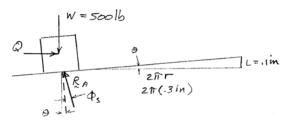
Assuming that in Problem 8.70 a right-handed thread is used on *both* rods *A* and *B*, determine the magnitude of the couple that must be applied to the sleeve in order to rotate it.

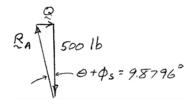
# **SOLUTION**

### Block on incline A:



$$\theta = \tan^{-1} \frac{0.1 \,\text{in.}}{2\pi (0.3 \,\text{in.})} = 3.0368^{\circ}$$

$$\phi_s = \tan^{-1} \mu_s = \tan^{-1} 0.12 = 6.8428^{\circ}$$

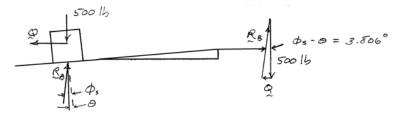


$$Q = (500 \,\mathrm{lb}) \tan 9.8796^{\circ}$$

$$= 87.08 \, lb$$

Couple at 
$$A = (0.3 \text{ in.})(87.08 \text{ lb})$$
  
= 26.124 lb·in.

### Block on incline *B*:



$$Q = (500 \text{ lb}) \tan 3.806^{\circ}$$

$$= 33.26 \, lb$$

Couple at 
$$B = (0.3 \text{ in.})(33.26 \text{ lb})$$

$$= 9.979 \, \text{lb} \cdot \text{in}$$
.

Total couple = 26.124 lb·in. + 9.979 lb·in.

Couple to turn =  $36.1 \, \text{lb} \cdot \text{in}$ .

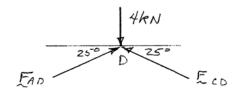
# A 25° B C M

### **PROBLEM 8.72**

The position of the automobile jack shown is controlled by a screw ABC that is single-threaded at each end (right-handed thread at A, left-handed thread at C). Each thread has a pitch of 2 mm and a mean diameter of 7.5 mm. If the coefficient of static friction is 0.15, determine the magnitude of the couple  $\mathbf{M}$  that must be applied to raise the automobile.

### SOLUTION

### FBD joint D:



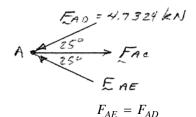
By symmetry:

$$F_{AD} = F_{CD}$$

$$\Sigma F_y = 0$$
:  $2F_{AD} \sin 25^\circ - 4 \text{ kN} = 0$ 

$$F_{AD} = F_{CD} = 4.7324 \text{ kN}$$

## FBD joint A:

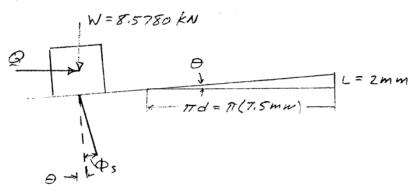


By symmetry:

$$\rightarrow \Sigma F_x = 0$$
:  $F_{AC} - 2(4.7324 \text{ kN})\cos 25^\circ = 0$ 

$$F_{AC} = 8.5780 \,\mathrm{kN}$$

### Block and incline A:



$$\theta = \tan^{-1} \frac{2 \text{ mm}}{\pi (7.5 \text{ mm})} = 4.8518^{\circ}$$

$$\phi_s = \tan^{-1} \mu_s = \tan^{-1} 0.15 = 8.5308^{\circ}$$

# **PROBLEM 8.72 CONTINUED**

$$Q = (8.578 \text{ kN}) \tan(13.3826^\circ)$$

 $= 2.0408 \, kN$ 

Couple at A: 
$$M_A = rQ$$

$$=\left(\frac{7.5}{2} \text{ mm}\right) (2.0408 \text{ kN})$$

 $M = 15.31 \,\mathrm{N} \cdot \mathrm{m} \blacktriangleleft$ 

 $= 7.653 \,\mathrm{N} \cdot \mathrm{m}$ 

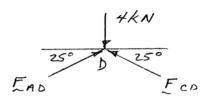
By symmetry: Couple at C:  $M_C = 7.653 \,\mathrm{N \cdot m}$ 

Total couple  $M = 2(7.653 \,\mathrm{N} \cdot \mathrm{m})$ 

For the jack of Problem 8.72, determine the magnitude of the couple **M** that must be applied to lower the automobile.

### **SOLUTION**

**FBD** joint *D*:



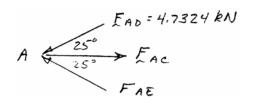
By symmetry:

$$F_{AD} = F_{CD}$$

$$\sum F_y = 0$$
:  $2F_{AD} \sin 25^\circ - 4 \text{ kN} = 0$ 

$$F_{AD} = F_{CD} = 4.7324 \text{ kN}$$

**FBD** joint *A*:



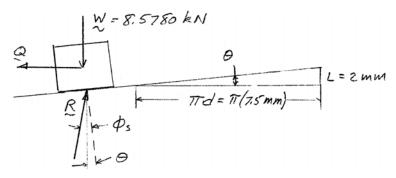
By symmetry:

$$F_{AE} = F_{AD}$$

$$\rightarrow \Sigma F_x = 0$$
:  $F_{AC} - 2(4.7324 \text{ kN})\cos 25^\circ = 0$ 

$$F_{AC} = 8.5780 \,\mathrm{kN}$$

### Block and incline at A:

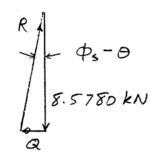


$$\theta = \tan^{-1} \frac{2 \text{ mm}}{\pi (7.5 \text{ mm})} = 4.8518^{\circ}$$

$$\phi_s = \tan^{-1} \mu_s = \tan^{-1} 0.15$$

$$\phi_{\rm s} = 8.5308^{\circ}$$

# **PROBLEM 8.73 CONTINUED**



$$\phi_s - \theta = 3.679^{\circ}$$

$$Q = (8.5780 \text{ kN}) \tan 3.679^{\circ}$$

$$Q=0.55156\,\mathrm{kN}$$

Couple at A:  $M_A = Qr$ 

$$= (0.55156 \, kN) \left( \frac{7.5 \, mm}{2} \right)$$

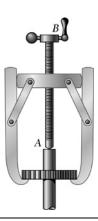
 $= 2.0683 \,\mathrm{N} \cdot \mathrm{m}$ 

By symmetry:

Couple at C:  $M_C = 2.0683 \text{ N} \cdot \text{m}$ 

Total couple  $M = 2(2.0683 \text{ N} \cdot \text{m})$ 

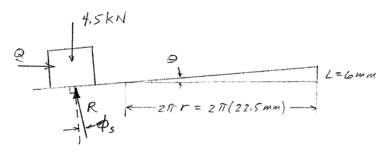
 $M = 4.14 \text{ N} \cdot \text{m} \blacktriangleleft$ 



In the gear-pulling assembly shown, the square-threaded screw AB has a mean radius of 22.5 mm and a lead of 6 mm. Knowing that the coefficient of static friction is 0.10, determine the couple which must be applied to the screw in order to produce a force of 4.5 kN on the gear. Neglect friction at end A of the screw.

### **SOLUTION**

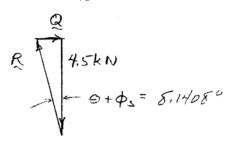
### **Block on incline:**



$$\theta = \tan^{-1} \frac{6 \text{ mm}}{2\pi (22.5 \text{ mm})} = 2.4302^{\circ}$$

$$\phi_s = \tan^{-1} \mu_s = \tan^{-1} 0.1$$

$$\phi_s = 5.7106^{\circ}$$



$$Q = (4.5 \text{ kN}) \tan 8.1408^{\circ}$$

$$= 0.6437 \text{ kN}$$

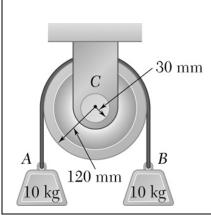
Couple 
$$M = rQ$$

$$= (22.5 \text{ mm})(0.6437 \text{ kN})$$

$$= 14.483 \text{ N} \cdot \text{m}$$

# **NOTE FOR PROBLEMS 8.75-8.89**

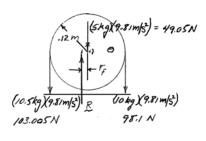
Note to instructors: In this manual, the singular  $\sin(\tan^{-1}\mu) \approx \mu$  is NOT used in the solution of journal bearing and axle friction problems. While this approximation may be valid for very small values of  $\mu$ , there is little if any reason to use it, and the error may be significant. For example, in Problems 8.76–8.79,  $\mu_s = 0.40$ , and the error made by using the approximation is about 7.7%.



A 120-mm-radius pulley of mass 5 kg is attached to a 30-mm-radius shaft which fits loosely in a fixed bearing. It is observed that the pulley will just start rotating if a 0.5-kg mass is added to block A. Determine the coefficient of static friction between the shaft and the bearing.

## **SOLUTION**

# FBD pulley:



$$\Sigma F_y = 0$$
:  $R - 103.005 \text{ N} - 49.05 \text{ N} - 98.1 \text{ N} = 0$ 

$$R = 250.155 \,\mathrm{N}$$

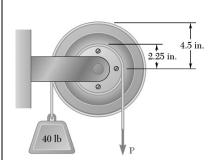
$$(\Sigma M_O = 0: (0.12 \text{ m})(103.005 \text{ N} - 98.1 \text{ N}) - r_f(250.155 \text{ N}) = 0$$

$$r_f = 0.0023529 \,\mathrm{m} = 2.3529 \,\mathrm{mm}$$

$$\phi_s = \sin^{-1} \frac{r_f}{r_s}$$

$$\mu_s = \tan \phi_s = \tan \left( \sin^{-1} \frac{r_f}{r_s} \right) = \tan \left( \sin^{-1} \frac{2.3529 \text{ mm}}{30 \text{ mm}} \right)$$

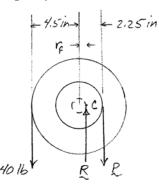
 $\mu_s = 0.0787 \blacktriangleleft$ 



The double pulley shown is attached to a 0.5-in.-radius shaft which fits loosely in a fixed bearing. Knowing that the coefficient of static friction between the shaft and the poorly lubricated bearing is 0.40, determine the magnitude of the force  $\bf P$  required to start raising the load.

# **SOLUTION**

FDB pulley:

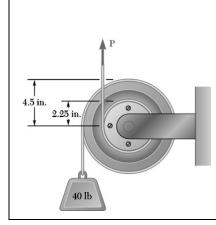


$$r_f = r_s \sin \phi_s = r_s \sin \left( \tan^{-1} \mu_s \right)^*$$

$$r_f = (0.5 \text{ in.}) \sin \left( \tan^{-1} 0.40 \right) = 0.185695 \text{ in.}$$

$$\left( \sum M_C = 0 : \left( 4.5 \text{ in.} + 0.185695 \text{ in.} \right) (40 \text{ lb}) - (2.25 \text{ in.} - 0.185695 \text{ in.}) P = 0$$

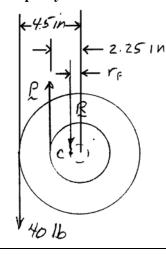
$$P = 90.8 \text{ lb} \blacktriangleleft$$



The double pulley shown is attached to a 0.5-in.-radius shaft which fits loosely in a fixed bearing. Knowing that the coefficient of static friction between the shaft and the poorly lubricated bearing is 0.40, determine the magnitude of the force **P** required to start raising the load.

# **SOLUTION**

# FBD pulley:

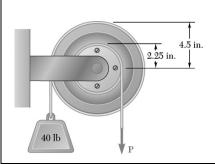


$$r_f = r_s \sin \phi_s = r_s \sin \left( \tan^{-1} \mu_s \right) = (0.5 \text{ in.}) \sin \left( \tan^{-1} 0.4 \right)^*$$

$$r_f = 0.185695 \text{ in.}$$

$$\left( \sum M_C = 0 : (4.5 \text{ in.} - 0.185695 \text{ in.}) (40 \text{ lb}) - (2.25 \text{ in.} - 0.185695 \text{ in.}) P = 0$$

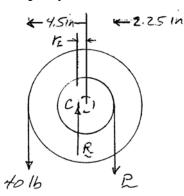
$$P = 83.6 \text{ lb} \blacktriangleleft$$



The double pulley shown is attached to a 0.5-in.-radius shaft which fits loosely in a fixed bearing. Knowing that the coefficient of static friction between the shaft and the poorly lubricated bearing is 0.40, determine the magnitude of the force **P** required to maintain equilibrium.

# **SOLUTION**

# FBD pulley:



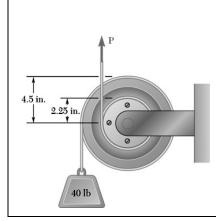
$$r_f = r_s \sin \phi_s = r_s \sin \left( \tan^{-1} \mu_s \right)^*$$

$$r_f = (0.5 \text{ in.})\sin(\tan^{-1}0.40) = 0.185695 \text{ in.}$$

$$(\Sigma M_C = 0: (4.5 \text{ in.} - 0.185695 \text{ in.})(40 \text{ lb})$$

$$-(2.25 \text{ in.} + 0.185695 \text{ in.})(P) = 0$$

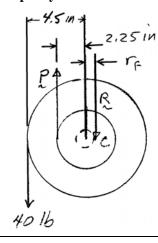
 $P = 70.9 \text{ lb} \blacktriangleleft$ 



The double pulley shown is attached to a 0.5-in.-radius shaft which fits loosely in a fixed bearing. Knowing that the coefficient of static friction between the shaft and the poorly lubricated bearing is 0.40, determine the magnitude of the force  $\bf P$  required to maintain equilibrium.

# **SOLUTION**

# FBD pulley:

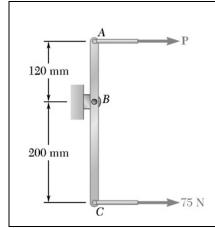


$$r_f = r_s \sin \phi_s = r_s \sin \left( \tan^{-1} \mu_s \right)^*$$

$$r_f = (0.5 \text{ in.}) \sin \left( \tan^{-1} 0.4 \right) = 0.185695 \text{ in.}$$

$$\left( \sum M_C = 0 : \left( 4.5 \text{ in.} + 0.185695 \text{ in.} \right) (40 \text{ lb}) - (2.25 \text{ in.} + 0.185695 \text{ in.}) P = 0$$

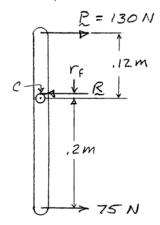
$$P = 77.0 \text{ lb} \blacktriangleleft$$



Control lever ABC fits loosely on a 18-mm-diameter shaft at support B. Knowing that  $P=130~\mathrm{N}$  for impending clockwise rotation of the lever, determine (a) the coefficient of static friction between the pin and the lever, (b) the magnitude of the force  $\mathbf{P}$  for which counterclockwise rotation of the lever is impending.

### **SOLUTION**

(a) **FBD lever** (Impending *CW* rotation):



$$(\Sigma M_C = 0: (0.2 \text{ m} + r_f)(75 \text{ N}) - (0.12 \text{ m} - r_f)(130 \text{ N}) = 0$$
  
 $r_f = 0.0029268 \text{ m} = 2.9268 \text{ mm}$ 

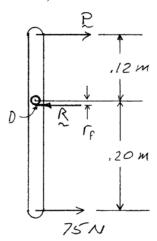
= 0.34389

$$\sin \phi_s = \frac{r_f}{r_s}$$

$$\mu_s = \tan \phi_s = \tan \left( \sin^{-1} \frac{r_f}{r_s} \right) = \tan \left( \sin^{-1} \frac{2.9268 \text{ mm}}{18 \text{ mm}} \right)^*$$

 $\mu_{\rm s} = 0.344$ 

(b) **FBD lever** (Impending *CCW* rotation):



$$(\Sigma M_D = 0: (0.20 \text{ m} - 0.0029268 \text{ m})(75 \text{ N})$$
  
 $-(0.12 \text{ m} + 0.0029268 \text{ m})P = 0$ 

 $P = 120.2 \text{ N} \blacktriangleleft$