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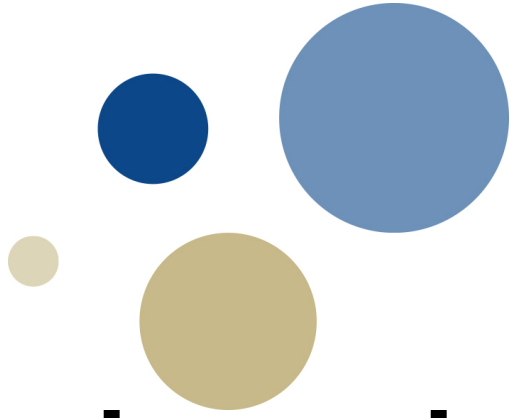

Identification of turbine dynamics using PMUs

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Department of electrical engineering

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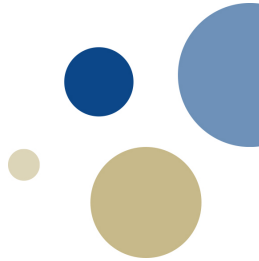
Outline



Background

Previous work

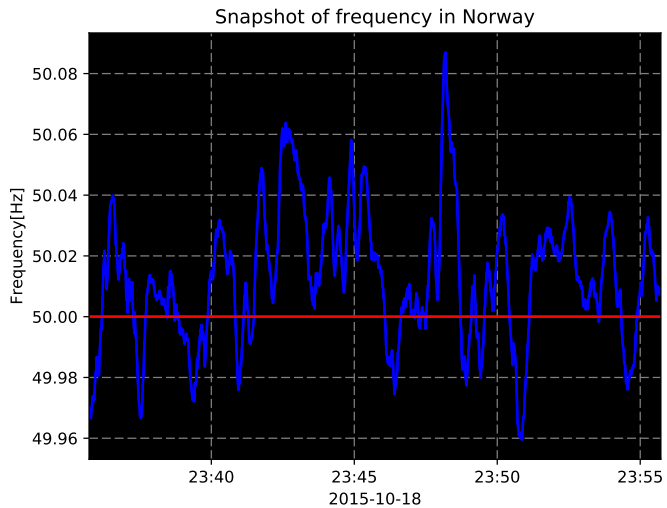
Theoretical validation

Results

Conclusions and further work

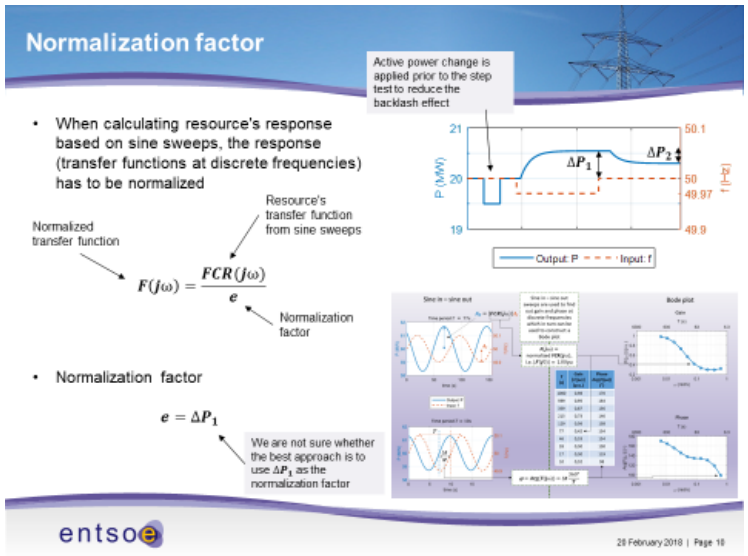
Frequency quality in the Nordics

- From 2008 the time the frequency has been outside its allowed band has increased
- The performance of hydro turbine governors play an important role



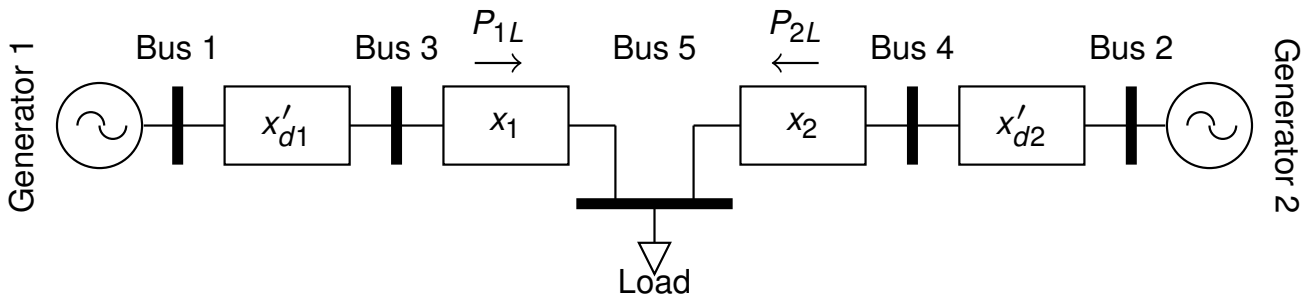
New requirements on FCR due to frequency quality

- Nordic TSOs are developing new requirements on FCR
- This includes offline testing and verification of performance



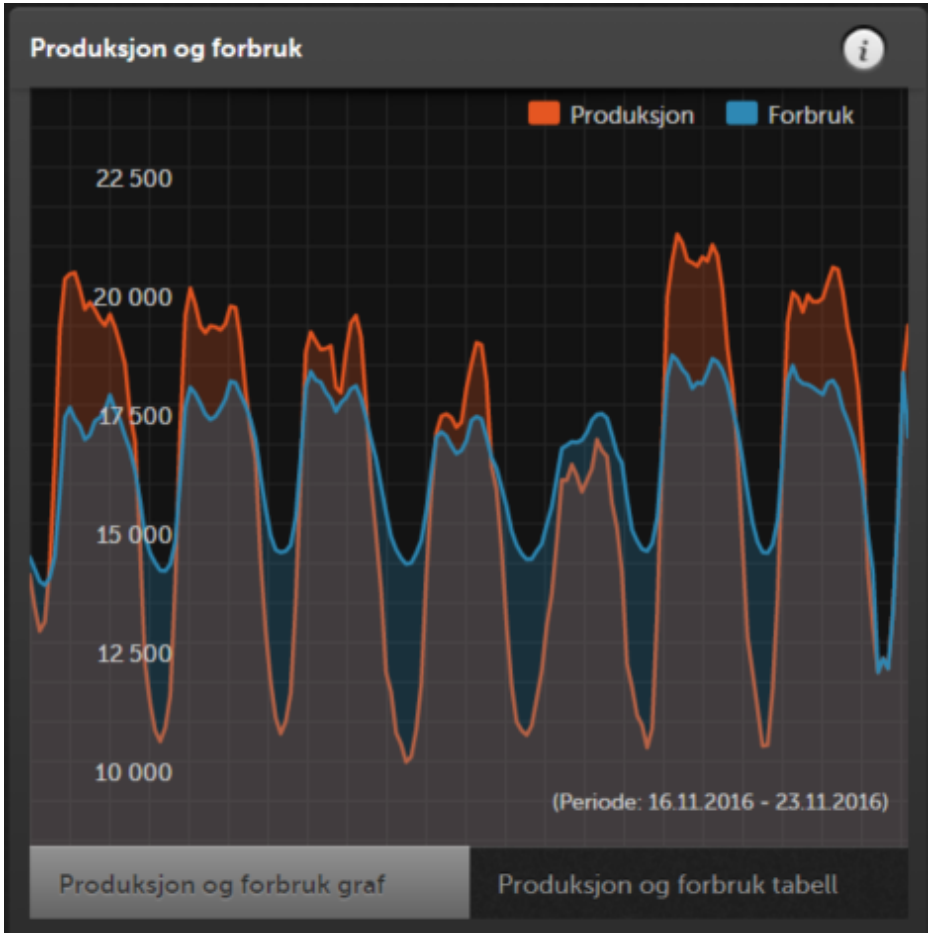
Idea on monitoring the FCR online

- Less intrusive



Idea on monitoring the FCR online

- Less intrusive
- The system is dynamic



Background
Challenges in operation

- Towards 100% renewable electricity generation
  - Larger variability
  - More uncertainty
  - Increasing complexity

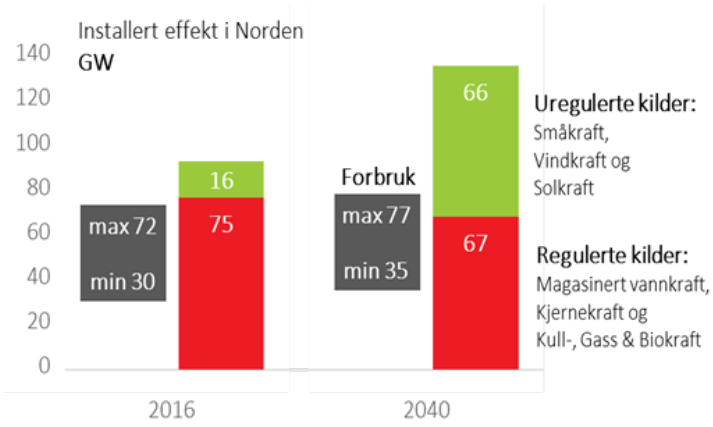


Figure: Present and future energy mix[Statnett]

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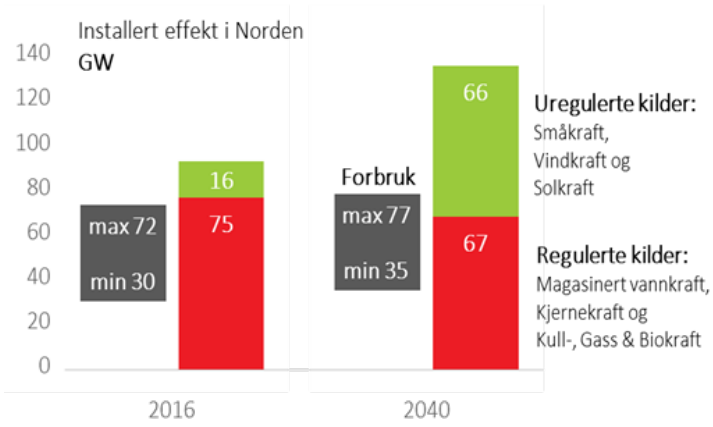

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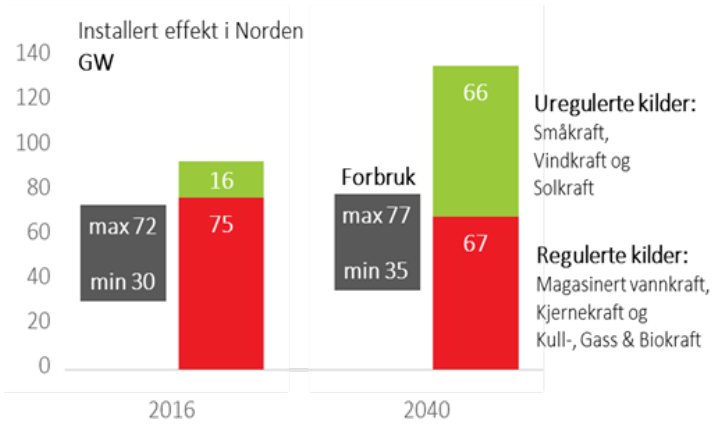

Figure: Present and future energy mix[Statnett]

Background
Challenges in operation

- Towards 100% renewable electricity generation
  - Larger variability
  - More uncertainty
  - Increasing complexity
- More dynamics
- Less time for actions
- **Hydropower** is the main resource for balancing

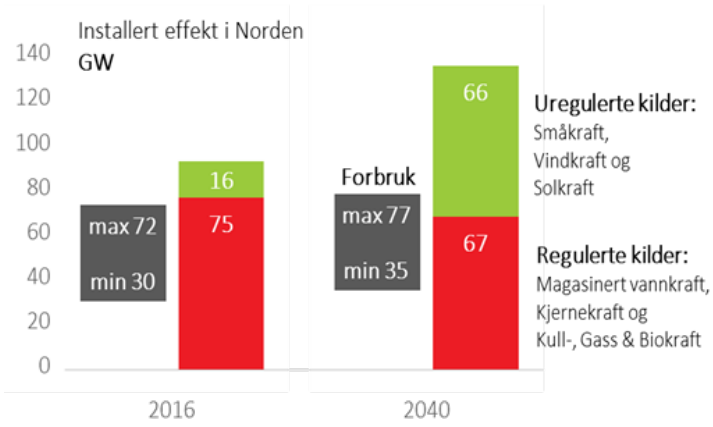

Figure: Present and future energy mix[Statnett]

1. Do the transmission system operator (TSO) know whether or not the hydropower plants deliver the FCR they are supposed to?

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2. Can the TSO measure it online?

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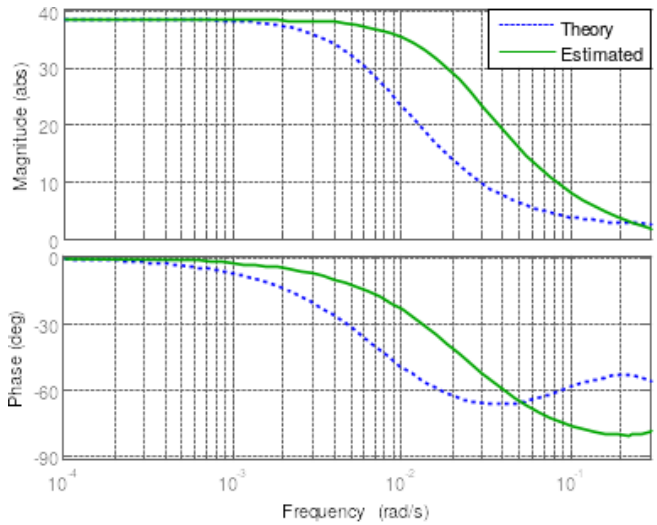
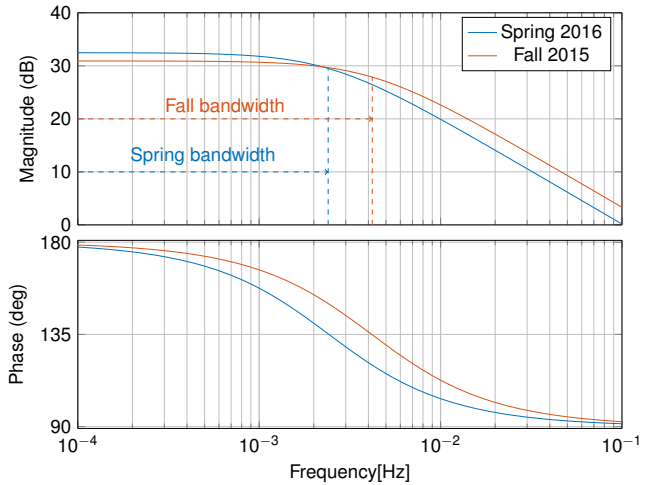
Previous articles

- Governor dynamics were identified using the ARX model structure



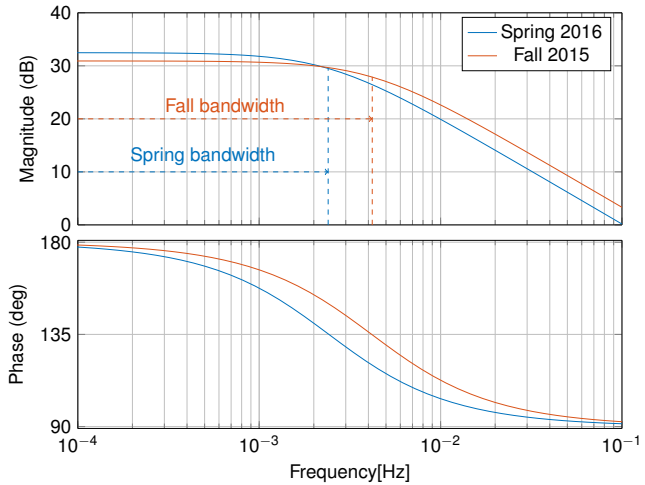
Previous articles

- Governor dynamics were identified using the ARX model structure
- Governor dynamics were identified using time domain vector fitting



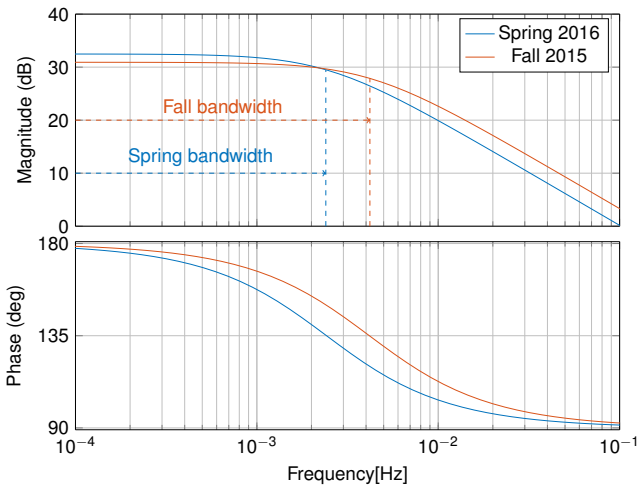
Previous articles

- Governor dynamics were identified using the ARX model structure
- Governor dynamics were identified using time domain vector fitting
- There are also other papers in the literature using other methods for online identification, however, mostly relying on data from disturbance recordings.



Question leading to this specific work

- Why do we get different results?



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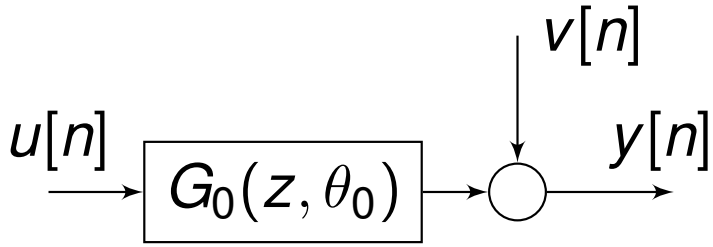
- The signals we use are corrupted by noise.



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- Why do we get different results?
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- Using system identification techniques we can estimate the variance of the covariance matrix of the parameter vector

$$a + b$$

Question leading to this specific work

- Why do we get different results?
- The signals we use are corrupted by noise.
- Using system identification techniques we can estimate the variance of the covariance matrix of the parameter vector
- However, first we have to prove that we will get consistent results.

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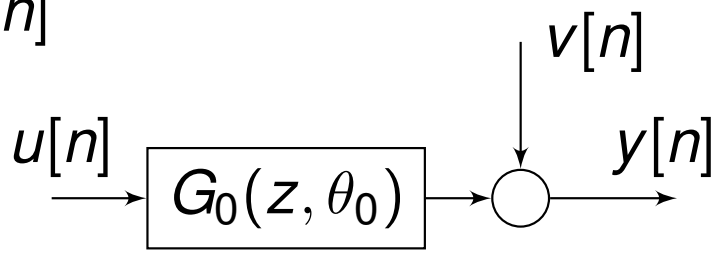
System identification basic

- Assume that a data set $Z^N = \{u[n], y[n] | n = 1 \dots N\}$ has been collected.
- The dataset Z^N is assumed generated by

$$\mathcal{S} : y[n] = G_0(z, \theta_0)u[n] + H_0(z, \theta_0)e[n] \tag{1}$$



- Using the data set Z^N we want to find the parameter vector θ^N minimizing

$$\hat{\theta}_N = \arg\min_{\theta} \frac{1}{N} \sum_{n=1}^{N} \epsilon^2(n, \theta) \tag{2}$$

- A consistent estimate means that the true parameter vector θ_0 is the unique solution to the asymptotic prediction error criterion.

$$\theta^* = \arg\min_{\theta} \bar{E}\epsilon^2(n,\theta) \tag{3}$$

with

$$\bar{E}\epsilon^2(n,\theta) = \lim_{N\to\infty} \frac{1}{N} \sum_{t=1}^{N} E\epsilon^2(n,\theta) \tag{4}$$

and

$$\epsilon(n,\theta) = H_1^{-1}(z,\theta)(y[n] - G_1(z,\theta)u[n]) \tag{5}$$

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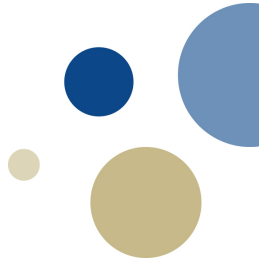
Results from the theoretical validation

- A consistent estimate of the closed loop transfer function of the turbine and electromechanical dynamics can be obtained by using:

Results from the theoretical validation



- A consistent estimate of the closed loop transfer function of the turbine and electromechanical dynamics can be obtained by using:
  - Measured PMU frequency as the output $u[n]$

Results from the theoretical validation

- A consistent estimate of the closed loop transfer function of the turbine and electromechanical dynamics can be obtained by using:
  - Measured PMU frequency as the output $u[n]$
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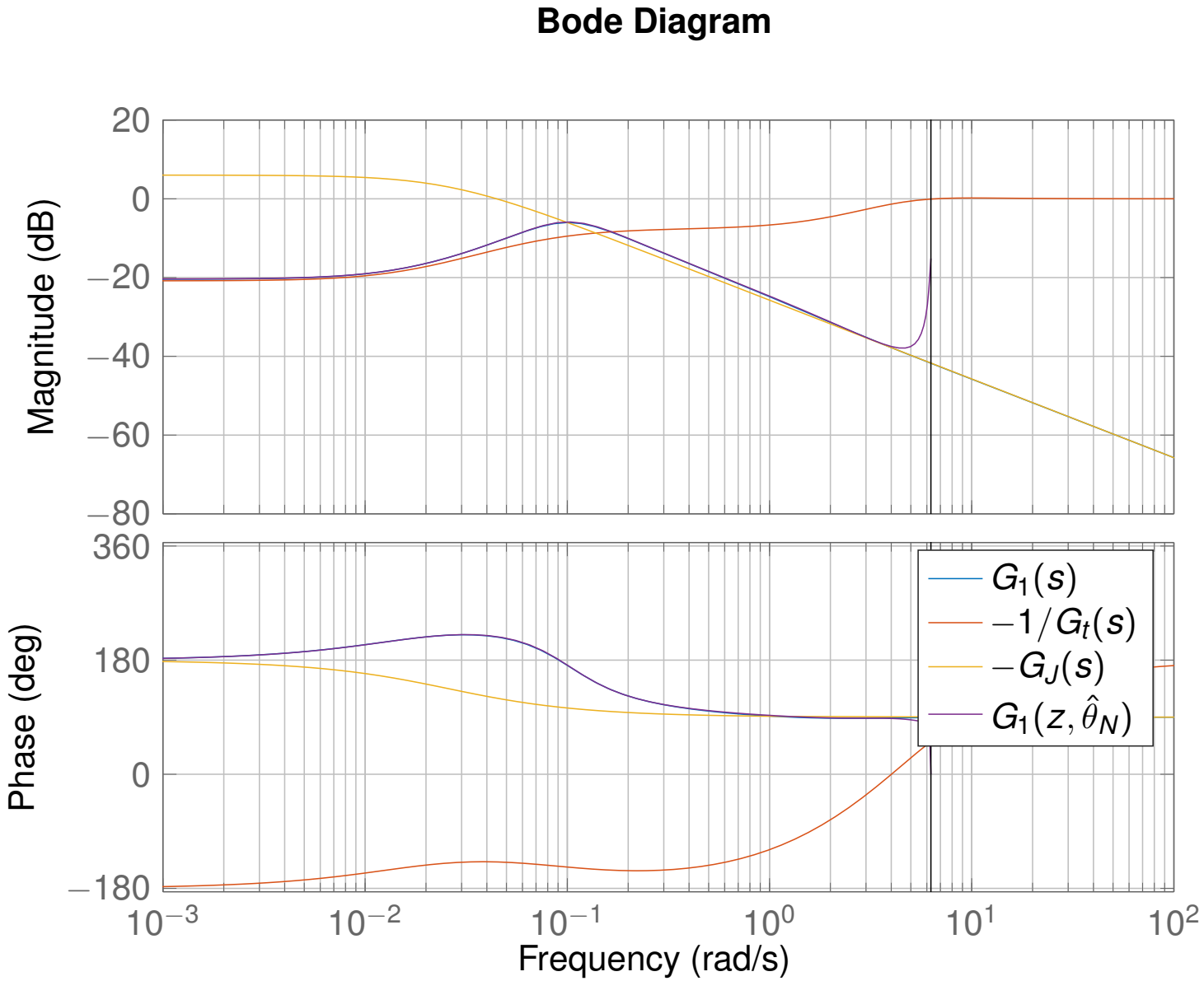
Results from the theoretical validation

- A consistent estimate of the closed loop transfer function of the turbine and electromechanical dynamics can be obtained by using:
  - Measured PMU frequency as the output $u[n]$
  - Measured PMU power as the input $y[n]$
- The proof was done with the following assumptions.
  - The system is excited by a load acting as a filtered white noise process
  - The measurement error of the electrical power is negligible.
  - The measured frequency is a good estimate of the generator speed.

Results from simulations



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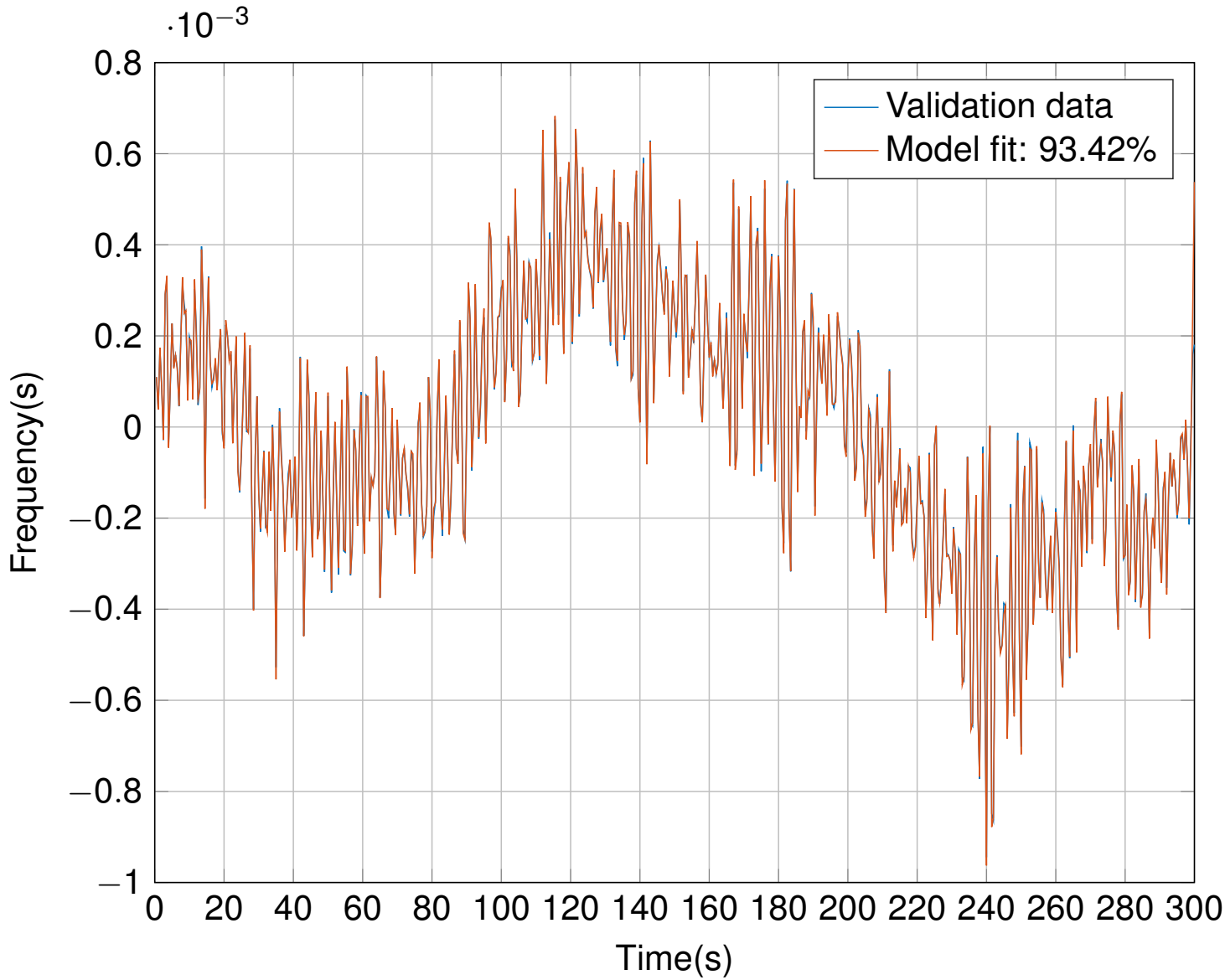

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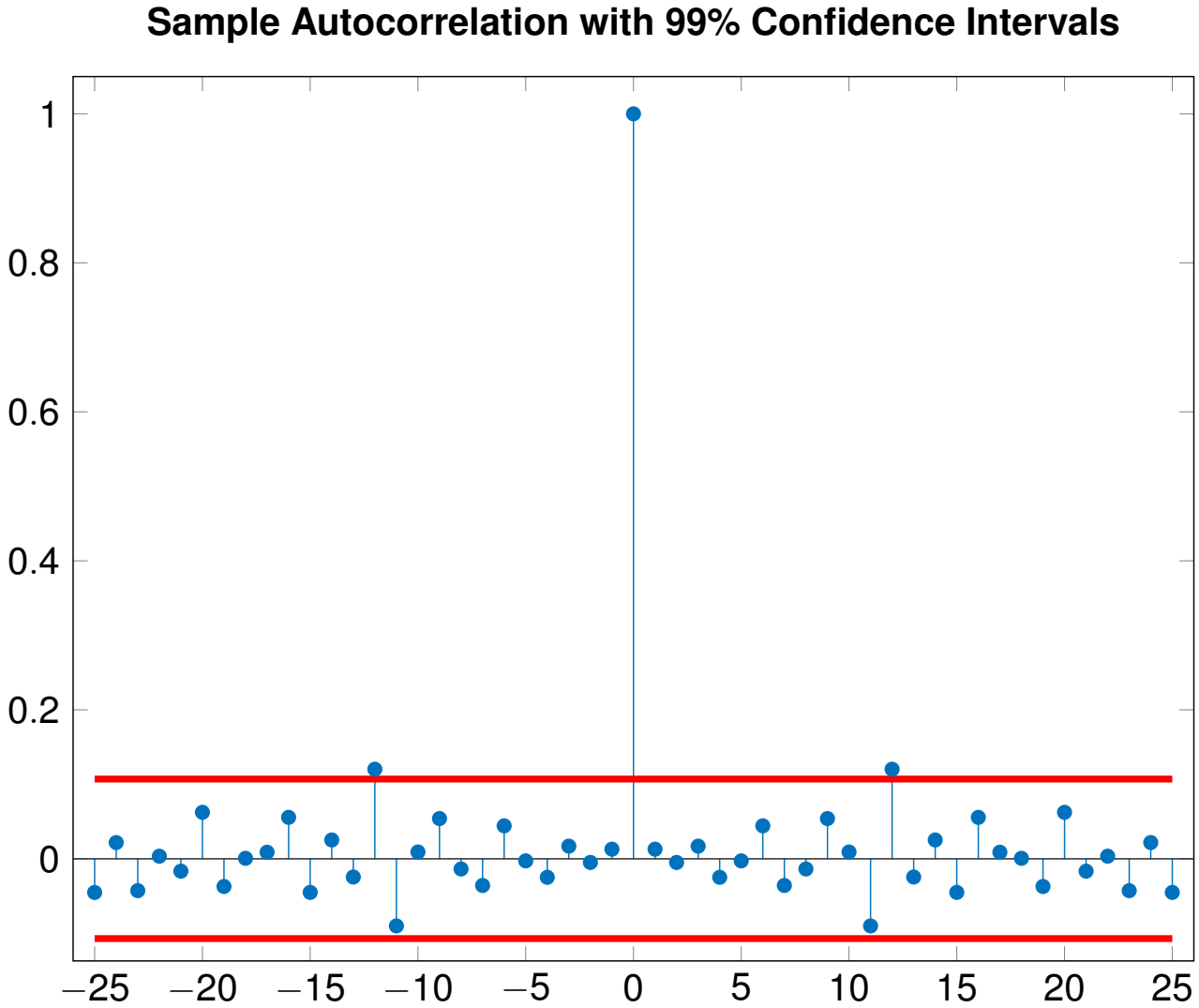
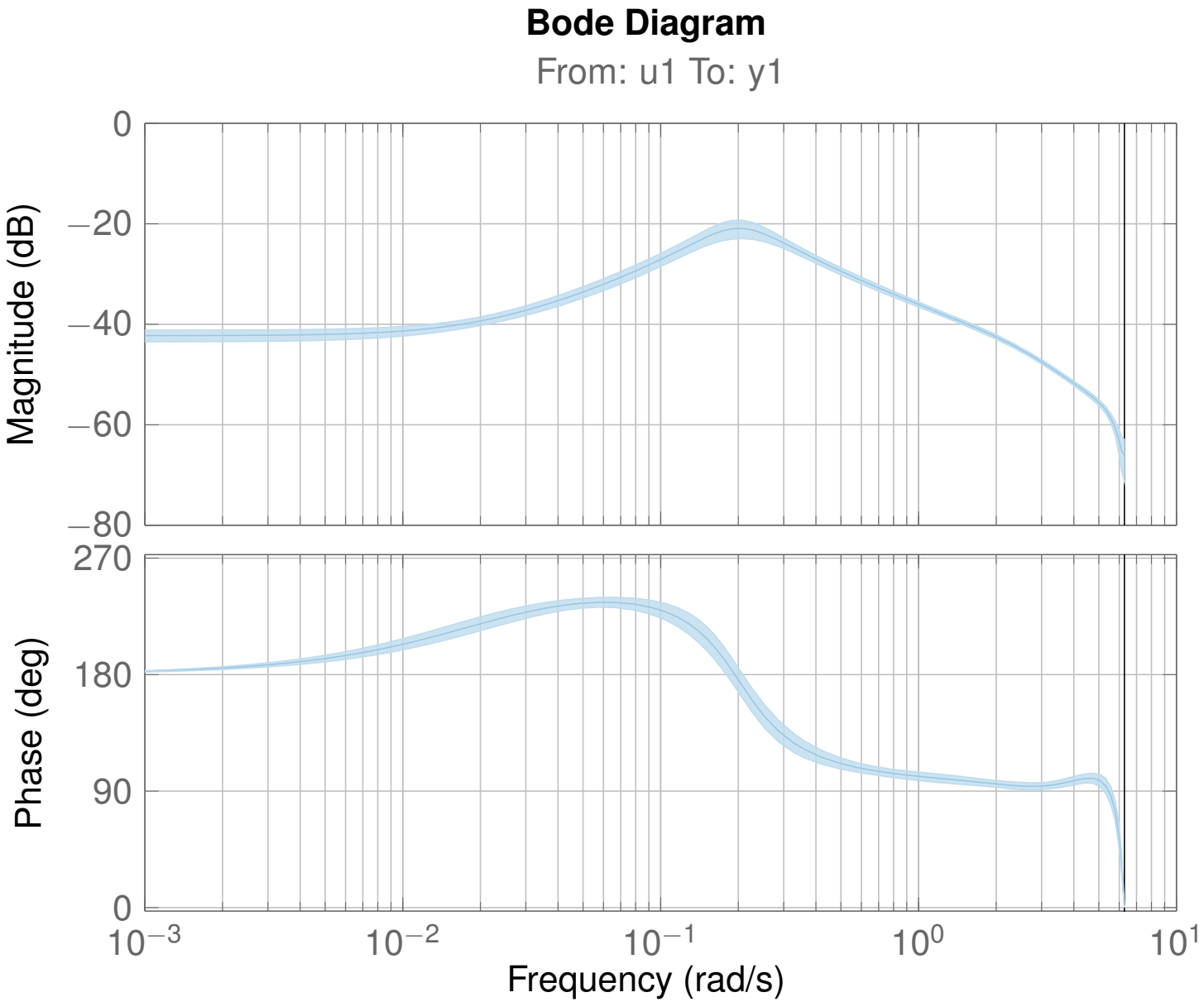


Results from the power system



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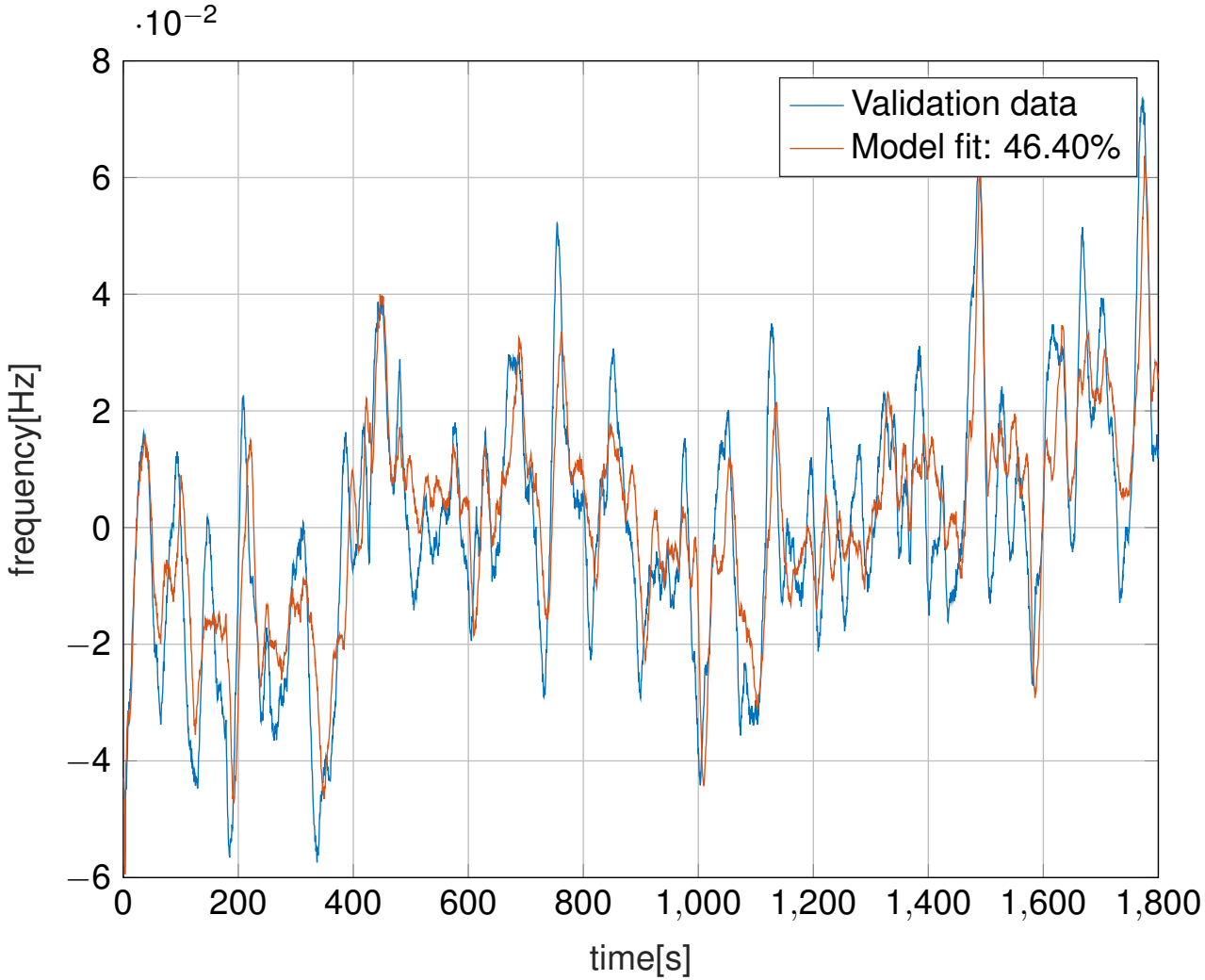

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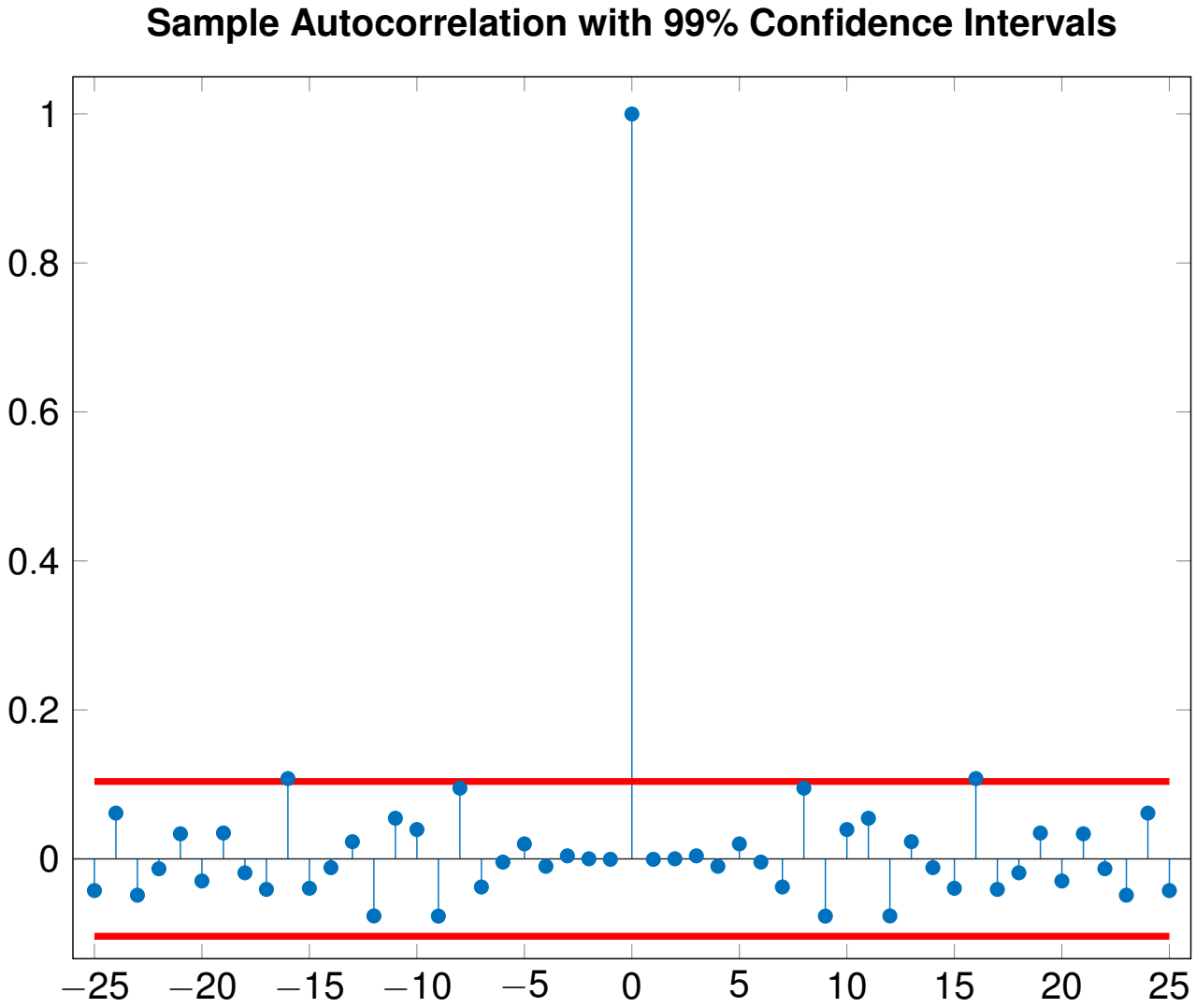

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- It is indeed possible to identify the turbine dynamics(closed loop with electromechanical dynamics) using PMU measurements.
- Look into the assumptions