

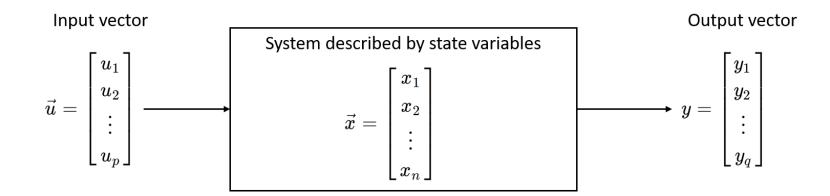
State Space Representation

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State of a Dynamic System

• A minimum set of variables, known as state variables, that fully describe the system and its response to any given set of inputs.



- The number of state variables, n, is equal to the number of independent "energy storage elements" in the system.
- The state equations

$$\dot{x_1} = f_1(x,u,t) \ \dot{x_2} = f_2(x,u,t) \ dots \ \dot{x_n} = f_n(x,u,t)$$

State Representation of LTI System

• We restrict attention primarily to linear and time-invariant (LTI) system. Then it becomes a set of n coupled first-order linear differential equations with constant coefficients.

$$\dot{x_1} = a_{11}x_1 + \dots + a_{1n}x_n + b_{11}u_1 + \dots + b_{1p}u_p$$
 $\dot{x_2} = a_{21}x_1 + \dots + a_{2n}x_n + b_{21}u_1 + \dots + b_{2p}u_p$
 \vdots
 $\dot{x_n} = a_{n1}x_1 + \dots + a_{nn}x_n + b_{n1}u_1 + \dots + b_{np}u_p$

Written compactly in a matrix form

$$egin{aligned} rac{d}{dt} egin{bmatrix} x_1 \ x_2 \ dots \ x_n \end{bmatrix} = egin{bmatrix} a_{11} & a_{12} & \cdots & a_{1n} \ & dots & dots \ & dots & dots \ &$$

$$\dot{x} = Ax + Bu$$

Output of LTI System

Output equations

$$y_1 = c_{11}x_1 + \dots + c_{1n}x_n + d_{11}u_1 + \dots + d_{1p}u_p$$
 $y_2 = c_{21}x_1 + \dots + c_{2n}x_n + d_{21}u_1 + \dots + d_{2p}u_p$
 \vdots
 $y_q = c_{q1}x_1 + \dots + c_{qn}x_n + d_{q1}u_1 + \dots + d_{qp}u_p$

$$egin{bmatrix} y_1 \ y_2 \ dots \ y_q \end{bmatrix} = egin{bmatrix} c_{11} & c_{12} & \cdots & c_{1n} \ & dots \ & do$$

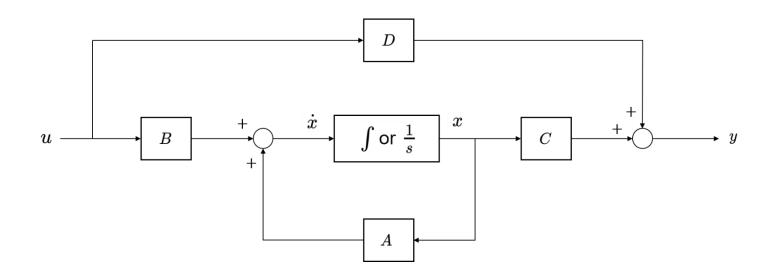
$$y = Cx + Du$$
 or $y = Cx$ for many physical systems the matrix D is the null matrix

Block Diagram of LTI System

• The complete system model for LTI system in the standard state space form

$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$

• Block diagram



Homogeneous State Response



Homogeneous State Response

• With zero input, u(t) = 0

$$\dot{x} = Ax$$

$$y(t) = e^{At}x(0)$$

- Let's figure out how such a system behaves
 - Start by ignoring the input term:

$$\dot{x} = Ax$$
$$x(t_0) = x_0$$

- What is the solution to this system?
 - If everything is scalar:

$$\dot{x} = ax$$
, $x(t_0) = x_0 \implies x(t) = e^{at}x_0$

– How do we know?

$$x(0) = e^0 x_0 = x_0$$
$$\frac{dx(t)}{dt} = ae^{at} x_0 = ax(t)$$

Homogeneous State Response

For higher-order systems, we just get a matrix version of this

$$\dot{x} = Ax, \quad x(0) = x_0 \implies x(t) = e^{At}x_0$$

The definition is just like for scalar exponentials

$$e^{at} = \sum_{k=0}^{\infty} \frac{(at)^k}{k!}, \qquad e^{At} = \sum_{k=0}^{\infty} \frac{(At)^k}{k!}$$

Derivative:

$$\frac{d}{dt}e^{At} = \frac{d}{dt}\sum_{k=0}^{\infty} \frac{(At)^k}{k!} = 0 + \sum_{k=1}^{\infty} \frac{kA^kt^{k-1}}{k!} = A\sum_{k=1}^{\infty} \frac{(At)^{k-1}}{(k-1)!} = A\sum_{k=0}^{\infty} \frac{(At)^k}{k!} = Ae^{At}$$

• The matrix exponential plays such an important role that it has its own name: the state transition matrix, $\Phi(t)$

$$\dot{x} = Ax \implies egin{aligned} x(t) &= \Phi(t)x(0) \ &= Ax &\Longrightarrow \ &= e^{At} &= \Phi(t) \end{aligned}$$

Properties of State Transition Matrix

• Properties of state transition matrix

$$egin{aligned} \Phi(0) &= I \ \Phi(-t) &= \Phi^{-1}(t) \ \Phi(t_1 + t_2) &= \Phi(t_1) \Phi(t_2) \end{aligned}$$

$$x(0) = \Phi(-t_0)x(t_0)$$

$$x(t) = \Phi(t)x(0) = \Phi(t)\Phi(-t_0)x(t_0)$$

$$= \Phi(t - t_0)x(t_0)$$

Example: State Transition Matrix

Example

$$\dot{x} = egin{bmatrix} -2 & 0 \ 1 & -1 \end{bmatrix} x, \qquad x(0) = egin{bmatrix} 2 \ 3 \end{bmatrix}$$

$$\Phi(t) = e^{At} = Se^{\Lambda t}S^{-1}$$

$$\lambda_1 = -2 \quad \Longrightarrow \quad egin{bmatrix} 0 & 0 \ 1 & 1 \end{bmatrix} egin{bmatrix} x_1 \ x_2 \end{bmatrix} egin{bmatrix} 0 \ 0 \end{bmatrix} \qquad \Longrightarrow \quad ec{x}_1 = egin{bmatrix} 1 \ -1 \end{bmatrix}$$

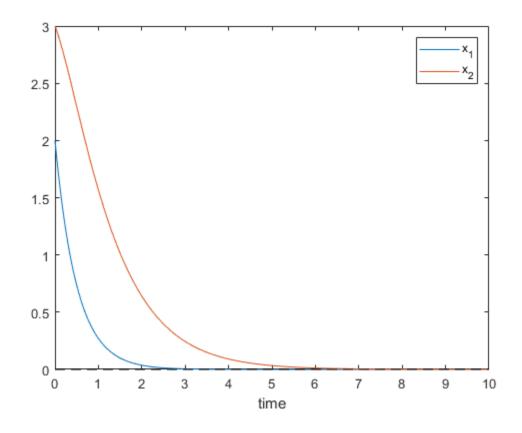
$$\lambda_2 = -1 \quad \Longrightarrow \quad egin{bmatrix} -1 & 0 \ 1 & 0 \end{bmatrix} egin{bmatrix} x_1 \ x_2 \end{bmatrix} egin{bmatrix} 0 \ 0 \end{bmatrix} \qquad \Longrightarrow \quad ec{x}_1 = egin{bmatrix} 0 \ 1 \end{bmatrix}$$

$$e^{\Lambda t} = egin{bmatrix} e^{-2t} & 0 \ 0 & e^{-t} \end{bmatrix}, \qquad S = egin{bmatrix} 1 & 0 \ -1 & 1 \end{bmatrix}, \qquad S^{-1} = egin{bmatrix} 1 & 0 \ 1 & 1 \end{bmatrix}$$

$$x(t)=Se^{\Lambda t}S^{-1}x(0)=\left[egin{array}{cc} 1&0\-1&1 \end{array}
ight]\left[egin{array}{cc} e^{-2t}&0\0&e^{-t} \end{array}
ight]\left[egin{array}{cc} 1&0\1&1 \end{array}
ight]\left[egin{array}{cc} 2\3 \end{array}
ight]=\left[egin{array}{cc} 2e^{-2t}\5e^{-t}-2e^{-2t} \end{array}
ight]$$

Example: State Transition Matrix

```
A = [-2, 0; 1, -1];
B = [0, 0]';
C = [1, 0;
     0, 1];
D = 0;
G = ss(A,B,C,D);
x0 = [2; 3];
t = linspace(0,10,500);
u = zeros(size(t));
[y, tout] = lsim(G,u,t,x0);
plot(tout,y,tout,zeros(size(tout)),'k--')
xlabel('time')
legend('x_1', 'x_2')
```





Forced State Response of LTI System



Forced State Response of LTI System

But what if we have the controlled system:

$$\dot{x} = Ax + Bu$$

• Consider the complete response of a linear system to an input u(t)

$$\dot{x}(t) - ax(t) = bu(t)$$

Derivation

$$e^{-at}\dot{x} - e^{-at}ax = \frac{d}{dt}(e^{-at}x(t)) = e^{-at}bu$$

$$\int_0^t \frac{d}{d\tau}(e^{-a\tau}x(\tau))d\tau = e^{-at}x(t) - x(0) = \int_0^t e^{-a\tau}bu(\tau)d\tau$$

Complete solution

$$x(t)=e^{at}x(0)+\int_0^t e^{a(t- au)}bu(au)d au$$



For Higher Order Systems

$$\dot{x} = Ax + Bu$$

Complete solution

$$x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)}Bu(\tau)d\tau$$

• The output

$$y = Cx + Du$$
 $y(t) = Ce^{At}x(0) + C\int_0^t e^{A(t- au)}Bu(au)d au + Du(t)$

- The first is a term similar to the system homogeneous response $x_h(t) = e^{At}x(0)$ that is dependent only on the system initial conditions x(0)
- The second term is in the form of a convolution integral, and it is the particular solution for the input u(t) with zero initial conditions

For Higher Order Systems

Note

$$x(t) = \Phi(t)x(0) + \int_0^t \Phi(t- au)Bu(au)d au$$

$$x(0) = \Phi(0)x(0) + \int_0^0 \Phi(0- au) Bu(au) d au = x(0)$$

$$\frac{d}{dt} \int_{t_0}^t f(t,\tau) d\tau = f(t,t) + \int_{t_0}^t \frac{\partial f(t,\tau)}{\partial t} d\tau \qquad \qquad \text{(Leibniz Integral Rule)}$$

$$\implies \Phi(0) Bu(t) + \int_{t_0}^t A\Phi(t-\tau) Bu(\tau) d\tau$$

$$egin{aligned} rac{d}{dt}x(t) &= A\left(\Phi(t)x(0) + \int_{t_0}^t \Phi(t- au)Bu(au)d au
ight) + Bu(t) \ rac{d}{dt}x(t) &= Ax + Bu \end{aligned}$$

Note: Leibniz Integral Rule

If
$$\mathbf{F}(t) = \int_{a(t)}^{b(t)} f(t,\tau) d au$$
, then $\frac{d\mathbf{F}}{dt} = \int_{a(t)}^{b(t)} \frac{\partial f(t,\tau)}{\partial t} d au + f(t,b(t)) \frac{db}{dt} - f(t,a(t)) \frac{da}{dt}$

Suppose f is a univariate function

$$F(t) = \int_{t_0}^t f(au) d au \quad \Longrightarrow \quad rac{dF(t)}{dt} = f(t)$$

$$F(t) = \int_t^{t_0} f(au) d au \implies rac{dF(t)}{dt} = -f(t)$$

Now suppose f is a function of two variables (a and b are constant)

$$F(t) = \int_a^b f(t,\tau)d\tau \implies \frac{dF(t)}{dt} = \int_a^b \frac{\partial f(t,\tau)}{\partial t}d\tau$$

Now suppose the limits of integration a and b themselves depend on t,

$$\mathbf{F}(t) = F(t,a(t),b(t)) = \int_{a(t)}^{b(t)} f(t, au) d au$$

$$rac{d\mathbf{F}(t)}{dt} = rac{\partial F}{\partial t} + rac{\partial F}{\partial a}rac{da}{dt} + rac{\partial F}{\partial b}rac{db}{dt}$$

$$egin{aligned} rac{d\mathbf{F}(t)}{dt} &= rac{\partial F}{\partial t} + rac{\partial F}{\partial a}rac{da}{dt} + rac{\partial F}{\partial b}rac{db}{dt} \ &= \int_{a(t)}^{b(t)} rac{\partial f(t, au)}{\partial t}d au + f(t,b(t))rac{db}{dt} - f(t,a(t))rac{da}{dt} \ &rac{d}{dt}\int_{t_0}^t f(t, au)d au &= \int_{t_0}^t rac{\partial f(t, au)}{\partial t}d au + f(t,t) \end{aligned}$$

Example

$$egin{bmatrix} \dot{x}_1 \ \dot{x}_2 \end{bmatrix} = egin{bmatrix} -2 & 0 \ 1 & -1 \end{bmatrix} egin{bmatrix} x_1 \ x_2 \end{bmatrix} + egin{bmatrix} 1 \ 0 \end{bmatrix} u,$$

$$\left| egin{array}{c} \dot{x}_1 \\ \dot{x}_2 \end{array} \right| = \left| egin{array}{ccc} -2 & 0 \\ 1 & -1 \end{array} \right| \left| egin{array}{c} x_1 \\ x_2 \end{array} \right| + \left| egin{array}{c} 1 \\ 0 \end{array} \right| u, \qquad u = 2u(t) \ \ ext{where} \ u(t) \ ext{is a step function}, \quad x(0) = \left| egin{array}{c} 0 \\ 0 \end{array} \right|$$

$$\Phi(t) = \begin{bmatrix} e^{-2t} & 0\\ e^{-t} - e^{-2t} & e^{-t} \end{bmatrix} = e^{At}$$

$$\Phi(t) = \begin{bmatrix} e^{-2t} & 0 \\ e^{-t} - e^{-2t} & e^{-t} \end{bmatrix} = e^{At} \qquad x(t) = \int_0^t e^{A(t-\tau)} Bu(\tau) d\tau = e^{At} \int_0^t e^{-A\tau} Bu(\tau) d\tau = \Phi(t) \int_0^t \Phi(-\tau) B1 d\tau$$

$$= \begin{bmatrix} e^{-2t} & 0 \\ e^{-t} - e^{-2t} & e^{-t} \end{bmatrix} \int_0^t \begin{bmatrix} e^{2\tau} & 0 \\ e^{\tau} - e^{2\tau} & e^{\tau} \end{bmatrix} \begin{bmatrix} 2 \\ 0 \end{bmatrix} d\tau$$

$$= \begin{bmatrix} e^{-2t} & 0 \\ e^{-t} - e^{-2t} & e^{-t} \end{bmatrix} \int_0^t \begin{bmatrix} 2e^{2\tau} \\ 2e^{\tau} - 2e^{2\tau} \end{bmatrix} d\tau$$

$$= \begin{bmatrix} e^{-2t} & 0 \\ e^{-t} - e^{-2t} & e^{-t} \end{bmatrix} \begin{bmatrix} e^{2\tau}|_0^t \\ (2e^{\tau} - e^{2\tau})|_0^t \end{bmatrix}$$

$$= \begin{bmatrix} e^{-2t} & 0 \\ e^{-t} - e^{-2t} & e^{-t} \end{bmatrix} \begin{bmatrix} e^{2t} - 1 \\ 2e^{t} - e^{2t} - 1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 - e^{-2t} \\ (e^{-t} - e^{-2t})(e^{2t} - 1) + e^{-t}(2e^{t} - e^{2t} - 1) \end{bmatrix}$$

$$= \begin{bmatrix} 1 - e^{-2t} \\ 1 + e^{-2t} \end{bmatrix}$$

The Response of LTI to the Singularity Input Functions

$$x(t)=e^{At}x(0)+\int_0^t e^{A(t- au)}Bu(au)d au$$

Impulse response

$$u(t) = K\delta(t) = egin{bmatrix} k_1 \ k_2 \ dots \ k_p \end{bmatrix} \delta(t)$$

$$x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)}BK\delta(\tau)d\tau$$

= $e^{At}x(0) + e^{At}BK$
= $e^{At}(x(0) + BK)$

• The effect of impulse inputs on the state response is similar to changing a set of initial conditions $x(0) \rightarrow x(0) + BK$

The Response of LTI to the Singularity Input Functions

Step response

$$u(t) = Ku_{ ext{step}} = egin{bmatrix} k_1 \ k_2 \ dots \ k_p \end{bmatrix} u_{ ext{step}}(t)$$

$$x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)}Bu(\tau)d\tau$$

$$= e^{At}x(0) + \int_0^t e^{A(t-\tau)}BKd\tau$$

$$= e^{At}x(0) + e^{At}\int_0^t e^{-A\tau}d\tau BK$$

$$= e^{At}x(0) + e^{At}[-A^{-1}e^{-A\tau}]_0^tBK$$

$$= e^{At}x(0) + e^{At}[-A^{-1}e^{-A\tau}]_0^tBK$$

$$= e^{At}x(0) + e^{At}[-A^{-1}e^{-At} + A^{-1}]BK$$

$$= e^{At}x(0) + e^{At}A^{-1}[I - e^{-At}]BK$$

$$= e^{At}x(0) + A^{-1}[e^{At} - I]BK \qquad (Ae^{At} = e^{At}A)$$

$$x(\infty) = -A^{-1}BK$$
 if the system is stable

The Response of LTI to the Singularity Input Functions

• Step response

$$\ddot{y} + \frac{c}{m}\dot{y} + \frac{k}{m}y = g\,u_{\mathrm{step}}(t)$$

$$egin{bmatrix} \dot{x_1} \ \dot{x_2} \end{bmatrix} = egin{bmatrix} 0 & 1 \ -rac{k}{m} & -rac{c}{m} \end{bmatrix} egin{bmatrix} x_1 \ x_2 \end{bmatrix} + egin{bmatrix} 0 \ g \end{bmatrix} \cdot 1 \cdot u_{ ext{step}}(t)$$

$$y = \left[egin{array}{cc} 1 & 0 \end{array}
ight] \left[egin{array}{c} x_1 \ x_2 \end{array}
ight]$$

$$x(\infty) = -A^{-1}BK = -egin{bmatrix} 0 & 1 \ -rac{k}{m} & -rac{c}{m} \end{bmatrix}^{-1}egin{bmatrix} 0 \ g \end{bmatrix} \cdot 1 \cdot = egin{bmatrix} rac{mg}{k} \ 0 \end{bmatrix}$$

