EE values: ")
311
    % disp(EE)
313 % disp("do they match? 0 = no, 1 = yes: ")
314 % isequal(round(points_to_plot, 4, "decimals"), round(EE, 4, "decimals"))
315
     %% Check when obstacle in way
316
317 %object
318 % object is a smaller cuboid, detail x,y,z dimensions
319 % i = initial, f = final
320 \% ob_x_i = 0.06;
    % ob_x_f = 0.12 ;
321
322 %
323 % ob_y_i = 0.01;
324 % ob_y_f = 0.07;
325 %
326 % ob_z_i = 0.12 ;
```

```
327 % ob_z_f = 0.18 ;
328
    EE_off_limits = [] ;
329
    for i = 1: (size(EE, 1))
330
         if ( ob_x_i \leq EE(i,1) ) && ( EE(i,1) \leq ob_x_f ) && ( ob_y_i \leq EE(i,2) ) && ( EE(i,2) \leq ob_y_f ...
331
             ) && ( ob_{z-i} \le EE(i,3) ) && ( EE(i,3) \le ob_{z-f} )
            disp("obstacle hit at point ")
332
333
            EE(i,:)
            EE_off_limits = [EE_off_limits, i];
334
335
336
    end
    % disp("off limit rows: " + EE_off_limits)
337
338
    disp(EE_off_limits)
339 length(EE_off_limits)
340 % Function to replot in this interval - go one back from the off limits to
341 % find EE values before the robot hits the object.
    avoid_obstacle = bug2(EE_off_limits(1)-1, EE_off_limits(end)+1, EE, object);
342
343
    % size(EE,1)
344
345 % remove off limit rows from EE
    for i = 1:length(EE_off_limits)
346
         \mathtt{EE}(\mathtt{EE\_off\_limits}(1),\;:) = [] ; % remove the first value each time to get correct one.
347
348
    % size(EE,1)
349
350
    % add in bug values to show navigating the obstacle.
351
    rerouted_EE = zeros((size(EE,1)+size(avoid_obstacle,1)),3);
    % length(rerouted_EE)
353
    for i = 1:size(rerouted_EE,1)
354
        if i < EE_off_limits(1)
355
356
               disp("add EE 1")
357
    응
               disp(i)
             rerouted_EE(i, :) = EE(i, :);
358
359
         elseif i < (EE_off_limits(1)+size(avoid_obstacle,1))</pre>
               disp("add ob avoid")
360
    읒
               disp(i)
361
362
             rerouted_EE(i, :) = avoid_obstacle((i-(EE_off_limits(1)-1)) , :);
363
               disp("add EE 2")
364
    응
365
               disp(i)
             rerouted_EE(i, :) = EE(i-size(avoid_obstacle,1), :);
366
367
         end
    end
368
    EE = rerouted_EE ;
369
370
371
    %% Run IK and FK again to get the new trajectory with obstacle avoidance.
372
    for j = 1:size(EE, 1)
373
374
        px = EE(j,1);
        py = EE(j,2);
375
        pz = EE(j,3);
376
377
        % mu and psi angles for orientation
378
379
        mu = 0; % mu is rotation of end effector relative to "wrist"
        psi = (0:pi/20:2*pi);
380
         for i = 1: length(psi)
381
             psi(i) = psi(i) - pi/2;
382
383
384
        End_Effector = [ px py pz ]';
         if norm(End_Effector) > 11+12+13+d1 % workspace is above ground
385
             error('desired position is out of the workspace')
386
        end
387
388
389
         %% %%%%%%%%%%% Inverse Kinematics of LynxMotion Arm %%%%%%%%%%%%%%%%%%%%
390
391
         % For details on calculations, view notes in ReadMe.
        % We must find values for the 5 joint angles below.
392
         sym q1; % single value
393
        q2 = [] ; % potentially many values
394
        q3 = []; % potentially many values
395
```

```
q4 = []; % potentially many values
396
        sym q5; % single value
397
398
         %% Simple angles to find:
399
400
        % Find q1
401
        q1 = atan2(py,px);
402
        % Find q5
403
        q5 = mu;
404
405
        %% Define extra variables to help us find q2,3,4
406
407
        % define (r,z) plane
408
        r = sqrt(px^2 + py^2); % r is hypotenues in x-y plane.
409
410
        % For each value of psi, there is a value of rw, zw and D
411
         r_w = (1:length(psi));
412
         z_w = (1:length(psi));
413
        D = (1:length(psi));
414
415
        for i = 1:length(psi)
         % define position of wrist in (r,z) plane
416
             r_w(i) = r - 13*cos(psi(i)); %r_w and z_w will be real as cos or sin of a real number is ...
417
                 a real number
418
             z_w(i) = pz - d1 - 13*sin(psi(i));
419
420
421
             % define D - a placeholder variable for a large combination we derived in
             % notes
422
423
            D(i) = - (r_w(i)^2 + z_w(i)^2 - 11^2 - 12^2) / (2*11*12);
424
425
            D(i) = round(D(i), 7); rounding D avoids fake imaginary numbers due to rounding
426
                              % errors.
        end
427
428
        %% get only real values
429
        psi_real = [] ;
430
         r_w_real = [] ;
431
         z_w_real = [];
432
        D_real = [] ;
433
         for i = 1:length(psi)
434
             if imag(sqrt(1-D(i)^2)) == 0 % for real values, append to real lists.
435
                 psi_real(end + 1) = psi(i);%round(psi(i),7); % round each list to get zeros rather ...
436
                     than e^-10 or something.
                 r_w_real(end + 1) = r_w(i); round(r_w(i), 7);
437
                 z_{w}=(end + 1) = z_{w}(i); round(z_{w}(i), 7);
438
                 D_{real}(end + 1) = D(i); %round(D(i), 7);
439
             end
440
441
442
        % we can see these four lists MUST have same length.
443
         % disp(psi_real)
444
        % disp(D_real)
445
        % disp(z_w_real)
446
447
        % disp(r_w_real)
448
        %% Find q3 possibilities
449
        \mbox{\ensuremath{\upsigma}} there are two posibilities for each value of D depending on
450
451
         for i = 1:length(D_real)
452
             q3(end+1) = atan2(sqrt(1-D_real(i)^2), -D_real(i));
453
454
             q3(end+1) = atan2(-sqrt(1-D_real(i)^2), -D_real(i));
        end
455
456
        % disp("q3")
457
         % disp(q3)
458
459
        %% Explaining list order.
        % matlab indexes from 1 not 0.
460
        \mbox{\%} if D has 3 values, we can see q3 will have 6, where
461
        % D(1) corresponds to q3(1 & 2)
462
        % D(2) corresponds to q3(3 \& 4)
463
```

```
464
                        % D(3) corresponds to q3(5 & 6)
                        % we can see D(i) corresponds to values
 465
 466
                        % q3(2*i -1) and q3(2*i)
                        \mbox{\%} we need to ensure this is \star\mbox{consistant}\star\mbox{ across all } q lists below.
 467
                        %% Find q2
 468
 469
                        % two options based on q3
 470
 471
                        for i = 1:length(D_real)
                                   % for each r_w,z_w value, find first q2 value using first q3 value.
 472
 473
                                    % Switching order here corrects angles... why?
                                    \texttt{q2}\,(\texttt{end+1}) \; = \; \texttt{atan2}\,(\texttt{z\_w\_real}\,(\texttt{i})\,, \texttt{r\_w\_real}\,(\texttt{i})) \; \; + \; \texttt{atan2}\,(\texttt{12} \times \texttt{sin}\,(\texttt{q3}\,(\texttt{2} \times \texttt{i}))\,, \;\; \texttt{11} + \texttt{12} \times \texttt{cos}\,(\texttt{q3}\,(\texttt{2} \times \texttt{i}))\,) \;\; ; \\ \texttt{q2}\,(\texttt{end+1}) \; = \; \texttt{atan2}\,(\texttt{z\_w\_real}\,(\texttt{i})\,, \texttt{r\_w\_real}\,(\texttt{i})) \; \; + \; \texttt{atan2}\,(\texttt{12} \times \texttt{sin}\,(\texttt{q3}\,(\texttt{2} \times \texttt{i}))\,, \;\; \texttt{11} + \texttt{12} \times \texttt{cos}\,(\texttt{q3}\,(\texttt{2} \times \texttt{i}))) \;\; ; \\ \texttt{q2}\,(\texttt{end+1}) \; = \; \texttt{atan2}\,(\texttt{z\_w\_real}\,(\texttt{i})\,, \texttt{r\_w\_real}\,(\texttt{i})) \;\; + \; \texttt{atan2}\,(\texttt{12} \times \texttt{sin}\,(\texttt{q3}\,(\texttt{2} \times \texttt{i}))\,, \;\; \texttt{11} + \texttt{12} \times \texttt{cos}\,(\texttt{q3}\,(\texttt{2} \times \texttt{i}))) \;\; ; \\ \texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}\,(\texttt{q3}
 474
 475
                                    % add +1 to
                                   q2 (end+1) = atan2(z_w_real(i), r_w_real(i)) + atan2(l2*sin(q3(2*i-1)), ...
 476
                                                11+12*cos(q3(2*i-1)));
 477
                        % disp("q2")
 478
                        % disp(q2)
 479
                        %% Find q4
 480
 481
 482
                        % two options based on two sets of q2,q3
                        % use psi = q2 + q3 + q4
 483
                        for i = 1:length(D_real)
 484
                                   q4(end+1) = psi_real(i) - q2(2*i -1) - q3(2*i -1) + pi/2;
 485
                                   q4 (end+1) = psi_real(i) - q2(2*i) - q3(2*i) + pi/2;
 486
                        end
 487
 488
 489
                        % disp("q4")
                        % disp(q4)
 490
                        %% Remove duplicate values
 491
 492
                        % make a matrix out of the lists where one row is one solution
 493
 494
                        % we know matrix will have initial size: no. of items in q2,3 or 4 \times 5
                        % angles
 495
 496
                        Solution_Matrix = zeros(length(q2), 5);
 497
                        for i = 1: length(q2)
                                   Solution_Matrix(i,1) = q1;
 498
 499
                                    Solution_Matrix(i,2) = q2(i);
                                   Solution_Matrix(i,3) = q3(i);
500
                                    Solution_Matrix(i,4) = q4(i);
501
                                   Solution_Matrix(i,5) = q5;
 502
 503
 504
                        % disp(Solution_Matrix)
                        % remove duplicate rows
505
                        Unique_Solutions = unique(Solution_Matrix, "rows", "stable") ;
 506
                        % stable prevents order being changed.
 507
 508
 509
                        \% we also know, q4 can't be more than 360 degrees. filter these out.
510
511
                        valid_Solutions = [];
                        for i = 1:size(Unique_Solutions,1)
512
                                     % condition for a valid solution: q4 is within 0 - 2pi, q2 is more
 513
514
                                    \mbox{\%} than 45% to avoid arm hitting the box
                                    if abs(Unique_Solutions(i,4)) < 2*pi && Unique_Solutions(i,2) > pi/3
515
516
                                               valid_Solutions = [valid_Solutions; Unique_Solutions(i,:)];
                                   end
517
                        end
 518
                        % stable prevents order being changed.
519
520
                                    for i = 1:5
                                               IK_OUTPUT(j,i) = valid_Solutions(1,i);
521
                                   end
522
            end
 523
524
525
526
           %% Plot the arm trajectory in 3d space
527
 528
            syms q1 q2 q3 q4 q5; % angle variables
529
          % Show our 5 tranformation matrices
530
531 T_01 =[
[\cos(q1), 0, \sin(q1), 0]
```

```
[\sin(q1), 0, -\cos(q1), 0]
                   0, d1]
534 [ 0, 1,
535
            0, 0,
                         0, 1]];
536
537 T<sub>-</sub>12 = [
[\cos(q2), -\sin(q2), 0, 11*\cos(q2)]
    [\sin(q2), \cos(q2), 0, 11*\sin(q2)]
539
540
           0,
                      0, 1,
            0,
                      0, 0,
541
                                      111:
542
543 \quad T_23 = [
    [\cos(q3), -\sin(q3), 0, 12*\cos(q3)]
[\sin(q3), \cos(q3), 0, 12*\sin(q3)]
544
545
         0,
                  0, 1,
546
            0,
                      0, 0,
                                      1]];
547
548
549
    T_34 = [
    [\cos(q4), 0, \sin(q4),
                                      0.1
550
    [\sin(q4), 0, -\cos(q4),
                                      0]
551
          0, 1,
                       0,
                                      0]
           0, 0,
                         0,
                                      111:
553
554
555 T_45 = [
[\cos(q5), -\sin(q5), 0, 0]
557 [sin(q5), cos(q5), 0, 0]
                      0, 1, 13]
0, 0, 1]];
           0,
558
559
            Ο,
                      0, 0,
560
561 % Get overall forward kinematics
T_e = T_01 * T_12 * T_23 * T_34 * T_45;
563
564 % extract the x,y,z elements of these
xt.element = T_{-e}(1,4); % the x transformation is the 4th element of the 1st row of our general ...
        transformation matrix, T_e.
566 yt-element = T-e(2,4); % the y transformation is the 4th element of the 2nd row of our general ...
        transformation matrix, T_e.
567
    zt-element = T-e(3,4); % the z transformation is the 4th element of the 3rd row of our general ...
        transformation matrix, T_e.
568
569 % Define all our angles in their own arrays
570 q1_set = [] ;
571 q2_set = [] ;
572 q3_set = [] ;
573 	 q4\_set = [];
574 	ext{ q5_set} = [];
    for i = 1:size(IK_OUTPUT,1) % i in range number of rows
575
        \% number of columns always 5 for q1-5
576
        q1\_set(i) = IK\_OUTPUT(i,1);
577
578
        q2\_set(i) = IK\_OUTPUT(i,2);
        q3\_set(i) = IK\_OUTPUT(i,3);
579
        q4\_set(i) = IK\_OUTPUT(i,4);
580
581
         q5\_set(i) = IK\_OUTPUT(i,5);
    end
582
583
584
585
    %Now simply plot using our FK
586
587
588
    % define variable for number of points
589
    NoP = size(IK_OUTPUT,1); % same as number of sets of q values.
590
591
592 %base is at origin
593 base = 0 ;
594
595
596 % next joint given by T01 translations (movement from base to joint 1)
597 % need to make into a 4 by 3 array.
598 Tj1_x = zeros(NoP,1) ; % x translation is zero
599 Tj1_y = zeros(NoP,1) ; % y translation is zero
```

```
| 600 \text{ Tj1_z} = \text{subs}(\text{zeros}(\text{NoP,1}), 0, d1) ; % z translation is d1
601
    % next joint given by T_01T_12 translations - movement from base to joint 2
603 % make our general elements for each array
604 movement = T_01*T_12;
605 xt_element = movement(1,4);
606 yt_element = movement(2,4);
    zt_element = movement(3,4);
608 % fill the joint 2 4x1 arrays
609 \quad T \dot{j} 2_x = [] ;
610 \text{ Tj2-y} = [];
611
   Tj2_z = [];
    for i = 1:length(q1_set)
612
        xt\_value = subs(xt\_element, [q1 q2], [q1\_set(i) q2\_set(i)]);
613
        yt_value = subs(yt_element, [ q1 q2], [q1_set(i) q2_set(i)]);
614
        zt_value = subs(zt_element, [ q1 q2], [q1_set(i) q2_set(i)]) ;
615
616
        Tj2_x(i,1) = xt_value;
        Tj2_y(i,1) = yt_value;
617
        Tj2_z(i,1) = zt_value;
618
619 end
    % above worked, now continue for the rest.
620
621
622
623 % next joint given by T_01T_12T_23 translations - movement from base to joint 3
624 % make our general elements for each array
625 movement = T_01 * T_12 * T_23;
626 xt_element = movement(1,4);
627 yt_element = movement(2,4);
628  zt_element = movement(3,4);
629 % fill the joint 2 4x1 arrays
630 \quad T \dot{j} 3_x = [];
    Tj3_y = [];
631
632 \quad T j 3_z = [];
633 for i = 1:length(g1_set)
        xt\_value = subs(xt\_element,[q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
634
        yt\_value = subs(yt\_element,[q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
635
        zt\_value = subs(zt\_element, [q1 q2 q3], [q1\_set(i) q2\_set(i) q3\_set(i)]);
636
        Tj3_x(i,1) = xt_value;
637
        Tj3_y(i,1) = yt_value;
638
        Tj3_z(i,1) = zt_value;
639
    end
640
641
642
^{643} % next joint given by T-01T-12T-23T-34 translations - movement from base to joint 4
644 % note there's no translation in this joint so no change from above.
    % make our general elements for each array
646 movement = T_01*T_12*T_23*T_34;
647 xt_element = movement(1,4);
648 yt_element = movement(2,4);
649  zt_element = movement(3,4);
   % fill the joint 2 4x1 arrays
651 \quad Tj4_x = [];
652 \quad T \dot{1}4_{-y} = [];
653 Tj4_z = [];
    for i = 1:length(q1_set)
654
        xt_value = subs(xt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
         yt\_value = subs(yt\_element, [q1 q2 q3 q4], [q1\_set(i) q2\_set(i) q3\_set(i) q4\_set(i)]); \\
656
657
        658
        Tj4_x(i,1) = xt_value;
        Tj4-y(i,1) = yt\_value;
659
        Tj4_z(i,1) = zt_value;
660
661 end
663 % final joint given by T_01T_12T_23T_34T_45 translations - movement from base to joint 4
664 % note there's no translation in this joint so no change from above.
665 % make our general elements for each array
666 movement = T_01*T_12*T_23*T_34*T_45;
667 xt_element = movement(1,4);
668 yt_element = movement(2,4);
669 zt_element = movement(3,4);
```

```
670 % fill the joint 2 4x1 arrays
671 EE = [] ; % End Effector Positions list
    for i = 1:length(q1_set)
        673
        yt_value = subs(yt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
674
675
        zt_value = subs(zt_element,[q1 q2 q3 q4], [q1_set(i) q2_set(i) q3_set(i) q4_set(i)]);
        EE(i,1) = xt_value ; % x values in column 1
676
677
        EE(i,2) = yt_value ; % y values in column 2
        EE(i,3) = zt\_value; % z values in column 3
678
679 end
680 %% Plot the graphs
681
    figure (2)
    % plot the object in the way
682
683 % object has 6 faces, 8 corners.
    ob.x = [ob.x.i, ob.x.i, ob.x.i, ob.x.i; ob.x.i, ob.x.f, ob.x.f, ob.x.i; ob.x.i, ob.x.f, ob.x.f, ...
        ob_x_i; ob_x_f, ob_x_f, ob_x_f, ob_x_f; ob_x_i, ob_x_i, ob_x_f, ob_x_f; ob_x_i, ob_x_i, ...
        ob_x_f, ob_x_f;
    ob_y = [ob_y_i, ob_y_f, ob_y_f, ob_y_i; ob_y_i, ob_y_i, ob_y_i, ob_y_i; ob_y_i, ob_y_f, ob_y_f, ob_y_f, ...
685
        ob_y_f; ob_y_f, ob_y_i, ob_y_i, ob_y_f; ob_y_i, ob_y_f, ob_y_f, ob_y_i; ob_y_i, ob_y_i, ...
        ob_y_f, ob_y_i];
    ob_z = [ob_z_i, ob_z_i, ob_z_f, ob_z_f; ob_z_i, ob_z_i, ob_z_f, ob_z_f; ob_z_f, ob_z_f, ob_z_i, ...
686
        ob_z_i; ob_z_f, ob_z_f, ob_z_i, ob_z_i; ob_z_f, ob_z_f, ob_z_f, ob_z_f; ob_z_i, ob_z_i, ...
        ob_z_i, ob_z_i];
687 fill3(ob_x(1,:),ob_y(1,:),ob_z(1,:),'r')
688 hold on
689 fill3(ob_x(2,:),ob_y(2,:),ob_z(2,:),'r')
690 hold on
691 fill3(ob_x(3,:),ob_y(3,:),ob_z(3,:),'r')
692 hold on
693 fill3(ob_x(4,:),ob_y(4,:),ob_z(4,:),'r')
694 hold on
    fill3(ob_x(5,:),ob_y(5,:),ob_z(5,:),'r')
696 hold on
697 fill3(ob_x(6,:),ob_y(6,:),ob_z(6,:),'r')
698 hold on
        % generate the graph. Note: only 4 joints will be visible as there is
699
        % no spatial distinction between joints three and 4.
700
    for i = 1:NoP % zeros is the base position, doesn't change.
701
        xx = [base; Tj1_x(i); Tj2_x(i); Tj3_x(i); Tj4_x(i); EE(i,1)];
702
703
        yy = [base; Tj1_y(i); Tj2_y(i); Tj3_y(i); Tj4_y(i); EE(i,2)];
        zz = [base; Tj1_z(i); Tj2_z(i); Tj3_z(i); Tj4_z(i); EE(i,3)];
704
        axis([ 0 0.2 0 0.2 0 0.3 ])
705
        plot3(xx,yy,zz,'ko-','Linewidth',2)
706
        hold on % CHANGE TO HOLD ON TO SEE ALL LINES AT ONCE.
707
        pause (0.3)
708
709
        % label axes, start point, end point.
710
        text(EE(1,1) + 0.002, EE(1,2) + 0.002, EE(1,3) + 0.002, 'Start');
711
        text(EE(end,1) + 0.002, EE(end,2) + 0.002, EE(end,3) + 0.002, 'End');
712
713
        % label end effector points
714
715
        \texttt{text} \, (\texttt{EE} \, (\texttt{i}, \texttt{1}) \, , \texttt{EE} \, (\texttt{i}, \texttt{2}) \, , \texttt{EE} \, (\texttt{i}, \texttt{3}) \, , \quad \texttt{'x'})
716 end
    title('Actual Points'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
717
718
719
    figure (3) % end points only
720
721
    % plot the object in the way
722
    % object has 6 faces, 8 corners
723
    ob_x = [ob_x_i, ob_x_i, ob_x_i, ob_x_i, ob_x_i, ob_x_i, ob_x_f, ob_x_f, ob_x_i, ob_x_i, ob_x_f, ...
        ob_x_i; ob_x_f, ob_x_f, ob_x_f, ob_x_f; ob_x_i, ob_x_i, ob_x_f, ob_x_f; ob_x_i, ob_x_i, ...
        ob_x_f, ob_x_f:
725 ob_y = [ob_y_i, ob_y_f, ob_y_f, ob_y_i; ob_y_i, ob_y_i, ob_y_i, ob_y_i; ob_y_f, ob_y_f, ob_y_f, ...
        ob_y_f; ob_y_f, ob_y_i, ob_y_i, ob_y_f; ob_y_i, ob_y_f, ob_y_f, ob_y_i; ob_y_i, ob_y_i, ...
        ob_y_f, ob_y_i];
726 ob_z = [ob_z_i, ob_z_i, ob_z_f, ob_z_f; ob_z_i, ob_z_i, ob_z_f, ob_z_f; ob_z_f, ob_z_f, ob_z_i, ...
        ob_z_i; ob_z_f, ob_z_f, ob_z_i, ob_z_i; ob_z_f, ob_z_f, ob_z_f, ob_z_f; ob_z_i, ob_z_i, ...
        ob_z_i, ob_z_i] ;
727 fill3(ob_x(1,:),ob_y(1,:),ob_z(1,:),'r')
```

```
728 hold on
   fill3(ob_x(2,:),ob_y(2,:),ob_z(2,:),'r')
729
730 hold on
731 fill3(ob_x(3,:),ob_y(3,:),ob_z(3,:),'r')
732 hold on
733 fill3(ob_x(4,:),ob_y(4,:),ob_z(4,:),'r')
734 hold on
735
    fill3(ob_x(5,:),ob_y(5,:),ob_z(5,:),'r')
736 hold on
   fill3(ob_x(6,:),ob_y(6,:),ob_z(6,:),'r')
738 hold on
739
    for i = 1:NoP
740
        plot3(EE(i,1), EE(i,2), EE(i,3), 'ko-', 'Linewidth',2)
741
742
743 end
    title('Actual End Points Only'); xlabel('x (m)'); ylabel('y (m)'); zlabel('z (m)');
744
    axis([ 0 0.2 0 0.2 0 0.3 ])
745
746
747
748
749
   %% Function to Find Where trajectory impacts the object and correct it.
750
   function [Obstacle_Navigation] = bug2(first_off_lim_point, final_off_lim_point, EE_list, object)
751
752
   % find entry point, correct this to be on object surface
753
    % dsearch in allows us to search object surface array for the nearest value
755 % to the entry values we give
756 Entry = EE_list(first_off_lim_point -1, :); % start bug from point before the robot enters the object
757 New_Entry = zeros(1,3);
758 New_Entry(1) = object(dsearchn(object(:,1), Entry(1)), 1);
    New_Entry(2) = object(dsearchn(object(:,2), Entry(2)), 2);
    New_Entry(3) = object(dsearchn(object(:,3), Entry(3)), 3);
760
762 % find exit point, correct this to be on object surface
763 Exit = EE_list(final_off_lim_point +1, :); % end bug from point after the robot enters the object
764 New_Exit = zeros(1,3);
765 New_Exit(1) = object(dsearchn(object(:,1), Exit(1)), 1);
766 New_Exit(2) = object(dsearchn(object(:,2), Exit(2)), 2);
767 New_Exit(3) = object(dsearchn(object(:,3), Exit(3)), 3);
768
769 disp("Meet and leave object surface at: ")
770 disp(New_Entry)
771 disp(New_Exit)
772
    % offset entry and exit points by a tiny amount so points are not on the
773
774 % surface but just outside.
775 New_Entry = New_Entry - 0.003;
776 New_Exit = New_Exit + 0.003;
777
    % Get 10 points between entry and exit points on the surface of our object.
779 % Define whole object using an array
780 % define points per line for each axis and object array
781  ZMotion_points_on_object = 5 ;
782 xyMotion_points_on_object = 10;
    Obstacle_Navigation = zeros(zMotion_points_on_object+xyMotion_points_on_object+1,3);
784
785
    % populate object array
786
    % first go up to top of object (z motion)
    for i = 1:(zMotion_points_on_object + 1)
787
        Obstacle_Navigation(i,1) = New_Entry(1);
788
        Obstacle_Navigation(i,2) = New_Entry(2);
789
        Obstacle_Navigation(i,3) = New_Entry(3) + (i-1)*(New_Exit(3) - ...
790
            New_Entry(3))/zMotion_points_on_object ;
791
    end
792
793
794
    %then go across the top of the object (x-y motion)
795
796 for i = 1:(xyMotion_points_on_object + 1)
```

Appendix G: Parallel Robot Inverse Kinematics

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_IK_PARALLEL_BOT.m

FINN_IK_PARALLEL_BOT.m

```
%% Inverse Kinematics Calculator for LynxMotion Arm
1
2 clear all %#ok<*CLALL> %#ok<*SAGROW>
3 close all
4 clc
   %% STEPS - FULL NOTES ON DRIVE
7
8 % 1. SPECIFY ROBOT PARAMETERS
9 % 2. SPECIFY DESIRED END POSITION (x-c, y-c, a)
10 % 3. SOLVE IK \rightarrow find (j1, j2, j3) for each arm.
11 % 4. PRINT THE 8 POSSIBLE ORIENTATIONS, DISPLAY 2 OF THESE IN FIGURES ONE
   % AND TWO.
_{\rm 13} % using q for arm 1 angles.
14 % using s for arm 2 angles (skipping r to avoid confusing with radius
15 % values.
16 % using t for arm 3 angles.
17 %% 1. SPECIFY ROBOT PARAMETERS
_{\rm 18} % these values are taken from coursework appendix
19 S_A = 0.17; % j1 to j2 link length
_{20} L = 0.13 ; % j2 to j3 link length
r_e = 0.13; % radius of circle formed by end effector joints
r_b = 0.29; % radius of circle formed by base joints
23
25
26 %% 2. SPECIFY DESIRED END POSITION (x_c, y_c, a)
27 \text{ x_c} = 0.25;
v_c = 0.21;
29 a = pi/6;
30
31
32 %% arm 1 - joint angles given by q
q3 = a + pi/6;
34 % two possibilities for q1, q2 as they form an "elbow"
35 q1 = [];
36 	 q2 = [];
  [q1(1), q1(2), q2(1), q2(2)] = find_line_eqn(S_A, L, r_e, x_c, y_c, q3);
37
38
40 %% arm 2 - joint angles given by s
41
42 % Find relative position of end effector in this arms frame.
x_c2 = x_c - sqrt(3) * r_b;
44 y_c2 = y_c;
45
46 % Find angles s1, s2, s3
s3 = a + 5*pi/6; % q3 + 120 degrees
48 % two possibilities for s1, s2 as they form an "elbow"
49 	 s1 = [];
50 	 S2 = [] ;
   [s1(1), s1(2), s2(1), s2(2)] = find_line_eqn(S_A, L, r_e, x_c2, y_c2, s3);
52
54 %% arm 3 - joint angles given by t
55
56
57 % Find relative position of end effector in this arms frame.
x_c3 = x_c - sqrt(3) * r_b/2;
59 \text{ y-c3} = \text{y-c} - (3/2) * \text{r-b};
```

```
60
61 % Find angles t1, t2, t3
   t3 = a + 3*pi/2; % s3 + 120 degrees, q3 + 240 degrees
63 % two possibilities for t1, t2 as they form an "elbow"
64 t1 = [];
65 	 t2 = [];
   [t1(1), t1(2), t2(1), t2(2)] = find_line_eqn(S_A, L, r_e, x_c3, y_c3, t3);
66
67
68
69
70\, %% Check that solutions are real
71
   in_workspace = false ;
   angles\_array = [q1(1), q2(1), q1(2), q2(2), q3, s1(1), s2(1), s1(2), s2(2), s3, t1(1), t2(1), ...
        t1(2), t2(2), t3];
_{74} if imag(angles_array) == zeros(1,15)
75
       in_workspace = true ;
76 end
   %% Display Solutions
77
   % there are 2 solutions for each of the 3 arms
   % therefore 2^3 total orientations = 8 total
79
    if in_workspace == true
        disp(" For a given position, there are 8 possible orientations: ")
81
        disp(" ")
82
83
    응
          pause(2)
84
85
        %Referring as arms being in orientation 1 or 2, we have:
        disp("solution 1: ")
86
        disp("orientation: 111")
87
        disp("********")
88
        disp("Arm 1 (q1, q2, q3): ")
89
        disp(q1(1) \star180/pi+ ", " + q2(1) \star180/pi + ", " + q3 \star180/pi)
90
        disp(" ")
91
        disp("Arm 2 (s1, s2, s3): ")
        disp(s1(1) *180/pi+ ", " + s2(1) *180/pi + ", " + s3 *180/pi)
93
        disp(" ")
94
95
        disp("Arm 3 (t1, t2, t3): ")
        disp(t1(1) *180/pi+ ", " + t2(1) *180/pi + ", " + t3 *180/pi)
96
        disp("********")
97
        disp(" ")
98
99
         pause(2)
100
101
        disp("solution 2: ")
102
        disp("orientation: 222")
103
        disp("********")
104
        disp("Arm 1 (q1, q2, q3): ")
105
        disp(q1(2) *180/pi+ ", " + q2(2) *180/pi + ", " + q3 *180/pi)
106
107
        disp(" ")
        disp("Arm 2 (s1, s2, s3): ")
108
        disp(s1(2) *180/pi+ ", " + s2(2) *180/pi + ", " + s3 *180/pi)
109
        disp(" ")
110
        disp("Arm 3 (t1, t2, t3): ")
111
        disp( t1(2) *180/pi+ ", " + t2(2) *180/pi + ", " + t3 *180/pi)
112
        disp("********")
113
        disp(" ")
114
         pause(2)
115
116
117
        disp("solution 3: ")
118
119
        disp("orientation: 121")
        disp("********")
120
        disp("Arm 1 (q1, q2, q3): ")
121
        disp(q1(1) *180/pi+ ", " + q2(1) *180/pi + ", " + q3 *180/pi)
122
        disp(" ")
123
124
        disp("Arm 2 (s1, s2, s3): ")
        disp(s1(2) *180/pi+ ", " + s2(2) *180/pi + ", " + s3 *180/pi)
125
        disp(" ")
126
        disp("Arm 3 (t1, t2, t3): ")
127
        disp(t1(1) *180/pi+ ", " + t2(1) *180/pi + ", " + t3 *180/pi)
128
```

```
129
        disp("*******")
        disp(" ")
130
          pause(2)
131
132
        disp("solution 4: ")
133
134
        disp("orientation: 112")
        disp("********")
135
136
        disp("Arm 1 (q1, q2, q3): ")
        disp(q1(1) *180/pi+ ", " + q2(1) *180/pi+ ", " + q3 *180/pi)
137
        disp(" ")
138
        disp("Arm 2 (s1, s2, s3): ")
139
        disp(s1(1) *180/pi+ ", " + s2(1) *180/pi + ", " + s3 *180/pi)
140
        disp(" ")
141
        disp("Arm 3 (t1, t2, t3): ")
142
        disp(t1(2) *180/pi+ ", " + t2(2) *180/pi + ", " + t3 *180/pi)
143
        disp("********")
144
        disp(" ")
145
146
          pause (2)
147
148
        disp("solution 5: ")
        disp("orientation: 211")
149
        disp("********")
150
        disp("Arm 1 (q1, q2, q3): ")
151
        disp(q1(2) *180/pi+ ", " + q2(2) *180/pi + ", " + q3 *180/pi)
152
153
        disp(" ")
        disp("Arm 2 (s1, s2, s3): ")
154
155
        disp(s1(1) *180/pi+ ", " + s2(1) *180/pi + ", " + s3 *180/pi)
        disp(" ")
156
        disp("Arm 3 (t1, t2, t3): ")
157
        disp(t1(1) *180/pi+ ", " + t2(1) *180/pi + ", " + t3 *180/pi)
158
        disp("********")
159
        disp(" ")
160
          pause(2)
161
162
        disp("solution 6: ")
163
        disp("orientation: 221")
164
        disp("********")
165
        disp("Arm 1 (q1, q2, q3): ")
166
        disp(q1(2) *180/pi+ ", " + q2(2) *180/pi + ", " + q3 *180/pi)
167
        disp(" ")
168
        disp("Arm 2 (s1, s2, s3): ")
169
        disp(s1(2) *180/pi+ ", " + s2(2) *180/pi + ", " + s3 *180/pi)
170
        disp(" ")
171
        disp("Arm 3 (t1, t2, t3): ")
172
        disp(t1(1) *180/pi+ ", " + t2(1) *180/pi + ", " + t3 *180/pi)
173
174
        disp("********")
        disp(" ")
175
176
          pause(2)
177
        disp("solution 7: ")
178
        disp("orientation: 212")
179
        disp("*******")
180
        disp("Arm 1 (q1, q2, q3): ")
181
        disp(q1(2) *180/pi+ ", " + q2(2) *180/pi + ", " + q3 *180/pi)
182
        disp(" ")
183
        disp("Arm 2 (s1, s2, s3): ")
184
        disp(s1(1) *180/pi+ ", " + s2(1) *180/pi + ", " + s3 *180/pi)
185
        disp(" ")
186
        disp("Arm 3 (t1, t2, t3): ")
187
        disp(t1(2) *180/pi+ ", " + t2(2) *180/pi + ", " + t3 *180/pi)
188
        disp("********")
189
        disp(" ")
190
191
          pause (2)
192
        disp("solution 8: ")
193
194
        disp("orientation: 122")
        disp("********")
195
        disp("Arm 1 (q1, q2, q3): ")
196
        disp(q1(1) *180/pi+ ", " + q2(1) *180/pi+ ", " + q3 *180/pi)
197
198
        disp(" ")
```

```
disp("Arm 2 (s1, s2, s3): ")
199
         disp(s1(2) *180/pi+ ", " + s2(2) *180/pi + ", " + s3 *180/pi)
200
         disp(" ")
201
         disp("Arm 3 (t1, t2, t3): ")
202
         disp(t1(2) *180/pi+ ", " + t2(2) *180/pi + ", " + t3 *180/pi)
203
204
         disp("********")
         disp(" ")
205
206
207
     else
208
         disp("Chosen Position is outside of robot workspace.")
     end
209
210
211
     %% Plot the position of the robot
212
213
214 figure(1) % orientation 1
     % plot the outer triangle
215
216 % bottom left, bottom right, top
217 \text{ tri_x} = [0, \text{ sqrt}(3)*r_b, (1/2)*sqrt(3)*r_b, 0];
218 tri_y = [0, 0, (3/2)*r_b, 0];
219 plot(tri_x,tri_y,'ro-','Linewidth',2)
    hold on
220
221
222
223 % Plot arm 1
224 \text{ xj1} = 0;
x_{225} x_{j2} = x_{j1} + S_A * cos(q1(1));
|_{226} xj3 = xj2 + L*cos(q2(1));
227 \text{ arm1}_x = [xj1, xj2, xj3];
228
229 yj1 = 0;
    yj2 = yj1 + S_A*sin(q1(1));
yj3 = yj2 + L*sin(q2(1));
232 \text{ arm1_y} = [yj1, yj2, yj3];
233
234 plot(arm1_x, arm1_y, 'co-', 'Linewidth', 2)
235
    hold on
236
237
238 % Plot arm 2
239 \text{ xj1} = \text{sqrt}(3) * r_b ;
x_{240} x_{12} = x_{11} + S_A * cos(s1(1));
241 	 xj3 = xj2 + L*cos(s2(1));
242 \text{ arm} 2_x = [xj1, xj2, xj3];
243
244 y j1 = 0;
    yj2 = yj1 + S_A*sin(s1(1));
245
246 \text{ yj3} = \text{yj2} + \text{L*sin}(\text{s2}(1));
247 \text{ arm} 2_y = [yj1, yj2, yj3];
248
    plot(arm2_x, arm2_y, 'co-','Linewidth',2)
249
250
    hold on
251
252 % Plot arm 3
253 \text{ xj1} = (1/2) * \text{sqrt}(3) * \text{r_b};
x_{254} x_{12} = x_{11} + S_A * cos(t1(1));
255 \text{ xj3} = \text{xj2} + \text{L} \cdot \cos(\text{t2}(1));
256 \text{ arm3}_x = [xj1, xj2, xj3];
257
_{258} yj1 = (3/2)*r_b;
    yj2 = yj1 + S_A*sin(t1(1));
260 \text{ yj3} = \text{yj2} + \text{L}*\sin(\text{t2}(1));
261 \text{ arm3_y} = [yj1, yj2, yj3];
262
263 plot(arm3_x, arm3_y, 'co-', 'Linewidth', 2)
264
    hold on
265
    %plot inner triangle
266
inner_triangle_x = [arm1_x(3), arm2_x(3), arm3_x(3), arm1_x(3)];
|_{268} inner_triangle_y = [arm1_y(3), arm2_y(3), arm3_y(3), arm1_y(3)];
```

```
269 plot(inner_triangle_x, inner_triangle_y, 'bo-', 'Linewidth', 2)
     hold on
270
271
272 axis([ -0.1 0.6 -0.1 0.6])
273 title('Parallel Robot First Orientation for a = pi/6'); xlabel('x (m)'); ylabel('y (m)');
subtitle ('End Effector at x = 0.25, y = 0.21');
275
276
277
278
     %**************
279 figure(2) % orientation 2
280
     % plot the outer triangle
281 % bottom left, bottom right, top
282 tri_x = [0, sqrt(3)*r_b, (1/2)*sqrt(3)*r_b, 0];
283 tri_y = [0, 0, (3/2)*r_b, 0];
284 plot(tri_x,tri_y,'ro-','Linewidth',2)
285
286
287
288 % Plot arm 1
289 \quad x \dot{1} = 0 ;
xj2 = xj1 + S_A * cos(q1(2));
xj3 = xj2 + L*cos(q2(2));
292 \text{ arm1}_x = [xj1, xj2, xj3];
293
294 yj1 = 0;
 yj2 = yj1 + S_A*sin(q1(2));
296 \text{ yj3} = \text{yj2} + \text{L}*\sin(\text{q2}(2));
    arm1_y = [yj1, yj2, yj3];
297
298
     plot(arm1_x, arm1_y, 'co-', 'Linewidth', 2)
299
     hold on
300
301
302
303 % Plot arm 2
304 \text{ xj1} = \text{sqrt}(3) * r_b;
     xj2 = xj1 + S_A * cos(s1(2));
306 \text{ xj3} = \text{xj2} + \text{L} \cdot \text{cos}(\text{s2}(2));
307 \text{ arm2}_{-x} = [xj1, xj2, xj3] ;
308
309 yj1 = 0;
310 \text{ yj2} = \text{yj1} + S_A * \sin(s1(2));
311 \text{ yj3} = \text{yj2} + \text{L*sin(s2(2))};
arm2_y = [yj1, yj2, yj3];
313
314 plot(arm2_x, arm2_y, 'co-', 'Linewidth', 2)
315
     hold on
316
317 % Plot arm 3
x_{318} x_{j1} = (1/2) * sqrt(3) * r_b;
xj2 = xj1 + S_A * cos(t1(2));
x_{320} x_{320}
arm3_x = [xj1, xj2, xj3];
322
323 \text{ yj1} = (3/2) * r_b;
     yj2 = yj1 + S_A * sin(t1(2));
325 \text{ yj3} = \text{yj2} + \text{L*sin(t2(2))};
326 \text{ arm3_y} = [yj1, yj2, yj3];
327
     plot(arm3_x, arm3_y, 'co-', 'Linewidth', 2)
328
     hold on
329
330
331 %plot inner triangle
inner_triangle_x = [arm1_x(3), arm2_x(3), arm3_x(3), arm1_x(3)];
inner_triangle_y = [arm1_y(3), arm2_y(3), arm3_y(3), arm1_y(3)];
     plot(inner_triangle_x, inner_triangle_y, 'bo-', 'Linewidth', 2)
334
335 hold on
336
337 axis([ -0.1 0.6 -0.1 0.6])
338 title('Parallel Robot Second Orientation for a = pi/6'); xlabel('x (m)'); ylabel('y (m)');
```

```
339 subtitle('End Effector at x = 0.25, y = 0.21');
340 %% Function to find angles 1 & 2 using angle 3 and coords of end effector
341 % arm base frame
342
343 function [angle1_a, angle1_b, angle2_a, angle2_b] = find_line_eqn(S_A, L, r_e, x_ee, y_ee, angle3)
344
345 % find x3, y3 the position of the joint at angle3
x3 = x_e - r_e * cos(angle3);
y3 = y_ee - r_e*sin(angle3);
348
349 % calculate both angle1 values
angle1_a = atan2(y3,x3) + acos((S_A^2 + x3^2 + y3^2 - L^2) / (2*S_A*sqrt(x3^2 + y3^2))); angle1_b = atan2(y3,x3) - acos((S_A^2 + x3^2 + y3^2 - L^2) / (2*S_A*sqrt(x3^2 + y3^2)));
352
353 % calculate both angle2 values
354
355 % for angle1_a,
angle2\_a = -(pi - angle1\_a - acos((S\_A^2 + L^2 - x3^2 - y3^2)/(2*S\_A*L)));
357 % for angle1_b,
358 angle2_b = +(pi + angle1_b - acos((S_A^2 + L^2 - x3^2 - y3^2)/(2*S_A*L)));
359
360 end
```

Appendix H: Parallel Robot WorkSpace

Code available at: https://github.com/Hinlo/MatLab-Simulation-of-Serial-and-Parallel-Robots/blob/main/FINN_WS_PARALLEL_BOT.m

FINN_WS_PARALLEL_BOT.m

```
%% Parallel Robot WorkSpace Plotter.
1
2 clear all %#ok<*CLALL> %#ok<*SAGROW>
3 close all
4 clc
6
   %% STEPS - FULL NOTES ON DRIVE
7
   % 1. SPECIFY ROBOT PARAMETERS
9 % 2. SPECIFY RANGE OF DESIRED END POSITIONS (x_c, y_c, a)
10 % 4. SOLVE IK \rightarrow find (j1, j2, j3) for each arm AT EACH POSITION.
11 % using q for arm 1 angles.
   % using s for arm 2 angles (skipping r to avoid confusing with radius
13 % values.
14 % using t for arm 3 angles.
15 % IGNORE IMAGINARY POSITIONS, PLOT REAL POSITIONS TO GET AN OUTLINE OF WS
16 %% 1. SPECIFY ROBOT PARAMETERS
17 % these values are taken from coursework appendix
18 S_A = 0.17; % j1 to j2 link length
19 L = 0.13; % j2 to j3 link length
r_e = 0.13; % radius of circle formed by end effector joints
r_b = 0.29; % radius of circle formed by base joints
22
23
25 %% 2. SPECIFY DESIRED END POSITION (x_c, y_c, a)
x_c = -0.1:0.01:0.6; % test ranges for x and y
   y_c = -0.1:0.01:0.6;
28 a = pi/12; % constant orientation - interesting values for plot: 0, pi/12, pi/6, pi/2.3
30\, % pre-make lists for the elbow angles
31 q1 = zeros(length(x_c) \star length(y_c),2); % 2 angles at each position for elbow angles 1 and 2
q2 = zeros(length(x_c)*length(y_c), 2);
33
s1 = zeros(length(x_c)*length(y_c),2); % Repeat for s angles
s2 = zeros(length(x_c)*length(y_c),2);
36
37
38 t1 = zeros(length(x_c) * length(y_c), 2); % Repeat for t angles
39 t2 = zeros(length(x_c) * length(y_c), 2);
40
  %% arm 1 - joint angles given by q
41
42 	 q3 = a + pi/6 ;
43 count = 1;
44 % two possibilities for q1, q2 as they form an "elbow"
45 for i = 1: length(x_c)
46
       for j = 1: length(y_c)
            [q1(count,1), \ q1(count,2), \ q2(count,1), \ q2(count,2)] = find\_line\_eqn(S\_A, \ L, \ r\_e, \ x\_c(i), \ \dots ] 
47
               y_c(j), q3);
48
           count = count + 1;
49
       end
   end
50
51
52 %% arm 2 - joint angles given by s
53
54 % Find relative position of end effector in this arms frame.
x_c2 = x_c - sqrt(3) *r_b;
56 \text{ y_c2} = \text{y_c};
58 % Find angles s1, s2, s3
```

```
s3 = a + 5*pi/6; % q3 + 120 degrees
   count = 1;
60
    % two possibilities for s1, s2 as they form an "elbow"
61
    for i = 1: length(x_c)
62
        for j = 1: length(y_c)
             [s1(count,1),\ s1(count,2),\ s2(count,1),\ s2(count,2)] = find\_line\_eqn(S\_A,\ L,\ r\_e,\ x\_c2(i),\ \dots ] 
64
                y_c2(j), s3);
65
            count = count + 1;
        end
66
67
    end
    % arm 3 - joint angles given by t
68
69
70
71 % Find relative position of end effector in this arms frame.
x_c3 = x_c - sqrt(3) * r_b/2;
y_c3 = y_c - 3*r_b/2;
74
    % Find angles t1, t2, t3
75
76 	 t3 = a + 3*pi/2 ; % s3 + 120 degrees, q3 + 240 degrees
   count = 1;
    % two possibilities for t1, t2 as they form an "elbow"
78
    for i = 1: length(x_c)
79
80
        for j = 1: length(y_c)
             [t1(count,1), t1(count,2), t2(count,1), t2(count,2)] = find_line_eqn(S_A, L, r_e, x_c3(i), ...
81
                y_c3(j), t3);
            count = count + 1;
82
83
        end
84
    end
85
86
    %% Generate array of only real solutions
87
    in_workspace = [];
    count = 1;
88
    for i = 1: length(x_c)
89
        for j = 1:length(y_c)
            angles\_array\_elbow1 = [x\_c(i), y\_c(j), q1(count,1), q2(count,1), q3, s1(count,1), ...
91
                s2(count,1), s3, t1(count,1), t2(count,1), t3];
            angles\_array\_elbow2 = [x\_c(i), y\_c(j), q1(count, 2), q2(count, 2), q3, s1(count, 2), \dots
92
                s2(count,2), s3, t1(count,2), t2(count,2), t3];
            if isreal(angles_array_elbow1) % boolean check for whether array contains imaginary numbers
93
               in_workspace = [in_workspace; angles_array_elbow1] ; % if passed, append the real row
94
95
            if isreal(angles_array_elbow2)% boolean check for whether array contains imaginary numbers
96
               in_workspace = [in_workspace; angles_array_elbow2] ; % if passed, append the real row
97
            count = count + 1:
99
100
101
    end
102
    disp(in_workspace)
103
104
    % print statement to let user know if no real solutions
105
106
    if isemptv(in_workspace)
        disp("Chosen value of *a* has no real workspace!")
107
108
    end
109
110
    % get only the position values from these.
111
   workspace_positions = [in_workspace(:,1) , in_workspace(:,2) ] ;
112
113
114
115 %% Display Solutions on Graph
116 figure (1)
117 % plot the outer triangle
118 % bottom left, bottom right, top
119 tri_x = [0, sqrt(3)*r_b, (1/2)*sqrt(3)*r_b, 0];
120 \text{ tri_y} = [0, 0, (3/2) * r_b, 0];
plot(tri_x,tri_y,'ro-','Linewidth',2)
122 hold on
123
124 % Plot the individual points
```

```
plot (workspace_positions(:,1), workspace_positions(:,2), "kx")
126 hold on
127
128
129 % Plot the workspace outline
outline = convhull(workspace_positions);
131 plot(workspace_positions(outline,1), workspace_positions(outline,2), "c")
132
133 legend("Robot Base", "End Effector Positions", "Workspace Area")
134 axis([ -0.1 0.6 -0.1 0.6])
135 title('Parallel Robot WorkSpace for a = ', num2str(a)); xlabel('x (m)'); ylabel('y (m)');
136
137 %% Function to find angles 1 & 2 using angle 3 and coords of end effector
138 % arm base frame
140 function [anglel_a, anglel_b, angle2_a, angle2_b] = find_line_eqn(S_A, L, r_e, x_ee, y_ee, angle3)
141
142 % find x3, y3 the position of the joint at angle3
x3 = x_ee - r_e*cos(angle3);
y3 = y_ee - r_e*sin(angle3);
145
146 % calculate both angle1 values
147 anglel_a = atan2(y3,x3) + acos((S_A^2 + x3^2 + y3^2 - L^2) / (2*S_A*sqrt(x3^2 + y3^2)));
148 angle1_b = atan2(y3,x3) - acos((S_A^2 + x3^2 + y3^2 - L^2) / (2*S_A*sgrt(x3^2 + y3^2)));
149
150 % calculate both angle2 values
151
152 % for angle1_a,
153 angle2_a = -(pi - angle1_a - acos((S_A^2 +L^2 - x3^2 - y3^2)/(2*S_A*L)));
154 % for angle1_b,
angle2_b = +(pi + angle1_b - acos((S_A^2 +L^2 - x3^2 - y3^2)/(2*S_A*L)));
156
157 end
```

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