# Finite Difference Method applied to DML simulation. Part 2b rev2.

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#### **Abstract**

Simulation of Distributed Mode Loudspeaker (DML) thanks to the Finite Difference Method (FDM) : eigenfrequencies

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**Disclaimer**: this paper is written in the context of DIY DML building. This document is not written in the context of any academic or scientific work. Its content is reviewed only by the feedback it can get while posting it in audio DIY forum like diyAudio.

Exported: April 6, 2025.

**Revision 1.**: The code is rewritten to be more compact and focused on the FDM operations.

Revision 2. : Base on the update of part1, 1b and 2, the free edge conditions are now included.

The pdf format of the paper is directly extracted from a python script See Github py2pdf for more information about this method.

## 1 Introduction

The part 2a is the application of part 1 and 1b in a Python script up to the calculation of the system matrix.

In this part 2b, the focus is on the modes (frequency and mode shape) and the comparison of the results of the script with some plate situations simulated with Elmer, Lisa or having exact solutions.

Elmer is a free multi-plateform FEM solver. More details about the simulation files used below.

The formulas to extend the simply supported plate case came first from [1] but were much too inaccurate. The Warburton approach [2] is now implemented.

Many thanks to Eric (Veleric@diyAudio) who helped by providing results from LISA. It was from a great help in bug fixing.

## 2 Eigenfrequencies

In part 1, the partial derevative equation (PDE) of the vibration of a plate was shown.

For an isotropic homogeneous material, the governing equation is :

$$D(\frac{\partial^4 w}{\partial x^4} + 2\frac{\partial^4 w}{\partial x^2 \partial y^2} + \frac{\partial^4 w}{\partial y^4}) = -q(x,y,t) - \mu \frac{\partial^2 w}{\partial t^2} \tag{1}$$

The PDE in the case of an orthotropic material was also shown (refer to part 1).

The calculation of the eigenfrequencies is a specific case where this equation is solved.

Looking for the natural resonance frequencies, the external load is assumed to be null : q(x, y, t) = 0.

The second assumption is to separate the plate deviation w in a product of 2 functions :

$$w(x, y, t) = W(x, y)cos(\omega t)$$

w being in the time a cosine function, its second derivative over the time is also a cosine so the time "disappears" from the equation which becomes :

$$D(\frac{\partial^4 W}{\partial x^4} + 2\frac{\partial^4 W}{\partial x^2 \partial y^2} + \frac{\partial^4 W}{\partial y^4}) = \mu \omega^2 W \tag{2}$$

Which is with the finite difference method (see also part 1) FDM in the form :

$$M_{sus}W = \mu\omega^2 W \tag{3}$$

The modes are the eigenfrequencies of the  ${\cal M}_{sus}$  and the mode shapes are the eigenvectors

This web page explains the concept of eigenvalue and of eigenvector; how numpy can extract them.

# 3 The testing plate

Different boundary conditions were tested and compare to FEM outputs.

The boundary conditions are denoted S (or SS) for simply supported, C for clamped or F for free for each edge and combined.

2 test cases denoted XXXX and OOOO were added where respectivly the 4 corners or the 4 central points of the edges have a null displacement condition.

See figure 1 for the plate representation in the FDM script.

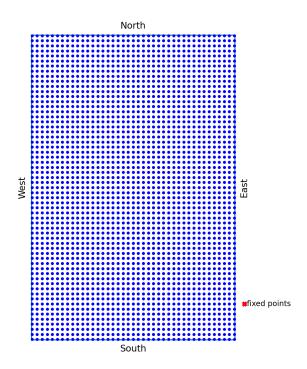


Figure 1: Testing plate

# 4 Computational efficiency

The time to get the result depends of course of the computer. For the one used for the first revisions, the results from Elmer were obtains much faster than with this FDM script which let suppose there are important possibilities of improvements but which need skills in coding.

By changing from an old I3 processor to a new (in 2023...) I7 (I7-1360P 13th generation), the response time is improved by a factor of about 20! With a 10mm grid and the 600x400mm test panel (2501 points), the modes are computed in few seconds. It is not an issue to get the results for more than 10 test cases. Note the performance change a lot with the power management options of the computer. Each case takes about 12s in energy saving mode on battery but only about 3s in performance mode on mains.

The execution time increases as the cube of the number of cells.

Possible heuristic :  $t_{exec} = cte + N_{cells}^3/K$ 

See figure 2

# 5 FDM performances

#### 5.1 First script with the specific SS and C boundary conditions implemented

With a 20mm grid, the precision for the 5 test cases are : -1.7, -.9, -1.2, -1.5, -1% over the 16th first modes.

With a 10mm grid, the precision for the 5 test cases are: .36, .21, .18, .36, .13% over the 16th first modes.

#### 5.2 Free edge script

While the free edge conditions are implemented, the simply supported and clamped boundary conditions are replaced by zero displacement at the edge which give excellent results in the simply supported conditions and most probably acceptable for clamped condition. The error seen for clamped edges comes from plate dimension reduction linked to the double row of zero displacement points.

Because of the improvement in the computation efficiency, the 10mm grid was the only tested.

The script was tested over the 25 first modes of different combinaitions of edge conditions. The exact error values are in the script output section. Roughly, the mean error over the 25 first modes is below 1.5%. It

Cells	dx mm	mesh	i3-4030U	Model (I3)	I5-6200u	I7-1260P	I7-1360P
176	40	11x16	4,48	4,25			0,007
425	25	17x25	7,95	4,84			0,125
651	20	21x31	10,15	6,50	0,43	0,29	0,2
1734	12	34x51	46,7	47,65			1,4
2501	10	41x61	132,38	134,56	14,8	7,38	5,2
3876	8	51x76	495	489,46	48,16	26,86	24
9801	5				750,7	538,6	384

cte	4,2
K	1,20E+08

# FDM script response time = f(nb of points)

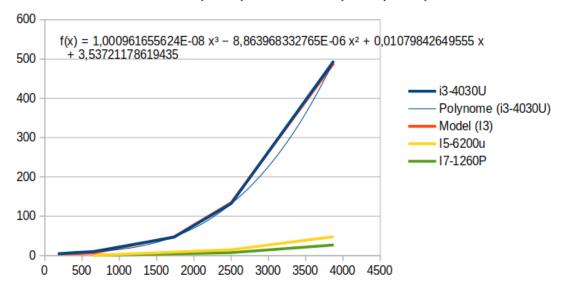


Figure 2: FDM performance

increases when 2 or more clamped edges are involved. The error with a clamped edge is a bit theoric related to the real panel dimensions, edge included or not.

To have a view beyond the 25 first modes, 250 modes were extracted from Elmer and the FDM and compared. The error seems to increase linearly with the frequency remaining below 5% up to 4kHz. This was not analyze to understand the role of the mesh size in the FDM and in Elmer.

See figure 3

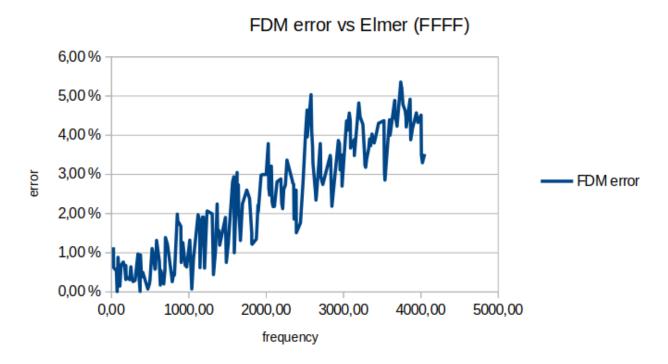


Figure 3: FDM performance

The formula tested from the Warburton's paper give very good results when simply supported and clamped edges are combined. Curiously, the results are not good when a free edge is involed while no bug was found...

# 6 Mode shapes

The FDM script extracts the mode shape. Below is an example presented in a colorized 2D. Other views are possible with matplotlib.

The mode shapes from the script were compare to the one from the FEM software LISA, at least for the first one of some configurations which was a good way to debug the script.

See figure 4

# 7 Conclusion on the FDM performances

The Python FDM script shows good enough performances in precision, computational time to be further used in DML design. Compared to other ways of simulation being very close to the reality in the description of the panel, it should offer an excellent flexibility to explore the different configuration of the DIYers' designs.

# 8 The script results

For each test case, a table is printed out with:

- FEM : eigenfrequencies in Hz from FEM tool (Elmer or Lisa)
- FDM: eigenfrequencies in Hz from the FDM script
- err% : FDM compared to FEM

## Mode shapes OOOO

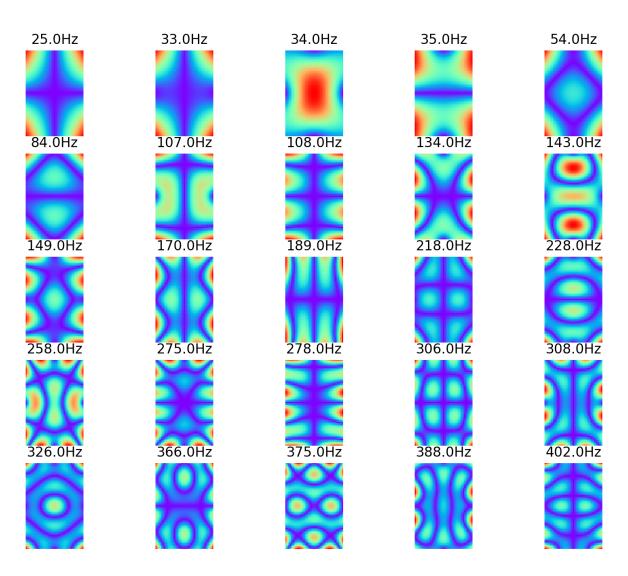


Figure 4: FDM performance

- Warb. : eigenfrequencies in Hz based on the formulas provided in the Warburton's paper
- err% : Warburton estimation compared to FEM

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The plate is Lx = 0.4 m by Ly = 0.6 m

The plate thickness is h = 0.015 m

The mesh is Nj = 41 points by Nk = 61 points

with a grid dx = 10.0 mm by dy = 10.0 mm

Young modulus E = 10 MPa, Density rho = 25.0 kg/m<sup>3</sup>

Bending stiffness Dx = Dy = 3.09 Nm, Areal density  $\mu$  = 0.375 kg/m<sup>2</sup>

with Poisson's ratio nux = 0.3 and nuy = 0.3

Excecution time (system matrix preparation) = 0.1035 seconds for 2501 points

-----

Case # 0
Boundary conditions ['F [north]', 'F [west]', 'F [south]', 'F [east]']
Excecution time (solver) = 14.3606 seconds for 2501 points

FEM	FDM	err%	Warb.	err%	
0	0	0	132	0	
0	0	0	196	0	
0	0	0	245	0	
25	25	0	277	1008	
27	27	0	319	1081	
58	58	0	380	555	
63	63	0	409	549	
72	73	1	411	470	
84	84	0	488	480	
107	108	0	505	371	
123	125	1	519	321	
151	151	0	584	286	
170	170	0	634	272	
183	184	0	650	255	
184	187	1	700	280	
188	189	0	711	278	
234	237	1	810	246	
249	249	0	837	236	
262	266	1	914	248	
276	278	0	930	236	
302	306	1	990	227	
339	339	0	1071	215	
349	351	0	1090	212	
365	370	1	1212	232	
371	371	0	1357	265	
error 0	51 %				

Mean error 0.51 % Max error 1.6 %

Case # 1

Boundary conditions ['O [north]', 'O [west]', 'O [south]', 'O [east]'] Excecution time (solver) = 11.2198 seconds for 2501 points

FEM	FDM	err%	Warb.	err%
25	25	0	0	-100
32	33	3	0	-100
33	34	3	0	-100
34	35	2	0	-100
53	54	1	0	-100
84	84	0	0	-100
104	107	2	0	-100
107	108	0	0	-100
130	134	3	0	-100
138	143	3	0	-100
147	149	1	0	-100

170	170	0	0	-100
188	189	0	0	-100
216	218	0	0	-100
225	228	1	0	-100
249	258	3	0	-100
269	275	2	0	-100
276	278	0	0	-100
297	306	3	0	-100
302	308	1	0	-100
319	326	2	0	-100
363	366	0	0	-100
372	375	0	0	-100
381	388	1	0	-100
397	402	1	0	-100

Mean error 1.72 % Max error 3.6 %

Case # 2
Boundary conditions ['F [north]', 'F [west]', 'S [south]', 'S [east]']
Excecution time (solver) = 10.6813 seconds for 2501 points

cecution	time (Solver)	- 10.00	sis seconds	101 2501	points	
FEM	FDM	err%	Warb.	err%		
6	6	0	101	1583		
27	27	0	155	474		
47	47	0	197	319		
69	69	0	228	230		
76	76	0	258	239		
124	125	0	323	160		
137	137	0	338	146		
145	145	0	348	140		
173	173	0	411	137		
194	195	0	439	126		
225	226	0	442	96		
231	231	0	496	114		
287	288	0	557	94		
298	297	0	562	88		
301	302	0	602	100		
326	325	0	620	90		
349	347	0	706	102		
379	379	0	729	92		
396	399	0	815	105		
406	406	0	823	102		
455	457	0	885	94		
491	487	0	946	92		
509	504	0	972	90		
517	518	0	1083	109		
536	532	0	1216	126		

Mean error 0.0 % Max error 0.8 %

Case # 3
Boundary conditions ['S [north]', 'F [west]', 'S [south]', 'F [east]']
Excecution time (solver) = 10.1673 seconds for 2501 points

Excecution	cime (Solver)	- 10.10	ors seconds	101 250	٠.
FEM	FDM	err%	Warb.	err%	
12	12	0	83	591	
26	27	3	132	407	
49	49	0	193	293	
68	69	1	203	198	
82	83	1	243	196	
110	110	0	296	169	
129	131	1	318	146	

131 133 1 361

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192	192	0	409	113
196	197	0	413	110
197	201	2	417	111
218	220	0	485	122
238	241	1	538	126
287	292	1	585	103
306	308	0	586	91
309	315	1	632	104
327	331	1	707	116
357	358	0	710	98
399	405	1	808	102
401	406	1	867	116
402	411	2	912	126
439	443	0	933	112
460	466	1	985	114
471	480	1	1086	130
516	529	2	1212	134

Mean error 1.24 % Max error 3.8 %

Case # 4

Boundary conditions ['F [north]', 'S [west]', 'F [south]', 'S [east]'] Excecution time (solver) = 10.7177 seconds for 2501 points

LYCECTION	cime (poiver)	- 10.71	iii seconds	101 2001	POINTS
FEM	FDM	err%	Warb.	err%	
27	27	0	65	140	
36	37	2	115	219	
64	65	1	156	143	
111	111	0	189	70	
114	114	0	211	85	
121	121	0	286	136	
153	154	0	288	88	
187	188	0	299	59	
206	208	0	358	73	
251	250	0	385	53	
261	260	0	412	57	
281	284	1	437	55	
286	286	0	498	74	
295	295	0	509	72	
350	352	0	538	53	
381	382	0	558	46	
411	408	0	640	55	
428	431	0	663	54	
448	444	0	744	66	
457	454	0	752	64	
491	490	0	814	65	
504	504	0	871	72	
529	532	0	898	69	
548	548	0	1004	83	
560	555	0	1133	102	

Mean error 0.21 % Max error 2.7 %

#### Case # 5

Boundary conditions ['S [north]', 'F [west]', 'F [south]', 'F [east]'] Excecution time (solver) = 10.5594 seconds for 2501 points

FEM	FDM	err%	Warb.	err%
0	0	0	120	0
12	12	0	176	1366
18	18	0	232	1188
42	43	2	251	497
60	60	0	295	391

69	69	0	347	402
88	89	1	378	329
102	102	0	398	290
130	130	0	463	256
155	156	0	467	201
157	158	0	482	207
179	178	0	550	207
211	211	0	607	187
223	222	0	621	178
232	234	0	659	184
249	249	0	685	175
270	272	0	775	187
327	328	0	790	141
339	337	0	887	161
349	346	0	901	158
350	352	0	965	175
367	366	0	1021	178
377	376	0	1054	179
434	435	0	1168	169
449	449	0	1305	190
_	^.			

Mean error 0.17 % Max error 2.29 %

Case # 6

Boundary conditions ['F [north]', 'S [west]', 'F [south]', 'F [east]'] Excecution time (solver) = 10.4949 seconds for 2501 points

FEM	FDM	err%	Warb.	err%	-
0	0	0	113	0	
12	12	0	174	1350	
36	36	0	210	483	
44	44	0	254	477	
57	57	0	280	391	
86	86	0	355	312	
93	94	1	361	288	
140	140	0	367	162	
146	147	0	435	197	
155	155	0	474	205	
160	160	0	480	200	
193	194	0	528	173	
223	224	0	570	155	
252	253	0	603	139	
260	259	0	640	146	
295	293	0	644	118	
306	305	0	740	141	
322	323	0	774	140	
334	336	0	836	150	
346	346	0	856	147	
383	381	0	910	137	
409	410	0	995	143	
437	439	0	1006	130	
445	444	0	1125	152	
494	496	0	1267	156	

Mean error 0.1 % Max error 1.0 %

Case # 7

Boundary conditions ['X [north]', 'X [west]', 'X [south]', 'X [east]'] Excecution time (solver) = 11.2234 seconds for 2501 points

FEM	FDM	err%	Warb.	err%
11	11	0	0	-100
26	27	3	0	-100

32	32	0	0	-100
42	42	0	0	-100
65	66	1	0	-100
72	73	1	0	-100
87	88	1	0	-100
110	113	2	0	-100
138	139	0	0	-100
139	142	2	0	-100
144	146	1	0	-100
170	170	0	0	-100
206	211	2	0	-100
209	212	1	0	-100
223	226	1	0	-100
226	230	1	0	-100
280	285	1	0	-100
283	287	1	0	-100
298	303	1	0	-100
307	316	2	0	-100
350	351	0	0	-100
350	354	1	0	-100
377	379	0	0	-100
386	391	1	0	-100
398	412	3	0	-100

Mean error 1.41 % Max error 3.8 %

Case # 8
Boundary conditions ['S [north]', 'S [west]', 'S [south]', 'S [east]']
Excecution time (solver) = 9.0550 seconds for 2501 points

FEM	FDM	err%	Warb.	err%	1	
40	40	0	40	0		
77	78	1	78	1		
124	125	0	125	0		
140	140	0	140	0		
161	162	0	162	0		
223	225	0	225	0		
227	227	0	228	0		
265	265	0	266	0		
302	302	0	303	0		
310	312	0	313	0		
340	339	0	341	0		
363	364	0	366	0		
423	423	0	425	0		
449	452	0	454	1		
463	459	0	463	0		
477	475	0	501	5		
499	497	0	563	12		
560	559	0	566	1		
560	559	0	651	16		
561	563	0	717	27		
640	635	0	754	17		
645	646	0	764	18		
699	699	0	817	16		
717	708	-1	905	26		
723	719	0	1017	40		

Mean error 0.03 % Max error 1.2 %

Case # 9

Boundary conditions ['C [north]', 'C [west]', 'C [south]', 'C [east]'] Excecution time (solver) = 9.6949 seconds for 2501 points

FEM	FDM	err%	Warb.	err%
76	80	5	77	1
118	124	5	119	0
186	197	5	189	1
188	198	5	190	1
225	238	5	229	1
285	297	4	289	1
290	307	5	295	1
353	375	6	358	1
383	404	5	390	1
389	414	6	397	2
407	425	4	413	1
452	481	6	462	2
502	528	5	512	1
542	575	6	553	2
554	577	4	584	5
573	609	6	623	8
609	648	6	672	10
647	679	4	687	6
658	697	5	776	17
670	715	6	866	29
725	754	4	893	23
757	808	6	906	19
799	845	5	969	21
816	854	4	1058	29
848	900	6	1172	38
	E D 9/			

Mean error 5.53 % Max error 6.7 %

Case # 10
Boundary conditions ['S [north]', 'S [west]', 'C [south]', 'C [east]']
Excecution time (solver) = 16.7274 seconds for 2501 points

Excecution	time (solver)	= 16.7	274 seconds	for 250	l points	
FEM	FDM	err%	Warb.	err%		
56	58	3	62	10		
96	99	3	105	9		
154	158	2	160	3		
163	167	2	173	6		
191	197	3	204	6		
255	261	2	267	4		
255	263	3	272	6		
308	316	2	315	2		
344	355	3	358	4		
345	355	2	365	5		
373	380	1	386	3		
406	420	3	426	4		
461	473	2	484	4		
494	510	3	520	5		
515	524	1	527	2		
517	530	2	570	10		
553	569	2	638	15		
603	616	2	638	5		
608	627	3	731	20		
614	633	3	795	29		
682	693	1	838	22		
700	723	3	849	21		
748	769	2	905	20		
769	784	1	998	29		
781	799	2	1116	42		

Mean error 2.65 % Max error 3.5 %

Case # 11
Boundary conditions ['S [north]', 'C [west]', 'S [south]', 'C [east]']
Excecution time (solver) = 9.5196 seconds for 2501 points

FEM	FDM	err%	Warb.	err%
71	74	4	71	0
99	103	4	100	1
155	158	1	157	1
183	194	6	185	1
213	224	5	216	1
239	241	0	241	0
266	278	4	270	1
346	350	1	351	1
349	358	2	352	0
350	372	6	355	1
381	404	6	387	1
434	458	5	442	1
452	463	2	459	1
485	485	0	522	7
512	537	4	581	13
571	595	4	614	7
585	607	3	627	7
603	640	6	670	11
617	641	3	749	21
646	643	0	854	32
656	696	6	863	31
734	751	2	897	22
744	770	3	953	28
747	775	3	1034	38
832	825	0	1138	36
n orror	2 10 %			

Mean error 3.48 % Max error 6.2 %

Case # 12

Boundary conditions ['S [north]', 'S [west]', 'C [south]', 'S [east]'] Excecution time (solver) = 9.0735 seconds for 2501 points

JACCCUUIOII	CIMC (BOLVCI)	3.0700	BCCOHGB	101 2001	POINTS
FEM	FDM	err%	Warb.	err%	
44	44	0	46	4	
88	89	1	90	2	
126	127	0	131	3	
157	160	1	159	1	
168	170	1	174	3	
236	240	1	243	2	
250	255	2	254	1	
267	266	0	271	1	
307	308	0	315	2	
330	336	1	337	2	
369	375	1	373	1	
373	377	1	384	2	
448	456	1	456	1	
464	461	0	469	1	
465	472	1	477	2	
503	502	0	512	1	
512	520	1	580	13	
567	570	0	597	5	
583	592	1	674	15	
591	601	1	722	22	
658	664	0	766	16	
679	689	1	793	16	
718	709	-1	834	16	
726	737	1	928	27	
756	749	0	1046	38	

```
Mean error 0.88 % Max error 2.0 %
```

## 9 Elmer

## 9.1 Geometry (rectangular\_plate.geo)

```
// Inputs
Lx = 0.4; //m
Ly = 0.6; //m
gridsize = Lx / 20;
// All numbering counterclockwise from bottom-left corner
Point(1) = \{-Lx/2, -Ly/2, 0, gridsize\};
Point(2) = \{Lx/2, -Ly/2, 0, gridsize\};
Point(3) = \{Lx/2, Ly/2, 0, gridsize\};
Point(4) = \{-Lx/2, Ly/2, 0, gridsize\};
Line(1) = \{1, 2\};
                                 // bottom line
Line(2) = \{2, 3\};
                                 // right line
Line(3) = \{3, 4\};
                                 // top line
Line(4) = \{4, 1\};
                                 // left line
Line Loop(5) = \{1, 2, 3, 4\};
// the order of lines in Line Loop is used again in surfaceVector[]
Plane Surface(6) = {5};
```

The rectangular plate.msh is obtain from the gmsh application.

#### 9.2 Mesh

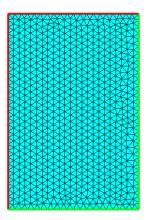


Figure 5: plate mesh

See figure 5

## 9.3 Solver (case.sif)

```
Header
CHECK KEYWORDS Warn
Mesh DB "." "."
Include Path ""
Results Directory ""
End
Simulation
Max Output Level = 5
```

```
Coordinate System = Cartesian
  Coordinate Mapping(3) = 1 2 3
  Simulation Type = Steady state
  Steady State Max Iterations = 1
  Output Intervals = 1
  Timestepping Method = BDF
  BDF Order = 1
  Solver Input File = case.sif
 Post File = case.vtu
End
Constants
  Gravity(4) = 0 -1 0 9.82
  Stefan Boltzmann = 5.67e-08
 Permittivity of Vacuum = 8.8542e-12
 Boltzmann Constant = 1.3807e-23
 Unit Charge = 1.602e-19
End
Body 1
  Target Bodies(1) = 1
  Name = "Body 1"
 Equation = 1
 Material = 1
End
Solver 1
  Equation = Elastic Plates
  Variable = -dofs 3 Deflection
 Eigen System Values = 25
 Eigen Analysis = True
  Eigen System Select = Smallest magnitude
  Procedure = "Smitc" "SmitcSolver"
  Exec Solver = Always
  Stabilize = True
  Bubbles = False
 Lumped Mass Matrix = False
  Optimize Bandwidth = True
  Steady State Convergence Tolerance = 1.0e-5
  Nonlinear System Convergence Tolerance = 1.0e-7
  Nonlinear System Max Iterations = 1
  Nonlinear System Newton After Iterations = 3
  Nonlinear System Newton After Tolerance = 1.0e-3
  Nonlinear System Relaxation Factor = 1
 Linear System Solver = Direct
  Linear System Direct Method = Umfpack
End
Equation 1
 Name = "Plate Equation"
  Active Solvers(1) = 1
End
Material 1
 Name = "EPS"
 Porosity Model = Always saturated
 Tension = 0.0
  Youngs modulus = 10e6
  Thickness = 0.015
  Poisson ratio = 0.
  Density = 25
```

```
Boundary Condition 1
Target Boundaries(2) = 3 4
Name = "fixed"
Deflection 2 = 0
Deflection 3 = 0
Deflection 1 = 0
End

Boundary Condition 2
Target Boundaries(2) = 1 2
Name = "Simply supported"
Deflection 1 = 0
End
```

The Elmer results are stored in the elmer() function to be displayed along with the script results.

## 10 Python script code

## 10.1 Import modules

```
import os # for py2pdf
import shutil # for py2pdf backup
import time # for script time performance
import christianpylib.py2pdf as p2p # import py2pdf library
import numpy as np
# from fdm_applied_to_dml_part2b1 import Bound_cond
import mod_fdm_print_FFFF as fdmp # import the module of specific functions to print and plot
import mod_fdm_FFFF as fdmbm # import the module of specific functions to build the matrices of a free
import mod_fdm_elmer as fdmelm
import matplotlib.pyplot as plt
from scipy import linalg
```

#### 10.2 Functions

Empty section : all the functions are in external modules

## 10.3 Prepare py2pdf

```
# lines to be included for py2pdf export
script_name = os.path.basename(__file__).split(".")[0] # get this script file name without extension
py2pdfdir = "../data/part2b2" # where the script logs are saved
logfile = py2pdfdir + "/DML_FDM3b.txt" # define the logfile
p2p.clearlog(logfile) # clear the logfile (in case script is ran several times)
logfile2 = py2pdfdir + "/DML_FDM3b_2.txt" # define the logfile to store eigenfrequencies of FFFF
p2p.clearlog(logfile2) # clear the logfile (in case script is ran several times)
```

#### 10.4 Parameters

```
# Test cases reported in this paper
# Boundary conditions C = clamped, SS = simply supported, F = free, North, West, South, East
BoundDict1 = {
    "North": "F",
    "West": "F",
    "South": "F",
    "East": "F"
}
BoundDict2 = {
```

```
"North": "0",
    "West": "0",
    "South": "0",
    "East": "0"
}
BoundDict3 = {
    "North": "F",
    "West": "F",
    "South": "SS",
    "East": "SS"
}
BoundDict4 = {
    "North": "SS",
    "West": "F",
"South": "SS",
    "East": "F"
}
BoundDict5 = {
   "North": "F",
    "West": "SS",
    "South": "F",
    "East": "SS"
}
BoundDict6 = {
    "North": "SS",
    "West": "F",
    "South": "F",
    "East": "F"
}
BoundDict7 = {
    "North": "F",
    "West": "SS",
    "South": "F",
    "East": "F"
}
BoundDict8 = {
    "North": "X",
    "West": "X",
    "South": "X",
    "East": "X"
BoundDict9 = {
    "North": "SS",
    "West": "SS",
"South": "SS",
    "East": "SS"
}
BoundDict10 = {
    "North": "C",
    "West": "C",
    "South": "C",
    "East": "C"
BoundDict11 = {
    "North": "SS",
    "West": "SS",
    "South": "C",
    "East": "C"
}
BoundDict12 = {
    "North": "SS",
```

```
"West": "C",
    "South": "SS",
    "East": "C"
}
BoundDict13 = {
    "North": "SS",
    "West": "SS",
    "South": "C",
    "East": "SS"
}
# New way to define boundary condition since part2a rev2
Bound_case2 = [BoundDict1, BoundDict2, BoundDict3, BoundDict4, BoundDict5, BoundDict6,
    BoundDict7, BoundDict8, BoundDict9, BoundDict10, BoundDict11, BoundDict12, BoundDict13]
# For compatibility with previous version
Direction = ["north", "west", "south", "east"]
case_number = 13
Bound_case = [
    ["F", "F", "F", "F"],
    ["0", "0", "0", "0"],
    ["F", "F", "S", "S"],
["S", "F", "S", "F"],
    ["F", "S", "F", "S"],
    ["S", "F", "F", "F"],
    ["F", "S", "F", "F"],
    ["X", "X", "X", "X"],
    ["S", "S", "S", "S"],
    ["C", "C", "C", "C"],
    ["S", "S", "C", "C"],
    ["S", "C", "S", "C"],
    ["S", "S", "C", "S"],
1
case2print = 1 # This test case will be plotted
# Modes to be displayed
m = 5
n = m # m by n modes are displayed
# Dimensions (in m otherwise mentionned)
# do not change the values (used in Elmer for comparison)
Lxmm = 400
Lymm = 600 # use locally mm to avoid rounding problems
h = 0.015 # plate thickness
# Material
# do not change the values (used in Elmer for comparison)
Ex = 10e6
Ey = 10e6 # Young modulus x and y direction in Pa
rho = 25.0 # density in kg/m<sup>3</sup>
nux = 0.3 # Poisson ration
nuy = nux
Dx = Ex * h**3 / 12 / (1 - nux**2) # bending stiffness
Dy = Ey * h**3 / 12 / (1 - nuy**2) # bending stiffness
mu = rho * h # areal density
meshmm = 10.1 #mm, dxmm and dymm will adjusted just less than mesh for Nj and Nk odd
```

```
\# dxmm = 10
# dymm = dxmm
# Some parameters
nj = int(Lxmm/meshmm/2) + 1
Nj = 2*nj+1
nk = int(Lymm/meshmm/2) + 1
Nk = 2*nk+1
# Nj = Lxmm // dxmm + 1 # number of points in the mesh, j index = x direction = horizontal sides
\# Nk = Lymm // dymm + 1 \# same in k index = y direction = vertical sides
# some conversion to meter
Lx = Lxmm / 1000
Ly = Lymm / 1000
\# dx = dxmm / 1000
\# dy = dymm / 1000
dx = Lx/(Nj-1)
dy = Ly/(Nk-1)
dxmm = int(100000 * dx)/100 # in mm and rounded. Do not use for calculation
dymm = int(100000 * dy)/100 # in mm and rounded. Do not use for calculation
# 2D matrix containing the index i of each points
plate2d = np.transpose(np.arange(Nk * Nj).reshape(Nj, Nk))
# Prepare the sub-areas
# AreasLim, AreasName, AreasMatrix are dictionaries
# key is the area short name (ie Sx, EW, IE...)
AreasLim, AreasName = fdmbm.AreasDict()
# AreasMatrix = fdmbm.AreasMat(AreasLim)
AreasSubMat = fdmbm.AreasMat(AreasLim, plate2d)
p2p.print_twice(logfile, "The plate is Lx =", Lx, "m by Ly =", Ly, "m")
p2p.print_twice(logfile, "The plate thickness is h =", h, "m")
p2p.print_twice(logfile, "The mesh is Nj =", Nj, "points by Nk =", Nk, "points")
p2p.print_twice(logfile, "with a grid dx =", dxmm, "mm by dy =", dymm, " mm")
p2p.print_twice(
    logfile, "Young modulus E =", int(Ex / 1e6), "MPa, Density rho =", rho, "kg/m3")
p2p.print_twice(
    logfile,
    "Bending stiffness Dx = Dy = ",
    int(Dx * 100) / 100, "Nm, Areal density \mu =", mu, "kg/m<sup>2</sup>")
p2p.print_twice(logfile, "with Poisson's ratio nux =", nux, "and nuy =", nuy)
10.5 System matrix filling process
tic = time.perf_counter() # optional, start of a timer for time performance check
# Fill the cell type matrix (inner, boundary...)
plate2d = np.zeros([Nk, Nj])
plate2d = fdmp.fillcelltype(plate2d)
Imat = np.transpose(np.arange(Nk * Nj).reshape(Nj, Nk))
# Create the system matrix
SysMat = np.zeros([Nk * Nj, Nk * Nj], dtype=float) # System Matrix
Sysmatcase = np.zeros([Nk * Nj, Nk * Nj], dtype=float) # System Matrix
# Let's fill the system submatrices
Ax, Ay, Axy = fdmbm.fill_main_matrices(Nj, Nk, nux, nuy, AreasSubMat)
# Magic : here is the System Matrix
SysMat = (Ax / dx**4 + Ay / dy**4 + 2*Axy / dx**2 / dy**2) # FFFF version
```

```
''' # For debug, to see the system matrix
N = 50 # number of elements to print
fdmp.report_mat(logfile, SysMat, plate2d, "SysMat raw", N)
SysMat = (Dx * SysMat) / mu
# -----
toc = time.perf_counter() # to evaluate time performance of the algorithm
p2p.print_twice(logfile, f"Excecution time (system matrix preparation) = {toc - tic:0.4f} seconds for "
p2p.print_twice(logfile, "-----")
p2p.print_twice(logfile, "")
10.6 Solver
for Case in range(case_number):
       BoundDict = Bound_case2[Case]
       Bound_cond = Bound_case[Case] # For compatibility with previous version (before adding free edge)
       # Fixed points -----
       # Apply Boundary Conditions
       if Bound_cond == ["X", "X", "X", "X"]:
              FixedPoints = np.array([0, Nk-1, Nk*(Nj-1), Nk*Nj -1])
       elif Bound_cond == ["0", "0", "0", "0"]:
              # FixedPoints = np.array([0, (Nk+1)/2, Nk*(Nj+1)/2, Nk*Nj -1 - (Nk+1)/2])
              FixedPoints = np.array([int((Nk-1)/2), int(Nk*(Nj-1)/2), int((Nj+1)/2*Nk-1), int(Nj*Nk-(Nk+1)/2*Nk-1), int(Nj*Nk-(Nk+1)/2*Nk-1), int(Nj*Nk-(Nk+1)/2*Nk-1), int(Nj*Nk-(Nk+1)/2*Nk-1), int(Nj*Nk-(Nk+1)/2*Nk-1), int(Nk*(Nj-1)/2*Nk-1), int(Nk*(Nj-1)/2*Nk-1)
       else:
              FixedPoints = fdmbm.Fixedpoints(BoundDict, AreasSubMat)
       # Apply fixed points
       Sysmatcase = fdmbm.applyfixedpoints(SysMat, FixedPoints)
       # Specific to FFFF, null mean displacement added
       # -----
       BC = fdmbm.boundcoeff(Bound_cond)
       BCname = ".join(Bound\_cond) # used to adress the test case in elmer() function
       plotboundcond = ["", "", "", ""]
       for i in range(4):
              plotboundcond[i] = Bound_cond[i] + " [" + Direction[i] + "]"
       p2p.print_twice(logfile, "Case #", Case)
       p2p.print_twice(logfile, "Boundary conditions", plotboundcond)
       # p2p.print_twice(logfile, "Boundary coeff. North=", BC[0], " West=", BC[1], " South=", BC[2], " Ea
       # Here is the solver (eigenfreq)
       tic = time.perf_counter() # optional, start of a timer for time performance check
       # Compute the eigenfrequencies and the mode shapes
       vals, vecs = linalg.eig(Sysmatcase) # vals is 1D NjNy points (complex values, 1+1j for the fixed po
       # Clean the results by removing 1 values and complex from the eigenvalues
       vals = vals[vals != 1.0 + 0j] # remove the value 1.+0j
       # print("vals (no 1):", vals.shape)
       vals = np.real(vals)
       modefreq = np.zeros([len(vals), 2]) # prepare an array for the eigenfrequencies
       modefreq[:, 1] = np.abs(vals)**0.5 / 2 / np.pi # extract the frequencies
       modefreq[:, 0] = np.arange(0, len(vals), 1) # give an index
       modefreq = modefreq[modefreq[:, 1].argsort()] # sort
       # for ii in range (50):
              print(modefreq[ii, 0], modefreq[ii, 1])
```

```
modefreq = modefreq.astype(int)  # keep interger format to reduce the number of digit
# now modefreq is filled : modefreq[i,0] = mode index, modefreq[i,1] = mode frequency
toc = time.perf_counter()  # to evaluate time performance of the algorithm
p2p.print_twice(logfile, f"Excecution time (solver) = {toc - tic:0.4f} seconds for ", Nj * Nk, " po
# Show the plate
if Case == 0:
    fdmp.plot_plate2(Nj, Nk, FixedPoints, py2pdfdir + "/plate.png")  # show the mesh
```

## 10.7 Script output printing

```
results = np.zeros([m * n, 8]) # prepare array result
# results table columns
                           3 | 4 |
# | 0 | 1 | 2
                      /
                                              5
\#\ /\ mx\ /\ ny\ /elmer\ freq/mode\ freq/\ error\ /theoric\ freq\ /\ error\ /mode\ shape\ index\ /
results[:, 3] = modefreq[: m * n, 1] # eigenfrequency in col 3
results[:, 7] = modefreq[: m * n, 0] # mode shape number in col 7
for i in range(m * n):
    \# results[i,6] = np.mean(vecs[:, int(results[i,7])]) \# mode shape mean value
    results[i, 2] = fdmelm.elmer(BCname, i, m * n - 1) # elmer result in col 2
drivingpoint = np.zeros([Nk, Nj])
if Case == case2print:
    # if Case >= 0: # plot all the cases
    fig = plt.figure(figsize=(10, 8)) # create the figure
for i in range(m * n):
    modeshape = np.real(np.transpose(vecs[:, int(results[i, 7])].reshape((Nj, Nk))))
    # modeshape is the 2D matrix showing the plate deviation in the plate coordinates
    ind = np.unravel index(
       np.argmax(np.absolute(modeshape), axis=None), modeshape.shape
    # ind returns the coordinates of the maximum sees in modeshape
    diry = modeshape[:, ind[1]]
    # diry is the 1D slice of modeshape in y direction at the maximum
    dirx = modeshape[ind[0], :]
    # dirx is the 1D slice of modeshape in x direction at the maximum
    # the mode numbers are obtains by checking how lany times dirx, diry signs change
    mx = fdmelm.signchange(dirx)
    ny = fdmelm.signchange(diry)
    fdmresult = results[i, 3]
    results[i, 0] = mx
    results[i, 1] = ny
    \# results[i, 5] = fdmelm.modes(Bound_cond, Lx, Ly, Dx, mu, mx, ny) \# formula result in 5
    \# results[i, 5] = fdmelm.warburton(Bound_cond, Lx, Ly, Dx, nux, mu, mx, ny)
    if results[i, 7] != 0: # test of driving point similar to Zenker's paper
       mode = np.absolute(modeshape)
        drivingpoint = drivingpoint + (mode / np.max(mode)) ** 0.3
        if i > 0:
            drivingpoint = drivingpoint / np.max(drivingpoint)
    111
    # if Case == case2print:
    if Case >= 0: # plot all the cases
       plt.subplot(m, n, i + 1)
        # if Case == 8: # FFFF in dirty mode
            # mode2print = np.absolute(modeshape)
```

```
# plt.imshow(np.absolute(mode2print - np.amax(mode2print)), cmap = 'rainbow')
            # else:
        plt.imshow(np.absolute(modeshape), cmap = 'rainbow')
        # plt.plot(ind[1], ind[0], "r*")
        # plt.title(str(int(results[i,0]))+","+str(int(results[i,1])))
        # plt.title(str(mx) + "," + str(ny))
        plt.title(str(fdmresult)+"Hz")
        plt.axis("equal")
        plt.axis("off")
mode_estimation = np.zeros([m * n, 1])
for i in range(m * n):
    mx = i//m + 1
    ny = i\%m + 1
    mode_estimation[i] = fdmelm.warburton(Bound_cond, Lx, Ly, Dx, nux, mu, mx, ny)
results[:, 5] = np.sort(mode_estimation, axis=None)
\# results[:,6] = 100*results[:,6]/np.max(abs(results[:,6]))
# results[:,6] = results[:,6].astype(int)
for i in range(m * n):
    if results[i, 2] != 0:
        error = 1000 * (results[i, 3].astype(int) / results[i, 2].astype(int) - 1)
        results[i, 4] = error.astype(int) / 10
    else:
        results[i, 4] = 0
mean_error = int(100 * np.average(results[:, 4])) / 100
max_error = int(100 * np.amax(results[:,4])) / 100
results[:, 4] = results[:, 4].astype(int)
for i in range(m * n):
    if results[i, 2] != 0:
        error = 1000 * (results[i, 5].astype(int) / results[i, 2].astype(int) - 1)
        results[i, 6] = error.astype(int) / 10
    else:
        results[i, 6] = 0
results[:, 6] = results[:, 6].astype(int)
# save the eigenfrequencies for comparison with Elmer (above the 25 first one)
for i in range(1000):
   p2p.print_twice(logfile2, modefreq[i, 1])
# print(results)
spacing = 10
legend = ["m", "n", "FEM", "FDM", "err%", "Warb.", "err%"]
ac = ""
for j in range(2, 7): # m, n no more printed out (no meaning with free edge)
    ab = legend[j]
   ab = (spacing - len(ab) - 1) * " " + ab + " "
    ac = ac + ab
p2p.print_twice(logfile, ac)
for i in range(m * n):
    ac = ""
    for j in range (2, 7):
        ab = str(int(results[i, j]))
        ab = (spacing - len(ab) - 1) * " " + ab + " "
        ac = ac + ab
    p2p.print_twice(logfile, ac)
p2p.print_twice(logfile, "Mean error", mean_error, "%")
p2p.print_twice(logfile, "Max error", max_error, "%")
```

#### 10.8 py2pdf

```
print("start py2pdf")
# WARNING : no output after this line can be recorded automatically (reason is the markdown is created
# export the markdown from the python file
msg, date_ext = p2p.py2md(script_name, "# ~~")
# prepare the command to launch the pdf report creation
markdownfile = "../docs/fdm_applied_to_dml_part2b2.md"
pdffile = "../docs/FDM_applied_to_DML_part2b2.pdf"
pdfbackup = "../p2pbackup/FDM_applied_to_DML_part2b2" + date_ext + ".pdf.bak"
cmd = ('pandoc --pdf-engine=xelatex --variable mainfont="Arial" '+ markdownfile + ' -s --citeproc --num
# Run the command and capture the return code
return_code = os.system(cmd)
# Check the return code to determine success or failure
if return code == 0:
    print("Pandoc command executed successfully. Hurrah the pdf was created!")
    shutil.copy(pdffile, pdfbackup)
    print("Error: Pandoc command failed with exit code.", return_code)
```

## 11 References

- [1] R. Maso, "Application of boundary edge effect corrections to the vibration of beams and rectangular plates." PhD thesis, Carleton University, 1993. Available: https://curve.carleton.ca/system/files/etd/10817845-5151-47ac-9066-6fc2e360a6f2/etd\_pdf/832572c0d80b3466b8f401a713c81266/maso-applicationofboundaryedgeeffectcorrections.pdf
- [2] G. Warburton, "The vibration of rectangular plates," *Proceedings of the Institution of Mechanical Engineers*, vol. 168, no. 1, pp. 371–384, 1954.
- [3] A. W. Leissa, *Vibration of plates*, vol. 160. Scientific and Technical Information Division, National Aeronautics and ..., 1969. Available: https://ntrs.nasa.gov/api/citations/19700009156/downloads/19700009156.pdf