

The minimization problem is generically defined as **[ABT: place-holder; needs constraints etc.]**

$$\operatorname{argmin}_{\text{admissible } \omega} J(\omega), \quad (1)$$

where J is some objective function on the micro structure. Letting S denote the compliance tensor, we choose

$$J(\omega) = \frac{1}{2} \|S^H(\omega) - S^*\|_F^2, \quad (2)$$

for a microstructure with shape ω . There are several other possible choices for the objective functional J , such as deviation of elasticity tensor or error in displacement. In our setting, we are interested in particular values of Poisson ratios and shear moduli and the compliance. **[ABT: Justification for use of compliance]**

The microstructure boundary $\partial\omega$ is parameterized by a vector \mathbf{p} , consisting of, for instance, wire mesh node offsets and thicknesses. With proper assumptions, the derivative of $\partial\omega$ with respect to \mathbf{p} is given by

$$\mathbf{v}_{p_\alpha}(\mathbf{y}, \mathbf{p}) := \frac{\partial \mathbf{y}}{\partial p_\alpha} \quad \text{for } \mathbf{y} \in \partial\omega, \quad (3)$$

and defines perturbation velocity fields over the boundary. Using \mathbf{p} the minimization problem can be written as

$$\operatorname{argmin}_{\text{admissible } \mathbf{p}} J(\mathbf{p}) \quad \text{where } J(\mathbf{p}) = \frac{1}{2} \|S^H(\mathbf{p}) - S^*\|_F^2. \quad (4)$$

The derivative of the objective function is then

$$\frac{\partial J}{\partial p_\alpha} = [S^H - S^*] : \frac{\partial S^H}{\partial p_\alpha} = [S^H - S^*] : dS^H[\mathbf{v}_{p_\alpha}], \quad (5)$$

where $dS^H[\mathbf{v}_{p_\alpha}]$ is the shape derivative of S^H with perturbation \mathbf{v}_{p_α} .

Shape derivative of elasticity tensor. The shape derivative of the homogenized elasticity tensor for microstructure with shape ω and perturbation \mathbf{v} is defined as the Gâteaux derivative [1]

$$dC^H[\mathbf{v}] := \lim_{t \downarrow 0} \frac{C^H(\omega(t, \mathbf{v})) - C^H(\omega)}{t}, \quad (6)$$

where $\omega(t, \mathbf{v}) := \{\mathbf{x} + t\mathbf{v} : \mathbf{x} \in \omega\}$. The homogenized elasticity tensor **[ABT: give ref]**, with a bit of manipulation, can be rewritten in the energy form as

$$C_{ijkl}^H = \frac{1}{|Y|} \int_{\omega} (\mathbf{e}^{ij} + \varepsilon(\mathbf{w}^{ij})) : C^{\text{base}} : (\mathbf{e}^{kl} + \varepsilon(\mathbf{w}^{kl})) \, d\mathbf{y}. \quad (7)$$

Using this form, taking its variation with respect to a *permissible* boundary perturbation, integrating by parts, using the divergence theorem, and the fact that \mathbf{w}^{ij} satisfies the cell problem, the shape derivative of C^H can be written as

$$dC_{ijkl}^H[\mathbf{v}] = \frac{1}{|Y|} \int_{\partial\omega} [(\mathbf{e}^{ij} + \varepsilon(\mathbf{w}^{ij})) : C^{\text{base}} : (\mathbf{e}^{kl} + \varepsilon(\mathbf{w}^{kl}))](\mathbf{v} \cdot \hat{\mathbf{n}}) \, dA(\mathbf{y}). \quad (8)$$

Shape derivative of compliance tensor. The compliance tensor is the inverse of elasticity tensor, i.e. $S : C = I$. Using direct differentiation

$$dS^H[\mathbf{v}] = -S^H : dC^H[\mathbf{v}] : S^H. \quad (9)$$

Combining the results from Eq. (5), Eq. (8), and Eq. (9), one can compute $\frac{\partial J}{\partial p_\alpha}$.

Numerical computation. The integrand in Eq. (7) is cubic over each boundary element ($\mathbf{e}^{ij} + \varepsilon(\mathbf{w}^{ij})$ and $\mathbf{v} \cdot \hat{\mathbf{n}}$ are linear) and we use quadrature that evaluate the cubic function exactly.

References

- [1] JEAN-P Zolésio and MC Delfour. Shapes and geometries: Analysis, differential calculus and optimization. *SIAM, Philadelphia*, 2001.