Constitutive modelling

CAM CLAY MODEL: NC SOIL

* Associated plastic flow rule

$$\dot{\varepsilon}_p = \Lambda \frac{\partial f}{\partial \delta}$$

Ép: plastic strain increment tensor

o': effective stress tensor

 Δ : plastic multiplier , >0, at the time of loading Δ = To express this isotropic nature of f_{ϕ} in a way that is easier to understand:

Mul 10 unausana: $\begin{cases}
\mathcal{E}_{v}^{P} = \Delta \frac{2f}{2p} \\
\text{Volumetric strain at critical}
\end{cases}$

state: $\dot{\varepsilon}_{\nu}^{p} = 0$ at q = Mp

Original Cam Clay: $\dot{\xi}_{V}^{P} = 0 \Rightarrow \frac{2f}{2p} = 0 \Leftrightarrow \begin{cases} f = \frac{-T+N}{V} \frac{q}{Mp} + \frac{\lambda - K}{V} \ln \frac{p}{p} - \xi^{p} \\ \frac{1}{V} \ln \frac{p}{Mp} + \frac{\lambda - K}{V} \ln \frac{p}{p} \end{cases}$

 $rac{N-T}{M} \left(\frac{-q}{p^2} \right) + \left(\lambda - K \right) \frac{1}{P} = 0$

 $N-T' = MP (\lambda - K)$ -9 - 1 $N-T = \lambda - K$

Modify Cam Clay: $\frac{\dot{\xi}^{P} = 0}{\partial p} = 0$ $\begin{cases}
f = \frac{1}{v} \left[\frac{N-\Gamma}{n_{2}} \ln \left\{ 1 + \left(\frac{q}{Mp} \right) \right\} + (\lambda - K) \ln \frac{q}{n_{2}} \right] + (\lambda - K) \ln \frac{q}{n_{2}} \\
\frac{N-\Gamma}{n_{2}} = 0
\end{cases}$ $\begin{cases}
\frac{N-\Gamma}{n_{2}}$

 $N-T = \ln 2 (\lambda - K)$ ET