

# Calculation of Reflection and Transmission Coefficients in SCUFF-TRANSMISSION

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## Contents

<b>1</b>	<b>The Setup</b>	<b>2</b>
<b>2</b>	<b>Scattering coefficients from surface currents</b>	<b>4</b>
2.1	Computation of $\tilde{\mathbf{b}}(\mathbf{q})$ . . . . .	6

## 1 The Setup

SCUFF-TRANSMISSION considers geometries with 2D periodicity, i.e. the structure consists of a unit-cell geometry of finite extent in the  $z$  direction that is infinitely periodically replicated in both the  $x$  and  $y$  directions. The structure is illuminated either from below (the default) or from above by a plane wave with propagation vector  $\mathbf{k}$  confined to the  $xz$  plane.

Working at angular frequency  $\omega$ , let the free-space wavelength be  $k_0 = \frac{\omega}{c}$ , and let the relative permittivity and permeability of the lowermost and uppermost regions in the geometry be  $\epsilon_{\text{L,U}}$  and  $\mu_{\text{L,U}}$ . The wavenumber and relative wave impedance in the uppermost and lowermost regions are

$$\begin{aligned} k_{\text{L}} &= \sqrt{\epsilon_{\text{L}}\mu_{\text{L}}} \cdot k_0, & Z_{\text{L}} &= \sqrt{\frac{\mu_{\text{L}}}{\epsilon_{\text{L}}}} \\ k_{\text{U}} &= \sqrt{\epsilon_{\text{U}}\mu_{\text{U}}} \cdot k_0, & Z_{\text{U}} &= \sqrt{\frac{\mu_{\text{U}}}{\epsilon_{\text{U}}}}. \end{aligned}$$

I will refer to region from which the planewave originates (either the uppermost or lowermost homogeneous region in the SCUFF-EM geometry) as the “source” region. The region into which the planewave eventually emanates is the “destination” region.

In what follows, I will use the symbols  $\mathbf{k}, Z$  and  $\mathbf{k}', Z'$  respectively to denote the wavevectors and relative wave impedances in the source and destination regions. Then I have

$$\begin{aligned} \text{wave incident from below:} & \quad \{|\mathbf{k}|, Z\} = \{k, Z\}_{\text{L}}, & \{|\mathbf{k}'|, Z'\} &= \{k, Z\}_{\text{U}} \\ \text{wave incident from above:} & \quad \{|\mathbf{k}|, Z\} = \{k, Z\}_{\text{U}}, & \{|\mathbf{k}'|, Z'\} &= \{k, Z\}_{\text{L}}. \end{aligned}$$

I will take  $\mathbf{k}$  to live in the  $xz$  plane (i.e.  $\mathbf{k}$  has no  $y$  component,  $k_y = 0$ ) and I will let  $\theta$  be the angle of incidence. Thus the incident wavevector is

$$\begin{aligned} \text{wave incident from below:} & \quad \mathbf{k} = k \sin \theta \hat{\mathbf{x}} + k \cos \theta \hat{\mathbf{z}} \\ \text{wave incident from above:} & \quad \mathbf{k} = k \sin \theta \hat{\mathbf{x}} - k \cos \theta \hat{\mathbf{z}} \end{aligned}$$

The transmitted wavevector is

$$\begin{aligned} \text{wave incident from below:} & \quad \mathbf{k}' = k' \sin \theta' \hat{\mathbf{x}} + k' \cos \theta' \hat{\mathbf{z}} \\ \text{wave incident from above:} & \quad \mathbf{k}' = k' \sin \theta' \hat{\mathbf{x}} - k' \cos \theta' \hat{\mathbf{z}} \end{aligned}$$

The incident and transmitted angles are related by

$$k' \sin \theta' = k \sin \theta.$$

For a general vector  $\mathbf{v}$ , I will define  $\hat{\mathbf{v}} = \mathbf{v}/|\mathbf{v}|$  to be a unit vector in the direction of  $\mathbf{v}$ .

### Definition of scattering coefficients

The incident, reflected, and transmitted fields may be written in the form

$$\begin{aligned}
 \mathbf{E}^{\text{inc}}(\mathbf{x}) &= E_0 \boldsymbol{\epsilon}_0^{\text{inc}} e^{i(k_x x \pm k_z z)} & \mathbf{H}^{\text{inc}}(\mathbf{x}) &= H_0 \bar{\boldsymbol{\epsilon}}_0^{\text{inc}} e^{i(k_x x \pm k_z z)} \\
 \mathbf{E}^{\text{refl}}(\mathbf{x}) &= r E_0 \boldsymbol{\epsilon}_0^{\text{refl}} e^{i(k_x x \mp k_z z)} & \mathbf{H}^{\text{refl}}(\mathbf{x}) &= r H_0 \bar{\boldsymbol{\epsilon}}_0^{\text{refl}} e^{i(k_x x \mp k_z z)} \\
 \mathbf{E}^{\text{trans}}(\mathbf{x}) &= t E_0 \boldsymbol{\epsilon}_0^{\text{trans}} e^{i(k_x x \pm k'_z z)} & \mathbf{H}^{\text{trans}}(\mathbf{x}) &= t H'_0 \bar{\boldsymbol{\epsilon}}_0^{\text{trans}} e^{i(k_x x \pm k'_z z)}
 \end{aligned} \tag{1}$$

where  $E_0$  is the incident field magnitude,  $\boldsymbol{\epsilon}_0^{\text{inc}}$  is the incident-field polarization vector,  $\pm$  is positive (negative) if the wave is incident from below (above), and

$$H_0 \equiv \frac{i|\mathbf{k}|E_0}{ZZ_0}, \quad H'_0 \equiv \frac{i|\mathbf{k}|E_0}{Z'Z_0}, \quad \bar{\boldsymbol{\epsilon}} = \hat{\mathbf{k}} \times \boldsymbol{\epsilon}, \quad \boldsymbol{\epsilon} = -\hat{\mathbf{k}} \times \bar{\boldsymbol{\epsilon}}.$$

Equations (1) define the reflection and transmission coefficients  $r$  and  $t$  computed by SCUFF-TRANSMISSION.

## 2 Scattering coefficients from surface currents

Next we consider an extended structure described by Bloch-periodic boundary conditions, i.e. all fields and currents satisfy

$$\mathbf{Q}(\mathbf{x} + \mathbf{L}) = e^{i\mathbf{k}_B \cdot \mathbf{L}} \mathbf{Q}(\mathbf{x}) \quad (2)$$

where  $\mathbf{Q}$  is a field ( $\mathbf{E}$  or  $\mathbf{H}$ ) or a surface current ( $\mathbf{K}$  or  $\mathbf{N}$ ) and the Bloch wavevector is<sup>1</sup>

$$\mathbf{k}_B = k \sin \theta \hat{\mathbf{x}} = k' \sin \theta' \hat{\mathbf{x}}.$$

For plane waves like (1), equation (2) actually holds for any arbitrary vector  $\mathbf{L}$ ; for our purposes we will only need to use it for certain special vectors  $\mathbf{L}$  determined by the structure of the lattice in our PBC geometry. We will derive expressions for the plane-wave reflection and transmission coefficients in terms of the surface-current distribution in the unit cell of the structure.

### Fields from surface currents

On the other hand, the scattered  $\mathbf{E}$  fields in the source and destination regions may be obtained in the usual way from the surface-current distributions on the surfaces bounding those regions. For example, at points in the destination medium, the scattered (that is, transmitted)  $\mathbf{E}$  field is given by

$$\begin{aligned} \mathbf{E}^{\text{trans}}(\mathbf{x}) &= \oint_{\mathcal{S}} \left\{ \Gamma^{\text{EE}}(\mathbf{x}, \mathbf{x}') \cdot \mathbf{K}(\mathbf{x}') + \Gamma^{\text{EM}}(\mathbf{x}, \mathbf{x}') \cdot \mathbf{N}(\mathbf{x}') \right\} d\mathbf{x}' \\ &= ik' \oint_{\mathcal{S}} \left\{ Z_0 Z' \mathbf{G}(k'; \mathbf{x}, \mathbf{x}') \cdot \mathbf{K}(\mathbf{x}') + \mathbf{C}(k'; \mathbf{x}, \mathbf{x}') \cdot \mathbf{N}(\mathbf{x}') \right\} d\mathbf{x}' \end{aligned} \quad (3)$$

where  $\mathcal{S}$  is the surface bounding the uppermost region and  $\mathbf{G}, \mathbf{C}$  are the homogeneous dyadic GFs. Using the Bloch periodicity of the surface currents, i.e.

$$\begin{Bmatrix} \mathbf{K}(\mathbf{x} + \mathbf{L}) \\ \mathbf{N}(\mathbf{x} + \mathbf{L}) \end{Bmatrix} = e^{i\mathbf{k}_B \cdot \mathbf{L}} \begin{Bmatrix} \mathbf{K}(\mathbf{x}) \\ \mathbf{N}(\mathbf{x}) \end{Bmatrix}$$

we can restrict the surface integral in (3) to just the lattice unit cell:

$$\mathbf{E}^{\text{trans}}(\mathbf{x}) = ik' \int_{\text{UC}} \left\{ Z_0 Z' \overline{\mathbf{G}}(k'; \mathbf{x}, \mathbf{x}') \cdot \mathbf{K}(\mathbf{x}') + \overline{\mathbf{C}}(k'; \mathbf{x}, \mathbf{x}') \cdot \mathbf{N}(\mathbf{x}') \right\} d\mathbf{x}' \quad (4)$$

where the periodic Green's functions are

$$\begin{Bmatrix} \overline{\mathbf{G}}(\mathbf{x}, \mathbf{x}') \\ \overline{\mathbf{C}}(\mathbf{x}, \mathbf{x}') \end{Bmatrix} \equiv \sum_{\mathbf{L}} e^{i\mathbf{k}_B \cdot \mathbf{L}} \begin{Bmatrix} \mathbf{G}(\mathbf{x}, \mathbf{x}' + \mathbf{L}) \\ \mathbf{C}(\mathbf{x}, \mathbf{x}' + \mathbf{L}) \end{Bmatrix} \quad (5)$$

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<sup>1</sup>Recall our conventions that **(a)** the propagation vector lives in the  $xy$  plane, **(b)** unprimed (primed) quantities refer to quantities in the source (destination) region.

I now invoke the following representation of the dyadic Green's functions (Chew, 1995): for  $z > z'$ ,

$$\mathbf{G}(k; \boldsymbol{\rho}, z; \boldsymbol{\rho}', z') = \int \frac{d\mathbf{q}}{(2\pi)^2} \tilde{\mathbf{G}}^\pm(k; \mathbf{q}) e^{i\mathbf{q} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} e^{\pm i q_z (z - z')} \quad (6a)$$

$$\mathbf{C}(k; \boldsymbol{\rho}, z; \boldsymbol{\rho}', z') = \int \frac{d\mathbf{q}}{(2\pi)^2} \tilde{\mathbf{C}}^\pm(k; \mathbf{q}) e^{i\mathbf{q} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} e^{\pm i q_z (z - z')} \quad (6b)$$

where  $\mathbf{q} = (q_x, q_y)$  is a two-dimensional Fourier wavevector,  $d\mathbf{q} = dq_x dq_y$ ,  $q_z = \sqrt{k^2 - |\mathbf{q}|^2}$ ,  $\pm = \text{sign}(z - z')$ , and

$$\begin{aligned} \tilde{\mathbf{G}}^\pm(k; \mathbf{q}) &= \frac{i}{2q_z} \left[ \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} - \frac{1}{k^2} \begin{pmatrix} q_x^2 & q_x q_y & \pm q_x q_z \\ q_y q_x & q_y^2 & \pm q_y q_z \\ \pm q_z q_x & \pm q_z q_y & q_z^2 \end{pmatrix} \right] \\ \tilde{\mathbf{C}}^\pm(k; \mathbf{q}) &= \frac{i}{2q_z k} \begin{pmatrix} 0 & \pm q_z & -q_y \\ -\pm q_z & 0 & q_x \\ q_y & -q_x & 0 \end{pmatrix}. \end{aligned}$$

Inserting (6) into (5), I obtain, for the periodic version of e.g. the  $\mathbf{G}$  kernel,

$$\begin{aligned} \overline{\mathbf{G}}(k; \boldsymbol{\rho}, z; \boldsymbol{\rho}', z) &= \int \frac{d\mathbf{q}}{(2\pi)^2} \tilde{\mathbf{G}}^\pm(k; \mathbf{q}) e^{i\mathbf{q} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} e^{\pm i q_z (z - z')} \underbrace{\sum_{\mathbf{L}} e^{i(\mathbf{k}_B - \mathbf{q}) \cdot \mathbf{L}}}_{\mathcal{V}_{\text{BZ}} \sum_{\mathbf{\Gamma}} \delta(\mathbf{q} - \mathbf{k} - \mathbf{\Gamma})} \\ &= \mathcal{V}_{\text{UC}}^{-1} \sum_{\mathbf{q} = \mathbf{k}_B + \mathbf{\Gamma}} \tilde{\mathbf{G}}^\pm(k; \mathbf{q}) e^{i\mathbf{q} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} e^{\pm i q_z (z - z')} \end{aligned}$$

where the sum over  $\mathbf{\Gamma}$  runs over reciprocal lattice vectors; the prefactor  $\mathcal{V}_{\text{BZ}}$ , the volume of the Brillouin zone, is related to the unit-cell volume by  $\mathcal{V}_{\text{BZ}} = 4\pi^2/V_{\text{UC}}$  for a 2D square lattice. Similarly, we find

$$\overline{\mathbf{C}}(k; \boldsymbol{\rho}, z; \boldsymbol{\rho}', z) = \mathcal{V}_{\text{UC}}^{-1} \sum_{\mathbf{q} = \mathbf{k}_B + \mathbf{\Gamma}} \tilde{\mathbf{C}}^\pm(k; \mathbf{q}) e^{i\mathbf{q} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} e^{\pm i q_z (z - z')}.$$

Keeping only the  $\mathbf{\Gamma} = 0$  term in these sums, the scattered  $\mathbf{E}$ -fields in the uppermost and lowermost regions are thus

$$\mathbf{E}^{\text{upper}}(\mathbf{x}) = e^{i(k_{\text{U}x}x + k_{\text{U}z}z)} \left[ i k_{\text{U}} Z_0 Z_{\text{U}} \tilde{\mathbf{G}}^+(k_{\text{U}}; \mathbf{k}_B) \tilde{\mathbf{K}}_{\text{U}}(\mathbf{k}_B) + i k_{\text{U}} \tilde{\mathbf{C}}^+(k_{\text{U}}; \mathbf{k}_B) \tilde{\mathbf{N}}(\mathbf{k}_B) \right] \quad (7)$$

$$\mathbf{E}^{\text{lower}}(\mathbf{x}) = e^{i(k_{\text{L}x}x - k_{\text{L}z}z)} \left[ i k_{\text{L}} Z_0 Z_{\text{U}} \tilde{\mathbf{G}}^-(k_{\text{L}}; \mathbf{k}_B) \tilde{\mathbf{K}}(\mathbf{k}_B) + i k_{\text{L}} \tilde{\mathbf{C}}^-(k_{\text{L}}; \mathbf{k}_B) \tilde{\mathbf{N}}(\mathbf{k}_B) \right] \quad (8)$$

where e.g.  $\tilde{\mathbf{K}}_{\text{U}}$  is something like the two-dimensional Fourier transform of the surface currents on the boundary of the uppermost region  $\mathcal{R}_{\text{U}}$ :

$$\tilde{\mathbf{K}}_{\text{U}}(\mathbf{k}_B) \equiv \frac{1}{\mathcal{V}_{\text{UC}}} \int_{\partial \mathcal{R}_{\text{U}}} \mathbf{K}(\boldsymbol{\rho}', z') e^{-i\mathbf{k}_B \cdot \boldsymbol{\rho}' - i q_z |z'|} d\mathbf{x}', \quad q_z^2 = k_{\text{U}}^2 - |\mathbf{k}_B|^2.$$

with  $\tilde{\mathbf{K}}_L$  and  $\tilde{\mathbf{N}}_{U,L}$  defined similarly.

Comparing this to (1c), we see that the transmission and reflection coefficients for the polarization defined by polarization vector  $\boldsymbol{\epsilon}$  are given by

$$\begin{Bmatrix} t \\ r \end{Bmatrix} = ik_U Z_0 Z_U \boldsymbol{\epsilon}^\dagger \tilde{\mathbf{G}}^+(k_U, \mathbf{k}_B) \tilde{\mathbf{K}}_U(\mathbf{k}_B) + ik_U \boldsymbol{\epsilon}^\dagger \tilde{\mathbf{C}}^+(k_U, \mathbf{k}_B) \tilde{\mathbf{N}}(\mathbf{k}_B) \quad (9)$$

$$\begin{Bmatrix} r \\ t \end{Bmatrix} = ik_L Z_0 Z_L \boldsymbol{\epsilon}^\dagger \tilde{\mathbf{G}}^+(k_L, \mathbf{k}_B) \tilde{\mathbf{K}}_L(\mathbf{k}_B) + ik_L \boldsymbol{\epsilon}^\dagger \tilde{\mathbf{C}}^+(k_L, \mathbf{k}_B) \tilde{\mathbf{N}}(\mathbf{k}_B) \quad (10)$$

The expressions on the RHS compute the upper (lower) quantities on the LHS for the case in which the plane wave is incident from below (above).

The  $\tilde{\mathbf{K}}$  and  $\tilde{\mathbf{N}}$  quantities are given by sums of contributions from individual basis functions; for example,

$$\tilde{\mathbf{K}}_U(\mathbf{q}) = \frac{1}{\mathcal{V}_{UC}} \sum_{\mathbf{b}_\alpha \in \partial\mathcal{R}_U} k_\alpha \widetilde{\mathbf{b}}_\alpha(\mathbf{q}), \quad \tilde{\mathbf{N}}_U(\mathbf{q}) = -\frac{Z_0}{\mathcal{V}_{UC}} \sum_{\mathbf{b}_\alpha \in \partial\mathcal{R}_U} n_\alpha \widetilde{\mathbf{b}}_\alpha(\mathbf{q})$$

where the sums are over all RWG basis functions that live on surfaces bounding the uppermost medium and  $\{k_\alpha, n_\alpha\}$  are the surface-current coefficients obtained as the solution to the SCUFF-EM scattering problem.

## 2.1 Computation of $\widetilde{\mathbf{b}}(\mathbf{q})$

For RWG functions the quantity  $\widetilde{\mathbf{b}}(\mathbf{q})$  may be evaluated in closed form:

$$\begin{aligned} \widetilde{\mathbf{b}}_\alpha(\mathbf{q}) &\equiv \int_{\sup \mathbf{b}_\alpha} \mathbf{b}_\alpha(\mathbf{x}) e^{-i\mathbf{q} \cdot \mathbf{x}} d\mathbf{x} \\ &= \ell_\alpha \int_0^1 du \int_0^u dv \left\{ e^{-i\mathbf{q} \cdot [\mathbf{Q}^+ + u\mathbf{A}^+ + v\mathbf{B}]} (u\mathbf{A}^+ + v\mathbf{B}) \right. \\ &\quad \left. - e^{-i\mathbf{q} \cdot [\mathbf{Q}^- + u\mathbf{A}^- + v\mathbf{B}]} (u\mathbf{A}^- + v\mathbf{B}) \right\} \\ &= \ell_\alpha \left\{ e^{-i\mathbf{q} \cdot \mathbf{Q}^+} \left[ f_1(\mathbf{q} \cdot \mathbf{A}^+, \mathbf{q} \cdot \mathbf{B}) \mathbf{A}^+ + f_2(\mathbf{q} \cdot \mathbf{A}^+, \mathbf{q} \cdot \mathbf{B}) \mathbf{B} \right] \right. \\ &\quad \left. - e^{-i\mathbf{q} \cdot \mathbf{Q}^-} \left[ f_1(\mathbf{q} \cdot \mathbf{A}^-, \mathbf{q} \cdot \mathbf{B}) \mathbf{A}^- + f_2(\mathbf{q} \cdot \mathbf{A}^-, \mathbf{q} \cdot \mathbf{B}) \mathbf{B} \right] \right\} \end{aligned}$$

where

$$\begin{aligned} f_1(x, y) &= \int_0^1 \int_0^u u e^{-i(ux+vy)} dv du \\ f_2(x, y) &= \int_0^1 \int_0^u v e^{-i(ux+vy)} dv du. \end{aligned}$$