

# TUWA

# Numericals

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# UNIT 1

Q. For a Tx line, RLCG components are given by  $R = 50 \Omega$ ,  $L = 1 \text{ mH}$ ,  $G = 0.1 \text{ mS}$ ,  $C = 1 \mu\text{F}$  respectively

Find  $Z_0$ ,  $\alpha$ ,  $\beta$ ,  $\gamma$  at  $f = 1 \text{ MHz}$

A.  $f = 10^6 \text{ Hz}$

$$Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = \sqrt{\frac{5+j(2\pi \times 10^6 \times 10^{-3})}{0.1+j(2\pi \times 10^6 \times 10^{-6})}} = 999.87^{0.5} \angle 0.266/2 = 31.62 \angle 0.433 \quad \left( \sqrt{\gamma} = \gamma^{0.5} \angle 0^\circ \right)$$

$$\gamma = \sqrt{(R+j\omega L)(G+j\omega C)} = \sqrt{(5+j(2\pi \times 10^6 \times 10^{-3}))(0.1+j(2\pi \times 10^6 \times 10^{-6}))} = 39493.429^{0.5} \angle 179.04/2 = 198.7 \angle 89.52 = 1.66 + j198.69$$

$$\gamma = \alpha + j\beta$$

$$\alpha = 1.66$$

$$\beta = 198.69$$

Q. A Generator of 1V, 1kHz supplies power to a 100km long line terminating in  $Z_0$  and having the characteristic constants given below. Calculate characteristic impedance, propagation constant, wavelength, velocity, voltage and efficiency.  $R = 10.4 \Omega/\text{km}$ ;  $L = 0.00367 \text{ H/km}$ ;  $G = 0.8 \times 10^{-6} \text{ S/km}$ ;  $C = 0.00835 \times 10^{-6} \text{ F/m}$

A. Given,  $Z_L = Z_0$ ,  $V_s = 1 \text{ V}$ ,  $f = 1 \text{ kHz} = 1000 \text{ Hz}$

$$Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = \sqrt{\frac{482443.7481 \angle -23.412}{694.58 \angle -11.706}} = 694.58 \angle -11.706 \quad \left( \sqrt{\gamma} = \gamma^{0.5} \angle 0^\circ \right)$$

$$Z_0 = \frac{R+j\omega L}{\gamma} \Rightarrow \gamma = \frac{10.4 + j(2\pi \times 10^3 \times 0.00367)}{694.58 \angle -11.706} = 0.036 \angle 77.42^\circ = 7.93 \times 10^{-3} + j0.0355 = \alpha + j\beta \Rightarrow \alpha = 0.00793 \text{ nepers/km}$$

$$\beta = 0.0355 \text{ rad/km}$$

$$\lambda = \frac{2\pi}{\beta} = \frac{2\pi}{0.0355} = \frac{2 \times 3.14}{0.0355} = 176.90 \text{ km}$$

$$v = \frac{\omega}{\beta} = \frac{2\pi \times 1000}{0.0355} = 176901.4 \text{ km/s}$$

$$Z_L = Z_0 \Rightarrow I_s = \frac{V_s}{Z_0} = \frac{1 \angle 0}{694.58 \angle -11.706} = 1.41 \times 10^{-3} + j2.92 \times 10^{-4} = 1.44 \times 10^{-3} \angle 11.706 \text{ A} = 1.44 \angle 11.706 \text{ mA}$$

$$P_s = I_s V_s = 1.44 \angle 11.706 \text{ mA} \times 1 \text{ V} = 1.44 \angle 11.706 \text{ mW}$$

$$I_R = I_s e^{-j\alpha} = 1.44 \angle 11.706 \times e^{-(6.00793 + j0.0355) \times 100} \text{ mA}$$

$$= 1.44 \angle 11.706 \times e^{-0.793} \times e^{-j3.55} \quad | \text{rad} = 57.3^\circ$$

$$= 1.44 \times 0.452 \angle 11.706 \times e^{-j(3.55 \times 57.3)}$$

$$= 1.44 \times 0.452 \angle 11.706 \times \angle -203.411$$

$$= 0.65 \angle -191.705 \text{ mA}$$

$$V_R = I_R Z_L = I_R Z_0 = 0.65 \times 10^{-3} \angle -191.705 \times 694.58 \angle -11.706$$

$$= 0.451477 \angle -203.411 \text{ V}$$

$$P_R = V_R I_R \cos \theta$$

$$= 0.451 \angle -203.411 \times 0.65 \times 10^{-3} \angle -191.705 \times \cos(-203.411 + 191.705)$$

$$= 0.287 \times 10^{-3}$$

$$\eta = \frac{P_R}{P_s} = \frac{0.287 \times 10^{-3}}{1.44 \times 10^{-3}} = 0.1993$$

$$\eta \% = 19.93\%$$

Q. A lossless line has a characteristic impedance of  $400 \Omega$ . Determine SWR if receiving impedance is  $800 \Omega$

A.  $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{800 - 400}{800 + 400} = \frac{400}{1200} = \frac{1}{3}$

$$\text{VSWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 1/3}{1 - 1/3} = \frac{4/3}{2/3} = 2$$

B. A  $50\Omega$  Tx line feeds  $75+j20\Omega$  dipole antenna. Find  $\Gamma$  & VSWR,  $R_{max}$  &  $R_{min}$

A.  $Z_L = 75+j20\Omega$

$Z_0 = 50\Omega$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75+j20 - 50}{75+j20 + 50} = \frac{25+j20}{125+j20} = 0.2529 / 29.56$$

$$VSWR = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.2529}{1 - 0.2529} = 1.677$$

$$R_{max} = VSWR \cdot Z_0 = 1.677 \times 50 = 83.85$$

$$R_{min} = \frac{Z_0}{VSWR} = \frac{50}{1.677} = 29.815$$

C. Determine the input impedance & SWR for a  $1.25\lambda$  long transmission line at the sending end with  $Z_0 = 50\Omega$  & the load impedance  $Z_L = 30+j40\Omega$

A.  $Z_0 = 50\Omega$

$Z_L = 30+j40\Omega$

$L = 1.25\lambda$

i) Find normalized load impedance

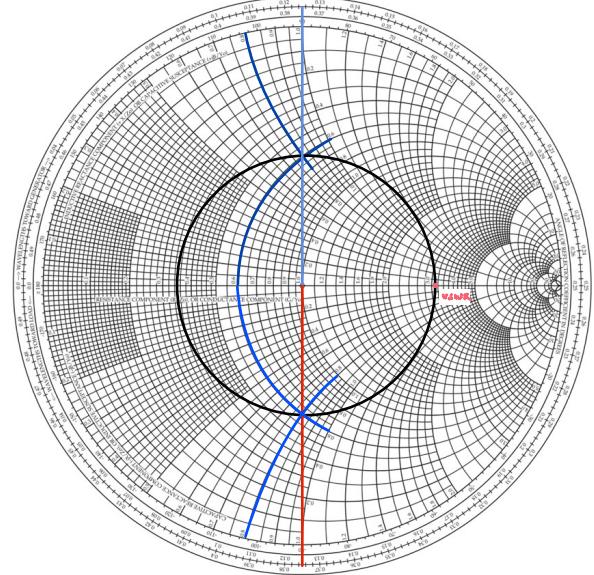
$$z_L = \frac{Z_L}{Z_0} = \frac{30+j40}{50} = 0.6+j0.8$$

ii) Plot normalized  $z_L$  on smith chart & draw impedance circle

$$\frac{z_L}{z_0} = 0.6 - j0.8$$

$$z_i = 30 - j40 \Omega$$

$$SWR = 3.1$$



B. A  $50\Omega$  Lossless Tx Line is terminated in a load impedance of  $Z_L = 25+j50\Omega$ . Find VSWR,  $\Gamma$ ,  $Z_{in}$  given line is  $3.3\lambda$  long,  $Y_{in}$

A.  $Z_L = 25+j50\Omega \quad \& \quad Z_0 = 50\Omega$

$$z_L = \frac{25+j50}{50} = 0.5+j1.0$$

$$z_i = 0.25 - j0.4$$

$$Z_i = 50(0.4 - j0.8) = 20 - j40 \Omega$$

$$VSWR = 4.6$$

$$VSWR = \frac{1 + \Gamma}{1 - \Gamma} \Rightarrow 4.6 - 4.6\Gamma = 1 + \Gamma \Rightarrow \Gamma = \frac{3.6}{5.6} = 0.643$$

$$\text{length} = 0.135\lambda + 3.3\lambda = 3.435\lambda$$

$$\Rightarrow 3.435\lambda - (6 \times 0.5\lambda) = 0.435\lambda \Rightarrow \text{Draw Line from origin to } 0.435\lambda$$

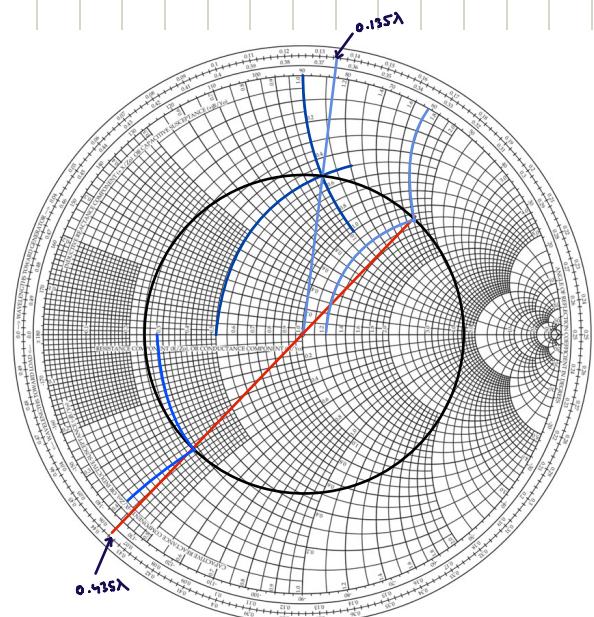
$$Z_{in} = 0.25 - j0.4$$

$$Z_{in} = Z_{in} \cdot Z_0 = 14 - j20 \Omega$$

To find admittance, stretch the  $Z_{in}$  line other side & find intersection

$$Y_{in} = 1.2 + j1.7$$

$$Y_{in} = Y_{in} \cdot \frac{1}{Z_0} = Y_{in} \cdot \frac{1}{50} = (1.2 + j1.7) \times \frac{1}{50} = 0.024 + j0.034 \text{ S}$$



Q. Use the smith chart to find the following quantities for the Tx line ckt shown in the figure

. Find VSWR,  $\Gamma$ ,  $y_L$ ,  $Z_{in}$ ,



$$A. \quad z_L = \frac{Z_L}{Z_0} = \frac{60 + j50}{50} = 1.2 + j1$$

$$0.175\lambda + 0.4\lambda = 0.575\lambda$$

$$0.575\lambda - (1 \times 0.5\lambda) = 0.075\lambda$$

VSWR = 2.5

$$\text{VSWR} = \frac{1+|\Gamma|}{1-|\Gamma|} \Rightarrow 2.5 - 2.5\Gamma = 1 + \Gamma \Rightarrow \Gamma = \frac{1.5}{3.5} = 0.43$$

$$y_L = 0.5 - j0.4 \quad (\text{Stretch opposite to } z_L, \text{ not } z_{in})$$

$$y_L = y_L \times \frac{1}{R_0} = \frac{0.5 - j0.4}{50} = 0.01 - j0.008 \text{ v}$$

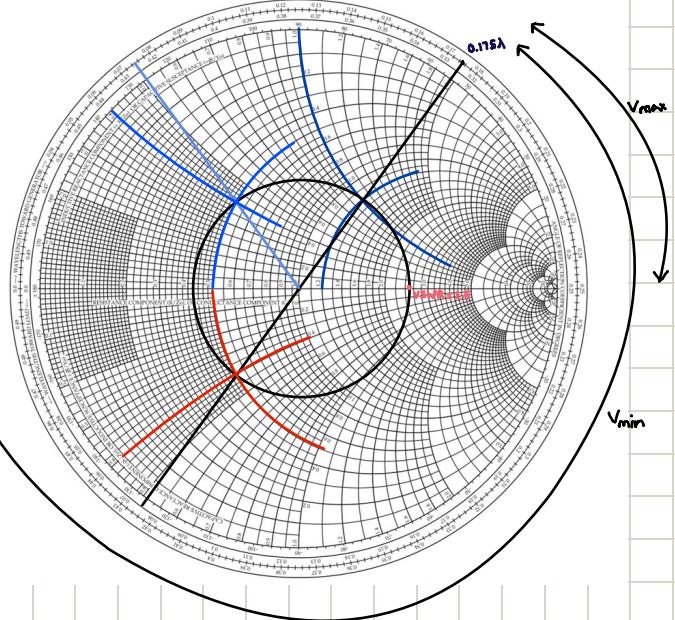
$$z_{in} = 0.5 + j0.4$$

$$Z_{in} = z_{in} \cdot Z_0 = (0.5 + j0.4) \times 50 = 25 + j20 \Omega$$

$$\Delta V_{min} = |0.5 - 0.175| \lambda = 0.325\lambda \quad \text{--- 1st minimum}$$

$$(0.325 + 0.5)\lambda = 0.825 \quad \text{--- 2nd minimum}$$

$$\Delta V_{max} = |0.25 - 0.175| \lambda = 0.075\lambda$$



Q. Let incident voltage =  $v_o^+$  & Reflected voltage =  $v_o^-$ , current =  $i_o^+$  in a Tx line. Normalize this by characteristic impedance  $z_0$

$$A. \quad V = V_o^+ + V_o^-$$

$$I = \frac{1}{z_0} [V_o^+ - V_o^-]$$

$$V_o^+ = \frac{V + Iz_0}{2}$$

$$V_o^- = \frac{V - Iz_0}{2}$$

$$\text{The normalized incident vector } a = \frac{V_o^+}{\sqrt{z_0}} = \frac{V + Iz_0}{2\sqrt{z_0}} = I_o^+ \sqrt{z_0}$$

$$\text{The normalized reflected vector } b = \frac{V_o^-}{\sqrt{z_0}} = \frac{V - Iz_0}{2\sqrt{z_0}} = I_o^- \sqrt{z_0}$$

$$\text{Now in terms of } a \& b, \text{ the incident power } P^+ = |a|^2$$

$$\text{the reflected power } P^- = |b|^2$$

$$\text{the reflected coefficient } \Gamma = \frac{b}{a}$$

$$\text{The actual power delivered to the load } P = |a|^2 - |b|^2$$

$$\text{VSWR of the termination } \rho = \frac{|a| + |b|}{|a| - |b|}$$

$$\text{For n-port network, } a_i = \frac{1}{2} \left( \frac{v_i + z_0 i_i}{\sqrt{z_0}} \right)$$

$$b_j = \frac{1}{2} \left( \frac{v_j - z_0 i_j}{\sqrt{z_0}} \right)$$

Q. Consider  $75\Omega$  Tx line that is terminated with a  $35 + j120\Omega$  load. Find the reflection coefficient at load & VSWR using wave vectors.

A. Normalizing the voltage source to 1,  $V_s = 1$

$$\text{then } V_0^+ = \frac{V_s}{2} = \frac{1}{2}$$

$$a = \frac{V_0^+}{\sqrt{Z_0}} = \frac{1}{2\sqrt{75}} = 0.0577$$

$$\frac{V_0^-}{V_0^+} = \Gamma_L = \left( \frac{Z_0 - Z_L}{Z_0 + Z_L} \right) = \frac{40 - j120}{40 + j120} = -0.377 - j0.679$$

$$V_0^- = V_0^+ (\Gamma_L) = \frac{-0.377 - j0.679}{2} = -0.188 - j0.34$$

$$b = \frac{V_0^-}{\sqrt{Z_0}} = \frac{-0.188 - j0.34}{\sqrt{75}} = -0.0217 - j0.039$$

$$\text{VSWR, } \rho = \frac{|a| + |b|}{|a| - |b|} = 7.97$$

Q. Given,  $Z_0 = 50\Omega$ ,  $Z_L = 25 + j25\Omega$ ,  $f = 1\text{GHz}$ . Calculate normalized load impedance, admittance, admittance at a distance d stub susceptance and stub length for a simple short circuited shunt stub.

A.  $Z_0 = 50\Omega$

$$Z_L = 25 + j25\Omega$$

$$f = 1\text{GHz}$$

$$Z_R = \frac{Z_L}{Z_0} = \frac{25 + j25}{50} = 0.5 + j0.5$$

$$Y_L = \frac{1}{Z_L} = 1 - j1$$

$$Z_{in} = \frac{Z_0(Z_L + jZ_0 \tan \beta L)}{(Z_0 + jZ_L \tan \beta L)} = 1$$

So,

$$\beta L = 45^\circ = \pi/4$$

$$\beta = \frac{2\pi}{\lambda} = \frac{2\pi f}{c} = \frac{2\pi \times 1 \times 10^9}{3 \times 10^8} = \frac{20\pi}{3} \Rightarrow \lambda = \frac{\pi/4}{\beta} = \frac{\pi/4}{20\pi/3} = \frac{3}{80} = 0.0375\text{m}$$

Q. Find voltage & current at  $z = 0.25\lambda$ , when the characteristic impedance is  $50\Omega$  & incident voltage is 10V with reflection coefficient of -0.5

A.  $V(z) = V_0^+ (e^{-j\beta z} + \Gamma e^{j\beta z})$

$$\beta z = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4} = \frac{\pi}{2}$$

$$V = 10(e^{-j\pi/2} + \Gamma e^{j\pi/2}) = 10(-j - 0.5(j)) = -j15\text{V} \Rightarrow |V| = 15\text{V}$$

$$I = \frac{V_0^+}{Z_0} (e^{-j\beta z} - \Gamma e^{j\beta z})$$

$$= \frac{10}{50} (e^{-j\pi/2} - (-0.5) e^{j\pi/2}) = 0.2 (-j + 0.5j) = -0.2 \times -0.5j = -0.1j \Rightarrow |I| = 0.1\text{A}$$

Q. A  $50\Omega$  Tx line is connected to a load impedance of  $60 + j10\Omega$ . The stub is connected short with the load. Find the position & length of the shorted stub required to match the line using Smith chart.

$$+ \beta L = \frac{60 + j10}{50} = 1.2 + j1.6$$

$$* Y_L = 0.3 - j0.4\Omega$$

$$* +j1.5 \text{ at } 0.175\lambda \quad \text{load to match at distance}$$

$$-j1.5 \text{ at } 0.325\lambda \quad \text{load to match at distance}$$

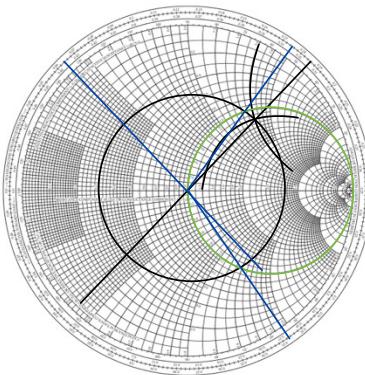
$$+ \Delta \therefore |0.175\lambda - 0.405\lambda| = 0.24\lambda$$

$$0.175\lambda + 0.065\lambda = 0.24\lambda \quad \text{load to match at distance}$$

$$* \Delta \therefore 0.32 - 0.32 = 0.07\lambda \quad \text{load to match at distance}$$

$$0.32\lambda = 0.07\lambda \quad \text{load to match at distance}$$

$$3.266\lambda = 0.07\lambda \quad \text{load to match at distance}$$



Q. A Tx. Line has  $\Gamma = 0.6$ . Find SWR

$$A. \text{ SWR} = \frac{1+|\Gamma|}{1-|\Gamma|} = \frac{1+0.6}{1-0.6} = 4$$

Q. Given,  $L = 2.54 \mu\text{H/m}$  &  $C = 100 \text{ pF/m}$ . For lossless line, find  $z_0$  &  $v_p$

$$A. z_0 = \sqrt{\frac{L}{C}} = \sqrt{\frac{2.5 \times 10^{-6}}{100 \times 10^{-12}}} = 158 \Omega$$

$$v_p = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{2.5 \times 10^{-6} \times 100 \times 10^{-12}}} = 2 \times 10^8 \text{ m/s}$$

Q. A lossless line of length  $\lambda/4$  is SC. Find  $z_{in}$

$$A. z_{in} = j z_0 \tan \beta l$$

$$\beta l = \frac{2\pi}{\lambda} \times \frac{\lambda}{4} = \frac{\pi}{2}$$

$$z_{in} = j z_0 \tan \frac{\pi}{2} = \infty \Rightarrow \text{Open circuit} \quad (\tan 90^\circ = \infty)$$

Q. A lossless Tx line of characteristic impedance  $z_0 = 50 \Omega$  & length  $\frac{\lambda}{4}$  is terminated with  $z_L = 200 \Omega$ . Find  $z_{in}$

$$A. z_0 = 50 \Omega, z_L = 200 \Omega$$

$$z_{in} = \frac{z_0^2}{z_L} = \frac{50 \times 50}{200} = 12.5 \Omega$$

Q. A lossless  $\Delta$  line has  $z_0 = 100 \Omega$ . The load is SC. Find  $z_{in}$

$$A. \text{ SC} \Rightarrow z_L = 0$$

$$z_{in} = \frac{z_0^2}{z_L} = \frac{100^2}{0} = \infty \Rightarrow \text{Open Circuit}$$

Q. A  $300 \Omega$  Tx line is connected to load impedance of  $450-j600 \Omega$  at 10 MHz. Find the position & length of SC stub to match the line using Smith chart

$$A. z_L = 450 - j600$$

$$z_0 = 300$$

$$Z_L = 1.5 - j2$$

$$y_L = 0.24 - j0.32$$

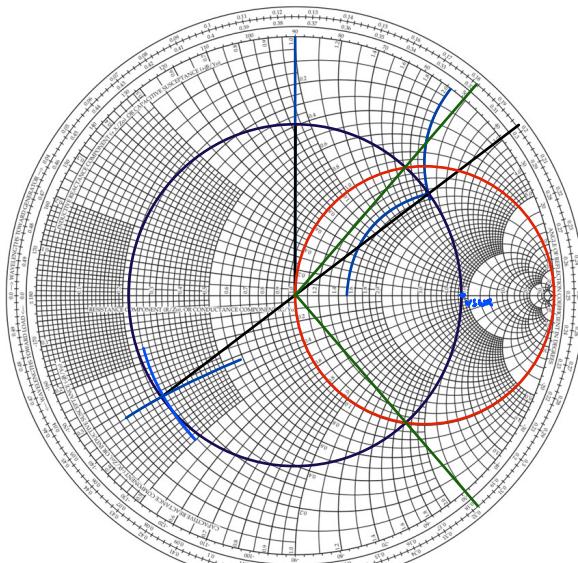
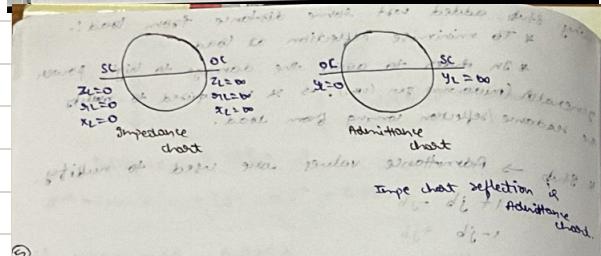
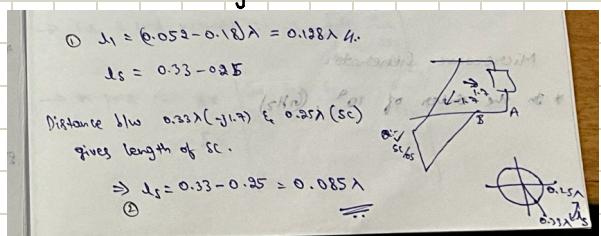
$$Y_L = 0.24 - j0.32 \times \frac{1}{300}$$

$$\text{VSWR} = 4.6$$

Now draw  $1+j0$  circle (in Red Colour)

Intersection point of SWR circle &  $1+j0$  circle at  $\pm j1.7$

Stub location =  $+j1.7$



# UNIT 2

Q. An air filled rectangular waveguide of inside dimension  $7 \times 3.5$  cm operates in a dominant mode. Find  $f_c$ , determine phase velocity of the wave in a waveguide operates at a frequency 3.5 GHz. Determine guide wavelength at same frequency.

A.  $a = 7$  cm,  $b = 3.5$  cm

$$TE_{01} \Rightarrow f_c = \frac{c}{2a} = \frac{3 \times 10^8}{2 \times 7 \times 10^{-2}} = 0.214 \times 10^{10} = 2.14 \text{ GHz}$$

$$v_p = \frac{\omega}{\beta} = \frac{c}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{3 \times 10^8}{\sqrt{1 - \left(\frac{2.14 \times 10^9}{3.5 \times 10^9}\right)^2}} = 3.79 \times 10^8 \text{ m/s} =$$

$$\lambda_g = \frac{\lambda_0}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{c/f}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{v_p}{f} = \frac{3.79 \times 10^8}{3.5 \times 10^9} = 0.108 \text{ m} = 10.8 \text{ cm}$$

Q. When a dominant mode is propagated in an air-filled rectangular waveguide, the guide wavelength for a freq of 9000 MHz is 4cm. Calculate breadth of the wave.

A.  $TE_{10} \Rightarrow m=1, n=0$

$$\lambda_g = 4 \text{ cm} = 0.04 \text{ m}$$

$$\lambda_0 = \frac{c}{f} = \frac{3 \times 10^8}{9 \times 10^9} = 0.033 \text{ m}$$

$$\lambda_g = \frac{\lambda_0}{\sqrt{1 - \left(\frac{\lambda_c}{\lambda_g}\right)^2}} = \frac{0.033}{\sqrt{1 - \left(\frac{0.033}{\lambda_c}\right)^2}} = 0.04 \Rightarrow \lambda_c = 0.0584 \text{ m}$$

$$\lambda_c = 2a \Rightarrow a = \frac{\lambda_c}{2} = 0.0292 \text{ m}$$

$$a = 2b \Rightarrow b = \frac{a}{2} = 0.0146 \text{ m} = 1.46 \text{ cm}$$

Q. Calculate resonant frequency of rectangular cavity resonator of dimensions  $3 \times 2 \times 4$  cm when filled with air & mode of operation is  $TE_{101}$ .

A.  $d = 4$  cm

$$a = 3 \text{ cm}$$

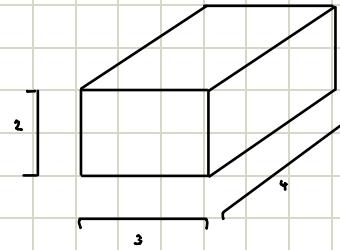
$$b = 2 \text{ cm}$$

& since  $TE_{101}, m=1, n=0, p=1$

$$f_r = \frac{c}{2\pi} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 + \left(\frac{p\pi}{d}\right)^2}$$

$$= \frac{3 \times 10^8 \pi}{2\pi} \sqrt{\left(\frac{1}{3 \times 10^{-2}}\right)^2 + \left(\frac{1}{4 \times 10^{-2}}\right)^2}$$

$$= 6.25 \text{ GHz}$$



Q. A rectangular metal waveguide filled with dielectric material of relative permittivity  $\epsilon_r = 4$  has inside dimensions  $3 \times 1.2$  cm. Calculate cutoff freq for dominant mode.

A. Dominant mode  $\Rightarrow TE_{10}$  (2D w.r.t rectangular metal waveguide)

$$a = 3 \text{ cm} \quad b = 1.2 \text{ cm}$$

$$f_c = \frac{c}{\sqrt{\epsilon_r \cdot 2\pi}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$= \frac{3 \times 10^8}{\sqrt{4 \times 2}} \sqrt{\left(\frac{1}{3 \times 10^{-2}}\right)^2} = 2.5 \times 10^9 \text{ Hz}$$

$$v = \frac{c}{\sqrt{\epsilon_r}} = 1.5 \times 10^8 \text{ m/s}$$

Q. For the dominant mode propagation along the  $z$  direction in air filled rectangular waveguide, the longitudinal magnetic field  $H_2 = \cos(100x) e^{j\beta z}$ . Determine dimensions of waveguide if the ratio  $a:b = 2:1$

$$A. H_2 = H_{02} \cos\left(\frac{m\pi}{a}\right)x \cdot \cos\left(\frac{n\pi}{b}\right)y \cdot e^{j\beta z}$$

$$= \cos(100x) e^{j\beta z}$$

$$\text{So, } H_{02} = 1, \frac{m\pi}{a} = 100$$

$$\text{TE}_{10} \Rightarrow m=1, n=0$$

$$\text{So, } a = \frac{\pi}{100} \quad \text{Then } \frac{a}{b} = \frac{2}{1} \Rightarrow b = \frac{a}{2} = \frac{\pi}{200}$$

Q. The rectangular waveguide with dimensions  $a = 1.07 \text{ cm}$   $b = 0.43 \text{ cm}$  filled with certain dielectric exhibits  $f_c = 31.03 \text{ GHz}$  for  $\text{TM}_{21}$  mode. Find the relative dielectric constant.

$$A. f_c = \frac{c}{\sqrt{\epsilon_r \cdot 2\pi}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$31.03 \times 10^9 = \frac{3 \times 10^8}{\sqrt{\epsilon_r \cdot 2\pi}} \sqrt{\left(\frac{2}{1.07 \times 10^{-2}}\right)^2 + \left(\frac{1}{0.43 \times 10^{-2}}\right)^2}$$

$$\epsilon_r = \left( \frac{3 \times 10^8}{31.03 \times 10^9 \cdot 2\pi} \right)^2 \times \left( \left(\frac{2}{1.07 \times 10^{-2}}\right)^2 + \left(\frac{1}{0.43 \times 10^{-2}}\right)^2 \right)$$

$$= 2.08$$

Q. The dimensions of waveguide are  $2.5 \times 1 \text{ cm}$  & frequency is  $8.6 \text{ GHz}$ , Find the following

i) Possible modes of operation ii) Cutoff freq. iii) wavelength

A. i) Condition for propagation  $\Rightarrow \lambda_c > \lambda_0$  (or)  $f_c < f_0$

$$\text{Here } \lambda_0 = \frac{c}{f_0} = \frac{3 \times 10^8}{8.6 \times 10^9} = 0.034 \text{ m}$$

$$\text{TE}_{01} \Rightarrow m=0, n=1 \quad \lambda_c = \frac{2ab}{\sqrt{m^2 + n^2}} = \frac{5 \times 10^{-2}}{2.5 \times 10^{-2}} = 2 \times 10^{-2} < \lambda_0 \quad \times$$

$$\text{TE}_{10} \Rightarrow m=1, n=0 \quad \lambda_c = \frac{5 \times 10^{-2}}{1 \times 10^{-2}} = 5 \times 10^{-2} \text{ cm} > \lambda_0 \quad \checkmark$$

$$\text{TE}_{11} \Rightarrow m=1, n=1 \quad \lambda_c = \frac{5 \times 10^{-2}}{\sqrt{6.25+1}} = 1.85 \times 10^{-2} \text{ cm} < \lambda_0 \quad \times$$

$$\text{ii) } f_c (\text{10 Mode}) = \frac{c}{\lambda_c} = \frac{3 \times 10^8}{5 \times 10^{-2}} = 6 \times 10^9 \text{ Hz} = 6 \text{ GHz}$$

$$\text{iii) } \lambda_g = \frac{\lambda_0}{\sqrt{1 - \left(\frac{\lambda_0}{\lambda_c}\right)^2}} = \frac{0.034}{\sqrt{1 - \left(\frac{0.034}{0.05}\right)^2}} = 4.637 \text{ cm}$$

Q. An air filled rectangular cavity resonator is operating in dominant mode. Determine resonant freq. of resonator if the field inside the resonator is  $H_2 = \cos(20\pi x) \cdot \sin(5\pi z)$ . Now if the resonator is filled with dielectric  $\epsilon_r = 4$ , determine new resonant freq.

$$A. H_2 = H_{02} \cos\left(\frac{m\pi}{a}\right)x \cdot \cos\left(\frac{n\pi}{b}\right)y \cdot e^{j\beta z}$$

$$= \cos(20\pi x) \cdot \sin(5\pi z)$$

$$m=1, n=0, p=1$$

$$\frac{m\pi}{a} = 20\pi \Rightarrow a = \frac{1}{20} = 0.05 \text{ m} = 5 \text{ cm}$$

$$\frac{p\pi}{d} = 5\pi \Rightarrow d = \frac{1}{5}$$

$$f_r = \frac{c}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2 + \left(\frac{p}{d}\right)^2} = \frac{3 \times 10^8}{2} \sqrt{\left(\frac{1}{0.05}\right)^2 + \left(\frac{1}{5}\right)^2} = 3.1 \text{ GHz}$$

$$\text{At } \epsilon_r, f_r = \frac{f_c}{\sqrt{\epsilon_r}} = \frac{3.1}{\sqrt{4}} = 1.55 \text{ GHz}$$

Q. For a dominant mode propagation, in an air filled rectangular waveguide, the longitudinal magnetic wavefield is given by  
 $H_2 = H_{02} \cos\left(\frac{m\pi}{a}x\right) \cdot e^{-j\beta z}$ . If operating freq. of wave is  $f = 8.333$  GHz, determine phase constant  $\beta$

A.  $H_2 = H_{02} \cos\left(\frac{m\pi}{a}x\right) \cdot \cos\left(\frac{n\pi}{b}y\right) \cdot e^{-j\beta z}$

$\text{TE}_{10} \Rightarrow m=1, n=0$

$$\frac{m\pi}{a} = \frac{100\pi}{3} \Rightarrow a = \frac{3}{100}$$

$$f_c = \frac{c}{2a} = \frac{3 \times 10^8}{2 \times 3} = 5 \times 10^9 = 54 \text{ Hz}$$

$$\beta = \frac{2\pi}{\lambda} = \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = \frac{2\pi f}{c} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = 139.54 \text{ rad/m}$$

B. The series RLC circuit has  $R=100\Omega$ ,  $L=0.5\text{H}$ ,  $C=0.4\mu\text{F}$ . Find resonant freq., half power freq & bandwidth



A.  $f_r = \frac{1}{2\pi\sqrt{LC}} = 355.88 \text{ Hz}$

$$f_1 = f_r - \frac{R}{4\pi L} = 339.96 \text{ Hz}$$

$$f_2 = f_r + \frac{R}{4\pi L} = 371.79 \text{ Hz}$$

$$\text{BW} = f_2 - f_1 = 31.83 \text{ Hz}$$