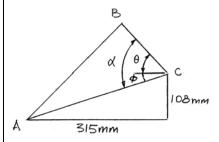


The position of crank BCD is controlled by the hydraulic cylinder AB. For the loading shown, determine the force exerted by the hydraulic cylinder on pin B knowing that  $\theta = 60^{\circ}$ .

#### **SOLUTION**



Have

$$d_{AC} = \sqrt{315^2 + 108^2} = 333 \text{ mm}$$
$$\tan \phi = \frac{108}{315}$$
$$\phi = 18.9246^{\circ}$$

or

Now, let

Then, by the Law of Cosines 
$$d_{AB} = 333^2 + 150^2 - 2(333)(150)\cos\alpha$$

or

$$d_{AB} = \sqrt{(13.3389 - 9.990\cos\alpha)} \times 10^2 \text{ (mm)}$$

and

$$\delta d_{AB} = \frac{499.5 \sin \alpha}{\sqrt{\left(13.3389 - 9.990 \cos \alpha\right)}} \delta \alpha \text{ (mm)}$$

With

$$\delta \alpha > 0$$

 $\alpha = \theta + \phi$ 

Virtual Work:

$$\delta U = 0$$
:  $P\delta y_D - F_{\text{cvl}}\delta d_{AB} = 0$ 

where P = 480 N, and

$$\delta y_D = d_{CD} \delta \alpha$$

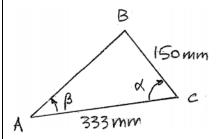
Then

$$(480 \text{ N})(120 \text{ mm})\delta\alpha - F_{\text{cyl}} \left\{ \left[ \frac{499.5 \sin \alpha}{\sqrt{(13.3389 - 9.990 \cos \alpha)}} \right] \text{ mm} \right\} \delta\alpha = 0$$

or 
$$(499.5 \sin \alpha) F_{\text{cyl}} = (57.6 \times 10^3) \sqrt{13.3389 - 9.990 \cos \alpha}$$

With  $\theta = 60^{\circ}$ :  $\alpha = 60^{\circ} + 18.9246^{\circ}$ 

# **PROBLEM 10.41 CONTINUED**



have

$$[499.5\sin(60^{\circ} + 18.9246^{\circ})]F_{\text{cyl}}$$

$$= (57.6 \times 10^{3})\sqrt{13.3389 - 9.990\cos(60^{\circ} + 18.9246^{\circ})}$$

or

$$F_{\rm cyl} = 397.08 \, {\rm N}$$

and

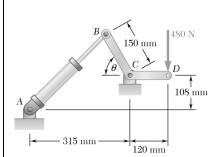
$$d_{AB} = 100\sqrt{13.3389 - 9.990\cos 78.9246^{\circ}} = 337.93 \text{ mm}$$

Then, by the Law of Sines

$$\frac{150}{\sin \beta} = \frac{337.93}{\sin 78.9246^{\circ}}$$
$$\beta = 25.824^{\circ}$$

or

$$\mathbf{F}_{\text{cyl}} = 397 \text{ N } \neq 44.7^{\circ} \blacktriangleleft$$



The position of crank BCD is controlled by the hydraulic cylinder AB. Determine the angle  $\theta$  knowing that the hydraulic cylinder exerts a 420-N force on pin B when the crank is in the position shown.

# **SOLUTION**

From Problem 10.41, we have

$$(499.5\sin\alpha)F_{\rm cyl} = (57.6 \times 10^3)\sqrt{13.3389 - 9.990\cos\alpha}$$

Then, with  $F_{\rm cyl} = 420 \ {\rm N}$ 

We have

$$499.5\sin\alpha(420) = (57.6 \times 10^3)\sqrt{13.3389 - 9.990\cos\alpha}$$

or

$$(3.64219\sin\alpha)^2 = 13.3389 - 9.990\cos\alpha$$

or

$$13.2655(1-\cos^2\alpha) = 13.3389 - 9.990\cos\alpha$$

or

$$13.2655\cos^2\alpha - 9.990\cos\alpha + 0.0734 = 0$$

Then

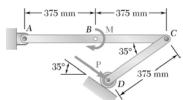
$$\cos \alpha = \frac{9.990 \pm \sqrt{(-9.990)^2 - 4(13.2655)(0.0734)}}{2(13.2655)}$$

or

$$\alpha = 41.7841^{\circ}$$
 and  $\alpha = 89.5748^{\circ}$ 

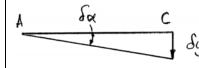
Now  $\theta = \alpha - \phi$  and  $\phi = 18.9246^{\circ}$ 

so that  $\theta = 22.9^{\circ}$  and  $\theta = 70.7^{\circ} \blacktriangleleft$ 



For the linkage shown, determine the force **P** required for equilibrium when  $M = 40 \text{ N} \cdot \text{m}$ .

# **SOLUTION**



55°

35°

For bar ABC, we have

$$\delta \alpha = \frac{\delta y_c}{2a}$$
 where  $a = 375 \text{ mm}$ 

and for bar CD, using the Law of Cosines

$$a^2 = L_C^2 + L_D^2 - 2L_C L_D \cos 55^\circ$$

Then, noting that a = constant, we have

$$0 = 2L_C \delta L_C + 2L_D \delta L_D - 2(\delta L_C) L_D \cos 55^\circ - 2L_C (\delta L_D) \cos 55^\circ$$

Then, because  $\delta L_C = -\delta y_C$ :

$$(L_C - L_D \cos 55^\circ) \delta y_C = (L_D - L_C \cos 55^\circ) \delta L_D$$

For the given position of member CD,  $\triangle CDE$  is isosceles.

$$L_D = a$$
 and  $L_C = 2a\cos 55^\circ$ 

Then

$$(2a\cos 55^{\circ} - a\cos 55^{\circ})\delta y_C = (a - 2a\cos^2 55^{\circ})\delta L_D$$

or

$$\delta L_D = \frac{\cos 55^{\circ}}{1 - 2\cos^2 55^{\circ}} \delta y_C$$

Now, Virtual Work:

$$\delta U = 0$$
:  $M\delta a - P\delta L_D = 0$ 

or

$$M\left(\frac{\delta y_C}{2a}\right) - P\left(\frac{\cos 55^{\circ}}{1 - 2\cos^2 55^{\circ}}\right) \delta y_C = 0$$

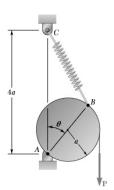
which gives

$$P = \frac{M}{2a} \frac{1 - 2\cos^2 55^\circ}{\cos 55^\circ}$$

Then

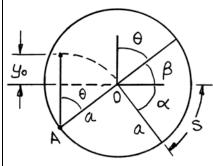
$$P = \frac{40 \text{ N} \cdot \text{m}}{2(0.375 \text{ m})} \frac{1 - 2\cos^2 55^\circ}{\cos 55^\circ}$$

or **P** = 31.8 N 
$$\sqrt{35.0}$$
°



A cord is wrapped around a drum of radius a that is pinned at A. The constant of the spring is  $3 \,\mathrm{kN/m}$ , and the spring is unstretched when  $\theta = 0$ . Knowing that  $a = 150 \,\mathrm{mm}$  and neglecting the mass of the drum, determine the value of  $\theta$  corresponding to equilibrium when a downward force **P** of magnitude 48 N is applied to the end of the cord.

# **SOLUTION**



First note

$$\theta + \beta = 90^{\circ}$$
 
$$\alpha + \beta = 90^{\circ} \quad \Rightarrow \quad \alpha = \theta$$

 $\therefore s = a\theta \qquad \text{Length of cord unwound for rotation } \theta$ 

Now  $y_0 = a(1 - \cos \theta)$ , the distance O moves down for rotation  $\theta$ 

$$y_P = y_O + s$$

 $\therefore y_P = a\theta + a(1 - \cos\theta)$  is the distance P moves down for rotation  $\theta$ 

Then

$$\delta y_P = (a + a\sin\theta)\delta\theta$$

Now, by the Law of Cosines

$$L_{SP}^2 = (4a)^2 + (2a)^2 - 2(4a)(2a)\cos\theta$$

or

$$L_{SR} = 2a\sqrt{5 - 4\cos\theta}$$

Then

$$\delta L_{SP} = 2a \frac{4\sin\theta}{2\sqrt{5 - 4\cos\theta}} \delta\theta$$
$$= \frac{4a\sin\theta}{\sqrt{5 - 4\cos\theta}} \delta\theta$$

Finally

$$F_{SP} = k \left[ L_{SP} - \left( L_{SP} \right)_0 \right]$$
$$= k \left( 2a\sqrt{5 - 4\cos\theta} - 2a \right)$$
$$= 2ka \left( \sqrt{5 - 4\cos\theta} - 1 \right)$$

Thus, by Virtual Work:  $\delta U = 0$ :  $P\delta y_P - F_{SP}\delta L_{SP} = 0$ 

# **PROBLEM 10.44 CONTINUED**

or

$$Pa(1+\sin\theta)\delta\theta - 2ka(\sqrt{5-4\cos\theta}-1)\left(\frac{4a\sin\theta}{\sqrt{5-4\cos\theta}}\delta\theta\right) = 0$$

or

$$\left[\frac{P}{8ka}(1+\sin\theta) - \sin\theta\right]\sqrt{5-4\cos\theta} + \sin\theta = 0$$

Substituting given values:

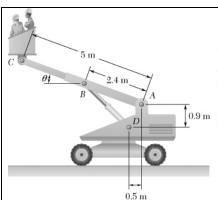
$$\left[\frac{48 \text{ N}}{8(3000 \text{ N/m})(0.15 \text{ m})}(1+\sin\theta) - \sin\theta\right] \sqrt{5-4\cos\theta} + \sin\theta = 0$$

or

$$\left[\frac{1}{75}(1+\sin\theta)-\sin\theta\right]\sqrt{5-4\cos\theta}+\sin\theta=0$$

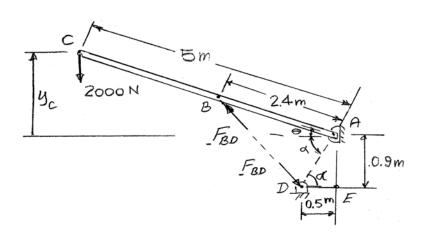
Solving numerically,

$$\theta = 15.27^{\circ}$$



The telescoping arm ABC is used to provide an elevated platform for construction workers. The workers and the platform together have a mass of 204 kg, and their combined center of gravity is located directly above C. For the position when  $\theta = 20^{\circ}$ , determine the force exerted on pin B by the single hydraulic cylinder BD.

# **SOLUTION**



In  $\triangle ADE$ :

$$\tan \alpha = \frac{AE}{DE} = \frac{0.9 \text{ m}}{0.5 \text{ m}}$$
$$\alpha = 60.945^{\circ}$$
$$AD = \frac{0.9 \text{ m}}{\sin 60.945^{\circ}} = 1.0296 \text{ m}$$

From the geometry:

$$y_C = (5 \text{ m})\sin\theta, \qquad \delta y_C = (5 \text{ m})\cos\theta\delta\theta$$

Then, in triangle *BAD*: Angle  $BAD = \alpha + \theta$ 

Law of Cosines:

$$BD^{2} = AB^{2} + AD^{2} - 2(AB)(AD)\cos(\alpha + \theta)$$

$$BD^{2} = (2.4 \text{ m})^{2} + (1.0296 \text{ m})^{2} - 2(2.4 \text{ m})(1.0296 \text{ m})\cos(\alpha + \theta)$$

$$BD^{2} = 6.82 \text{ m}^{2} - (4.942\cos(\alpha + \theta)) \text{ m}^{2}$$
(1)

or

# **PROBLEM 10.45 CONTINUED**

And then

$$2(BD)(\delta BD) = (4.942\sin(\alpha + \theta))\delta\theta$$
$$\delta BD = \frac{4.942\sin(\alpha + \theta)}{2(BD)}\delta\theta$$

Virtual work:

$$\delta U = 0$$
:  $-P\delta y_C + F_{BD}\delta BD = 0$  Substituting  $-(2000 \text{ N})(5 \text{ m})\cos\theta\delta\theta + F_{BD}\delta\theta$ 

or

$$F_{BD} = \left[ 4047 \frac{\cos \theta}{\sin(\alpha + \theta)} BD \right] \text{N/m}$$
 (2)

Now, with  $\theta = 20^{\circ}$  and  $\alpha = 60.945^{\circ}$ 

Equation (1):

$$BD^2 = 6.82 - 4.942\cos(60.945^\circ + 20^\circ)$$
$$BD^2 = 6.042$$

$$BD = 2.46 \text{ m}$$

Equation (2)

$$F_{BD} = \left[ 4047 \frac{\cos 20^{\circ}}{\sin (60.945^{\circ} + 20^{\circ})} (2.46 \text{ m}) \right] \text{N/m}$$

or

$$F_{BD} = 9473 \text{ N}$$

$$\mathbf{F}_{BD} = 9.47 \text{ kN} \setminus \blacktriangleleft$$

Solve Problem 10.45 assuming that the workers are lowered to a point near the ground so that  $\theta = -20^{\circ}$ .

# **SOLUTION**

Using the figure and analysis of Problem 10.45, including Equations (1) and (2), and with  $\theta = -20^{\circ}$ , we have

Equation (1): 
$$BD^2 = 6.82 - 4.942\cos(60.945^\circ - 20^\circ)$$

$$BD^2 = 3.087$$

$$BD = 1.757 \text{ m}$$

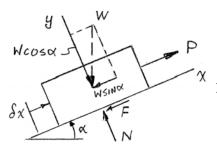
Equation (2): 
$$F_{BD} = 4047 \frac{\cos(-20^{\circ})}{\sin(60.945^{\circ} - 20^{\circ})} (1.757)$$

$$F_{BD} = 10196 \text{ N}$$

or  $\mathbf{F}_{BD} = 10.20 \text{ kN } \setminus \blacktriangleleft$ 

A block of weight W is pulled up a plane forming an angle  $\alpha$  with the horizontal by a force  $\mathbf{P}$  directed along the plane. If  $\mu$  is the coefficient of friction between the block and the plane, derive an expression for the mechanical efficiency of the system. Show that the mechanical efficiency cannot exceed  $\frac{1}{2}$  if the block is to remain in place when the force  $\mathbf{P}$  is removed.

# **SOLUTION**



Input work = 
$$P\delta x$$

Output work = 
$$(W \sin \alpha) \delta x$$

Efficiency:

$$\eta = \frac{W \sin \alpha \delta x}{P \delta x}$$
 or  $\eta = \frac{W \sin \alpha}{P}$  (1)

$$+/\sum \Sigma F_x = 0$$
:  $P - F - W \sin \alpha = 0$  or  $P = W \sin \alpha + F$  (2)

$$+ \sum F_y = 0$$
:  $N - W \cos \alpha = 0$  or  $N = W \cos \alpha$ 

$$F = \mu N = \mu W \cos \alpha$$

Equation (2): 
$$P = W \sin \alpha + \mu W \cos \alpha = W (\sin \alpha + \mu \cos \alpha)$$

Equation (1): 
$$\eta = \frac{W \sin \alpha}{W(\sin \alpha + \mu \cos \alpha)}$$
 or  $\eta = \frac{1}{1 + \mu \cot \alpha} \blacktriangleleft$ 

If block is to remain in place when P=0, we know (see page 416) that  $\phi_s \geq \alpha$  or, since

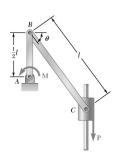
$$\mu = \tan \phi_s, \qquad \mu \ge \tan \alpha$$

Multiply by 
$$\cot \alpha$$
:  $\mu \cot \alpha \ge \tan \alpha \cot \alpha = 1$ 

Add 1 to each side: 
$$1 + \mu \cot \alpha \ge 2$$

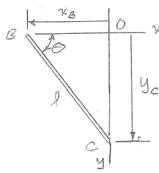
Recalling the expression for 
$$\eta$$
, we find

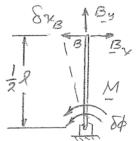
$$\eta \leq \frac{1}{2} \blacktriangleleft$$

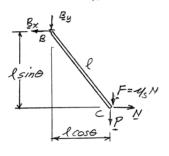


Denoting by  $\mu_s$  the coefficient of static friction between collar C and the vertical rod, derive an expression for the magnitude of the largest couple  $\mathbf{M}$  for which equilibrium is maintained in the position shown. Explain what happens if  $\mu_s \geq \tan \theta$ .

# **SOLUTION**







Member BC: Have

$$x_B = l\cos\theta$$

$$\delta x_B = -l\sin\theta\delta\theta\tag{1}$$

and  $y_C = l \sin \theta$ 

$$\delta y_C = l\cos\theta\delta\theta \tag{2}$$

Member AB: Have

$$\delta x_B = \frac{1}{2} l \delta \phi$$

Substituting from Equation (1),

$$-l\sin\theta\delta\theta = \frac{1}{2}l\delta\phi$$

or

$$\delta\phi = -2\sin\theta\delta\theta\tag{3}$$

Free body of rod BC

For  $M_{\text{max}}$ , motion of collar C impends upward

+) 
$$\Sigma M_B = 0$$
:  $Nl\sin\theta - (P + \mu_s N)(l\cos\theta) = 0$   
 $N\tan\theta - \mu_s N = P$   

$$N = \frac{P}{\tan\theta - \mu_s}$$

Virtual Work

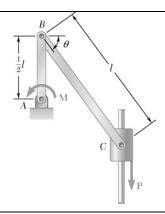
$$\delta U = 0: \quad M \, \delta \phi + (P + \mu_s N) \, \delta y_C = 0$$
$$M \left( -2\sin\theta \delta \theta \right) + (P + \mu_s N) l \cos\theta \delta \theta = 0$$

$$M_{\text{max}} = \frac{\left(P + \mu_s N\right)}{2 \tan \theta} l = \frac{P + \mu_s \frac{P}{\tan \theta - \mu_s}}{2 \tan \theta} l$$

or

$$M_{\text{max}} = \frac{Pl}{2(\tan\theta - \mu_s)} \blacktriangleleft$$

If  $\mu_s = \tan \theta$ ,  $M = \infty$ , system becomes *self-locking* 



Knowing that the coefficient of static friction between collar C and the vertical rod is 0.40, determine the magnitude of the largest and smallest couple **M** for which equilibrium is maintained in the position shown when  $\theta = 35^{\circ}$ , l = 30 in., and P = 1.2 kips.

# **SOLUTION**

From the analysis of Problem 10.48, we have

$$M_{\text{max}} = \frac{Pl}{2(\tan\theta + \mu_s)}$$

With

$$\theta = 35^{\circ}$$
,  $l = 30 \text{ in.}$ ,  $P = 1.25 \text{ kips}$ 

$$M_{\text{max}} = \frac{(1200 \text{ lb})(30 \text{ in.})}{2(\tan 35^{\circ} - 0.4)} = 59,958.5 \text{ lb} \cdot \text{in.}$$
$$= 4996.5 \text{ lb} \cdot \text{ft}$$
$$= 4.9965 \text{ kip} \cdot \text{ft}$$

 $M_{\text{max}} = 5.00 \text{ kip} \cdot \text{ft} \blacktriangleleft$ 

For  $M_{\min}$ , motion of C impends downward and F acts upward. The equations of Problem 10.48 can still be used if we replace  $\mu_s$  by  $-\mu_s$ . Then

$$M_{\min} = \frac{Pl}{2(\tan\theta + \mu_s)}$$

Substituting,

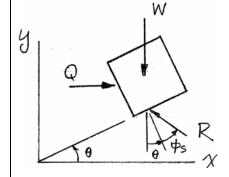
$$M_{\min} = \frac{(1200 \text{ lb})(30 \text{ in.})}{2(\tan 35^{\circ} + 0.4)} = 16,360.5 \text{ lb} \cdot \text{in.}$$
$$= 1363.4 \text{ lb} \cdot \text{ft}$$
$$= 1.3634 \text{ kip} \cdot \text{ft}$$

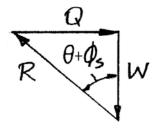
 $M_{\min} = 1.363 \text{ kip} \cdot \text{ft} \blacktriangleleft$ 

Derive an expression for the mechanical efficiency of the jack discussed in Section 8.6. Show that if the jack is to be self-locking, the mechanical efficiency cannot exceed  $\frac{1}{2}$ .

# **SOLUTION**

Recall Figure 8.9a. Draw force triangle





$$Q = W \tan(\theta + \phi_s)$$

$$y = x \tan \theta$$
 so that  $\delta y = \delta x \tan \theta$ 

Input work = 
$$Q\delta x = W \tan(\theta + \phi_s)\delta x$$

Output work = 
$$W \delta y = W(\delta x) \tan \theta$$

$$\eta = \frac{W \tan \theta \delta x}{W \tan (\theta + \phi_s) \delta x}; \qquad \eta = \frac{\tan \theta}{\tan (\theta + \phi_s)} \blacktriangleleft$$

$$\eta = \frac{\tan \theta}{\tan(\theta + \phi_s)} \blacktriangleleft$$

From page 432, we know the jack is self-locking if

$$\phi_{\rm s} \geq \theta$$

Then

$$\theta + \phi_s \ge 2\theta$$

so that

$$\tan(\theta + \phi_s) \ge \tan 2\theta$$

From above

$$\eta = \frac{\tan \theta}{\tan (\theta + \phi_s)}$$

It then follows that

$$\eta \le \frac{\tan \theta}{\tan 2\theta}$$

But

$$\tan 2\theta = \frac{2\tan\theta}{1-\tan^2\theta}$$

Then

$$\eta \le \frac{\tan \theta \left(1 - \tan^2 \theta\right)}{2 \tan \theta} = \frac{1 - \tan^2 \theta}{2}$$

$$\therefore \quad \eta \leq \frac{1}{2} \blacktriangleleft$$