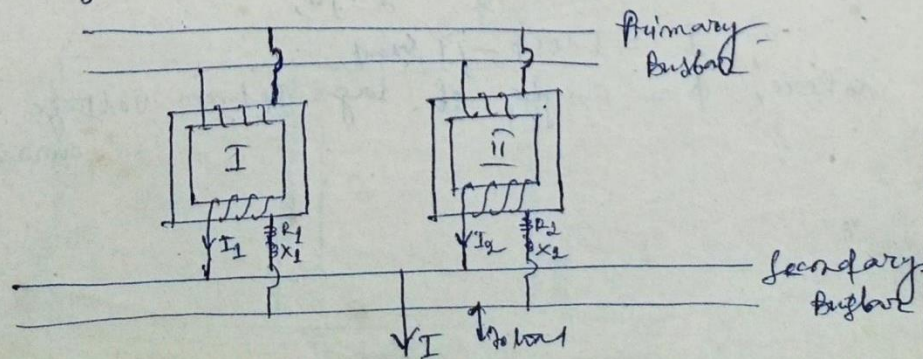


Parallel operation of Single phase transformers:-

For supplying a load in excess of the rating of an existing transformer, a second transformer may be connected in parallel with it.

Conditions for parallel operation are -

- (i) Primary windings of the transformers should be suitable for the supply system voltage and frequency.
- (ii) The transformers should be properly connected with regard to polarity.
- (iii) The voltage ratings of both primaries and secondaries should be identical.
- (iv) The percentage impedances should be equal in magnitude and have the same $\frac{X}{R}$ - ratio in order to avoid circulating currents and operation at different power factors.
- (v) With transformers having different KVA-ratings, the equivalent impedances should be inversely proportional to the individual KVA-rating if circulating currents are to be avoided.



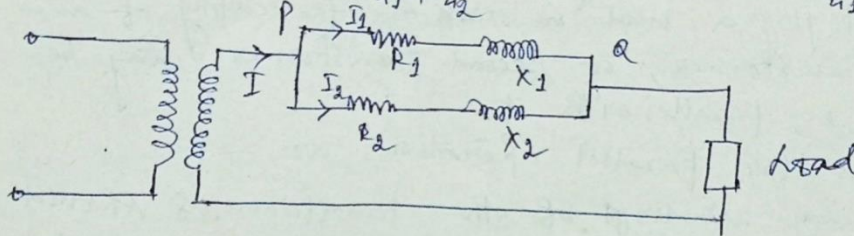
If the transformation ratios are same, the voltages across the secondary terminals will be the same. When these are connected to form a secondary bus, the voltage will not vary with the changing load.

If $\frac{R_1}{X_1} = \frac{R_2}{X_2}$, then I_1 and I_2 will be in phase.

R_1, X_1 and R_2, X_2 - are equivalent resistances, reactances of transformers I and II - respectively.

$$\frac{I_1}{I_2} = \frac{Z_2}{Z_1} \quad \text{and} \quad I_1 + I_2 = I$$

$$\therefore I_1 = \frac{Z_2}{Z_1 + Z_2} \cdot I \quad \text{and} \quad I_2 = \frac{Z_1}{Z_1 + Z_2} \cdot I$$



$$Z_1 = R_1 + jX_1 \quad \text{and} \quad Z_2 = R_2 + jX_2$$

Currents, $I_1 = x_1 + jy_1$ and $I_2 = x_2 + jy_2$.

Since, voltage drop across PQ are same,

$$(R_1 + jX_1)I_1 = (R_2 + jX_2)I_2$$

$$\text{and} \quad I_1 + I_2 = I$$

$$\therefore I_1 = \frac{(R_2 + jX_2) I}{(R_1 + R_2) + j(X_1 + X_2)}$$

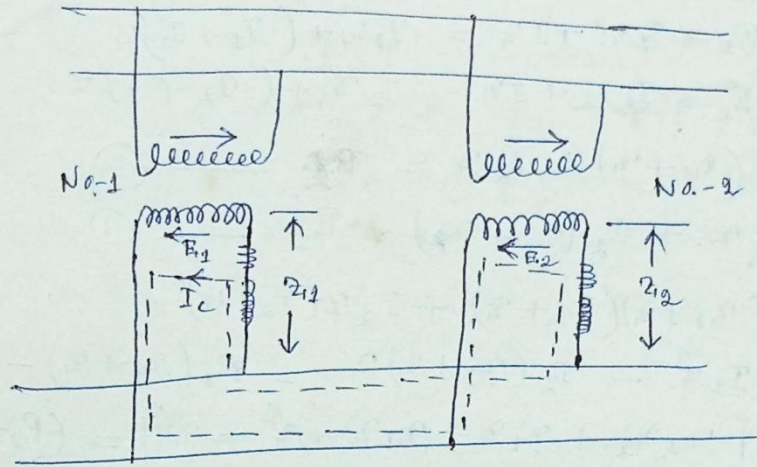
$$I_2 = \frac{(R_1 + jX_1) I}{(R_1 + R_2) + j(X_1 + X_2)}$$

Taking V_2 as secondary terminal voltage V_2 as reference vector, $V_2 = V_2 + j0$,

$$I = I \cos \phi - jI \sin \phi$$

where, ϕ = angle of lag between voltage and current.

Inequality of turns ratio:-



If the turns-ratios are not equal, the secondary induced e.m.f.s are not equal. The inequality will produce a circulating current which will flow even on no-load condition. On load, this circulating current will be super-imposed on the load currents.

Let, $E_1 > E_2$.

∴ Difference in voltage acting on the local circuit,

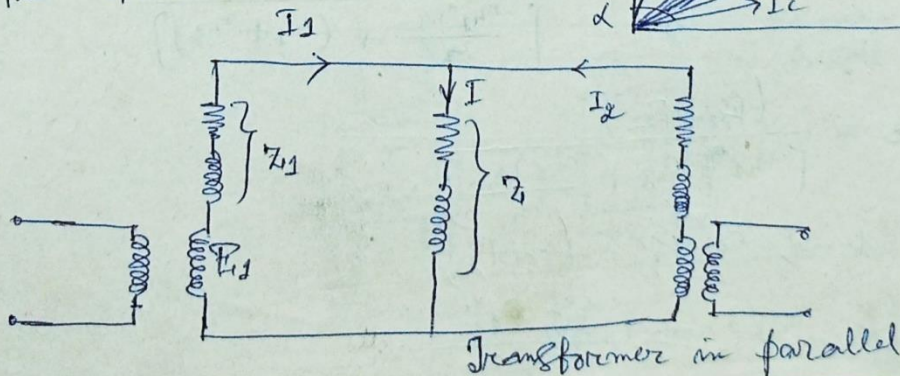
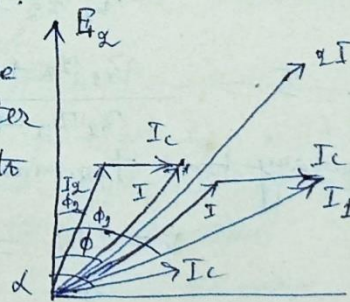
$$E_c = E_1 - E_2$$

$$I_c = \frac{E_1 - E_2}{Z_1 + Z_2}$$

This current will lag E_c by an angle α , where,

$$\alpha = \tan^{-1} \left(\frac{X_1 + X_2}{R_1 + R_2} \right)$$

It is seen that, the effect of circulating current is to reduce the power factor having the greater no-load induced e.m.f. and to increase the power factor of the other.



z_1, z_2 are transformer impedances
 z is the load impedance.

$$E_1 = I_1 z_1 + I z = I_1 z_1 + (I_1 + I_2) z$$

$$E_2 = I_2 z_2 + I z = I_2 z_2 + (I_1 + I_2) z$$

$$\therefore I_1 (z_2 + z) + I_2 z = E_1 \quad \text{--- (1)}$$

$$I_1 z + I_2 (z_1 + z) = E_2 \quad \text{--- (2)}$$

$$\therefore I_1 (z_1 + z)(z_2 + z) + I_2 z (z_2 + z) - I_1 z^2 - I_2 (z_2 + z) z = E_1 (z_2 + z) - E_2 z$$

$$\Rightarrow I_1 [z_1 z_2 + z_2 z + z_1 z + \cancel{z^2} - \cancel{z^2}] = (E_1 - E_2) z + E_1 z_2$$

$$\Rightarrow I_1 = \frac{E_1 z_2 + (E_1 - E_2) z}{z_1 z_2 + (z_1 + z_2) z}$$

$$I_1 (z_1 + z) z + I_2 z^2 - I_1 z (z_1 + z) - I_2 (z_2 + z) (z_1 + z) = E_1 z - E_2 (z_1 + z)$$

$$\Rightarrow I_2 [z_1 z_2 + z_1 z + z_2 z - \cancel{z^2}] = (E_1 - E_2) z - E_2 z_1$$

$$\Rightarrow I_2 = \frac{(E_1 - E_2) z - E_2 z_1}{z_1 z_2 + (z_1 + z_2) z}$$

$$= \frac{E_2 z_1 - (E_1 - E_2) z}{z_1 z_2 + (z_1 + z_2) z}$$

$$\therefore I = \frac{E_1 z_2 + E_2 z_1}{z_1 z_2 + (z_1 + z_2) z}$$

Secondary load terminal voltage

$$V = I z = \frac{(E_1 z_2 + E_2 z_1)}{\left[\frac{z_1 z_2}{z} + (z_1 + z_2) \right]}$$

$$I_c = \frac{(E_1 - E_2)}{\left[z_1 + z_2 + \frac{z_1 z_2}{z} \right]}$$

At no-load, z is infinity,

$$\therefore I_c = \frac{E_1 - E_2}{z_1 + z_2}$$