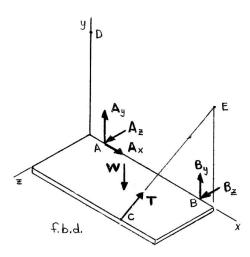


Solve Problem 4.126 assuming that cable DCE is replaced by a cable attached to point E and hook C.

**P4.126** A 285-lb uniform rectangular plate is supported in the position shown by hinges A and B and by cable DCE, which passes over a frictionless hook at C. Assuming that the tension is the same in both parts of the cable, determine (a) the tension in the cable, (b) the reactions at A and B. Assume that the hinge at B does not exert any axial thrust.

## **SOLUTION**



First note

$$\lambda_{CE} = \frac{(9 \text{ in.})\mathbf{i} + (22.5 \text{ in.})\mathbf{j} - (15 \text{ in.})\mathbf{k}}{28.5 \text{ in.}}$$
$$= \frac{1}{28.5} (9\mathbf{i} + 22.5\mathbf{j} - 15\mathbf{k})$$
$$\mathbf{W} = -(285 \text{ lb})\mathbf{j}$$

From f.b.d. of plate

(a) 
$$\Sigma M_x = 0: \quad (285 \text{ lb})(7.5 \text{ in.}) - \left[ \left( \frac{22.5}{28.5} \right) T \right] (15 \text{ in.}) = 0$$

$$\therefore \quad T = 180.500 \text{ lb}$$

or  $T = 180.5 \text{ lb} \blacktriangleleft$ 

$$\Sigma F_x = 0: \quad A_x + T\left(\frac{9}{28.5}\right) = 0$$

$$A_x + 180.5 \text{ lb}\left(\frac{9}{28.5}\right) = 0$$

$$\therefore \quad A_x = -57.000 \text{ lb}$$

## **PROBLEM 4.127 CONTINUED**

$$\Sigma M_{B(z\text{-axis})} = 0: \quad -A_y (26 \text{ in.}) + W (13 \text{ in.}) - \left[ T \left( \frac{22.5}{28.5} \right) \right] (6 \text{ in.}) = 0$$

$$-A_y (26 \text{ in.}) + (285 \text{ lb}) (13 \text{ in.}) - \left[ (180.5 \text{ lb}) \left( \frac{22.5}{28.5} \right) \right] (6 \text{ in.}) = 0$$

$$\therefore A_y = 109.615 \text{ lb}$$

$$\Sigma M_{B(y\text{-axis})} = 0: \quad A_z \left(26 \text{ in.}\right) - \left[T\left(\frac{15}{28.5}\right)\right] \left(6 \text{ in.}\right) + \left[T\left(\frac{9}{28.5}\right)\right] \left(15 \text{ in.}\right) = 0$$

$$A_z \left(26 \text{ in.}\right) + \left(180.5 \text{ lb}\right) \left(\frac{45}{28.5}\right) = 0$$

$$A_z = -10.9615 \text{ lb}$$

or 
$$\mathbf{A} = -(57.0 \text{ lb})\mathbf{i} + (109.6 \text{ lb})\mathbf{j} - (10.96 \text{ lb})\mathbf{k} \blacktriangleleft$$

$$\Sigma F_y = 0$$
:  $B_y - W + T \left( \frac{22.5}{28.5} \right) + A_y = 0$ 

$$B_y - 285 \text{ lb} + (180.5 \text{ lb}) \left( \frac{22.5}{28.5} \right) - 109.615 \text{ lb} = 0$$

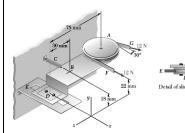
$$B_y = 32.885 \text{ lb}$$

$$\Sigma F_z = 0$$
:  $B_z + A_z - T\left(\frac{15}{28.5}\right) = 0$ 

$$B_z - 10.9615 \text{ lb} - 180.5 \text{ lb}\left(\frac{15}{28.5}\right) = 0$$

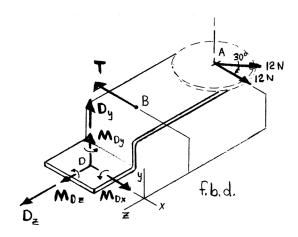
:. 
$$B_z = 105.962 \text{ lb}$$

or 
$$\mathbf{B} = (32.9 \text{ lb})\mathbf{j} + (106.0 \text{ lb})\mathbf{k} \blacktriangleleft$$



The tensioning mechanism of a belt drive consists of frictionless pulley A, mounting plate B, and spring C. Attached below the mounting plate is slider block D which is free to move in the frictionless slot of bracket E. Knowing that the pulley and the belt lie in a horizontal plane, with portion F of the belt parallel to the x axis and portion G forming an angle of  $30^{\circ}$  with the x axis, determine (a) the force in the spring, (b) the reaction at D.

## **SOLUTION**



From f.b.d. of plate B

(a) 
$$\Sigma F_x = 0$$
:  $12 \text{ N} + (12 \text{ N})\cos 30^\circ - T = 0$ 

$$T = 22.392 \text{ N}$$

or T = 22.4 N

$$(b) \Sigma F_{v} = 0: D_{v} = 0$$

$$\Sigma F_z = 0$$
:  $D_z - (12 \text{ N}) \sin 30^\circ = 0$ 

$$D_z = 6 \text{ N}$$

or **D** = 
$$(6.00 \text{ N})\mathbf{k}$$

$$\Sigma M_x = 0$$
:  $M_{D_x} - [(12 \text{ N})\sin 30^\circ](22 \text{ mm}) = 0$ 

$$M_{D_x} = 132.0 \text{ N} \cdot \text{mm}$$

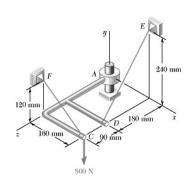
$$\Sigma M_{D(y\text{-axis})} = 0: \quad M_{D_y} + (22.392 \text{ N})(30 \text{ mm}) - (12 \text{ N})(75 \text{ mm}) - [(12 \text{ N})\cos 30^\circ](75 \text{ mm}) = 0$$

$$\therefore M_{D_y} = 1007.66 \text{ N} \cdot \text{mm}$$

$$\Sigma M_{D(z-\text{axis})} = 0: \quad M_{D_z} + (22.392 \text{ N})(18 \text{ mm}) - (12 \text{ N})(22 \text{ mm}) - [(12 \text{ N})\cos 30^\circ](22 \text{ mm}) = 0$$

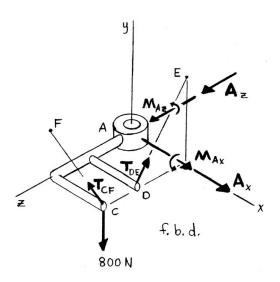
$$M_{D_z} = 89.575 \text{ N} \cdot \text{mm}$$

or 
$$\mathbf{M}_D = (0.1320 \text{ N} \cdot \text{m})\mathbf{i} + (1.008 \text{ N} \cdot \text{m})\mathbf{j} + (0.0896 \text{ N} \cdot \text{m})\mathbf{k} \blacktriangleleft$$



The assembly shown is welded to collar A which fits on the vertical pin shown. The pin can exert couples about the x and z axes but does not prevent motion about or along the y axis. For the loading shown, determine the tension in each cable and the reaction at A.

## **SOLUTION**



First note

or

$$\mathbf{T}_{CF} = \lambda_{CF} T_{CF} = \frac{-(0.16 \text{ m})\mathbf{i} + (0.12 \text{ m})\mathbf{j}}{\sqrt{(0.16)^2 + (0.12)^2} \text{ m}} T_{CF}$$

$$= T_{CF} (-0.8\mathbf{i} + 0.6\mathbf{j})$$

$$\mathbf{T}_{DE} = \lambda_{DE} T_{DE} = \frac{(0.24 \text{ m})\mathbf{j} - (0.18 \text{ m})\mathbf{k}}{\sqrt{(0.24)^2 + (0.18)^2} \text{ m}} T_{DE}$$

$$= T_{DE} (0.8\mathbf{j} - 0.6\mathbf{k})$$

(a) From f.b.d. of assembly

$$\Sigma F_y = 0$$
:  $0.6T_{CF} + 0.8T_{DE} - 800 \text{ N} = 0$   
 $0.6T_{CF} + 0.8T_{DE} = 800 \text{ N}$  (1)

 $\Sigma M_y = 0$ :  $-(0.8T_{CF})(0.27 \text{ m}) + (0.6T_{DE})(0.16 \text{ m}) = 0$ 

or 
$$T_{DE} = 2.25T_{CF}$$
 (2)

#### **PROBLEM 4.129 CONTINUED**

Substituting Equation (2) into Equation (1)

$$0.6T_{CF} + 0.8 \lceil (2.25)T_{CF} \rceil = 800 \text{ N}$$

$$T_{CF} = 333.33 \text{ N}$$

or 
$$T_{CF} = 333 \text{ N} \blacktriangleleft$$

and from Equation (2)

$$T_{DE} = 2.25(333.33 \text{ N}) = 750.00 \text{ N}$$

or 
$$T_{DE} = 750 \text{ N} \blacktriangleleft$$

(b) From f.b.d. of assembly

$$\Sigma F_z = 0$$
:  $A_z - (0.6)(750.00 \text{ N}) = 0$ 

$$\therefore A_z = 450.00 \text{ N}$$

$$\Sigma F_x = 0$$
:  $A_x - (0.8)(333.33 \text{ N}) = 0$   $\therefore A_x = 266.67 \text{ N}$ 

$$A_x = 266.67 \text{ N}$$

or 
$$\mathbf{A} = (267 \text{ N})\mathbf{i} + (450 \text{ N})\mathbf{k} \blacktriangleleft$$

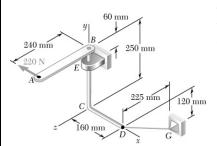
$$\Sigma M_x = 0$$
:  $M_{A_x} + (800 \text{ N})(0.27 \text{ m}) - [(333.33 \text{ N})(0.6)](0.27 \text{ m}) - [(750 \text{ N})(0.8)](0.18 \text{ m}) = 0$ 

$$\therefore M_{A_r} = -54.001 \,\mathrm{N} \cdot \mathrm{m}$$

$$\Sigma M_z = 0$$
:  $M_{A_z} - (800 \text{ N})(0.16 \text{ m}) + [(333.33 \text{ N})(0.6)](0.16 \text{ m}) + [(750 \text{ N})(0.8)](0.16 \text{ m}) = 0$ 

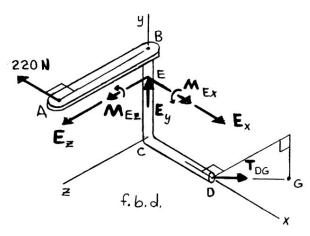
$$\therefore M_{A_7} = 0$$

or 
$$\mathbf{M}_A = -(54.0 \,\mathrm{N} \cdot \mathrm{m})\mathbf{i} \blacktriangleleft$$



The lever AB is welded to the bent rod BCD which is supported by bearing E and by cable DG. Assuming that the bearing can exert an axial thrust and couples about axes parallel to the x and z axes, determine (a) the tension in cable DG, (b) the reaction at E.

## **SOLUTION**



First note

$$\mathbf{T}_{DG} = \lambda_{DG} T_{DG} = \frac{-(0.12 \text{ m})\mathbf{j} - (0.225 \text{ m})\mathbf{k}}{\sqrt{(0.12)^2 + (0.225)^2} \text{ m}} T_{DG}$$
$$= \frac{T_{DG}}{0.255} (-0.12\mathbf{j} - 0.225\mathbf{k})$$

(a) From f.b.d. of weldment

$$\Sigma M_y = 0$$
:  $\left[ \left( \frac{0.225}{0.255} \right) T_{DG} \right] (0.16 \text{ m}) - (220 \text{ N})(0.24 \text{ m}) = 0$ 

$$T_{DG} = 374.00 \text{ N}$$

or 
$$T_{DG} = 374 \text{ N} \blacktriangleleft$$

(b) From f.b.d. of weldment

$$\Sigma F_x = 0$$
:  $E_x - 220 \text{ N} = 0$ 

$$E_x = 220.00 \text{ N}$$

$$\Sigma F_y = 0$$
:  $E_y - (374.00 \text{ N}) \left( \frac{0.12}{0.255} \right) = 0$ 

$$E_y = 176.000 \text{ N}$$

# **PROBLEM 4.130 CONTINUED**

$$\Sigma F_z = 0$$
:  $E_z - (374.00 \text{ N}) \left( \frac{0.225}{0.255} \right) = 0$ 

$$E_z = 330.00 \text{ N}$$

or 
$$\mathbf{E} = (220 \text{ N})\mathbf{i} + (176.0 \text{ N})\mathbf{j} + (330 \text{ N})\mathbf{k} \blacktriangleleft$$

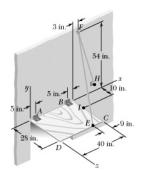
$$\Sigma M_x = 0$$
:  $M_{E_x} + (330.00 \text{ N})(0.19 \text{ m}) = 0$ 

$$\therefore M_{E_x} = -62.700 \text{ N} \cdot \text{m}$$

$$\Sigma M_z = 0$$
:  $(220 \text{ N})(0.06 \text{ m}) + M_{E_z} - \left[ (374.00 \text{ N}) \left( \frac{0.12}{0.255} \right) \right] (0.16 \text{ m}) = 0$ 

$$\therefore M_{E_z} = -14.9600 \text{ N} \cdot \text{m}$$

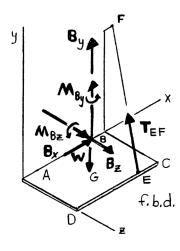
or 
$$\mathbf{M}_E = -(62.7 \text{ N} \cdot \text{m})\mathbf{i} - (14.96 \text{ N} \cdot \text{m})\mathbf{k} \blacktriangleleft$$



Solve Problem 4.124 assuming that the hinge at *A* is removed and that the hinge at *B* can exert couples about the *y* and *z* axes.

**P4.124** A small door weighing 16 lb is attached by hinges A and B to a wall and is held in the horizontal position shown by rope EFH. The rope passes around a small, frictionless pulley at F and is tied to a fixed cleat at H. Assuming that the hinge at A does not exert any axial thrust, determine (a) the tension in the rope, (b) the reactions at A and B.

#### SOLUTION



From f.b.d. of door

(a) 
$$\Sigma \mathbf{M}_{B} = 0: \quad \mathbf{r}_{G/B} \times \mathbf{W} + \mathbf{r}_{E/B} \times \mathbf{T}_{EF} + \mathbf{M}_{B} = 0$$

where

$$\mathbf{W} = -(16 \text{ lb})\mathbf{j}$$

$$\mathbf{M}_B = M_{B_{\mathbf{y}}}\mathbf{j} + M_{B_{\mathbf{z}}}\mathbf{k}$$

$$\mathbf{T}_{EF} = \lambda_{EF} T_{EF} = \frac{(12 \text{ in.})\mathbf{i} + (54 \text{ in.})\mathbf{j} - (28 \text{ in.})\mathbf{k}}{\sqrt{(12)^2 + (54)^2 + (28)^2}} T_{EF}$$
$$= \frac{T_{EF}}{31} (6\mathbf{i} + 27\mathbf{j} - 14\mathbf{k})$$

$$\mathbf{r}_{G/B} = -(15 \text{ in.})\mathbf{i} + (14 \text{ in.})\mathbf{k}$$

$$\mathbf{r}_{E/B} = -(4 \text{ in.})\mathbf{i} + (28 \text{ in.})\mathbf{k}$$

$$\begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ -15 & 0 & 14 \\ 0 & -1 & 0 \end{vmatrix} (16 \text{ lb}) + \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ -4 & 0 & 28 \\ 6 & 27 & -14 \end{vmatrix} \left( \frac{T_{EF}}{31} \right) + \left( M_{B_y} \mathbf{j} + M_{B_z} \mathbf{k} \right) = 0$$

or 
$$(224 - 24.387T_{EF})\mathbf{i} + (3.6129T_{EF} + M_{B_y})\mathbf{j}$$

$$+ \left(240 - 3.4839T_{EF} + M_{B_z}\right)\mathbf{k} = 0$$

From i-coefficient

$$224 - 24.387T_{EF} = 0$$

$$T_{FF} = 9.1852 \text{ lb}$$

or 
$$T_{FF} = 9.19 \text{ lb} \blacktriangleleft$$

$$3.6129(9.1852) + M_{B_v} = 0$$

$$\therefore M_{B_v} = -33.185 \text{ lb} \cdot \text{in}.$$

# **PROBLEM 4.131 CONTINUED**

From **k**-coefficient 
$$240 - 3.4839(9.1852) + M_{B_z} = 0$$

$$\therefore M_{B_z} = -208.00 \text{ lb} \cdot \text{in}.$$

or 
$$\mathbf{M}_B = -(33.2 \text{ lb} \cdot \text{in.})\mathbf{j} - (208 \text{ lb} \cdot \text{in.})\mathbf{k} \blacktriangleleft$$

$$\Sigma F_x = 0$$
:  $B_x + \frac{6}{31} (9.1852 \text{ lb}) = 0$ 

:. 
$$B_x = -1.77778 \text{ lb}$$

$$\Sigma F_y = 0$$
:  $B_y - 16 \text{ lb} + \frac{27}{31} (9.1852 \text{ lb}) = 0$ 

$$B_y = 8.0000 \text{ lb}$$

$$\Sigma F_z = 0$$
:  $B_z - \frac{14}{31} (9.1852 \text{ lb}) = 0$ 

:. 
$$B_z = 4.1482 \text{ lb}$$

or 
$$\mathbf{B} = -(1.778 \text{ lb})\mathbf{i} + (8.00 \text{ lb})\mathbf{j} + (4.15 \text{ lb})\mathbf{k} \blacktriangleleft$$

# PROBLEM 4.132 The frame shown is su

420 mm

420 mm

400 mm

60 mm

650 mm

650 mm

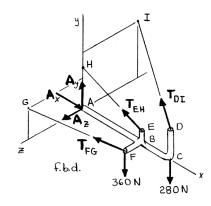
200 mm

320 mm

320 mm

The frame shown is supported by three cables and a ball-and-socket joint at A. For  $\mathbf{P} = 0$ , determine the tension in each cable and the reaction at A.

## **SOLUTION**



First note

$$\mathbf{T}_{DI} = \lambda_{DI} T_{DI} = \frac{-(0.65 \text{ m})\mathbf{i} + (0.2 \text{ m})\mathbf{j} - (0.44 \text{ m})\mathbf{k}}{\sqrt{(0.65)^2 + (0.2)^2 + (0.44)^2 \text{ m}}} T_{DI}$$

$$= \frac{T_{DI}}{0.81} (-0.65\mathbf{i} + 0.2\mathbf{j} - 0.44\mathbf{k})$$

$$\mathbf{T}_{EH} = \lambda_{EH} T_{EH} = \frac{-(0.45 \text{ m})\mathbf{i} + (0.24 \text{ m})\mathbf{j}}{\sqrt{(0.45)^2 + (0.24)^2 \text{ m}}} T_{EH}$$

$$= \frac{T_{EH}}{0.51} (-0.45\mathbf{i}) + (0.24 \text{ j})$$

$$\mathbf{T}_{FG} = \lambda_{FG} T_{FG} = \frac{-(0.45 \text{ m})\mathbf{i} + (0.2 \text{ m})\mathbf{j} + (0.36 \text{ m})\mathbf{k}}{\sqrt{(0.45)^2 + (0.2)^2 + (0.36)^2 \text{ m}}} T_{FG}$$

$$= \frac{T_{FG}}{0.61} (-0.45\mathbf{i} + 0.2\mathbf{j} + 0.36\mathbf{k})$$

From f.b.d. of frame

$$\Sigma \mathbf{M}_{A} = 0: \quad \mathbf{r}_{D/A} \times \mathbf{T}_{DI} + \mathbf{r}_{C/A} \times (-280 \text{ N}) \mathbf{j} + \mathbf{r}_{H/A} \times \mathbf{T}_{EH} + \mathbf{r}_{F/A} \times \mathbf{T}_{FG} + \mathbf{r}_{F/A} \times (-360 \text{ N}) \mathbf{j} = 0$$
or
$$\begin{vmatrix}
\mathbf{i} & \mathbf{j} & \mathbf{k} \\
0.65 & 0.2 & 0 \\
-0.65 & 0.2 & -0.44
\end{vmatrix} \begin{pmatrix}
\underline{T_{DI}} \\
0.81
\end{pmatrix} + \begin{vmatrix}
\mathbf{i} & \mathbf{j} & \mathbf{k} \\
0.65 & 0 & 0 \\
0 & -1 & 0
\end{vmatrix} \begin{pmatrix}
280 \text{ N} \\
-0.45 & 0.24 & 0
\end{vmatrix} \begin{pmatrix}
\underline{T_{EH}} \\
0.51
\end{pmatrix} + \begin{vmatrix}
\mathbf{i} & \mathbf{j} & \mathbf{k} \\
0.45 & 0 & 0.06 \\
-0.45 & 0.2 & 0.36
\end{vmatrix} \begin{pmatrix}
\underline{T_{FG}} \\
0.61
\end{pmatrix}$$

$$+ \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ 0.45 & 0 & 0.06 \\ 0 & -1 & 0 \end{vmatrix} (360 \text{ N}) = 0$$

or 
$$(-0.088\mathbf{i} + 0.286\mathbf{j} + 0.26\mathbf{k})\frac{T_{DI}}{0.81} + (-0.65\mathbf{k})280 \text{ N} + (0.144\mathbf{k})\frac{T_{EH}}{0.51} + (-0.012\mathbf{i} - 0.189\mathbf{j} + 0.09\mathbf{k})\frac{T_{FG}}{0.61} + (0.06\mathbf{i} - 0.45\mathbf{k})(360 \text{ N}) = 0$$

#### **PROBLEM 4.132 CONTINUED**

From **i**-coefficient 
$$-0.088 \left( \frac{T_{DI}}{0.81} \right) - 0.012 \left( \frac{T_{FG}}{0.61} \right) + 0.06 \left( 360 \text{ N} \right) = 0$$

$$\therefore 0.108642T_{DI} + 0.0196721T_{FG} = 21.6 \tag{1}$$

From **j**-coefficient

$$0.286 \left( \frac{T_{DI}}{0.81} \right) - 0.189 \left( \frac{T_{FG}}{0.61} \right) = 0$$

$$T_{FG} = 1.13959T_{DI}$$
 (2)

From k-coefficient

$$0.26 \left(\frac{T_{DI}}{0.81}\right) - 0.65 \left(280 \text{ N}\right) + 0.144 \left(\frac{T_{EH}}{0.51}\right) + 0.09 \left(\frac{T_{FG}}{0.61}\right) - 0.45 \left(360 \text{ N}\right) = 0$$

$$\therefore 0.32099T_{DI} + 0.28235T_{EH} + 0.147541T_{FG} = 344 \text{ N}$$
 (3)

Substitution of Equation (2) into Equation (1)

$$0.108642T_{DI} + 0.0196721(1.13959T_{DI}) = 21.6$$

$$T_{DI} = 164.810 \text{ N}$$

or

$$T_{DI} = 164.8 \text{ N} \blacktriangleleft$$

Then from Equation (2)

$$T_{FG} = 1.13959(164.810 \text{ N}) = 187.816 \text{ N}$$

or

$$T_{FG} = 187.8 \text{ N} \blacktriangleleft$$

And from Equation (3)

$$0.32099(164.810 \text{ N}) + 0.28235T_{EH} + 0.147541(187.816 \text{ N}) = 344 \text{ N}$$

$$T_{FH} = 932.84 \text{ N}$$

or

$$T_{FH} = 933 \text{ N} \blacktriangleleft$$

The vector forms of the cable forces are:

$$\mathbf{T}_{DI} = \frac{164.810 \text{ N}}{0.81} (-0.65\mathbf{i} + 0.2\mathbf{j} - 0.44\mathbf{k})$$

$$= -(132.25 \text{ N})\mathbf{i} + (40.694 \text{ N})\mathbf{j} - (89.526 \text{ N})\mathbf{k}$$

$$\mathbf{T}_{EH} = \frac{932.84 \text{ N}}{0.51} (-0.45\mathbf{i} + 0.24\mathbf{j}) = -(823.09 \text{ N})\mathbf{i} + (438.98 \text{ N})\mathbf{j}$$

$$\mathbf{T}_{FG} = \frac{187.816 \text{ N}}{0.61} (-0.45\mathbf{i} + 0.2\mathbf{j} + 0.36\mathbf{k})$$

$$= -(138.553 \text{ N})\mathbf{i} + (61.579 \text{ N})\mathbf{j} + (110.842 \text{ N})\mathbf{k}$$

# **PROBLEM 4.132 CONTINUED**

Then, from f.b.d. of frame

$$\Sigma F_x = 0$$
:  $A_x - 132.25 - 823.09 - 138.553 = 0$ 

$$A_x = 1093.89 \text{ N}$$

$$\Sigma F_y = 0$$
:  $A_y + 40.694 + 438.98 + 61.579 - 360 - 280 = 0$ 

$$A_y = 98.747 \text{ N}$$

$$\Sigma F_z = 0$$
:  $A_z - 89.526 + 110.842 = 0$ 

$$A_z = -21.316 \text{ N}$$

or 
$$\mathbf{A} = (1094 \text{ N})\mathbf{i} + (98.7 \text{ N})\mathbf{j} - (21.3 \text{ N})\mathbf{k} \blacktriangleleft$$