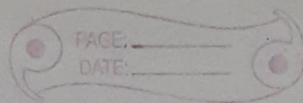


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Roll. no :- 20110160



Assignment :- 2

2) Here, we need to prove $RS(a)R^T = S(Ra)$

And, we are give R as the rotational matrix

Now, let us take any $\vec{b} \in \mathbb{R}^3$

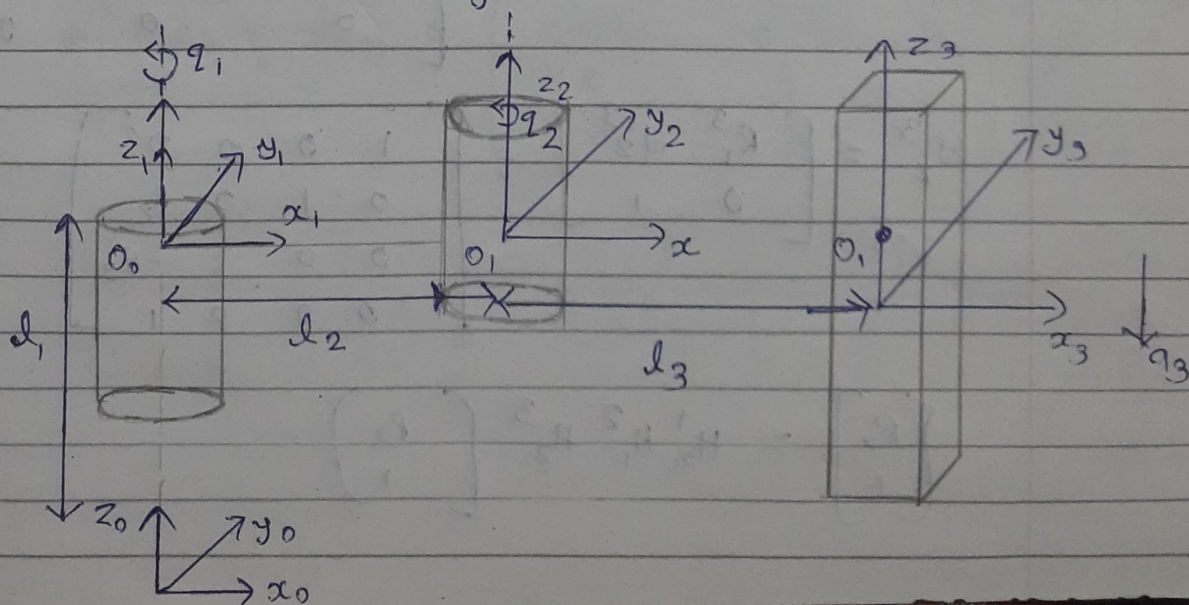
$$\begin{aligned} RS(\vec{a})R^T\vec{b} &= R(\vec{a} \times R^T\vec{b}) \quad (\because S(a) \cdot \vec{p} = \vec{a} \times \vec{p}) \\ &= (R\vec{a}) \times (RR^T\vec{b}) \end{aligned}$$

but we know that $RR^T = I$ (Identity matrix)

$$\begin{aligned} RS(\vec{a})R^T\vec{b} &= (R\vec{a}) \times \vec{b} \\ &= S(R\vec{a})\vec{b} \end{aligned}$$

Hence, $RS(\vec{a})R^T = S(R\vec{a})$

2) SCARA (RRP) Configuration



We can write the rotation matrices as follows:

$$R_0^1 = R_{z, q_1} = \begin{bmatrix} \cos q_1 & -\sin q_1 & 0 \\ \sin q_1 & \cos q_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, d_0^1 = \begin{bmatrix} l_1 \cos q_1 \\ l_1 \sin q_1 \\ 0 \\ 1 \end{bmatrix}$$

$$R_1^2 = R_{z, q_2} = \begin{bmatrix} \cos q_2 & -\sin q_2 & 0 \\ \sin q_2 & \cos q_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}, d_1^2 = \begin{bmatrix} l_2 \cos q_2 \\ l_2 \sin q_2 \\ 0 \\ 1 \end{bmatrix}$$

$$R_2^3 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, d_2^3 = \begin{bmatrix} 0 \\ 0 \\ -l_3 \\ 1 \end{bmatrix}, P_3 = \begin{bmatrix} 0 \\ 0 \\ -l_3 \\ 1 \end{bmatrix}$$

$$H_0^1 = \begin{bmatrix} R_0^1 & d_0^1 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos q_1 & -\sin q_1 & 0 & l_1 \cos q_1 \\ \sin q_1 & \cos q_1 & 0 & l_1 \sin q_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

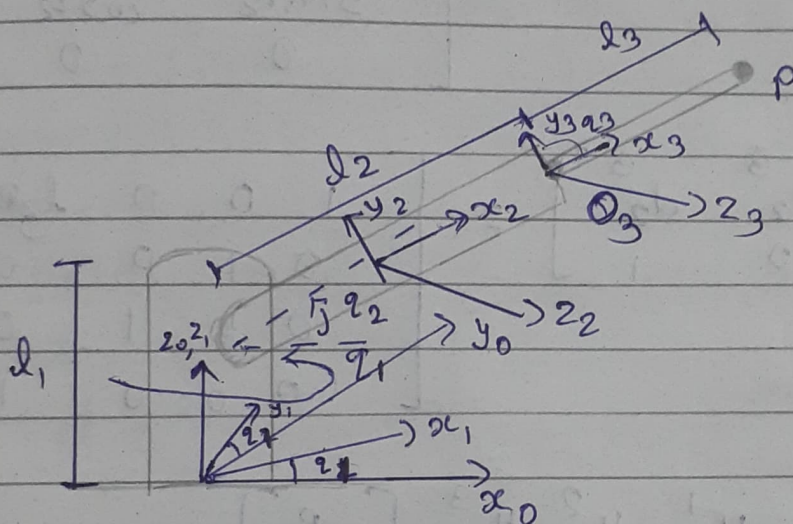
$$H_1^2 = \begin{bmatrix} R_1^2 & d_1^2 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos q_2 & -\sin q_2 & 0 & l_2 \cos q_2 \\ \sin q_2 & \cos q_2 & 0 & l_2 \sin q_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_2^3 = \begin{bmatrix} R_2^3 & d_2^3 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & -l_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} P_0 \\ 1 \end{bmatrix} = H_0^1 H_1^2 H_2^3 \begin{bmatrix} P_3 \\ 1 \end{bmatrix}$$

$$P_0 = \begin{bmatrix} -l_1 \cos q_1 + l_2 \cos(q_1 + q_2) \\ l_1 \sin q_1 + l_2 \sin(q_1 + q_2) \\ -l_3 - d \end{bmatrix}$$

4) Stanford - type (RRP) Configuration



We can write down the rotation matrices as following

$$R_0^1 = R_{z, q_1} = \begin{bmatrix} \cos q_1 & -\sin q_1 & 0 \\ \sin q_1 & \cos q_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, d_0^1 = \begin{bmatrix} 0 \\ 0 \\ l_1 \end{bmatrix}$$

$$R_1^2 = R_{x, \frac{\pi}{2}} R_{z, q_2} = \begin{bmatrix} \cos q_2 & -\sin q_2 & 0 \\ 0 & 0 & -1 \\ \sin q_2 & \cos q_2 & 0 \end{bmatrix}, d_1^2 = \begin{bmatrix} l_2 \\ 0 \\ 0 \end{bmatrix}$$

$$R_2^3 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, d_2^3 = \begin{bmatrix} l_3 \\ 0 \\ 0 \end{bmatrix}, P_3 = \begin{bmatrix} 0 \\ 0 \\ d \end{bmatrix}$$

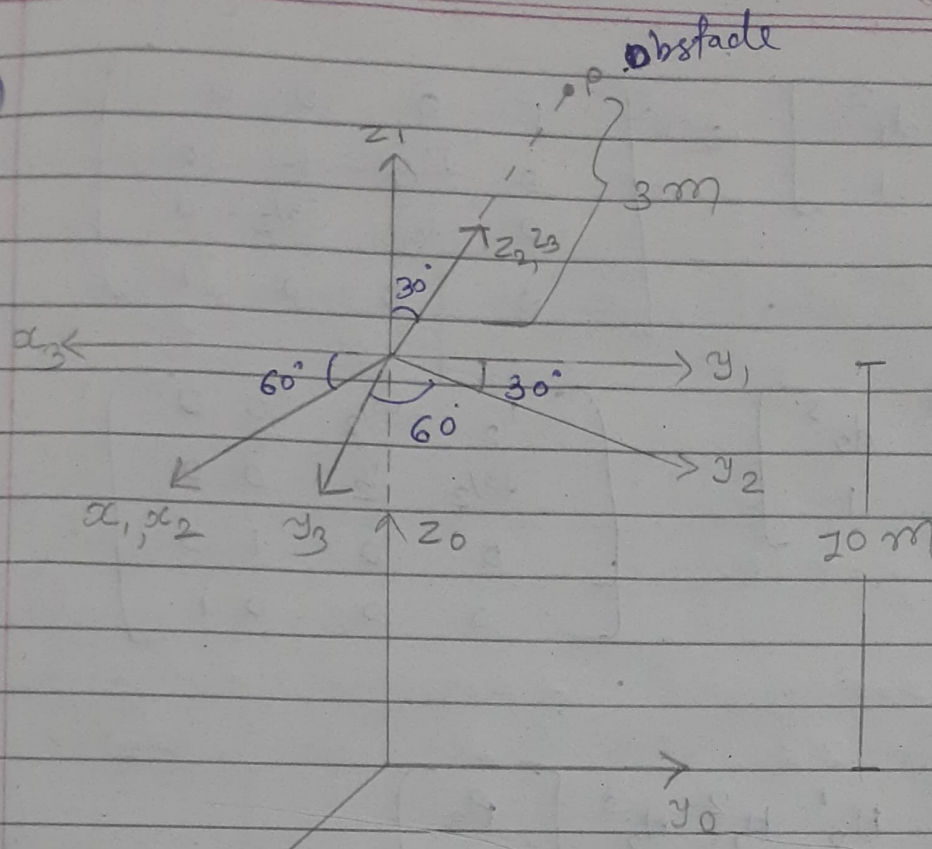
$$H_0^1 = \begin{bmatrix} R_0^1 & d_0^1 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 & 0 & 0 \\ \sin \theta_1 & \cos \theta_1 & 0 & 0 \\ 0 & 0 & 1 & l_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_1^2 = \begin{bmatrix} R_1^2 & d_1^2 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & l_2 \\ 0 & 0 & -1 & 0 \\ \sin \theta_2 & \cos \theta_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_2^3 = \begin{bmatrix} R_2^3 & d_2^3 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & l_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} P_0 \\ 1 \end{bmatrix} = H_0^1 \cdot H_1^2 \cdot H_2^3 \begin{bmatrix} P_3 \\ 1 \end{bmatrix}$$

5



$$d_0^1 = \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix}$$

$$d_1^2 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, d_2^3 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$P_3 = \begin{bmatrix} 0 \\ 0 \\ 3 \end{bmatrix}$$

$$R_0^1 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_1^2 = R_{\alpha, 30} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos 30 & -\sin 30 \\ 0 & \sin 30 & \cos 30 \end{bmatrix}$$

$$R_1^2 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \sqrt{3}/2 & -1/2 \\ 0 & 1/2 & \sqrt{3}/2 \end{bmatrix}$$

$$R_2^3 = R_{\alpha, 60} = \begin{bmatrix} \cos 60 & -\sin 60 & 0 \\ \sin 60 & \cos 60 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_2^3 = \begin{bmatrix} 1/2 & -\sqrt{3}/2 & 0 \\ \sqrt{3}/2 & 1/2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$H_0^1 = \begin{bmatrix} R_0^1 & d_0^1 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 10 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_1^2 = \begin{bmatrix} R_1^2 & d_1^2 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \sqrt{3}/2 & -1/2 & 0 \\ 0 & 1/2 & \sqrt{3}/2 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_2^3 = \begin{bmatrix} R_2^3 & d_2^3 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1/2 & -\sqrt{3}/2 & 0 & 0 \\ \sqrt{3}/2 & 1/2 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

So,

$$\begin{bmatrix} P_0 \\ 1 \end{bmatrix} = H_0^1 H_1^2 H_2^3 \begin{bmatrix} P_3 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} P_0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ -3/2 \\ 3\sqrt{3}/2 + 10 \\ 1 \end{bmatrix}$$

So,

$$P_0 = \begin{bmatrix} 0 \\ -3/2 \\ 10 + \frac{3\sqrt{3}}{2} \end{bmatrix} = \begin{bmatrix} 0 \\ -1.5 \\ 12.598 \end{bmatrix}$$

Qn 6)

Planetary Gearbox:

- Pros: High torque output, compact size, and high efficiency due to many gear connections. Suitable for applications requiring precise motion control and limited areas, such as robotic arms and CNC machines.
- Cons: Slightly more complex and pricey than other types of gearboxes.

Worm Gearbox:

- Pros: The self-locking system prevents back-driving, making it ideal for applications that need retaining positions without power. It is effective in applications like conveyor belts and hoisting mechanisms.
- Cons: Lower efficiency from sliding contact can result in heat generation and a shorter lifespan.

Spur Gearbox:

- Pros: Simple design, low cost, and suitability for a wide range of applications. When properly developed, it provides good efficiency.
- Cons: Larger in size than planetary gears for comparable torque output. More noise and vibration may be produced.

Harmonic Drive Gearbox:

- Pros: zero backlashes, great precision, and an excellent torque-to-weight ratio. Ideal for high precision and compactness applications such as robotic joints and medical equipment.
- Cons: Higher cost and worse efficiency compared to other gearboxes.

Adding a gearbox would raise the cost of manufacturing a drone and complicate the mechanical system. Consumer drones are typically meant to be affordable, with manufacturers aiming to reach a balance between performance and cost-effectiveness. Drones are also designed to be lightweight in order to increase flying time and maneuverability. Adding a gearbox would increase weight, affecting the drone's overall efficiency and flight durability. Consumer drones emphasize portability when doing hovering photography or filmmaking. The use of a gearbox in a drone is determined by the application's specific requirements, which must balance considerations such as payload capacity and flight time against the extra weight and expense of the gearbox.

⑦ For SCARA manipulator (RPP) Jacobian can be given as following

$$J = \begin{bmatrix} J_v \\ J_w \end{bmatrix} = \begin{bmatrix} Z_0 \times (o_3 - o_0) & Z_1 (o_3 - o_1) & \text{prismatic joint} \\ Z_0 & Z_1 & \begin{pmatrix} z_2 \\ 0 \end{pmatrix} \end{bmatrix}$$

$$O_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad O_1 = \begin{bmatrix} l_1 c_1 \\ l_1 s_1 \\ 0 \end{bmatrix}, \quad O_2 = \begin{bmatrix} l_1 c_1 + l_2 c_2 \\ l_1 s_1 + l_2 s_2 \end{bmatrix}$$

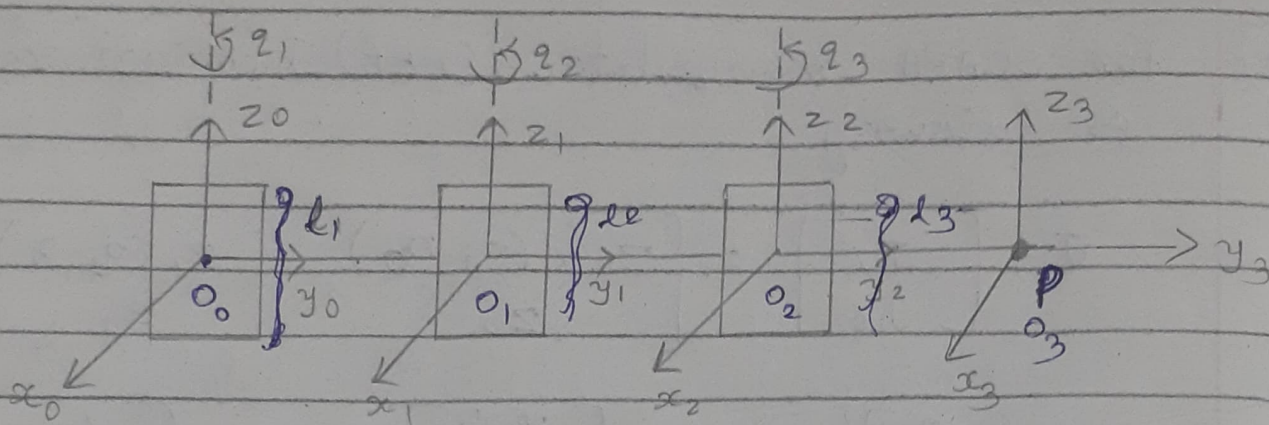
$$H_0^1 = \begin{bmatrix} c_1 & -s_1 & 0 & l_1 c_1 \\ s_1 & c_1 & 0 & l_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}, \quad H_0^2 = \begin{bmatrix} l_1 c_1 + l_2 c_2 \\ l_1 s_1 + l_2 s_2 \\ d_3 - d_4 \\ 1 \end{bmatrix}$$

$$H_0^2 = H_0^1 \cdot H_1^2 = \begin{bmatrix} c_{12} & -s_{12} & 0 & l_1 c_1 + l_2 c_2 \\ s_{12} & c_{12} & 0 & l_1 s_1 + l_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_0^3 = H_0^2 \cdot H_2^3 = \begin{bmatrix} c_{12} & -s_{12} & 0 & l_1 c_1 + l_2 c_2 \\ s_{12} & c_{12} & 0 & l_1 s_1 + l_2 s_2 \\ 0 & 0 & 1 & d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$Z_0 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = Z_1, \quad \& \quad Z_2 = Z_3 = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix}$$

$$So, \quad J = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} & -l_2 s_{12} & 0 \\ l_1 c_1 + l_2 c_{12} & l_2 c_{12} & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 0 \end{bmatrix}$$



Jacobian is given as,

$$J = \begin{bmatrix} z_0 \times (O_3 - O_0) & z_1 \times (O_3 - O_1) & z_2 \times (O_3 - O_2) \\ z_0 & z_1 & z_2 \end{bmatrix}$$

$$O_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \quad O_1 = \begin{bmatrix} l_1 c_1 \\ l_1 s_1 \\ 0 \end{bmatrix}, \quad O_2 = \begin{bmatrix} l_1 c_1 + l_2 c_{12} \\ l_1 s_1 + l_2 s_{12} \\ 0 \end{bmatrix}$$

$$O_3 = \begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix}$$

$$z_0 = z_1 = z_2 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad (\text{here all the } z \text{ axis directions are parallel to each other})$$

So,

$$J = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$