

Loudspeaker Measurement (Lab 3)

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Summary

This report regards to the third laboratory exercise of Audio Technology at NTNU. In this laboratory a loudspeaker was measured in an anechoic room. The measurement was done in three different ways.

In the first task a microphone was placed in front of a loudspeaker at a distance of 1.2m. The influence of the length of the impulse time window was analyzed. It can be obtained that the frequency response get more and more smoothened when decreasing the time window size, but especially at low frequencies the results may be wrong. With full time window the frequency response is shown in a way which is expected for loudspeakers.

In the second measurement the loudspeaker was turned with a turntable in 15° -steps. The influence of directivity at different angles should be measured. It could be obtained, that the loudspeaker becomes more and more directional with increasing frequency, while at low frequencies the loudspeaker is more or less omnidirectional.

At the last measurement the influence of a reflecting surface was measured. Constructive and destructive interferences can be obtained at some frequencies.

1 Introduction

Most music reproduction is done using loudspeakers. For optimal listening experience a constant quality of these reproduction devices is mandatory to ensure high listening quality. Therefore measurement of loudspeaker parameters is important to ensure high listening experience.

Some parameters for defining the quality of a loudspeaker are the directivity (given as directivity index DI or directivity factor DF) and the frequency response of the loudspeaker. Using the directivity, an optimal placement of the speakers to the listener can be found. The frequency response tells how the different frequencies are amplified or dampened from the speaker.

In this laboratory exercise the measurement of the frequency response and the directivity of a loudspeaker should be measured. This is done in three different exercises, which each of them covers a specific part of the parameter. In the first exercise the general influence of measurement parameters should be obtained. Therefore a sine sweep was recorded and the influence of the FFT window length should be obtained. In a second measurement the directivity of the loudspeaker was measured with recording sine sweeps in different off-axis angles. In the last measurement the influence of reflections on the measurement were obtained with placing a reflective surface between loudspeaker and measurement microphone.

2 Theory

2.1 Sensitivity, Efficiency

In loudspeakers most energy is not transformed into sound power but into heat. The efficiency is defined as the relation of transmitted sound power and the total electrical power input. It can be written as

$$\eta = \frac{W_{sound,out}}{W_{el,in}} \quad (1)$$

Typical values for loudspeaker efficiency are 1-2% while horn loudspeakers or high efficient loudspeakers can get up to 10%.

Instead of the efficiency often the loudspeakers sensitivity is listened by manufacturers. The sensitivity is defined as sound pressure level at 1W electrical input at a measurement distance of 1m. A typical voltage level for this measurement is $V_{RMS} = 2.83V$. This defines the input power of 1W at a speaker impedance of 8Ω , which is a quite common loudspeaker impedance level.

For calculations of sound pressure following formula can be applied:

$$p_{RMS}^2 = W_{lsp} \cdot \rho_0 \cdot c \cdot \frac{DF}{4\pi \cdot r^2} \quad (2)$$

where

- p_{RMS}^2 : sound pressure in listening position
- W_{lsp} : radiated sound power
- ρ_0 : density of medium, ($\rho_{0,air} = 1.2 \frac{kg}{m^3}$)
- c : speed of sound propagation ($c = 343.6 \frac{m}{s}$ at 20°)

2.2 Maximum output level

For an optimal listening experience or public sound reproduction places the maximum reachable output level often should be known. This maximum output level can be calculated using following formula:

$$L_{P,max} = L_W + 10 \cdot \log\left(\frac{DF}{4\pi \cdot r^2} + \frac{4}{A}\right) \quad (3)$$

where

- $L_{P,max}$: maximum sound power level
- L_W : sound power level
- A : room asorption (calculation using Sabine's formula)
- DF : directivity factor
- r : distance from sound source

2.3 Measurement distance

Measurements should be done in the far field, so it must be ensured that the distance of the measurement microphone is within this distance. This is often critical around the crossover frequency, where low-frequency and mid/high-frequency elements are radiating equally strong. The critical distance can be calculated using the Rayleigh-distance, using following formula:

$$R_R = \frac{\pi \cdot a^2}{\lambda} \quad (4)$$

where

- a : diameter of the radiating loudspeaker membrane
- λ : radiated wavelength

2.4 Impulse response

To determine the quality of a loudspeaker the impulse response and so the amplification of different frequencies has to be measured. Often this is done in an anechoic chamber, but can also be done in ordinary rooms. Then the measured impulse response has to be cut before the first wall reflections occur. Therefore the time distance between direct sound and first reflections has to be long enough. The lowest frequency which can be measured accurately is defined by

$$\frac{1}{\Delta t} \quad (5)$$

with

- $\Delta t = t_{first\ reflection} - t_{direct}$

3 Measurements

3.1 Equipment

For this laboratory exercise following equipment was used:

- 1 measurement microphone: Norsonic 1201/30517
- 1 loudspeaker: Genelec 1029A
- 1 laser distance meter: Bosch PLR30
- 1 loudspeaker turntable
- Software:
 - WinLMS 2004
 - Matlab 2012b

3.2 Influence of the time window size

The time window size defines how many fourier coefficients for the calculation of the frequency response are covered. The longer the used time window is the higher is the accuracy of the resulting frequency response. To obtain this one measurement with a microphone in front of a loudspeaker was done. A frequency sweep was recorded and the response was calculated using WinLMS. After this four different frequency responses with different time windows were created. The used time windows were

- full time window
- 3ms after the initial response
- 10ms
- 50ms.

The time windows can be found in Appendix B.1. The measured frequency responses can be seen in figure 1. It can be obtained that the smaller the time window size the more smooth the resulting frequency is. This is quite accurate for high frequencies where more coefficients for calculating the frequency response exist. Especially at very low frequencies it can be seen, that the result differs quite much depending on the length of the time window. For a length of 3ms or 10ms the results can not be used, because it can be seen that they are wrong. The frequency response for 50ms is quite useful and near to the result with full time window.

3.3 Influence of incidence angle

In an anechoic chamber (almost) no reflections should occur. So this fits perfectly for measuring the directivity of a loudspeaker. For this measurement a loudspeaker was put on a turntable, a measurement microphone in front. The speaker was turned in 15° steps, in every step a frequency sweep was measured and the frequency response calculated using WinLMS. A time window of 50ms was chosen. The different measurements were then compared together.

A comparison of different frequency responses for different incident angles can be found in figure 2. All measurements in 15° steps are listed in Appendix B.2. Here it can be seen that at low frequencies the sound propagates almost omnidirectional in each direction. When the frequency increases, the loudspeaker gets more and more directional. That can be seen at decreasing amplitudes and more reflections in the frequency response. The more the loudspeaker gets off-axis and the higher the frequency, the more the sound amplitude decreases.

3.4 Influence of reflecting surfaces

In this measurement the frequency response of the loudspeaker on axis should be compared to a new measurement with reflective surfaces. For this reason a wooden plate was placed on the floor between the loudspeaker and the measurement microphone. The measurement was done with a frequency sweep. Comparing the frequency response with reflections and the one without (listed in Figure 3) huge differences can be seen. This is because of strong constructive and destructive interferences between the direct sound signal from the speaker to the microphone and those frequency components which are reflected from the reflective surface. It also can be obtained, that the influence is stronger at low frequencies, where the difference between constructive and destructive interference is almost 15dB, while at higher frequencies more interferences occur, but with less intensity. At very high frequencies the difference is about 1dB.

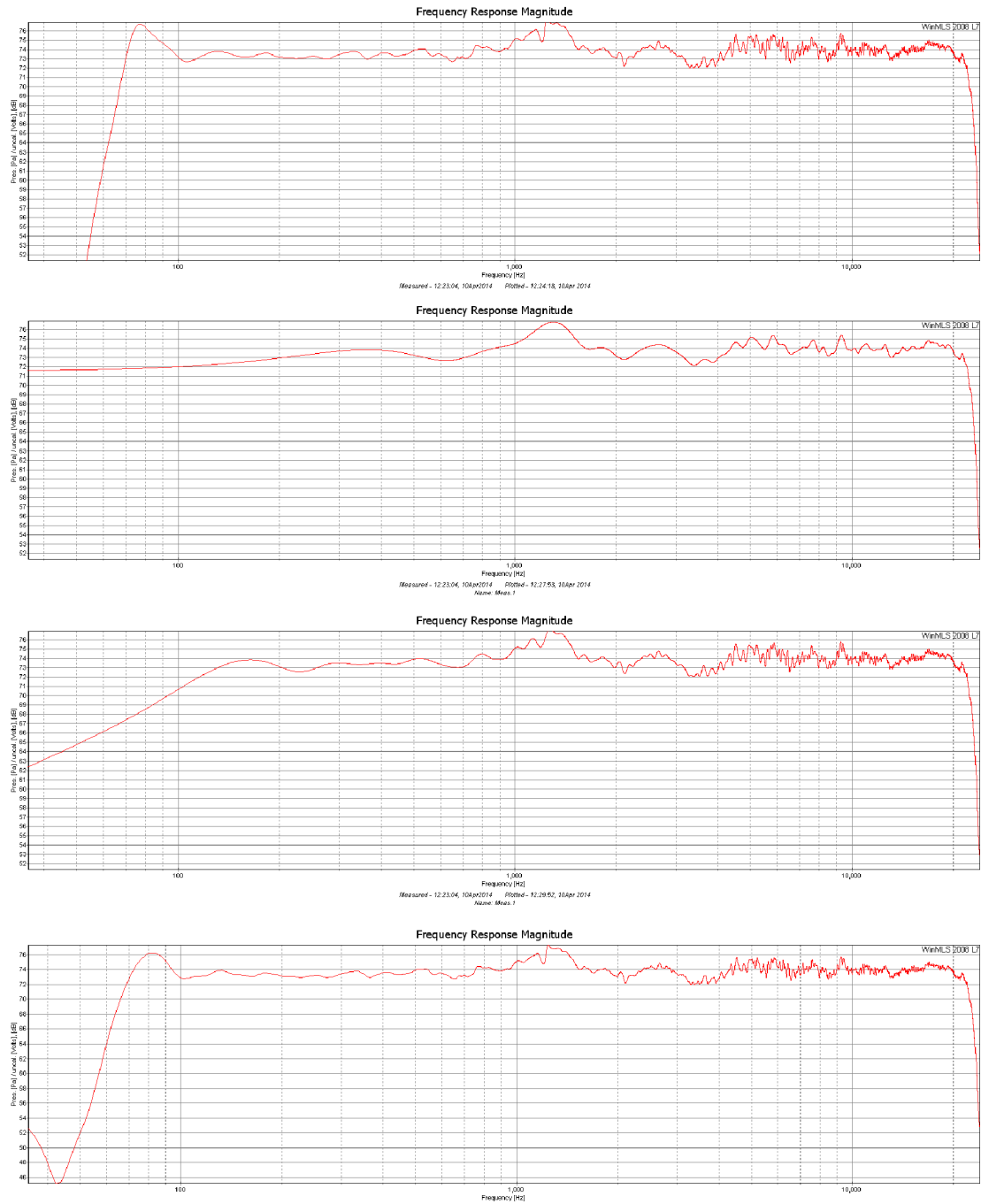
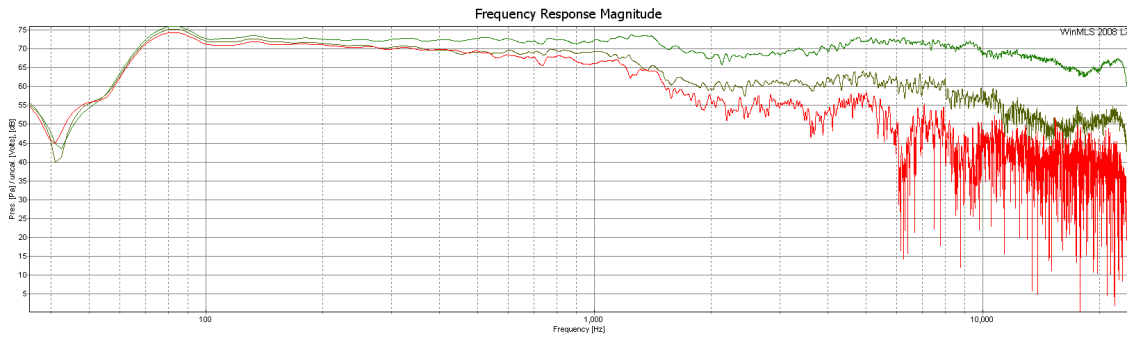


Figure 1: Frequency response with (a) full time window, (b) 3ms, (c) 10ms and (d) 50ms window length



Figur 2: Directivity for 45°, 90° and 180° off-axis measurement

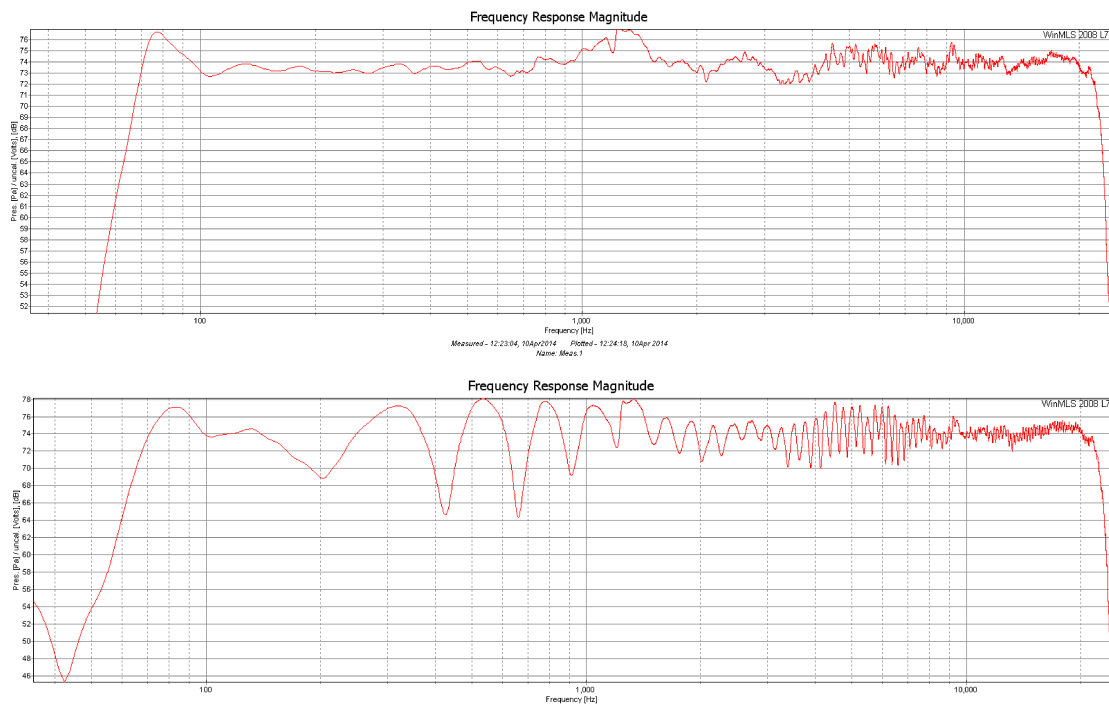


Figure 3: Frequency response (a) without and (b) with reflective surface

4 Conclusion

In this laboratory measurements of loudspeaker parameters were done. Therefore a loudspeaker was placed on a turntable and put in front of a measurement microphone. This was done in an anechoic chamber. In a first measurement it can be obtained, that especially at low frequencies resulting frequency responses get wrong when the FFT time window is chosen too short. But in an other way the frequency response gets more smooth and less calculations have to be done. In a second step the directivity of the loudspeaker was measured. In this measurement it could be obtained that the directivity occurs mainly in higher frequencies, while at low frequencies the loudspeaker emits sound almost omnidirectional. The higher the frequency is the more directional the sound source becomes. In a last measurement the influence of reflections to the measurement was measured. Here it could be seen that reflections have huge interactions with the resulting frequency responses, large constructive and destructive interferences could be obtained.

References

- Svensson, Peter, *lecture notes*

A Example calculations

A.1 Efficiency

A sound pressure level of 74dB at a distance of 1.5m in an anechoic room was measured. A voltage of $V_{RMS} = 1V$ was applied to the loudspeaker (8Ω). The loudspeaker's efficiency shall be calculated.

$$\begin{aligned}
 W_{el,in} &= \frac{(1V)^2}{8\Omega} = 0.125W \\
 W_{lsp,out} &= \frac{0.1^2}{1.2 \frac{kg}{m^3} \cdot 343 \frac{m}{s} \cdot \frac{1}{4\pi \cdot 1.5^2}} \\
 W_{lsp,out} &= 0.0006869 \\
 \eta &= \frac{W_{lsp,out}}{W_{el,in}} = \frac{0.0006869}{0.125} = 0.5495\%
 \end{aligned}$$

A.2 Sensitivity

A loudspeaker sensitivity of 84dB/1m/1W is given. This is equal to a sound pressure level of 84dB at 1m distance when a voltage of 2.83V was applied. Do these numbers correspond to the efficiency calculated in Appendix A.1?

$$\begin{aligned}
 W_{el,in} &= \frac{(2.83V)^2}{8\Omega} = 1.0011W = 1W \\
 W_{lsp,out} &= \frac{0.32^2}{1.2 \frac{kg}{m^3} \cdot 343 \frac{m}{s} \cdot \frac{1}{4\pi \cdot 1^2}} \\
 W_{lsp,out} &= 0.003126 \\
 \eta &= \frac{W_{lsp,out}}{W_{el,in}} = \frac{0.003126}{1} = 0.31\%
 \end{aligned}$$

The numbers does not correspond equally, the efficiency in this example is less than at the first calculation.

A.3 Maximum output level

The given loudspeaker has a maximum input power of 100W. Which sound pressure level could be reached if this loudspeaker is used in a room of $150m^3$? The room has a reverberation time of 0.7s. The maximum sound pressure level in the diffuse reverberation field shall be calculated. For simplified calculations the loudspeaker is assumed as omnidirectional ($DF = 1$).

$$\begin{aligned}
 A &= \frac{0.161 \cdot V}{T_{60}} = \frac{0.161 \cdot 150m^3}{0.7s} = 34.5 \\
 p^2 &= W_{lsp} \cdot \rho_0 \cdot c \left(\frac{DF}{4\pi \cdot r^2} + \frac{4}{A} \right) \\
 p^2 &= 100W \cdot 1.2 \frac{kg}{m^3} \cdot 343 \frac{m}{s} \cdot \left(\frac{1}{4\pi} + \frac{4}{34.5} \right) \\
 p &= 89.71dB
 \end{aligned}$$

A.4 Measurement distance

A two-way loudspeaker with 40cm height and 25cm width is assumed. The LF element has a diameter of 20cm, the HF-Element 3cm. The center-to-center distance is 14cm, the crossover frequency at 2.5kHz. The minimum measurement distance that will ensure that we are in the far field at the crossover frequency shall be calculated.

$$\begin{aligned}
 \lambda &= \frac{343 \frac{m}{s}}{2500Hz} = 0.1372m \\
 R_R &= \frac{\pi \cdot 0.15^2}{0.1372} = 0.515m
 \end{aligned}$$

A.5 Truncated impulse responses

A room with a ceiling height of 2.7m is assumed. The measurement is done at the shortest possible distance, the loudspeaker of previous calculations is used. What is the longest time we can get between the direct sound and the first reflections? How low in frequency can the frequency response be measured? The shortest possible measurement distance is 0.5m. So the direct sound will reach the microphone after

$$\frac{0.5m}{343 \frac{m}{s}} = 1.458ms$$

The distance the first reflection has to travel is to the ceiling (2.7m) and back to the microphone (2.7m-0.5m). So the total distance is 4.9m. It reaches the microphone after

$$\frac{4.9m}{343 \frac{m}{s}} = 14.286ms$$

The lowest possible frequency is calculated the following way:

$$\Delta t = 14.286ms - 1.458ms = 12.828ms$$

$$f = \frac{1}{\Delta t} = \frac{1}{12.828ms} = 77.95Hz = 78Hz$$

A.6 Edge reflection/diffraction

A loudspeaker enclosure causes reflections at the edges. This will lead to uneven frequency responses. The time difference between the direct sound and the first edge reflection at a measurement distance of 1.5m shall be calculated. Which frequencies are amplified with positive interference?

Those frequencies, which arrives at the same time at the measurement microphone with positive peaks will amplify. If the distance from the edge to the direct sound equals to an integer multiple of the wavelength the frequency will be amplified.

B Further plots

B.1 FFT time windows

In this section the FFT time windows for chapter 3.2 are listed (figures 4 - 7).

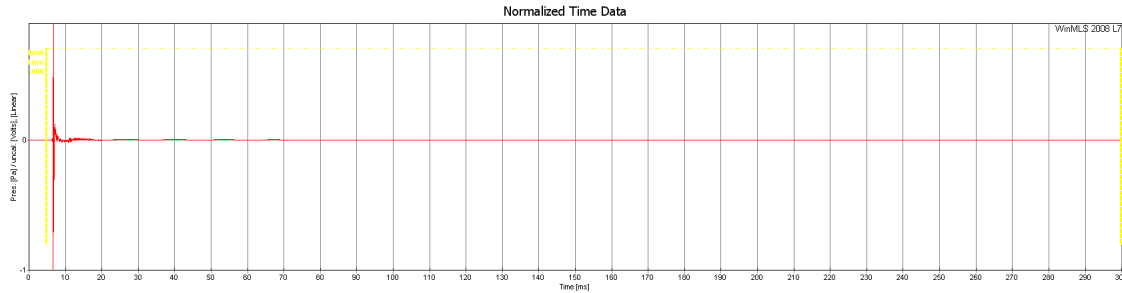


Figure 4: Full FFT time window

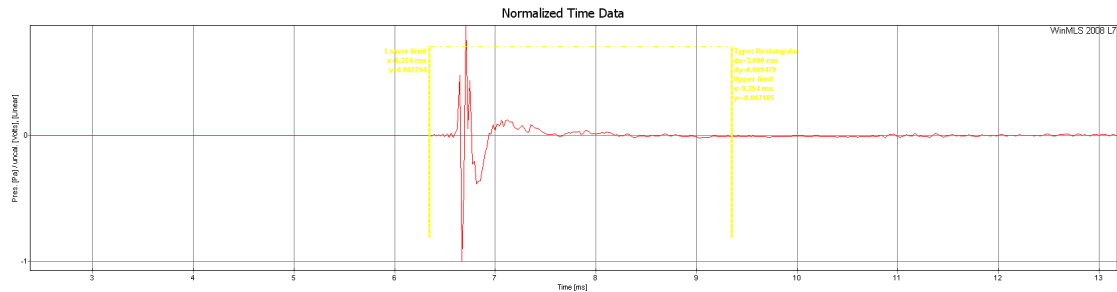


Figure 5: Time window length 3ms

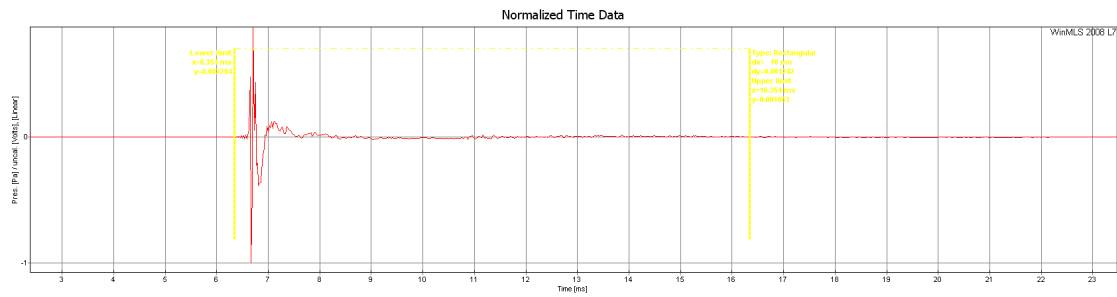


Figure 6: Time window length 10ms

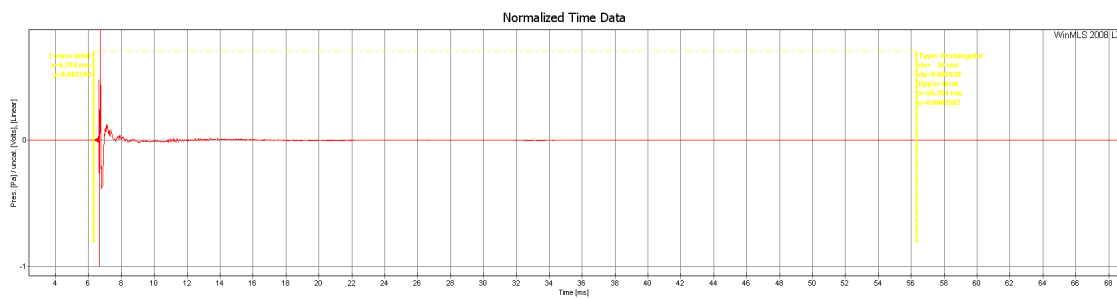
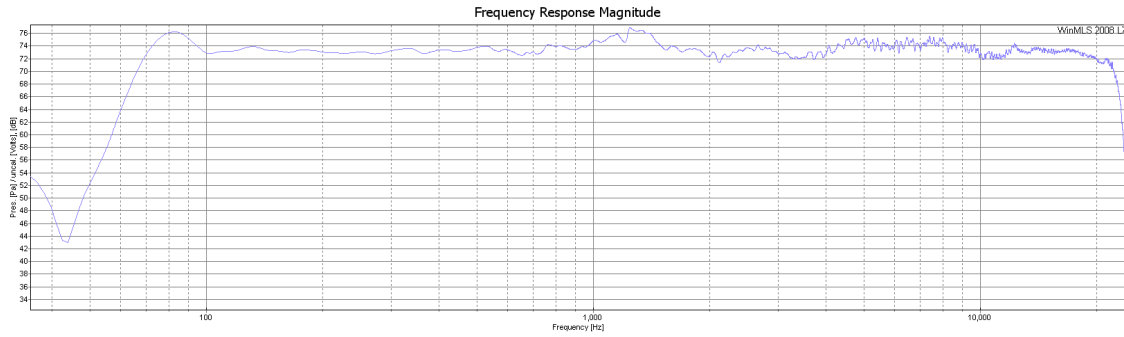


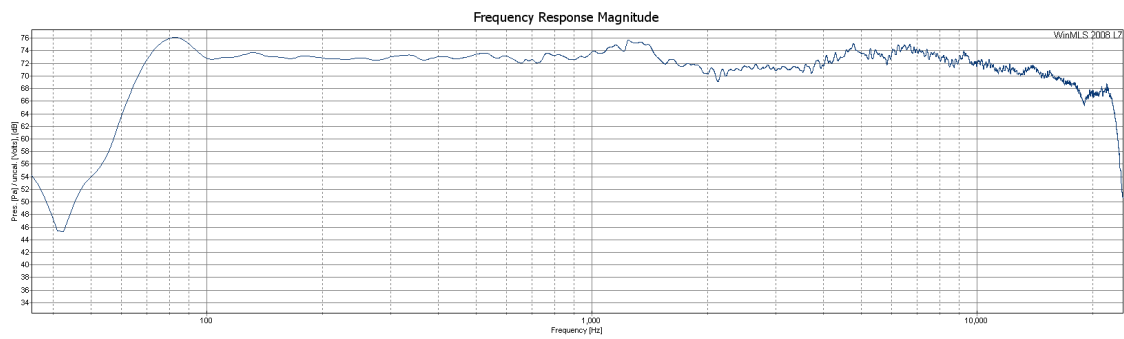
Figure 7: Time window length 50ms

B.2 Frequency responses

In this section further plots of frequency responses of chapter 3.3 are listed (figures 8 - 19).



Figur 8: Frequency response with 15° off axis loudspeaker placement



Figur 9: Frequency response with 30° off axis loudspeaker placement

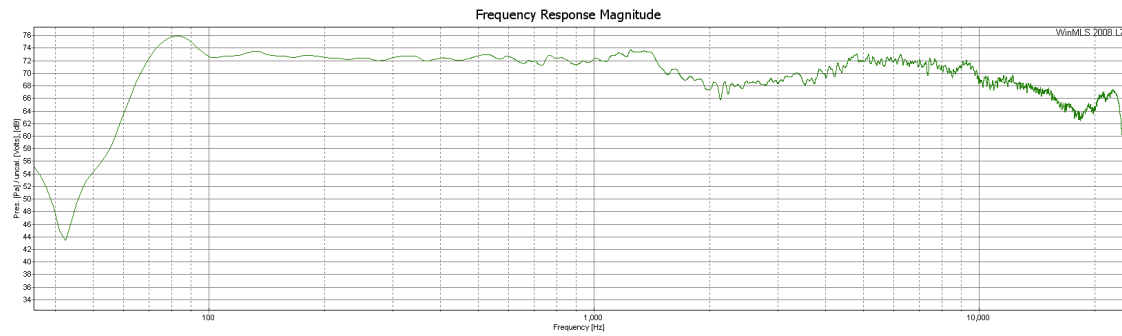


Figure 10: Frequency response with 45° off axis loudspeaker placement

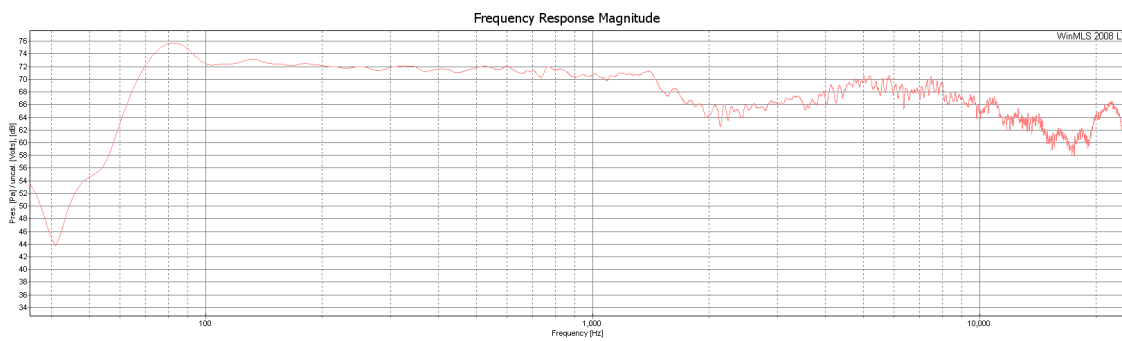


Figure 11: Frequency response with 60° off axis loudspeaker placement

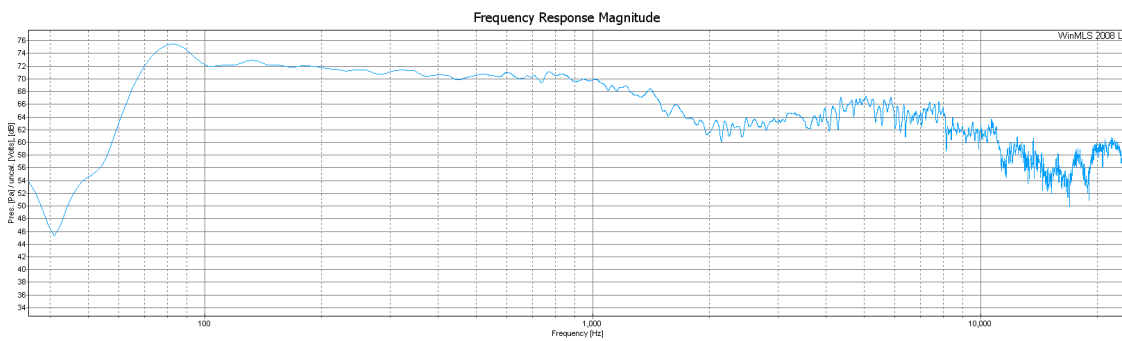
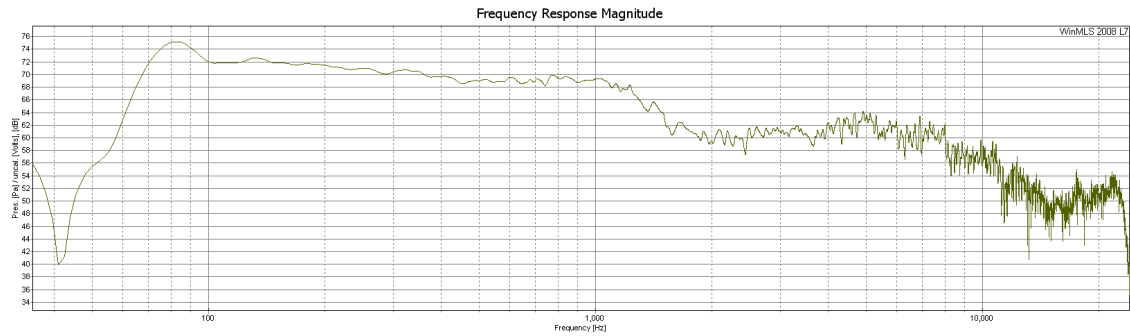
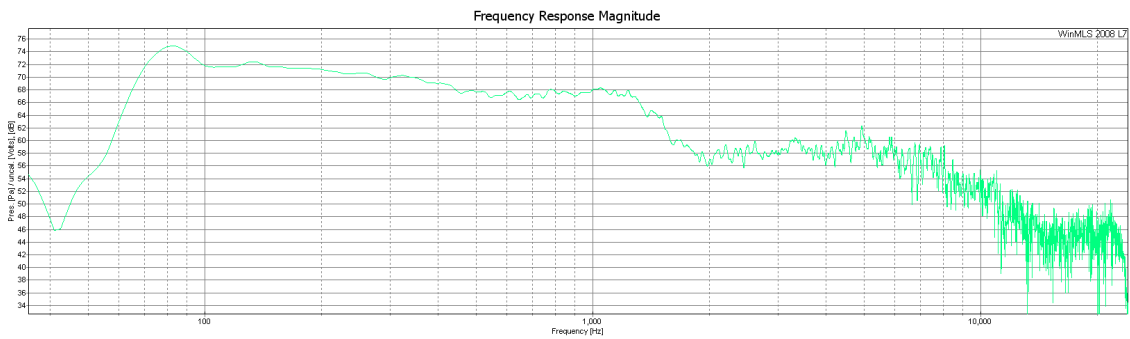


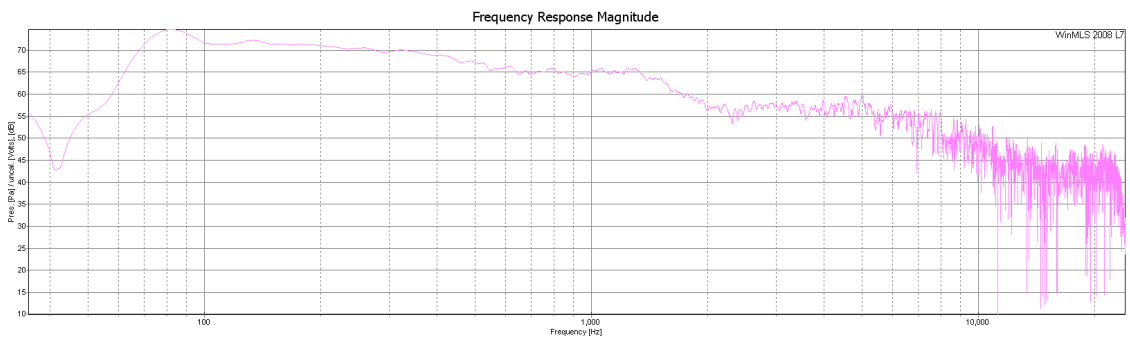
Figure 12: Frequency response with 75° off axis loudspeaker placement



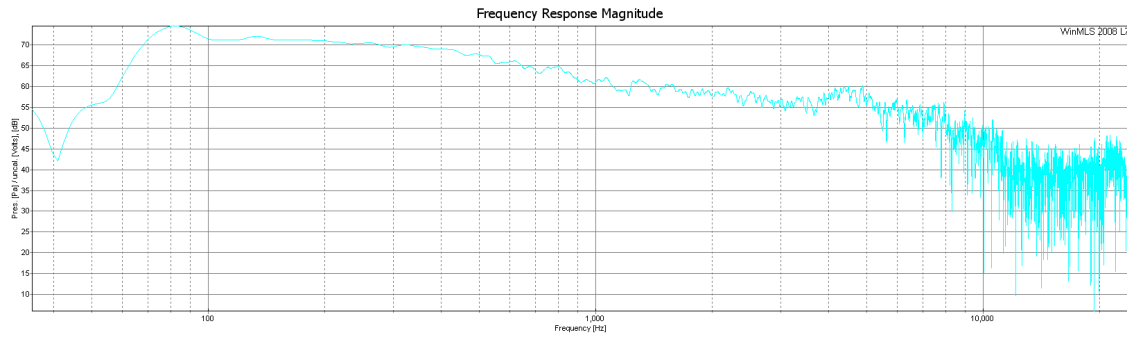
Figur 13: Frequency response with 90° off axis loudspeaker placement



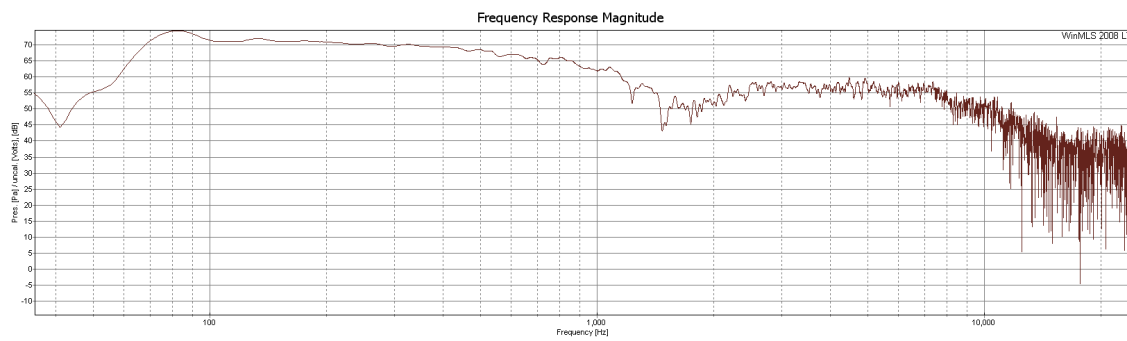
Figur 14: Frequency response with 105° off axis loudspeaker placement



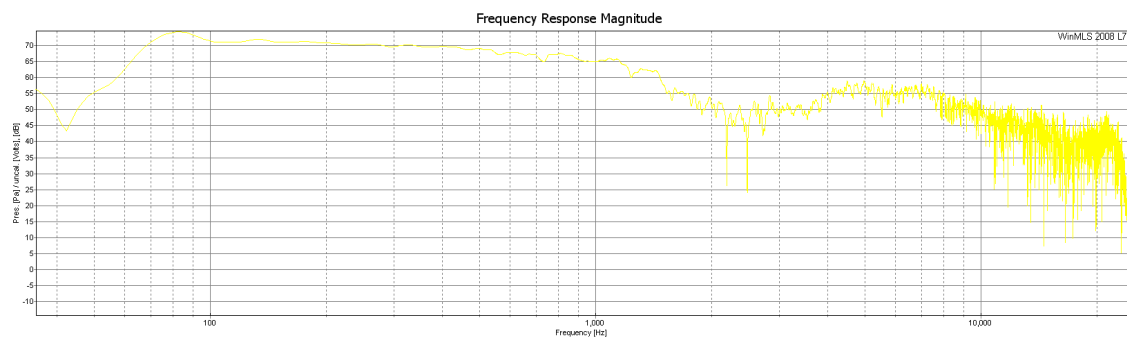
Figur 15: Frequency response with 120° off axis loudspeaker placement



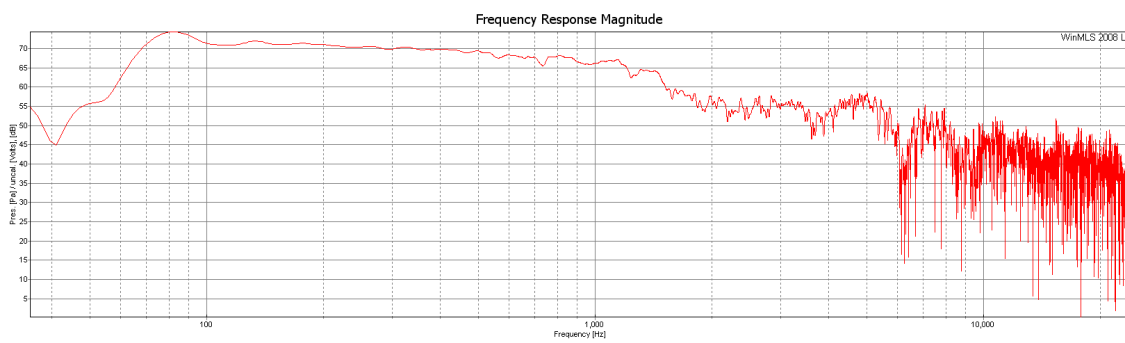
Figur 16: Frequency response with 135° off axis loudspeaker placement



Figur 17: Frequency response with 150° off axis loudspeaker placement



Figur 18: Frequency response with 165° off axis loudspeaker placement



Figur 19: Frequency response with 180° off axis loudspeaker placement