1. Show that RS(O) RT = 5(Ra), Risa hotation matrix.

$$S(Ra) \cdot Ra = (Ra) \times (Ra) \qquad [75(a) p = a \times p]$$

$$= R \cdot (a \times a)$$

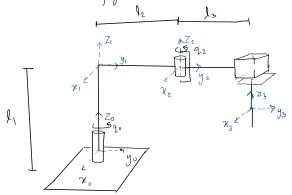
$$= R \cdot S(a) a$$

$$= R \cdot S(a) T_{5 \times 3} a$$

$$= R \cdot S(a) R^{T} R a \qquad [70 R^{T} = R^{-1}]$$

$$5(R^{\alpha}) \cdot R^{\alpha} = R \cdot S(\alpha) R^{T} \cdot R^{\alpha}$$
  
Comparing RHS and LHS, we get:  
 $5(R^{\alpha}) = R \cdot S(\alpha) R^{T}$ 

2. SCARA: RRP Configuration



3 → Prismahi joint, 2,00 revolute

$$R_1^2 = R_{Z_1 q_2}$$
  $A_1^2 = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$ 

$$R_{b}^{i} = R_{z_{1}q_{1}} \quad d_{b}^{i} = \begin{bmatrix} 0 \\ 0 \\ l_{1} \end{bmatrix}$$

$$\begin{bmatrix} \rho_0^{-1} & H_0^1 & H_1^2 \\ 0 \end{bmatrix} = \begin{bmatrix} cq_1 & -sq_1 & 0 & 0 \\ sq_1 & cq_1 & 0 & 0 \\ 0 & 0 & 1 & l_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} cq_1 & sq_1 & 0 & 0 \\ sw_1 & cq_2 & 0 & l_2 \\ 0 & 0 & 1 & b \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} cq_{1}cq_{2} - sq_{1}sq_{2} & -(cq_{1}sq_{2} + sq_{1}cq_{2}) & 0 & -l_{2}sq_{1} \\ sq_{1}cq_{2}+cq_{1}sq_{2} & -sq_{1}sq_{2} + cq_{1}cq_{2} & 0 & l_{2}cq_{1} \\ 0 & 0 & 0 & l & l_{3} \\ 0 & 0 & 0 & l & l_{3} \end{bmatrix} \begin{bmatrix} l_{3} & 0 & 0 & l_{3} \\ 0 & 1 & 0 & l_{3} \\ 0 & 0 & 1 & -q_{3} \end{bmatrix} \begin{bmatrix} l_{3} & 0 & 0 & l_{3} \\ 0 & 0 & 1 & -q_{3} \\ 0 & 0 & 0 & l & l_{3} \end{bmatrix}$$

$$= \begin{bmatrix} c(q_{1}+q_{2}) & -5(q_{1}+q_{2}) & 0 & -\{15q_{1}\} \\ 5(q_{1}+q_{2}) & c(q_{1}+q_{2}) & 0 & 1_{2}cq_{1} \\ 0 & 0 & 1 & 1_{3} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 1_{3} \\ 0 & 0 & 1 & -q_{3} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} p_{3} \\ 1 \end{bmatrix}$$

$$= \begin{bmatrix} c(q_1+q_2) & -s(q_1+q_2) & 0 & -l_3 s(q_1+q_2) - l_2 sq_1 \\ s(q_1+q_2) & c(q_1+q_2) & 0 & l_3 c(q_1+q_2) + l_2 cq_1 \\ 0 & 0 & 1 & l_1-q_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ -l_4 \\ 1 \end{bmatrix}$$

4. Stanford-type: RRP configuration.
$$\rho_{3} = \begin{bmatrix} \ell_{3} \\ 0 \end{bmatrix}$$

$$R_{1}^{2} = R_{3} \cdot r_{3} \cdot r_{3}$$

$$R_{1}^{2} = R_{3} \cdot r_{3} \cdot$$

$$= \begin{bmatrix} c\pi/3 & -5\pi/3 & 0 & 0 \\ c\pi/6 & 5\pi/3 & c\pi/6 & c\pi/6 & 0 \\ 5\pi/6 & 5\pi/3 & c\pi/6 & c\pi/6 & 10 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 3 \\ 1 \end{bmatrix}$$

$$= \begin{bmatrix} 0 \\ -3 & 5 & 10 & 1/6 \\ 3 & cos & 1/6 \\ 1 \end{bmatrix} \begin{bmatrix} p_0 = -\frac{3}{2} & \hat{j} + \left| \frac{3\sqrt{3}}{2} + 10 \right| \hat{k} \\ \frac{3}{2} & cos & 1/6 \\ \frac{3}{2} & cos & 1/6 \end{bmatrix} \begin{bmatrix} p_0 = -\frac{3}{2} & \hat{j} + \left| \frac{3\sqrt{3}}{2} + 10 \right| \hat{k} \\ \frac{3}{2} & cos & 1/6 \end{bmatrix} \begin{bmatrix} p_0 = -\frac{3}{2} & \hat{j} + \left| \frac{3\sqrt{3}}{2} + 10 \right| \hat{k} \\ \frac{3}{2} & cos & 1/6 \end{bmatrix} \begin{bmatrix} p_0 = -\frac{3}{2} & \hat{j} + \left| \frac{3\sqrt{3}}{2} + 10 \right| \hat{k} \end{bmatrix}$$

- 6. A gearbox is a mechanical component used to change the speed (RPM) and increase the motor's torque. Some types of gearboxes commonly used in robotics:
  - Spur Gearbox: used in applications that require low to medium torque transmission like in small robotic arms.
     Pros- Simple design, high efficiency and compact size.
     Cons- Lower torque transmission capability, noise generation.
  - Planetary Gearbox: used in applications that require high torque such as heavy robotic arms.
     Pros- High torque transmission capacity, compact size, and efficient power distribution
     Cons- Higher cost and complexity compared to spur gearboxes.
  - Worm Gearbox: used in applications with the requirement of high-torque transmission and self-locking, such as
    robotic lifting mechanisms.
     Pros: High torque transmission, self-locking feature, and ability to handle heavy loads. Cons: Lower efficiency,
    higher wear and tear, and limited speed reduction capability.

Typically, gearboxes are not used in drones. This is mainly because drones require lightweight and efficient power transmission systems, and direct drive motors or specialized propeller attachments are more suitable for their needs. Adding an additional gearbox would introduce unnecessary weight, complexity, and potential points of failure.

Manipulator Jacobium for SCARA: RRP

$$J = \begin{bmatrix} J_1 & J_2 & J_3 \end{bmatrix}_{(X3)}$$

$$O_n = \{0 = \begin{bmatrix} -\left(l_3 s(q_1 + q_1) + l_1 s q_1\right) \\ l_3 c(q_1 + q_2) + l_1 c q_1 \\ l_1 - l_4 - q_3 \end{bmatrix}$$

$$J_{\text{From Ans 2}} \begin{bmatrix} z_{1-1} \times (o_n - o_{1-1}) \\ z_{1-1} = R_0^{1-1} & (k_1 + k_2 + k_3 + k_4 + k_$$

 $O_{n} - O_{1} = \begin{bmatrix} -l_{3} & 5(q_{1} + q_{2}) \\ l_{3} & c(q_{1} + q_{2}) \end{bmatrix} \qquad J_{1} = \begin{bmatrix} -l_{3} & 5(q_{1} + q_{2}) \\ k \end{bmatrix} - l_{3} & c(q_{1} + q_{2}) \end{bmatrix}$ 

 $0_{1} = R \times Z_{q_{1}} \quad \begin{bmatrix} 0 \\ l_{1} \\ l_{1} \end{bmatrix} = \begin{bmatrix} cq_{1} & -sq_{1} & 0 \\ sq_{1} & cq_{1} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ l_{1} \\ l_{1} \end{bmatrix} = \begin{bmatrix} -l_{2}sq_{1} \\ l_{2}cq_{1} \\ l_{3} \end{bmatrix}$ 

Jour (R): Z1 = Roke k

 $J_{2} \in \left[ \hat{k} \times (0_{N} - 0_{1}) \right]$ 

$$O_{n} - o_{1} = \begin{bmatrix} -l_{3} & S(q_{1} + q_{2}) \\ l_{3} & C(q_{1} + q_{2}) \\ -l_{4} - q_{5} \end{bmatrix}$$

$$\exists_{1} = \begin{bmatrix} -l_{3} & S(q_{1} + q_{2}) & f \\ \hat{k} \end{bmatrix}$$

Joint (3 (P) 
$$^{1}$$
  $Z_{2} = \hat{k}$   $J_{3} = \begin{bmatrix} Z_{2} \\ 0 \end{bmatrix}$ 

9. RRR configuration w/ all axes parallel. 
$$(z_0=Z_1 \in Z_2 \in Z_3 \in \hat{k})$$
  $l_1, l_2, l_3 \rightarrow lengths$  of links 
$$J = \begin{bmatrix} Z_0 \times (0_3-0_0) & Z_1 \times (0_3-0_1) & Z_2 \times (0_3-0_2) \end{bmatrix}$$

$$\begin{bmatrix} O_{0} \\ I \end{bmatrix} = \begin{bmatrix} \rho_{0} \\ I \end{bmatrix} = H_{0}^{1} H_{0}^{2} H_{2}^{2} \begin{bmatrix} \rho_{3} \\ I \end{bmatrix}$$

$$\rho_{3} = \begin{bmatrix} \rho_{3} \\ I \end{bmatrix}$$

$$R_{0}^{2} = R_{Z_{1}} q_{2} \qquad d_{1}^{2} = \begin{bmatrix} l_{1} \\ 0 \\ 0 \end{bmatrix}$$

$$R_{0}^{1} = R_{Z_{1}} q_{1} \qquad C(q_{1} + q_{2}) = Cq_{1}q_{2}$$

$$C(q_{1} + q_{2}) = Cq_{1}q_{2}$$

$$\begin{bmatrix} 0_{3} \\ 1 \end{bmatrix} = \begin{bmatrix} cq_{1} & -sq_{1} & 0 & 0 \\ sq_{1} & cq_{1} & 6 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} cq_{2} & -sq_{1} & 0 & l_{1} \\ sq_{1} & cq_{2} & cq_{3} & 0 & l_{1} \\ sq_{1}q_{2} & cq_{2} & cq_{3} & 0 & l_{2} \\ sq_{1}q_{2} & cq_{2} & cq_{3} & 0 & l_{3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} cq_{2} & -sq_{3} & 0 & l_{2} \\ sq_{1}q_{2} & cq_{2} & cq_{3} & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} cq_{3} & -sq_{3} & 0 & l_{2} \\ sq_{1}q_{2} & cq_{2} & cq_{3} & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} cq_{3} & -sq_{3} & 0 & l_{2} \\ sq_{1}q_{2} & cq_{2} & cq_{3} & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} c_{q_1q_1q_3} & -s_{q_1q_1q_3} & 0 & l_1c_{q_1q_2} + l_1c_{q_1} \\ s_{q_1q_1q_3} & c_{q_1q_1q_3} & 0 & l_2s_{q_1q_2} + l_1s_{q_1} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} l_3 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} l_3c_{q_1q_1q_3} + l_2c_{q_1q_2} + l_1c_{q_1} \\ l_3s_{q_1q_1q_3} + l_2s_{q_1q_2} + l_1s_{q_1} \\ 0 & 0 & 1 \\ 1 & 0 & 1 \end{bmatrix}$$

$$O_{o} \subset \left[ \begin{array}{c} 0 \\ 0 \\ 0 \end{array} \right]$$