

# Virtual and Augmented Reality

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## Problem 1

The following functional interfaces were created:

**Table 1:** Functional interfaces implemented and their inputs/outputs

| Functional interface                            | Inputs  | Outputs   |
|---|---|---|
| Euler angle $\rightarrow$ quaternion conversion | Euler angles in radians of format $(x, y, z)$   | A quaternion of format $(w, x, y, z)$               |
| Quaternion $\rightarrow$ Euler angle conversion | A quaternion of format $(w, x, y, z)$           | Euler angles in radians of format $(x, y, z)$       |
| Quaternion conjugate calculation                | A quaternion of format $(w, x, y, z)$           | The conjugate of the input: $(w, -x, -y, -z)$       |
| Quaternion product calculation                  | Two quaternions $a, b$ of format $(w, x, y, z)$ | The product of $a$ and $b$ of format $(w, x, y, z)$ |

Similar descriptions for each function are also included in the code.

## Problem 3

Several different alpha values were investigated for the tilt-corrected orientation tracking. They are listed in Table 2 below, along with a description of the findings:

**Table 2:** Effect of Alpha Values on Drift Compensation in Tilt-Corrected Orientation Tracking

| alpha | Description  |
|-------|--|
| 0.01  | Minimal change from simple dead reckoning filter. Slightly reduces the manifestation of gimbal lock in $X$ and $Y$ axes during the $-90^\circ$ rotation around $Y$ . $X$ and $Y$ rotations are marginally further from 0 at the end of the sequence.   |
| 0.03  | Slight increase in the manifestation of gimbal lock compared to an alpha of 0.01. $X$ and $Y$ components converge marginally closer to 0 than alpha of 0.01 and in dead reckoning filter, although the change is extremely subtle.   |
| 0.05  | Significantly compressed gimbal lock manifestation when $Y \simeq \pm 90$ . $X$ , $Y$ and $Z$ all converge to 0 at the end of the sequence, however the last rotation of $90^\circ$ in $Z$ has decayed to $\sim 45^\circ$ .  |
| 0.10  | Complete decay of all angles to 0 after $t \sim 8s$ . Before this the $90^\circ$ rotation around $X$ occurs, which reaches $90^\circ$ then quickly falls towards 0, instead of staying $\sim 90$ for a few seconds as expected. The orientation tracking has completely failed, as the (imperfect) corrections introduced by the tilt correction completely overpower any actual rotations registered after the first few seconds. This effect becomes more extreme as alpha is further increased. |

An alpha value of 0.03 was chosen as the best value, as this causes the  $X$  and  $Y$  components to be closest to 0 at the end of the sequence without decaying the tracking of any of the  $\pm 90^\circ$  rotations.

## Problem 4

As for Problem 3 above, several alpha values were investigated for the yaw-corrected orientation tracking. They are listed in Table 3 below, along with a description of the findings. All investigation was done with an alpha of 0.03 for tilt-correction; the alpha listed below is specifically the alpha used for yaw-correction.

**Table 3:** Effect of Alpha Values on Drift Compensation in Yaw-Corrected Orientation Tracking

| alpha  | Description   |
|--------|---|
| 0.0001 | The $Z$ component is slightly closer to 0 at the end of the sequence, but there is still significant drift present. Thus, the yaw correction being applied is not strong enough.  |
| 0.0002 | At this alpha value the $Z$ component is reduced to 0 at the end of the sequence (around $t \sim 24s$ ), without decaying the $90^\circ$ rotations or causing any visible inconsistencies in the graph.   |
| 0.0005 | The yaw drift is over-compensated, resulting in a significant drift in the $Z$ component at the end of the sequence, reaching $\sim \frac{-\pi}{2}$ . This decay of the $Z$ component is noticeable from the end of the $-90^\circ$ rotation around $Y$ at $t \sim 16s$ . |
| 0.0010 | Similar results as with $\alpha = 0.0005$ , but more extreme. The $Z$ rotation is decayed by $\sim \frac{-\pi}{2}$ from $t \sim 16s$ to the end of the sequence.  |
| 0.0100 | The decay of $\sim \frac{-\pi}{2}$ in the $Z$ component is constant starting from $t \sim 2s$ . Significant noise is present in the $Z$ rotation, making it rapidly ‘jitter.’   |
| 0.1000 | The $Z$ rotation shows the same general shape as for $\alpha = 0.01$ , but the amount of noise is significantly larger. There are also occasional jumps from $-\pi$ to $+\pi$ , for example when the headset is rotated by $-90^\circ$ around the $Z$ axis.               |

An alpha value of 0.0002 was chosen as the best value, as this caused the  $Z$  component to converge with  $X$  and  $Y$  at 0 at the end of the sequence. Additionally, with this alpha there is no noticeable distortion or over-correction at any point during the sequence.

## Problem 5

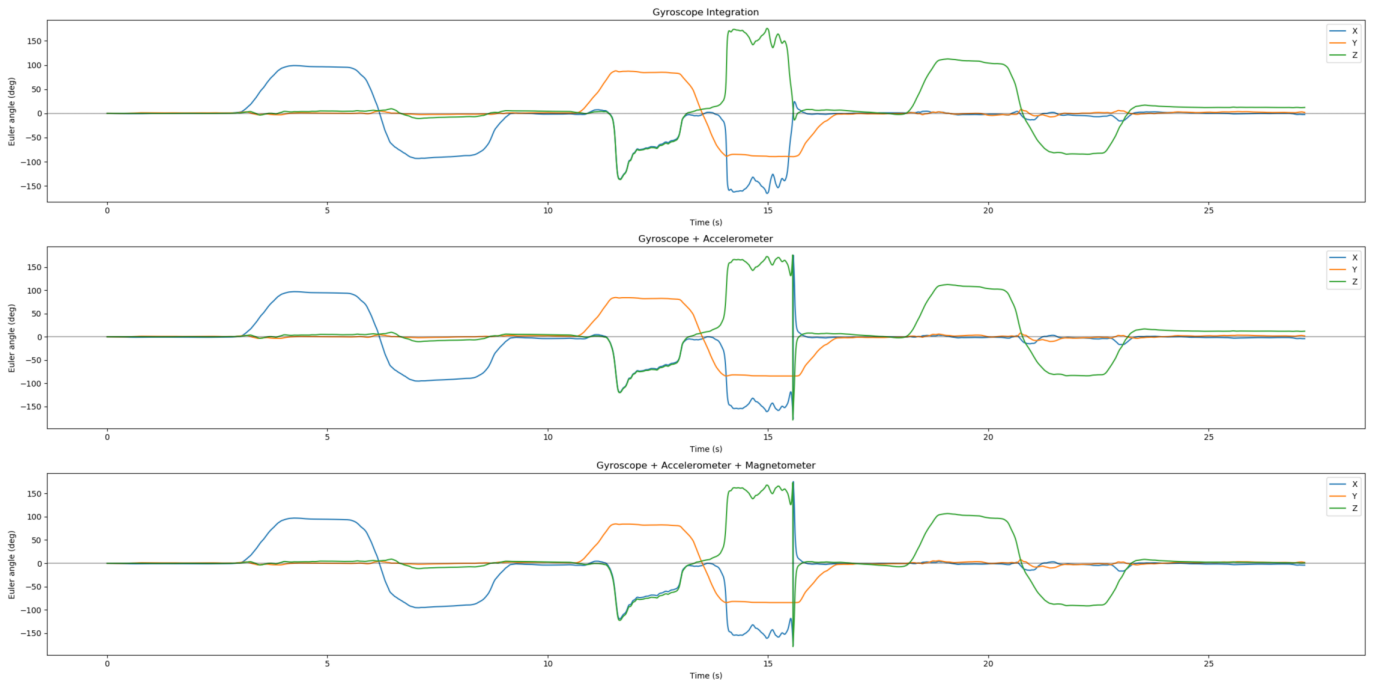
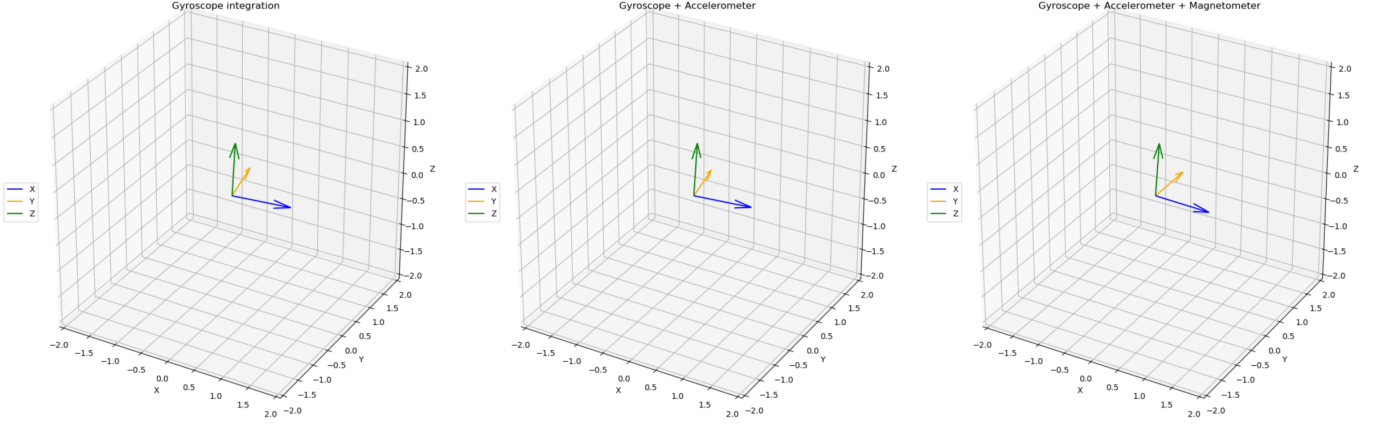
**Figure 1:** 2D Visualization of Various Methods for Head Orientation Tracking

Figure 1 show 2D plots of the results of head orientation tracking for the three different methods: simple dead reckoning (gyroscope integration), tilt correction (gyroscope + accelerometer), yaw correction (gyroscope + accelerometer + magnetometer). The  $x$  axis represents time in seconds, and the  $y$  axis of each plot represents the Euler angle for each axis in degrees, where  $Z$  is vertical (the axis of yaw),  $Y$  is horizontal (the axis of pitch), and  $X$  is depth (the axis of roll).

The simple dead reckoning and tilt-corrected orientation tracking approaches produce very similar results. Because the simple dead reckoning suffers from very little drift in the  $X$  and  $Y$  axes, there is little change once this drift is corrected for. The tilt correction does slightly improve the results however.

As expected, the most stable method is the yaw-corrected head orientation tracking. This can be clearly seen by looking at the  $Z$  component values at the end of the sequences. In both the simple dead reckoning and tilt-corrected orientation tracking approaches the  $Z$  component suffers from gyroscopic drift, which is successfully corrected for by the yaw correction.

This can also be clearly seen in the 3D plot shown in Figure 2. This is a snapshot from the end of the sequence of rotations, and thus the gyroscopic drift is relatively high. In this image both the simple dead reckoning and tilt correction suffer from yaw drift, while the yaw corrected tracking does not (most noticeable when comparing the  $Y$  component vectors). This further showcases the improved stability of orientation tracking achieved by yaw correction.



**Figure 2:** Example 3D Result of Head Orientation Tracking

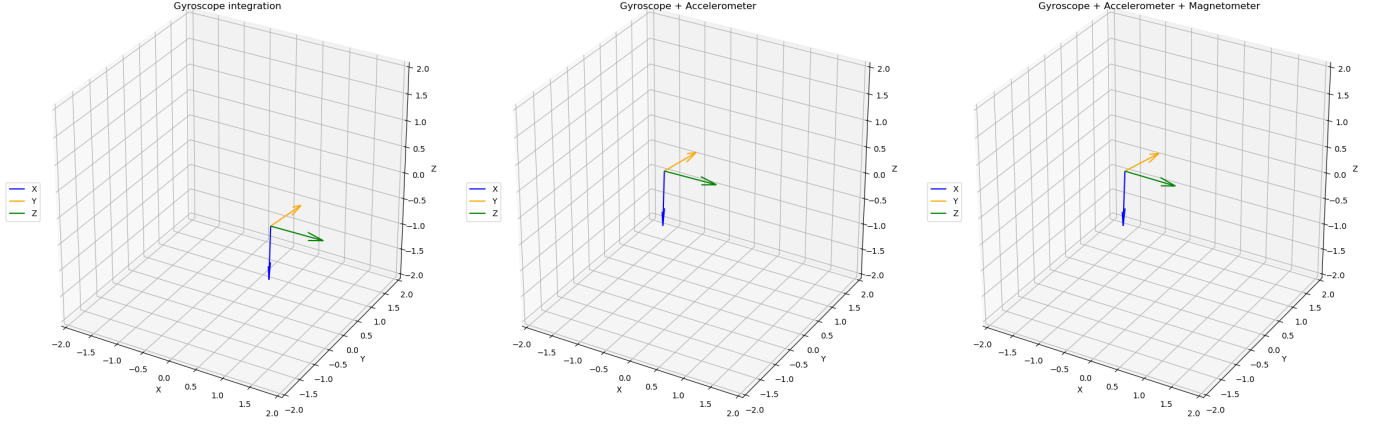
## Problem 6

In order to try to achieve positional tracking using the IMU, I double integrated the accelerometer readings and applied a two-bar kinematic head model. This assumes that the head is locked to the neck, the neck can be rotated at the joint to the torso, and the torso can be rotated around the waist. This was applied as follows:

1. Convert acceleration readings to global acceleration by rotating the readings by the current head orientation estimate
2. Extract linear acceleration by subtracting gravity (1) from the  $Z$  component
3. Integrate the linear acceleration into velocity and convert into angular velocity as  $\omega = \frac{a_l * \Delta t}{l_t}$ , where  $a_l$  is linear acceleration,  $\Delta t$  is the time since the last time step, and  $l_t$  is the length of the torso. Note: this makes the assumption that the linear acceleration is caused by a rotation of the body, not of the neck and body combined
4. Add the previous angular velocity reading to produce the current angular velocity
5. Apply the simple dead reckoning filter to get an estimate for the orientation of the torso,  $q_1$
6. Calculate the position of the torso relative to the origin (the waist) as  $r_1 = q_1 * (0, 0, l_t) * q_1^{-1}$
7. Apply the simple kinematic head model to get the position of the head relative to the torso,  $r$ , as  $r = q * (0, 0, l_n) * q^{-1}$ , where  $l_n$  is the estimated length of the neck, and  $q$  is the current estimated head orientation
8. Compose the two positions to get the global position of the head as  $p = r_1 + r$

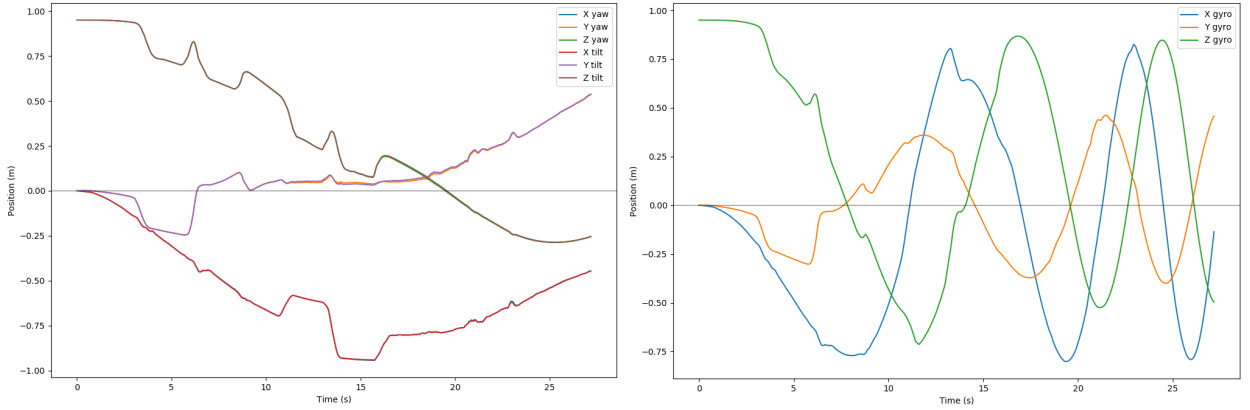
This approach constrains the position of the head to what could physically be reached by a person anchored at the waist, e.g. when sitting down. Even with these constraints and the short duration of the data sequence (around 28s) there is significant drift in the positional tracking. One example of this is shown in Figure 3. This shows a snapshot of the head position tracking for all three methods of orientation tracking, shortly after the  $+90^\circ$  rotation about the  $Y$  axis ( $t \sim 12s$ ). In this image the gyroscope integration based method shows extremely high drift in the  $X$  and  $Y$  components. The other two tracking methods show slight drift, as they have a lower  $X$  position than would be expected, but fare much better than the

gyroscope integration. This is likely due to the poor performance of the gyroscope integration orientation tracking resulting in much larger errors due to the quadratic growth of drift error.



**Figure 3:** Example 3D Result of Various Methods for Head Orientation Tracking

Figure 4 shows the tri-axial position tracking output for the three types of tracking. The left image shows tilt-corrected and yaw-corrected tracking: these produce extremely similar positions. The right image shows gyroscopic integration position tracking. This is vaguely similar to the other graph until  $t \sim 5s$ , where the positions all enter sinusoidal patterns. This is quite incorrect, and such tracking would likely make a user of the system ill very quickly. As previously mentioned, this drastic difference in positional tracking performance is likely due to the lacking performance of gyroscopic integration for orientation tracking, as well as the compounding of errors amplified by integration which are not corrected for.



**Figure 4:** Example 3D Result of Various Methods for Head Orientation Tracking

All methods of orientation tracking show significant drift in all three axes in positional tracking. This is likely caused by two main factors. Firstly, there is a large assumption made that the linear acceleration corresponds to rotation of the torso about the waist, rather than the neck around the base of the neck (or likely a combination of the two). This assumption was made in order to simplify the kinematic system, and justified by the fact that the neck often only slightly moves around its base, and most movement of the head relative to the waist is due to a rotation/movement of the torso. Secondly, a large amount of error is introduced by the double integration of the accelerometer readings. Numerical integration by itself produces inaccurate results, and this is only made worse by applying a double integration to already noisy data (as the accelerometer itself has inherent noise, and the local to global frame conversion is based on an imperfect head orientation estimate). All these sources of noise compound to produce potentially massive errors in the result, which are propagated in each time step to the next. Thus, any positional tracking based only on the IMU with no external frame of reference is going suffer from large drift and propagated errors.