

# Nuclear radius parameters ( $r_0$ ) for even-even nuclei from alpha decay

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The decay data for 186 even-even alpha emitters have been analyzed, and used as input in the ALPHAD code to extract nuclear radius parameters ( $r_0$ ) for the daughter nuclides. The ALPHAD code employs Preston's spin-independent formalism to calculate alpha decay probabilities. A suite of databases available at the website of the National Nuclear Data Center (NNDC), Brookhaven National Laboratory was consulted to ensure the completeness and reliability of available experimental data pertaining to alpha decays of all the even-even nuclides in the entire nuclear landscape. The literature available up to June 2020 has been consulted. In addition to updating  $Q_\alpha$  values, half-lives, and other relevant quantities for all the even-even alpha emitters, 26 new even-even alpha emitters, and 164 references published since 1997, mostly in primary nuclear physics journals, have been added to the previous evaluation by Y.A. Akovali [1] in 1998, with a literature cutoff date of January 1997. We also present systematics of  $r_0$  parameters for even-even nuclides, and find that the radius chain parameters in an isotopic chain exhibit a regular pattern as a function of parent neutron number, showing a minimum at major closed shells, e.g. at  $N=126$ , increasing sharply above the closed shells, followed by a smoothly decreasing trend towards the next shell closure. The  $r_0$  parameters for even-even nuclides can be used as input parameters to calculate hindrance factors for the alpha decay of odd-A and odd-odd nuclides. We have also modified the original ALPHAD code so that the  $r_0$  parameters for the odd-A and the odd-odd nuclei can be automatically calculated using the present data file for  $r_0$  parameters of even-even daughter nuclides.

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### I. INTRODUCTION

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### VI. EXPLANATION AND POLICIES OF TABLE II

1 Preston's spin-independent formulation of 1947 [2] is  
2 one of the original theoretical frameworks proposed to  
3 explain and quantify alpha radioactivity. This model  
3 was formulated by considering a preformed alpha par-  
3 ticle inside a nucleus having a rectangular potential well  
3 of depth  $V_0$ , where  $V_0 = \text{constant}$  for  $r < r_0$ ,  $r$  is the dis-  
3 tance from the center of the daughter nucleus and  $r_0$  is  
3 the radius of the daughter nucleus [2]. The field beyond  
3 an effective nuclear radius was assumed to be generated  
3 by a Coulomb potential ( $2Ze^2/r$ , where  $Z$  is the atomic  
3 number of the daughter nucleus and  $e$  is the elementary  
3 charge) between the alpha particle and the daughter nu-  
15 cleus. The radius parameter calculated in the present  
15 study is related to nuclear radius  $R = r_0 A^{1/3}$ ; however,  
17 this calculated value of  $r_0$  parameter lies in the range of  
17 1.4–1.6  $fm$ , which is different from the generally accepted  
17 value of 1.2  $fm$ . The difference may be due to constrain-  
17 ing the alpha hindrance factor of 1.0 for the ground-state  
17 to ground-state alpha transitions in even-even nuclei [1].

Accessibility of high-performance computing resources and refinements in the nuclear potential has led to various macroscopic approaches, such as cluster models [3–7], generalized liquid drop model [8, 9], unified fission

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model [10], density dependent M3Y effective interaction [11–14], etc., which have been employed to calculate theoretical half-lives for alpha emitters in various mass regions, all the way up to the heaviest nuclei experimentally discovered so far. Additionally, some microscopic approaches based on the shell model and fission models [13–17] have also been used to analyze alpha decay data. Semi-empirical formulations proposed by Viola and Seaborg [18], Royer [19, 20], Parkhomenko and Sobiczewski [21], and others [22–27] have been successfully employed to analyze alpha-decay energies to reproduce experimental  $\alpha$ -decay half-lives of heavy and superheavy nuclei. The calculated alpha-decay energies ( $Q_\alpha$ ) and theoretical half-lives ( $T_{1/2}$ ) using above-mentioned approaches generally depend on the fitting procedures, tuning of the nuclear potential, and associated adjustable parameters; hence, we do not prefer these theoretical  $Q_\alpha$  and  $T_{1/2}$  values in the present analysis of nuclear radius parameters ( $r_0$ ).

Rasmussen [28] derived a more realistic potential using optical model analysis of elastic scattering data, and calculated barrier penetration factors by numerical integration in the WKB approximation. The model potential includes centrifugal barrier effects but ignores the non-central component of nuclear interactions. This approach is adopted by many researchers to deduce experimental reduced  $\alpha$ -decay widths relative to the ground state to ground state  $\alpha$ -transitions in even-even and odd-A nuclei [29–31]. These reduced widths exhibit similar patterns at major shell closures as shown by the nuclear radius parameters obtained by us (see e.g., Fig. 1). Although alpha decay widths deduced from Rasmussen’s approach [28] exhibit the same pattern as shown by the radius parameters, the validity of this approach depends upon the nature of the potential (beyond the outermost turning point) [32] and range of mean lifetime ( $\tau$ ) [32, 33], which prompted us to keep Preston’s spin-independent formulation [2], as in the previous review by Y.A. Akovali [1].

The  $r_0$  parameters calculated in the present study can further be used to deduce the hindrance factors (HFs) - the ratio of experimental to theoretical partial half-lives of given alpha transitions. The alpha transitions for which HFs lie between 1 and 4 are called favored transitions, and take place between nuclear states having similar configurations, and hence, these HFs can be used to ascertain spin-parity assignments for a given daughter (parent) state if those of the parent (daughter) are known [34]. Additionally, the systematics of alpha-decay HFs can be used to deduce a variety of quantities such as total alpha branching, intensities of unobserved alpha groups, excitation energy of the level fed in daughter nucleus, and nuclear structure characteristics, but such a study is outside the scope of the present work.

## II. METHODOLOGY AND RESULTS

In the present study, the spin-independent part of Preston’s equations [2] are used for the alpha decay probabilities. This formalism contains the radius of the daughter nuclide,  $r_0$ , as a free parameter [2, 35]. By setting HF=1 for the ground-state to ground-state alpha branch for an even-even nuclide [1], the radius parameter for the daughter nuclide can be extracted.

In order to deduce  $r_0$  parameters, the Evaluated Nuclear Structure Data File (ENSDF) analysis code ALPHAD [36] was used, which also calculates theoretical half-lives and Hindrance Factors (HFs) for excited states  $\alpha$ -branches by assuming HF=1.0 for ground-state to ground-state  $\alpha$  transitions [2]. The experimental quantities required to calculate  $r_0$  parameter using this program are: energy available for  $\alpha$ -decay ( $Q_\alpha$ ), half-life ( $T_{1/2}$ ) of the parent nuclide, branching ratio ( $\% \alpha$ ) for alpha-decay mode, and alpha intensity ( $I_\alpha$ ) for ground-state to ground-state  $\alpha$ -transition. The ENSDF, eXperimental Unevaluated Nuclear Data List (XUNDL), Nuclear Science References (NSR), and NUBASE-2016 databases [37–39] were consulted to ensure that, in our input data files, we have covered all the relevant and available experimental data for the quantities listed above to current date.

The deduced  $r_0$  parameters for 186 even-even alpha decays (ground state to ground state) are presented in Table I, including 26 new even-even alpha emitters added to the previous evaluation [1], while the details of the evaluated quantities and deduced radius parameters are provided in Table II. It should be pointed out that for the reported  $^{104}\text{Te}$  alpha decay [40] to  $^{100}\text{Sn}$ , the  $T_{1/2}$  ( $< 18$  ns) is given as an upper limit, with no estimate of a lower bound, so the calculated radius parameter for the upper limit  $T_{1/2} = 18$  ns is  $> 1.77$  fm. Moreover, a recent experimental study [41] casts doubt on the existence of this decay mode as they could assign only two tentative events to the  $^{108}\text{Xe} \rightarrow ^{104}\text{Te} \rightarrow ^{100}\text{Sn}$  decay chain in their experiment, and  $T_{1/2}$  ( $< 4$  ns) for  $^{104}\text{Te}$   $\alpha$  decay. For the  $^{198}\text{Hg}$  and the  $^{106}\text{Sn}$  daughter nuclides, the values of  $\% \alpha = 7.6 \times 10^{-4}$  [42] (for  $^{106}\text{Sn}$ ) and  $< 1$  [43] (for  $^{198}\text{Hg}$ ) are not experimental values, and calculated radius parameters 1.604(41) fm for  $^{106}\text{Sn}$  and 1.510 fm for  $^{198}\text{Hg}$  are based on  $\% \alpha = 7.6 \times 10^{-4}$  and  $\% \alpha = 1$ , respectively. Due to the tentative nature of the deduced radius parameters for these three nuclei, these values are not included in Table I, Table II, and the systematics presented in Fig. 1 and Figs. 2–6.

Global systematics of  $r_0$  parameters with neutron number of parents for different nuclides are presented in Fig. 1, and by Z number of parents in Figs. 2–6. These figures show that the radius parameters lie on fairly smooth curves with exceptions at major and minor shell closures. In other words, the calculated  $r_0$  parameters for all the daughter nuclides decrease gradually with increasing parent neutron number between neighboring closed shells, exhibiting a minimum at  $N(\text{parent})=126$  (a major shell

closure), and increase thereafter, decreasing again toward the next major shell. Fig. 1 clearly shows that there is a shallow minimum at  $N(\text{parent})=152$ , which indicates a minor shell closure, consistent with the recent mapping of  $N=152$  shell effects in Ref. [42].

### III. DISCUSSION

It is appropriate to discuss the behavior of the deformed actinides from Th to Cf parent nuclei, as shown in Fig. 7. Thorium isotopes touch  $N(\text{parent})=126$  on the extreme left and show a sharp dip at  $N(\text{parent})=126$ , as expected. However, the behavior of these nuclides from Th to Cf after  $N(\text{parent})=126$  is different and interesting. These isotopic chains display a sequence of minima, not all of them accessible in each chain of the isotopes. But the Th, U and Pu isotopes display two minima, which keep shifting by two neutrons to the right. These minima lie at  $N=134$  and  $140$  for Th, at  $N=136$  and  $142$  for U, and at  $N=138$  and  $144$  for Pu. Due to large error bars at  $N=138$  minimum of Pu (Fig. 7), this minimum is questionable but  $N=144$  is a definite minimum. Thereafter, Pu and Cm have a minimum at  $N=150$ , and Fm, Cf at  $N=152$ . It is, therefore, clear that the much discussed  $N=152$  minimum is also a transient minimum. This behavior of shifting minima for these heavy nuclides is interesting and, in our view, has not yet been explored in the literature and explained on the basis of theoretical considerations.

For light lead isotopes, whether  $Z=82$  is a good magic number or not remains an open question in the literature [3, 30, 43, 44]. On the basis of shell model calculations, Wauters *et al.* [30] showed that  $Z=82$  is a good magic number, but on the other hand Buck *et al.* [3, 43] and Brown [44] suggested the disappearance of  $Z=82$  shell closure. In order to investigate the magicity of  $Z=82$  proton shell closure, we present in Fig. 8 the systematics of the  $r_0$  parameter as a function of parent proton number for six isotonic chains with parent neutron numbers  $N=102, 104, 106, 108, 110$  and  $112$ . This figure shows that the isotonic chains with  $N=104, 106$  and  $112$  exhibit a minimum at  $Z=82$ , which indicates the role of  $Z=82$  proton shell closure, consistent with the shell model prediction of Wauters *et al.* [30]. However, the shell effect at  $Z=82$  disappears for the isotonic chains with  $N=102, 108$  and  $110$  as suggested by Buck *et al.* [3, 43] and Brown [44]. Further calculations are required to elucidate the issue of the  $Z=82$  proton shell closure.

### IV. ALPHAD.RadD CODE

As discussed above, in the present study, radius parameters of even-even alpha emitters were calculated using Preston's formula for alpha decay transition probabilities [2, 35] and using the analysis code ALPHAD [36]. The evaluated radius parameters from Table I can further

be used to deduce  $r_0$  parameters of odd-A and odd-odd nuclides by interpolation or extrapolation as discussed by M.J. Martin [45]. The evaluated radius parameters can be used to deduce hindrance factors for alpha-fed excited states in even-even nuclides and for alpha-fed ground and excited states in odd-A and odd-odd nuclides, all relative to  $HF=1$  for the even-even ground-state alpha branch, which provide tools to extract spectroscopic information about spins and parities of nuclear states, as well as rotational band structures in deformed nuclei.

The original program ALPHAD [36] has been extended to automatically deduce the radius parameters and calculate the corresponding hindrance factors for the odd-A and odd-odd nuclides using the  $r_0$  values from Table I. The new program is ALPHAD.RadD [46]. Additionally, the code provides an option of inputting a user-supplied radius parameter.

### V. CONCLUSIONS

We present an updated evaluation of nuclear radius parameters of 186 even-even nuclides lying in the region  $Z = 50 - 116$  and  $N = 52 - 174$  ( $^{102}\text{Sn} - ^{290}\text{Lv}$ ) from the analysis of all the even-even alpha emitters. This includes 26 new even-even alpha emitters, and 164 additional references published since the previous such evaluation by Y.A. Akovali [1] in 1998. Plots of systematics reveal that the nuclear radius parameter of isotopic chains decreases gradually with increasing parent neutron number between neighboring closed shells, exhibiting a minimum at  $N(\text{parent})=126$  (a major shell closure), and increases thereafter, decreasing again toward the next major shell. Another interesting behavior regarding "shifting minimum" in Th, U, Pu, Cm, Cf and Fm isotopes, which indicates the transient nature of the  $N=152$  shell closure, is also identified. An issue pertaining to the disappearance of  $Z=82$  proton shell closure in neutron deficient lead isotopes is also discussed. We believe that the present work on updated  $r_0$  parameters for even-even nuclei and the revised ALPHAD.RadD code will facilitate the evaluation of alpha decay data sets for the ENSDF database, through an automatic calculation of the radius parameters and hindrance factors for all the  $\alpha$  emitters.

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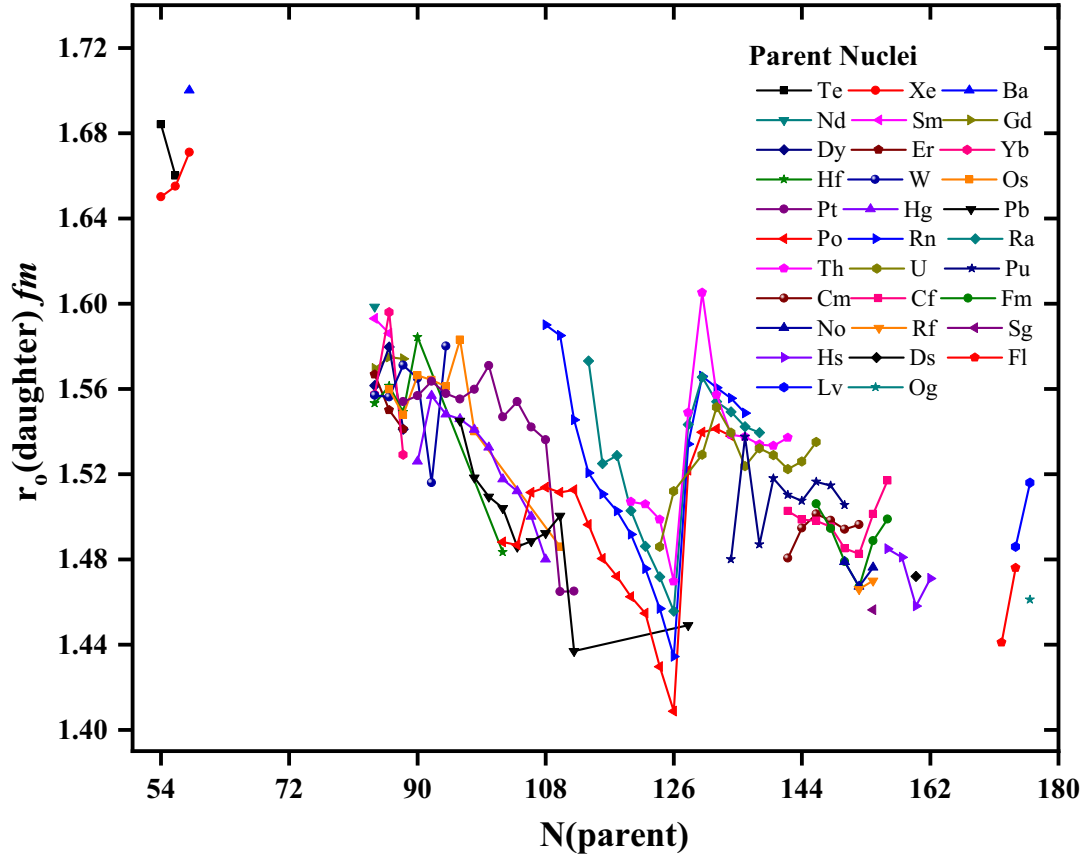


FIG. 1. (Color online) Systematics of  $r_0$  parameters as a function of parent neutron number for different Z chains listed in Table I.

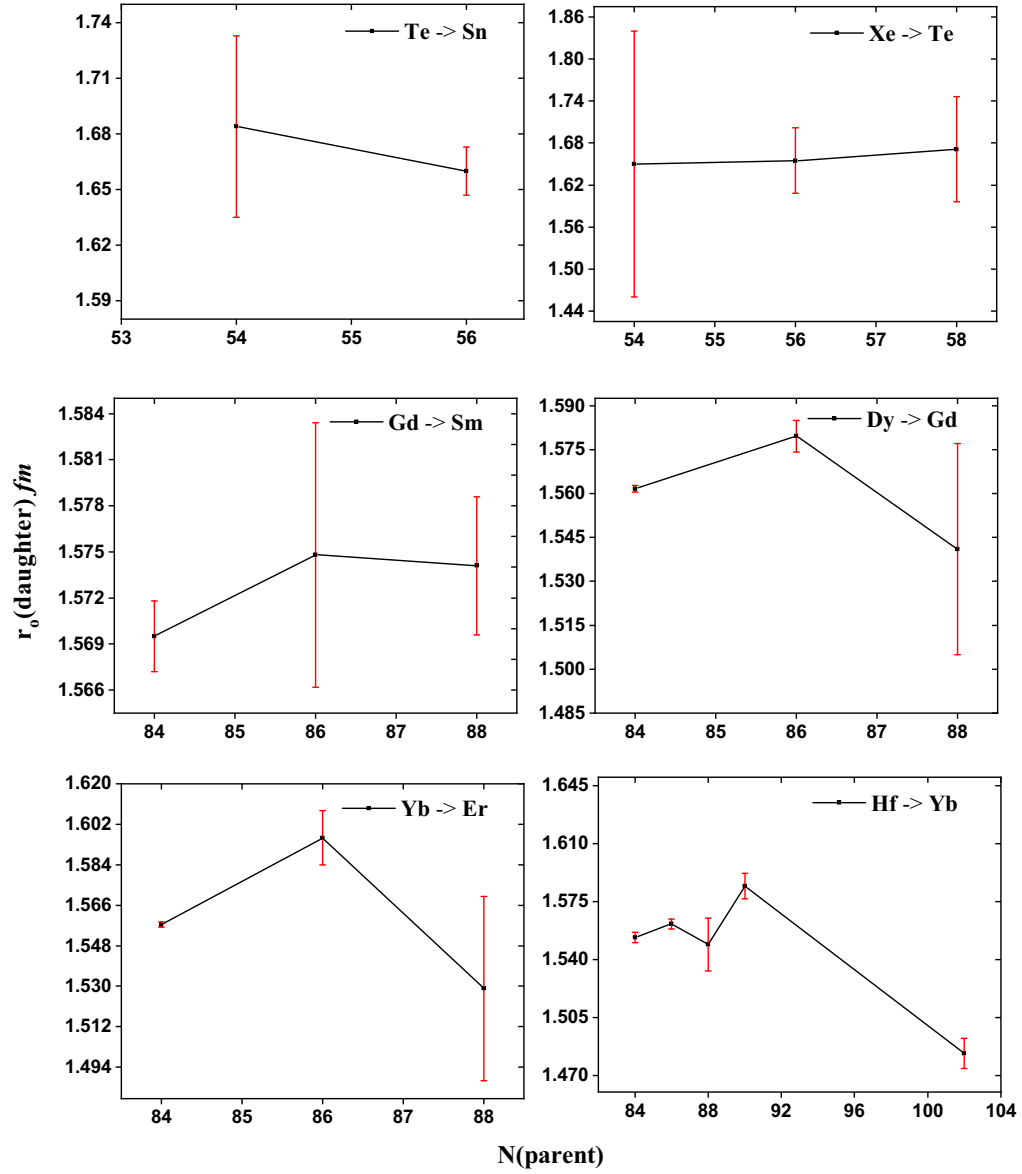


FIG. 2. (Color online) Systematics of  $r_0$  parameter with parent neutron number for Te, Xe, Gd, Dy, Yb and Hf nuclides. The overall uncertainties in  $r_0$  is indicated with error bars and determined by propagating all the relevant uncertainties within the operation of the ALPHAD code [36].

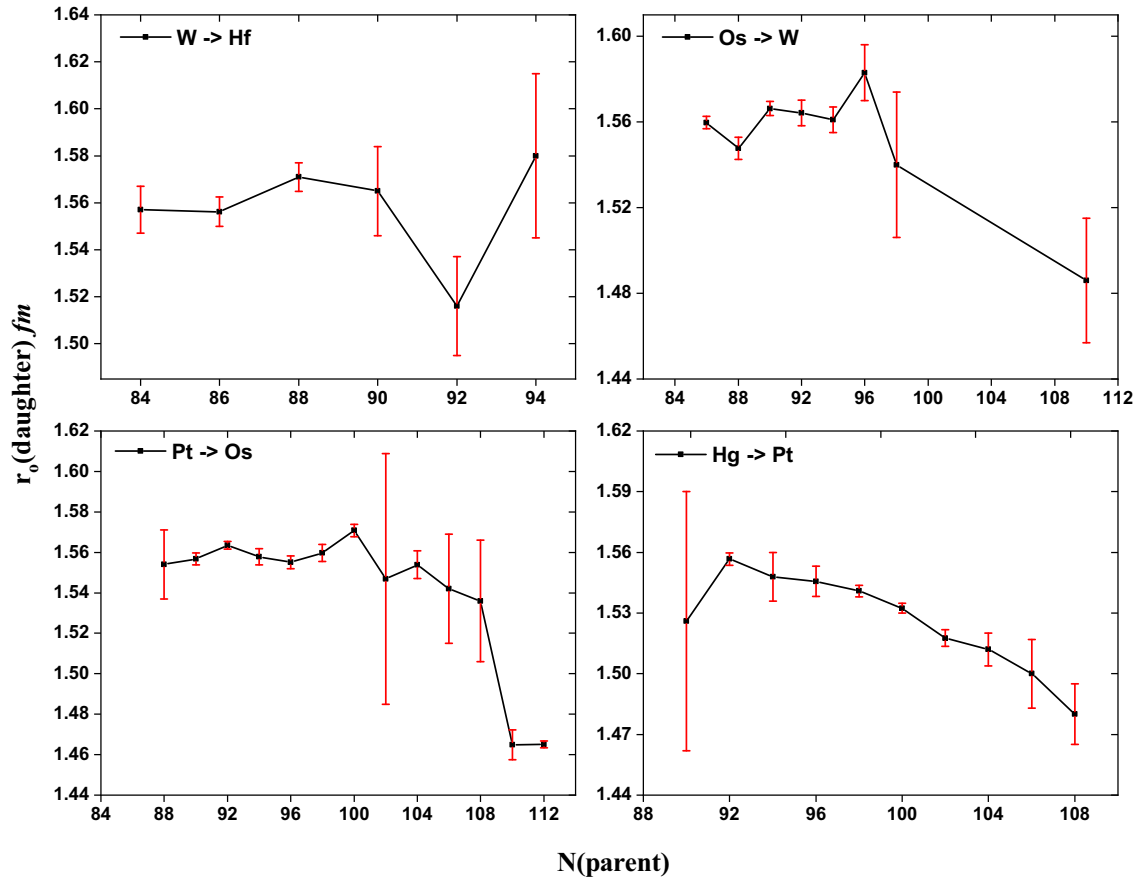


FIG. 3. (Color online) Same as Fig. 2 but for W, Os, Pt and Hg nuclides.

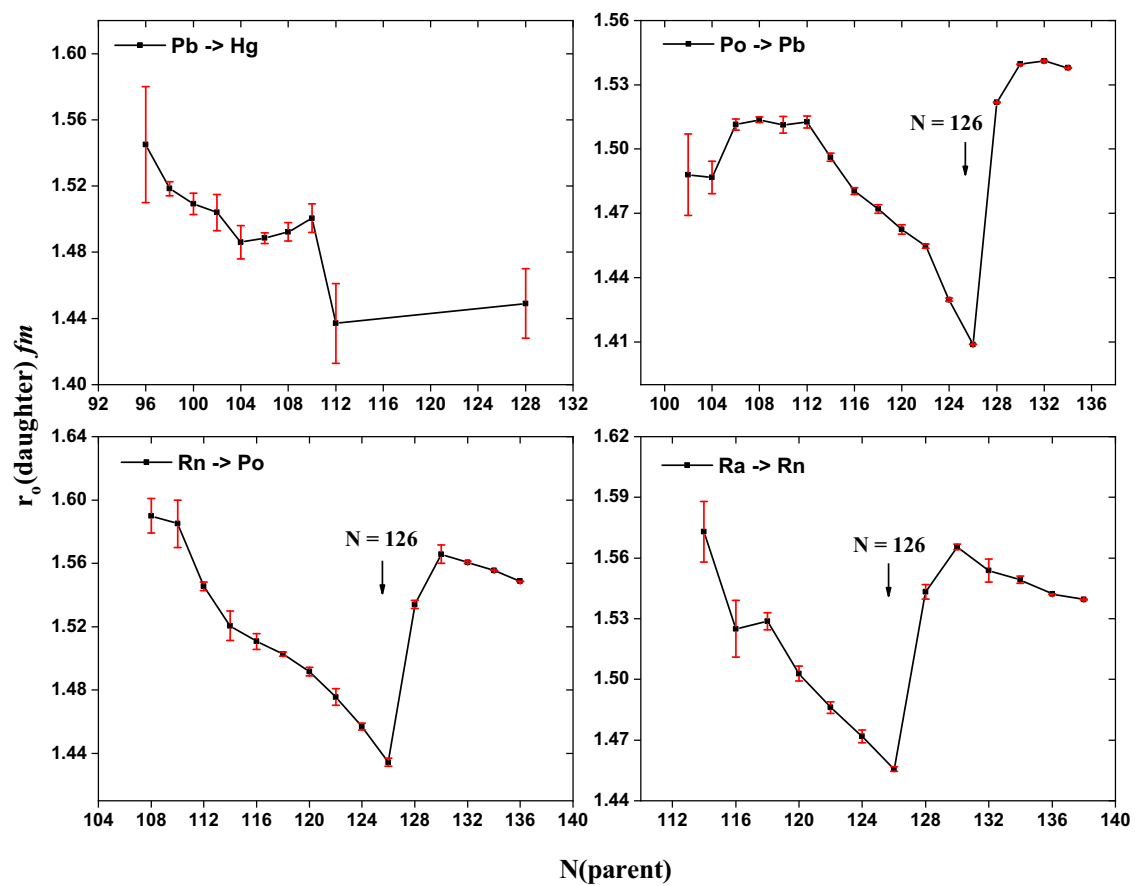


FIG. 4. (Color online) Same as Fig. 2 but for Pb, Po, Rn and Ra nuclides. The major shell closure at  $N=126$  is indicated with an arrow.

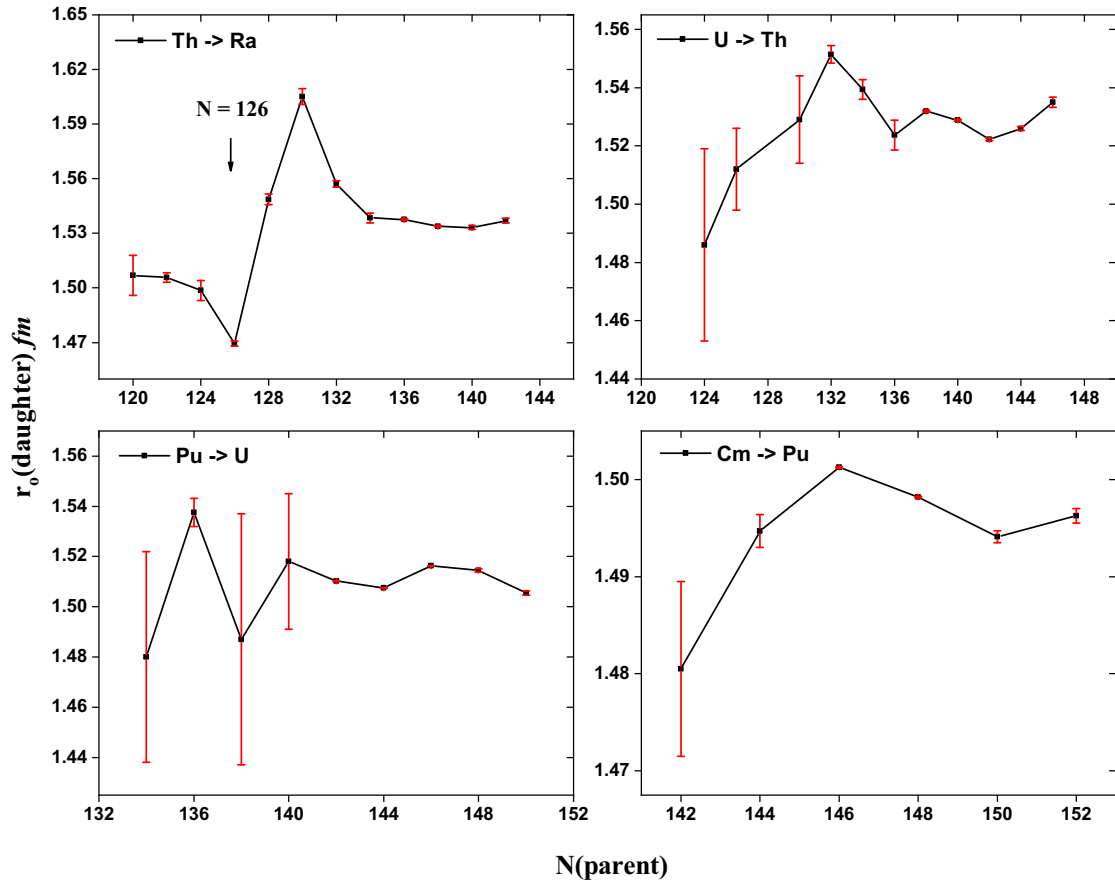


FIG. 5. (Color online) Same as Fig. 2 but for Th, U, Pu and Cm nuclides. The major shell closure at  $N=126$  is indicated with an arrow.



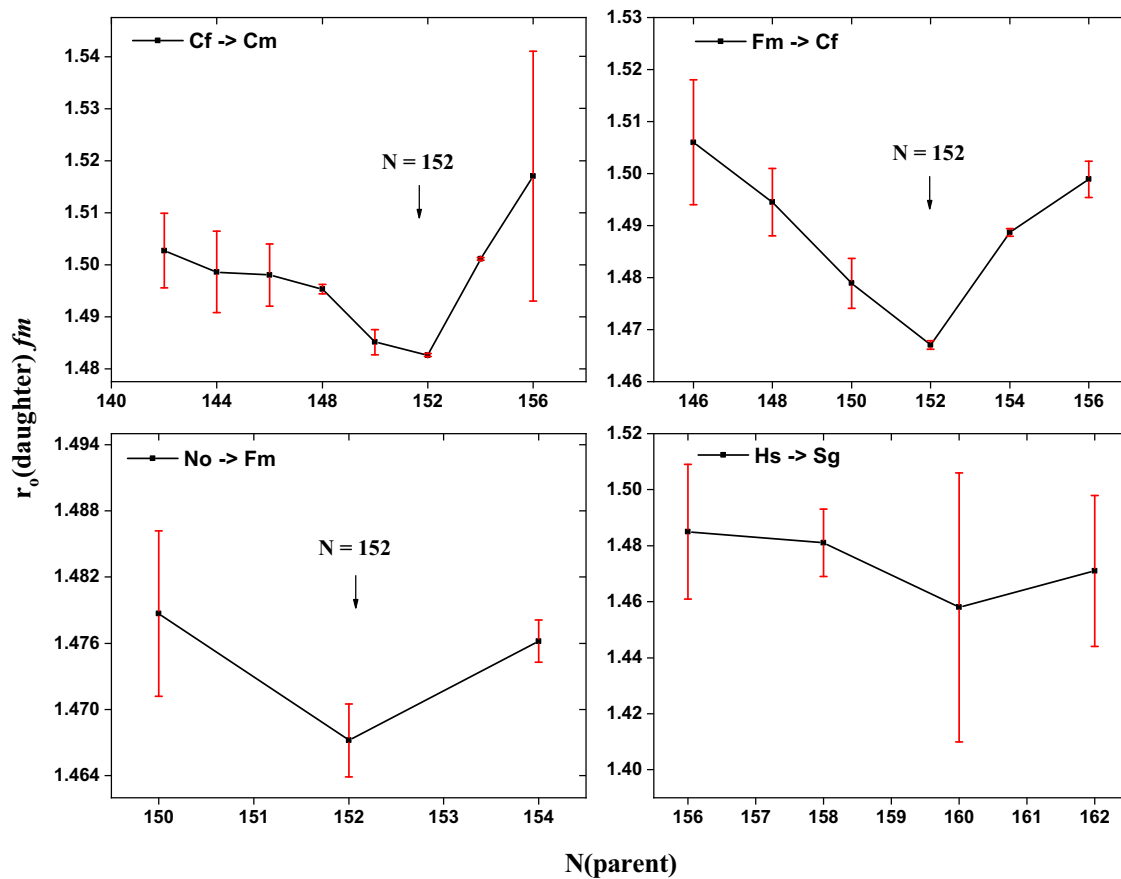


FIG. 6. (Color online) Same as Fig. 2 but for Cf, Fm, No and Hs nuclides. The minor shell closure at  $N=152$  is indicated with an arrow.

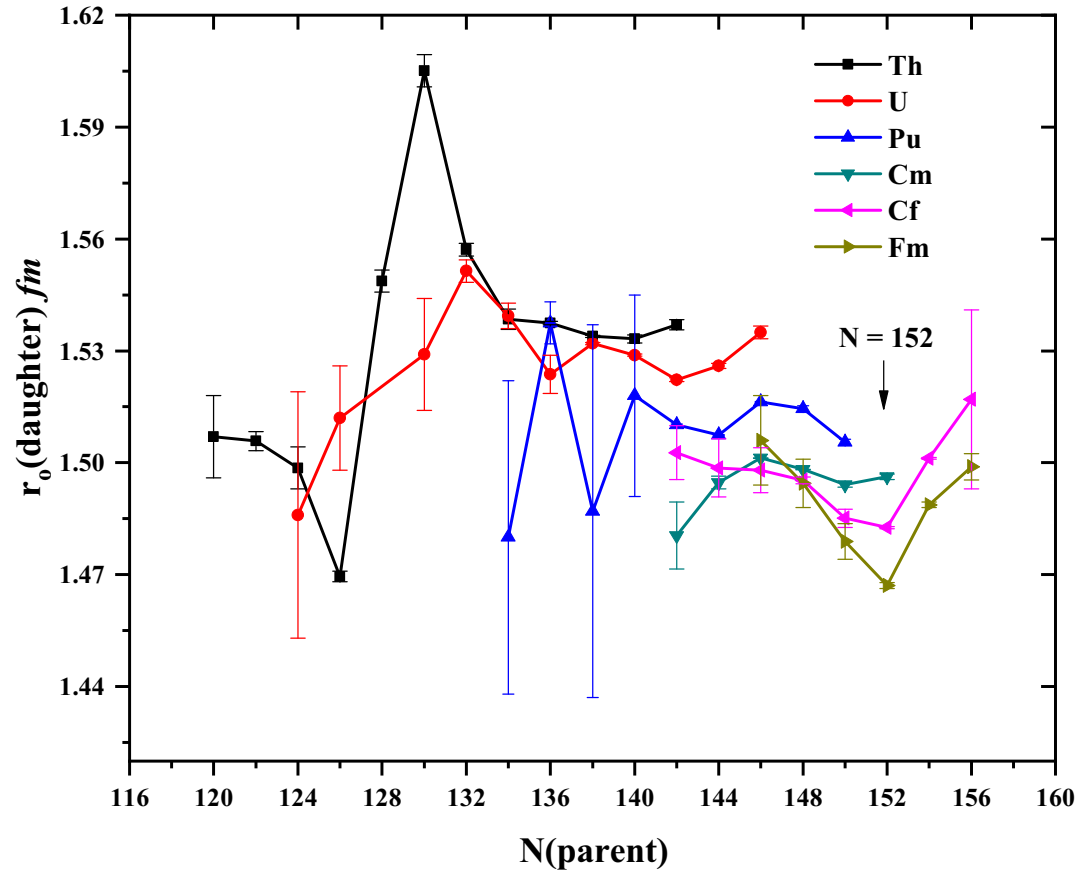


FIG. 7. (Color online) Same as Fig. 1 but for deformed actinides from Th to Cf. The Th, U and Pu nuclides exhibit shifting of minimum by two neutrons and the transient minimum at  $N=152$  [42] is indicated by an arrow.

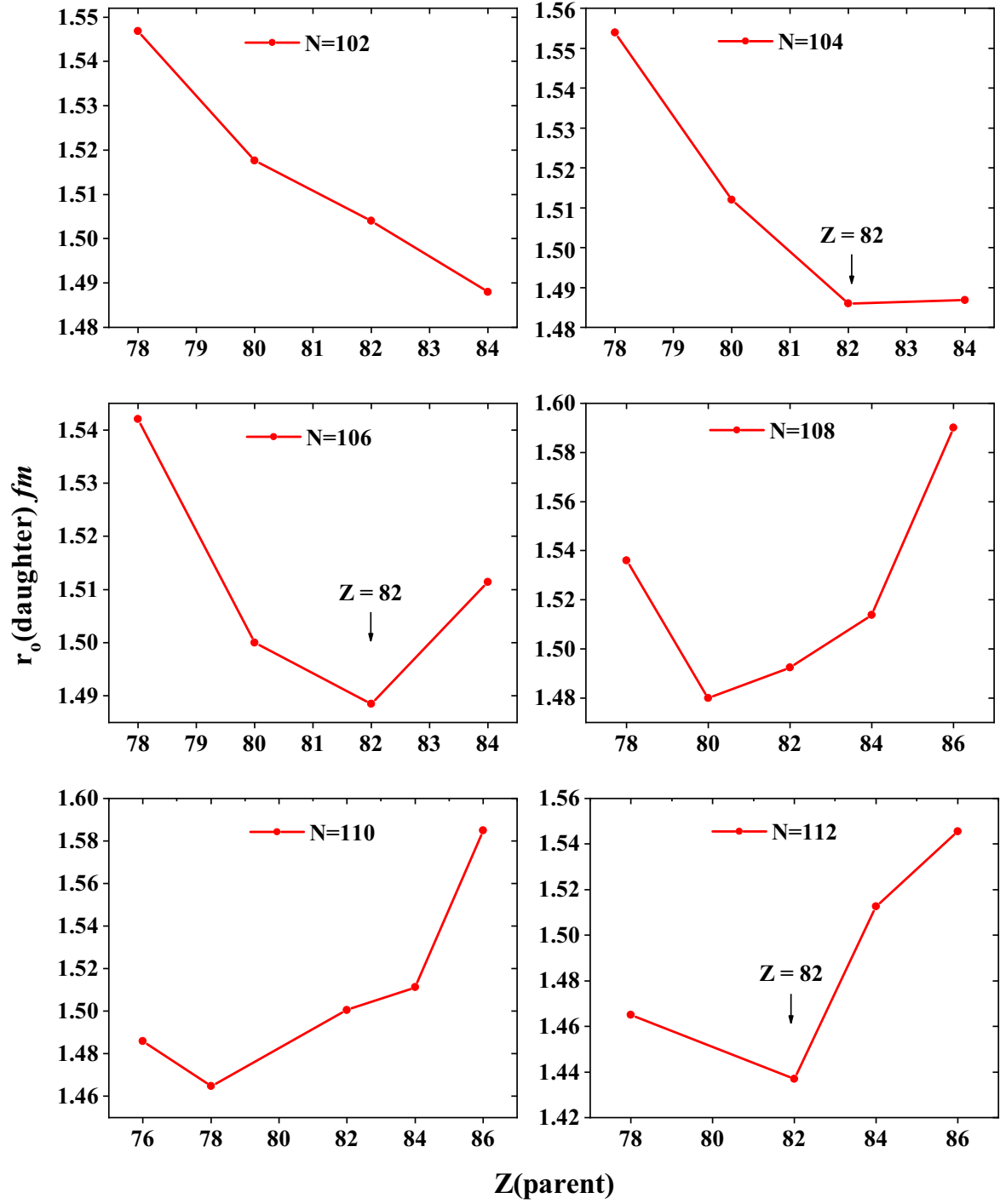


FIG. 8. (Color online) Systematics of  $r_0$  parameter as function of parent proton number for  $N(\text{parent})=102, 104, 106, 108, 110$  and  $112$  isotones. The major shell closure at  $Z=82$ , wherever observed, is indicated with an arrow.

TABLE I: List of extracted radius parameters ( $r_0$ ) for even-even daughter nuclei. The quoted uncertainty is in the last significant digits.

Parent Nuclide				Daughter Nuclide				Daughter $r_0$
Element	Z	N	A	Element	Z	N	A	(fm)
Te	52	54	106	Sn	50	52	102	1.684(49)
	52	56	108		50	54	104	1.660(13)
Xe	54	54	108	Te	52	52	104	1.65(19)
	54	56	110		52	54	106	1.655(47)
Ba	54	58	112	Xe	52	56	108	1.671(75)
	56	58	114		54	56	110	1.700(47)
Nd	60	84	144	Ce	58	82	140	1.5986(81)
Sm	62	84	146	Nd	60	82	142	1.5930(74)
	62	86	148		60	84	144	1.586(12)
Gd	64	84	148	Sm	62	82	144	1.5695(23)
	64	86	150		62	84	146	1.5748(86)
Dy	64	88	152	Gd	62	86	148	1.5741(45)
	66	84	150		64	82	146	1.5616(12)
Er	66	86	152	Dy	64	84	148	1.5796(54)
	66	88	154		64	86	150	1.541(36)
Yb	68	84	152	Er	66	82	148	1.5667(27)
	68	86	154		66	84	150	1.550(16)
Hf	68	88	156	Yb	66	86	152	1.541(26)
	70	84	154		68	82	150	1.5574(12)
W	70	86	156	Hf	68	84	152	1.596(12)
	70	88	158		68	86	154	1.529(41)
Os	72	84	156	W	70	82	152	1.5532(31)
	72	86	158		70	84	154	1.5614(31)
Pt	72	88	160	Os	70	86	156	1.549(16)
	72	90	162		70	88	158	1.5842(77)
Hg	72	102	174	Pt	70	100	170	1.4833(91)
	74	84	158		72	82	154	1.557(10)
Au	74	86	160	Au	72	84	156	1.5562(63)
	74	88	162		72	86	158	1.5710(61)
Tl	74	90	164	Tl	72	88	160	1.565(19)
	74	92	166		72	90	162	1.516(21)
Pb	74	94	168	Pb	72	92	164	1.580(35)
	76	86	162		74	84	158	1.5597(29)
Bi	76	88	164	Bi	74	86	160	1.5477(44)
	76	90	166		74	88	162	1.5663(32)
Po	76	92	168	Po	74	90	164	1.5642(59)
	76	94	170		74	92	166	1.5611(60)
At	76	96	172	At	74	94	168	1.583(13)
	76	98	174		74	96	170	1.540(34)
Rn	76	110	186	Rn	74	108	182	1.486(29)
	78	88	166		76	86	162	1.554(17)
Fr	78	90	168	Fr	76	88	164	1.5568(29)
	78	92	170		76	90	166	1.5636(19)
Ra	78	94	172	Ra	76	92	168	1.5578(40)
	78	96	174		76	94	170	1.5551(32)
Ac	78	98	176	Ac	76	96	172	1.5597(42)
	78	100	178		76	98	174	1.5708(31)
Th	78	102	180	Th	76	100	176	1.5468(62)
	78	104	182		76	102	178	1.5539(68)
Pa	78	106	184	Pa	76	104	180	1.542(27)
	78	108	186		76	106	182	1.536(30)
U	78	110	188	U	76	108	184	1.4648(74)
	78	112	190		76	110	186	1.4651(16)
Np	80	90	170	Np	78	88	166	1.526(64)
	80	92	172		78	90	168	1.5567(30)
Pu	80	94	174	Pu	78	92	170	1.548(12)
	80	96	176		78	94	172	1.5457(75)
Am	80	98	178	Am	78	96	174	1.5409(29)
	80	100	180		78	98	176	1.5324(24)

Continuation of Table I								
Parent Nuclide				Daughter Nuclide				Daughter $r_0$
Element	Z	N	A	Element	Z	N	A	(fm)
Hg	80	102	182	Pt	78	100	178	1.5176(41)
	80	104	184		78	102	180	1.5120(81)
	80	106	186		78	104	182	1.500(17)
	80	108	188		78	106	184	1.480(15)
Pb	82	96	178	Hg	80	94	174	1.545(35)
	82	98	180		80	96	176	1.5184(43)
	82	100	182		80	98	178	1.5093(64)
	82	102	184		80	100	180	1.504(11)
	82	104	186		80	102	182	1.486(10)
	82	106	188		80	104	184	1.4885(32)
	82	108	190		80	106	186	1.4923(55)
	82	110	192		80	108	188	1.5005(86)
	82	112	194		80	110	190	1.437(24)
	82	128	210		80	126	206	1.449(21)
Po	84	102	186	Pb	82	100	182	1.488(19)
	84	104	188		82	102	184	1.4868(76)
	84	106	190		82	104	186	1.5114(26)
	84	108	192		82	106	188	1.5137(13)
	84	110	194		82	108	190	1.5113(39)
	84	112	196		82	110	192	1.5126(28)
	84	114	198		82	112	194	1.4962(19)
	84	116	200		82	114	196	1.4803(16)
	84	118	202		82	116	198	1.4720(20)
	84	120	204		82	118	200	1.4625(22)
	84	122	206		82	120	202	1.4547(10)
	84	124	208		82	122	204	1.42967(74)
	84	126	210		82	124	206	1.408790(38)
	84	128	212		82	126	208	1.52177(18)
	84	130	214		82	128	210	1.539616(24)
	84	132	216		82	130	212	1.54117(28)
	84	134	218		82	132	214	1.53788(19)
Rn	86	108	194	Po	84	106	190	1.590(11)
	86	110	196		84	108	192	1.585(15)
	86	112	198		84	110	194	1.5455(27)
	86	114	200		84	112	196	1.5205(93)
	86	116	202		84	114	198	1.5106(49)
	86	118	204		84	116	200	1.5026(13)
	86	120	206		84	118	202	1.4917(27)
	86	122	208		84	120	204	1.4755(52)
	86	124	210		84	122	206	1.4568(22)
	86	126	212		84	124	208	1.4343(25)
	86	128	214		84	126	210	1.5340(25)
	86	130	216		84	128	212	1.5658(59)
	86	132	218		84	130	214	1.56062(74)
	86	134	220		84	132	216	1.55548(10)
Ra	88	136	222		84	134	218	1.54863(17)
	88	114	202	Rn	86	112	198	1.573(15)
	88	116	204		86	114	200	1.525(14)
	88	118	206		86	116	202	1.5287(42)
	88	120	208		86	118	204	1.5029(36)
	88	122	210		86	120	206	1.4861(29)
	88	124	212		86	122	208	1.4718(31)
	88	126	214		86	124	210	1.4557(12)
	88	128	216		86	126	212	1.5433(36)
	88	130	218		86	128	214	1.5655(13)
	88	132	220		86	130	216	1.5539(57)
Th	88	134	222		86	132	218	1.5492(18)
	88	136	224		86	134	220	1.542177(86)
	88	138	226		86	136	222	1.53945(26)
	90	120	210	Ra	88	118	206	1.507(11)

Continuation of Table I								
Parent Nuclide				Daughter Nuclide				Daughter $r_0$
Element	Z	N	A	Element	Z	N	A	(fm)
Th	90	122	212	Ra	88	120	208	1.5058(26)
	90	124	214		88	122	210	1.4986(56)
	90	126	216		88	124	212	1.4695(14)
	90	128	218		88	126	214	1.5487(30)
	90	130	220		88	128	216	1.6051(43)
	90	132	222		88	130	218	1.5571(17)
	90	134	224		88	132	220	1.5385(27)
	90	136	226		88	134	222	1.53749(45)
	90	138	228		88	136	224	1.53389(32)
	90	140	230		88	138	226	1.5332(11)
U	90	142	232	Th	88	140	228	1.5370(14)
	92	124	216		90	122	212	1.486(33)
	92	126	218		90	124	214	1.512(14)
	92	130	222		90	128	218	1.529(15)
	92	132	224		90	130	220	1.5514(30)
	92	134	226		90	132	222	1.5394(34)
	92	136	228		90	134	224	1.5237(51)
	92	138	230		90	136	226	1.53197(29)
	92	140	232		90	138	228	1.52885(29)
	92	142	234		90	140	230	1.52224(49)
Pu	92	144	236	U	90	142	232	1.52595(66)
	92	146	238		90	144	234	1.5350(17)
	94	134	228		92	132	224	1.480(42)
	94	136	230		92	134	226	1.5375(56)
	94	138	232		92	136	228	1.487(50)
	94	140	234		92	138	230	1.518(27)
	94	142	236		92	140	232	1.51022(22)
	94	144	238		92	142	234	1.50745(13)
	94	146	240		92	144	236	1.51631(11)
	94	148	242		92	146	238	1.51448(75)
Cm	94	150	244	Pu	92	148	240	1.50549(82)
	96	142	238		94	140	234	1.4805(90)
	96	144	240		94	142	236	1.4947(17)
	96	146	242		94	144	238	1.501258(57)
	96	148	244		94	146	240	1.498180(88)
Cf	96	150	246	Cm	94	148	242	1.49412(62)
	96	152	248		94	150	244	1.49627(74)
	98	142	240		96	140	236	1.5027(72)
	98	144	242		96	142	238	1.4986(78)
	98	146	244		96	144	240	1.498(60)
	98	148	246		96	146	242	1.49528(88)
	98	150	248		96	148	244	1.4851(24)
	98	152	250		96	150	246	1.48260(30)
Fm	98	154	252	Cf	96	152	248	1.50113(23)
	98	156	254		96	154	250	1.517(24)
	100	146	246		98	144	242	1.506(12)
	100	148	248		98	146	244	1.4945(65)
	100	150	250		98	148	246	1.4789(48)
	100	152	252		98	150	248	1.46703(81)
No	100	154	254	Fm	98	152	250	1.48871(75)
	100	156	256		98	154	252	1.4989(35)
	102	150	252		100	148	248	1.4787(75)
	102	152	254		100	150	250	1.4672(33)
Rf	102	154	256	No	100	152	252	1.4762(19)
	104	152	256		102	150	252	1.466(26)
Sg	104	154	258	Rf	102	152	254	1.470(18)
	106	154	260		104	152	256	1.4562(75)
Hs	106	156	264	Sg	106	154	260	1.485(24)
	108	158	266		106	156	262	1.481(12)
	108	160	268		106	158	264	1.458(48)

Continuation of Table I									
Parent Nuclide				Daughter Nuclide				Daughter $r_0$	
Element	Z	N	A	Element	Z	N	A	(fm)	
Hs	108	162	270	Sg	106	160	266	1.471(27)	
Ds	110	160	270	Hs	108	158	266	1.472(12)	
Fl	114	172	286	Cn	112	170	282	1.441(15)	
	114	174	288		112	172	284	1.476(10)	
Lv	116	174	290	Fl	114	172	286	1.486(28)	
	116	176	292		114	174	288	1.516(18)	
Og	118	176	294	Lv	116	174	290	1.461(24)	

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## VI. EXPLANATION AND POLICIES OF TABLE II

**Alpha Decay:** The parent and daughter nuclides involved in a given alpha decay are listed in the first column of the table. Nuclei are listed with increasing atomic number; various isotopes are grouped together and placed with increasing mass number within the same group.

**$Q_\alpha$ :** Energy available for alpha decay in units of keV, adopted from M. Wang *et al.* [Chinese Physics C 41, 030003 (2017)] and in some cases where  $Q_\alpha$  values, are derived from recent precise measurements of  $E_\alpha$ , are indicated with appropriate comments.

**$\% \alpha$ :** Alpha-decay branching from the ground state of the parent adopted from the ENSDF database supplemented by data from literature available up to June 2020. The decay branchings listed as approximate values in the literature are taken as exact values with appropriate overlap of uncertainties.

**$T_{1/2}$ :** Half-life of parent nuclide from the ENSDF database, supplemented by data from recent literature available up to June 2020. For cases where  $T_{1/2}$  values are re-evaluated, appropriate comments are given. The most current value(s), from the same lab and the same experimental group using the same method, is adopted, when reported by authors in different papers over time.

**$I_\alpha$ :** Alpha intensities per 100 decays of the parent nuclei. These are adopted from the ENSDF database or from more recent literature, with listing of source reference(s), when required. Whenever alpha intensities appeared with  $\approx$ ,  $<$ ,  $>$ ,  $\leq$  or  $\geq$  signs, the uncertainties in these cases are assigned as:

(a) When only one alpha branch is seen or when  $I_\alpha$  is  $\approx 100$ , then  $I_\alpha$  is assumed as 100 for deduction of radius parameter.

(b) For approximate values, we assumed 25% uncertainty e.g., for  $^{196}\text{Po}$  alpha decay, for  $I_{\alpha 1} = 99.978(6)$  and  $I_{\alpha 2} = 0.022$ , 25% uncertainty assumed for the latter.

(c) For the nuclides having  $I_\alpha <$  a certain value, we assumed a value overlapping 0 and the limit e.g., for  $I_\alpha < 1$  for  $^{174}\text{Pt}$  alpha decay,  $I_\alpha = 0.5(5)$  was used.

**$r_0$ :** Radius parameter for daughter nuclides extracted from alpha decay with the most current values of  $Q_\alpha$ ,  $\% \alpha$ ,  $T_{1/2}$  and  $I_\alpha$ .

For cases with large ( $>30\%$  or so) uncertainties either in half-lives or alpha branches, we executed ALPHAD for three values of input quantities, i.e., mean value, mean value + upper limit and mean value - lower limit. In cases where uncertainties are large in both the half-life as well as  $\% \alpha$  branch, we obtained the mean value, then ran two cases, one with the maximum  $\% \alpha$  branch (value + uncertainty) and the minimum half-life (value - uncertainty); the other with the minimum  $\% \alpha$  branch (value - uncertainty) and the maximum half-life (value + uncertainty). The final value of  $r_0$  in such procedures generally results in asymmetric uncertainties, where we adopt the final uncertainty in  $r_0$  as an arithmetic average of the upper and lower uncertainties, since the ALPHAD and ALPHAD-RadD codes can handle only symmetric uncertainty in the  $r_0$  parameter.

**Rounding of uncertainties:** In the averaging procedure, final uncertainty is not lower than the lowest experimental uncertainty in a dataset that is being averaged.

**References:** References are listed in terms of NSR keynumbers, and extracted from the NSR database.

### Abbreviations

**ENSDF:** Evaluated Nuclear Structure Data File: [www.nndc.bnl.gov/ensdf/](http://www.nndc.bnl.gov/ensdf/)

**XUNDL:** eXperimental Unevaluated Nuclear Data List: [www.nndc.bnl.gov/xundl/](http://www.nndc.bnl.gov/xundl/)

**UWA:** Unweighted Average

**WA:** Weighted Average

**NRM:** Weighted Average by Normalized Residuals Method [M.F James *et al.* Nucl. Instrum. Methods A 313, 277 (1992).]

TABLE II: Table of evaluated input quantities, and deduced  $r_0$  parameters for daughter nuclides.

Alpha Decay	Input Parameters	$r_0$ (fm)
$^{106}\text{Te} \rightarrow ^{102}\text{Sn}$	$Q_\alpha = 4290(9)$ . $\% \alpha = 100$ , $I_\alpha = 100$ (2009DE21). $T_{1/2} = 73 \mu\text{s}$ (+20-10). $T_{1/2}$ : WA of $70 \mu\text{s}$ (+20-15) (2016CA33), $80 \mu\text{s}$ (+25-15) (2005JA03), $60 \mu\text{s}$ (+40-20) (1994PA11) and $60 \mu\text{s}$ (+30-10) (1981SC17).	1.684(49)
$^{108}\text{Te} \rightarrow ^{104}\text{Sn}$	$Q_\alpha = 3420(8)$ . $\% \alpha = 51(6)$ . $T_{1/2} = 2.1 \text{ s}$ (1), $I_\alpha = 100$ (2007BL18). $\% \alpha$ : WA of $49(4)$ (1994PA11) and $68(12)$ (1978RO19).	1.660(13)
$^{108}\text{Xe} \rightarrow ^{104}\text{Te}$	$Q_\alpha = 4600(200)$ . $\% \alpha = 100$ , $T_{1/2} = 0.06 \text{ ms}$ (+11-2) (2018AU04). $I_\alpha = 100$ . $Q_\alpha$ : From 2018AU04, based on $E_\alpha = 4400 \text{ keV}$ (200).	1.65(19)
$^{110}\text{Xe} \rightarrow ^{106}\text{Te}$	$Q_\alpha = 3872(9)$ . $\% \alpha = 64(35)$ , $T_{1/2} = 93 \text{ ms}$ (3) (2012GU09). $I_\alpha = 100$ (2008DE09). $T_{1/2}$ : $95 \text{ ms}$ (+25-20) (2016CA33), $105 \text{ ms}$ (+35-25) (2005JA03) and $160 \text{ ms}$ (+290-60) (2002MA19) are imprecise, thus not considered here.	1.655(47)
$^{112}\text{Xe} \rightarrow ^{108}\text{Te}$	$Q_\alpha = 3330(6)$ , $\% \alpha = 1.2(8)$ , $T_{1/2} = 2.7 \text{ s}$ (8) (2015LA02). $I_\alpha = 100$ (2000BL21).	1.671(75)
$^{114}\text{Ba} \rightarrow ^{110}\text{Xe}$	$Q_\alpha = 3592(19)$ . $T_{1/2} = 410 \text{ ms}$ (+190-110). $\% \alpha = 0.9(3)$ , $I_\alpha = 100$ (2012GU09). $T_{1/2}$ : WA of $380 \text{ ms}$ (+190-110) (2016CA33) and $430(+300-150) \text{ ms}$ (1997JA12).	1.700(47)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{144}\text{Nd} \rightarrow ^{140}\text{Ce}$	$Q_\alpha = 1903.2(16)$ . $\% \alpha = 100$ , $I_\alpha = 100$ (2018NI16). $T_{1/2} = 2.40 \times 10^{15} \text{ y}$ (30). $T_{1/2}$ : WA of $2.65 \text{ y} \times 10^{15}$ (37) (1987AL28), $2.4 \text{ y} \times 10^{15}$ (3) (1961MA05) and $2.1 \text{ y} \times 10^{15}$ (4) (1965IS01).	1.5986(81)
$^{146}\text{Sm} \rightarrow ^{142}\text{Nd}$	$Q_\alpha = 2528.8(28)$ . $\% \alpha = 100$ , $T_{1/2} = 6.8 \times 10^7 \text{ y}$ (7) (2016KH07). $I_\alpha = 100$ (2011JO05).	1.5930(74)
$^{148}\text{Sm} \rightarrow ^{144}\text{Nd}$	$Q_\alpha = 1986.8(4)$ . $T_{1/2} = 6.4 \times 10^{15} \text{ y}$ (+12-13) (2016CA43). $\% \alpha = 100$ (2014NI05). $I_\alpha = 100$ (2001SO16).	1.586(12)
$^{148}\text{Gd} \rightarrow ^{144}\text{Sm}$	$Q_\alpha = 3271.29(3)$ . $\% \alpha = 100$ , $I_\alpha = 100$ (2014NI05). $T_{1/2} = 74.6 \text{ y}$ (30) (1981PR06). $T_{1/2}$ : In 2014NI05, $T_{1/2}$ is WA of $74.6 \text{ y}$ (30) (1981PR06) and $70.9 \text{ y}$ (10) (2003FU10); latter is a preliminary result, thus not considered here.	1.5695(23)
$^{150}\text{Gd} \rightarrow ^{146}\text{Sm}$	$Q_\alpha = 2807(6)$ . $\% \alpha = 100$ , $T_{1/2} = 1.79 \times 10^6 \text{ y}$ (8), $I_\alpha = 100$ (2016KH07).	1.5748(86)
$^{150}\text{Dy} \rightarrow ^{146}\text{Gd}$	$Q_\alpha = 4351.3(15)$ . $\% \alpha = 33.6(18)$ , $I_\alpha = 100$ (2016KH07). $T_{1/2} = 7.175 \text{ min}$ (25). $T_{1/2}$ : WA of $7.17 \text{ min}$ (5) (1973BI06) and $7.3 \text{ min}$ (1) (1982BO04).	1.5616(12)
$^{152}\text{Gd} \rightarrow ^{148}\text{Sm}$	$Q_\alpha = 2204.4(10)$ . $\% \alpha = 100$ , $T_{1/2} = 1.08 \times 10^{14} \text{ y}$ (8), $I_\alpha = 100$ (2014NI05).	1.5741(45)
$^{152}\text{Dy} \rightarrow ^{148}\text{Gd}$	$Q_\alpha = 3727(4)$ . $\% \alpha = 0.100(7)$ , $T_{1/2} = 2.38 \text{ h}$ (2), $I_\alpha = 100$ (2014NI05).	1.5796(54)
$^{152}\text{Er} \rightarrow ^{148}\text{Dy}$	$Q_\alpha = 4934.3(16)$ . $\% \alpha = 91(4)$ , $T_{1/2} = 10.3 \text{ s}$ (1), $I_\alpha = 100$ (2014NI05).	1.5667(27)
$^{154}\text{Dy} \rightarrow ^{150}\text{Gd}$	$Q_\alpha = 2945(5)$ . $\% \alpha = 100$ , $T_{1/2} = 3.0 \times 10^6 \text{ y}$ (15), $I_\alpha = 100$ (2013BA31).	1.541(36)
$^{154}\text{Er} \rightarrow ^{150}\text{Dy}$	$Q_\alpha = 4279.7(26)$ . $\% \alpha = 0.47(13)$ , $T_{1/2} = 3.73 \text{ min}$ (9), $I_\alpha = 100$ (2013BA31).	1.550(16)
$^{154}\text{Yb} \rightarrow ^{150}\text{Er}$	$Q_\alpha = 5474.3(17)$ . $\% \alpha = 92.6(12)$ , $T_{1/2} = 0.409 \text{ s}$ (2), $I_\alpha = 100$ (2013BA31).	1.5574(12)
$^{156}\text{Er} \rightarrow ^{152}\text{Dy}$	$Q_\alpha = 3481(25)$ . $\% \alpha = 5.0 \times 10^{-6}(2)$ (1995KAZS), $T_{1/2} = 19.5 \text{ min}$ (10), $I_\alpha = 100$ (2013MA77). $\% \alpha$ : $5.0 \times 10^{-6}(2)$ (1995KAZS), $1.2 \times 10^{-5}(3)$ (1996BYZY), $5 \times 10^{-6}(2)$ (1992KAZP), $1.0 \times 10^{-4}$ (2002KAZR) and corresponding radius parameter comes out as $1.541 \text{ fm}$ (26), $1.588 \text{ fm}$ (30), $1.541 \text{ fm}$ (26) and $1.704 \text{ fm}$ (27), respectively. From systematics of radius parameter values in adjacent nuclides ( $r_0 = 1.5661 \text{ fm}$ (28) and $1.550 \text{ fm}$ (16) for $^{148}\text{Dy}$ and $^{150}\text{Dy}$ ), the most likely value for $^{152}\text{Dy}$ is the one resulting from $\% \alpha = 5.0 \times 10^{-6}(2)$ (1995KAZS).	1.541(26)
$^{156}\text{Yb} \rightarrow ^{152}\text{Er}$	$Q_\alpha = 4810(4)$ . $\% \alpha = 10(2)$ , $T_{1/2} = 26.1 \text{ s}$ (7), $I_\alpha = 100$ (2013MA77).	1.596(12)
$^{156}\text{Hf} \rightarrow ^{152}\text{Yb}$	$Q_\alpha = 6029(4)$ . $\% \alpha = 100$ , $T_{1/2} = 23 \text{ ms}$ (1), $I_\alpha = 100$ (2013MA77).	1.5532(31)
$^{158}\text{Yb} \rightarrow ^{154}\text{Er}$	$Q_\alpha = 4170(7)$ . $\% \alpha = 0.0021(12)$ , $T_{1/2} = 1.49 \text{ min}$ (13) (2017NI05). $I_\alpha = 100$ (2009RE14).	1.529(41)
$^{158}\text{Hf} \rightarrow ^{154}\text{Yb}$	$Q_\alpha = 5404.8(27)$ . $\% \alpha = 44.3(19)$ , $T_{1/2} = 2.85 \text{ s}$ (7) (2017NI05). $I_\alpha = 100$ (2009RE14).	1.5614(31)
$^{158}\text{W} \rightarrow ^{154}\text{Hf}$	$Q_\alpha = 6613(3)$ . $\% \alpha = 100$ , $T_{1/2} = 1.25 \text{ ms}$ (21) (2017NI05). $I_\alpha = 100$ (2009RE14).	1.557(10)
$^{160}\text{Hf} \rightarrow ^{156}\text{Yb}$	$Q_\alpha = 4901.9(26)$ . $\% \alpha = 0.7(2)$ , $T_{1/2} = 13.6 \text{ s}$ (2), $I_\alpha = 100$ (2012RE18).	1.549(16)
$^{160}\text{W} \rightarrow ^{156}\text{Hf}$	$Q_\alpha = 6066(5)$ . $\% \alpha = 87(8)$ , $T_{1/2} = 91 \text{ ms}$ (5), $I_\alpha = 100$ (2012RE18).	1.5562(63)
$^{162}\text{Hf} \rightarrow ^{158}\text{Yb}$	$Q_\alpha = 4416(5)$ . $\% \alpha = 0.008(1)$ , $T_{1/2} = 39.4 \text{ s}$ (9), $I_{\alpha_1} = 99.77(23)$ , $I_{\alpha_2} = 0.23(23)$ (2017NI05).	1.5842(77)
$^{162}\text{W} \rightarrow ^{158}\text{Hf}$	$Q_\alpha = 5678.3(24)$ . $\% \alpha = 45(2)$ . $T_{1/2} = 1.19 \text{ s}$ (12), $I_\alpha = 100$ (2017NI05). $\% \alpha$ : WA of $46(4)$ (1981HO10), $49(4)$ (1989WO02) and $44(2)$ (1996PA01).	1.5710(61)
$^{162}\text{Os} \rightarrow ^{158}\text{W}$	$Q_\alpha = 6767(3)$ . $\% \alpha = 100$ , $T_{1/2} = 2.1 \text{ ms}$ (1), $I_\alpha = 100$ (2017NI05).	1.5597(29)
$^{164}\text{W} \rightarrow ^{160}\text{Hf}$	$Q_\alpha = 5278.3(20)$ . $\% \alpha = 3.8(12)$ , $T_{1/2} = 6.3 \text{ s}$ (2) (2018SI01). $I_\alpha = 99.5(5)$ (2005RE18).	1.565(19)
$^{164}\text{Os} \rightarrow ^{160}\text{W}$	$Q_\alpha = 6479(5)$ . $\% \alpha = 96(+4-5)$ , $T_{1/2} = 21 \text{ ms}$ (1) (2018SI01). $I_\alpha = 95(5)$ (2005RE18).	1.5477(44)
$^{166}\text{W} \rightarrow ^{162}\text{Hf}$	$Q_\alpha = 4856(4)$ . $\% \alpha = 0.035(12)$ , $T_{1/2} = 19.2 \text{ s}$ (6) (2008BA14). $I_\alpha = 100$ (2007RE16).	1.516(21)
$^{166}\text{Os} \rightarrow ^{162}\text{W}$	$Q_\alpha = 6143(3)$ . $\% \alpha = 83(4)$ . $T_{1/2} = 213 \text{ ms}$ (5) (2008BA14). $I_\alpha = 100$ (ENSDF updates Feb.-2016). $\% \alpha$ : WA of $72(13)$ (1981HO10) and $84(4)$ (2008BI15).	1.5663(32)
$^{166}\text{Pt} \rightarrow ^{162}\text{Os}$	$Q_\alpha = 7286(15)$ . $T_{1/2} = 0.280 \text{ ms}$ (+100-60). $\% \alpha = 100$ (2008BA14). $I_\alpha = 100$ (2007RE16). $T_{1/2}$ : WA of $0.260 \text{ ms}$ (+100-60) (2019HI06) and $0.3 \text{ ms}$ (1) (1996BI07).	1.554(17)
$^{168}\text{W} \rightarrow ^{164}\text{Hf}$	$Q_\alpha = 4500(11)$ . $\% \alpha = 0.0032(10)$ , $T_{1/2} = 50.9 \text{ s}$ (19), $I_\alpha = 97.7(23)$ (2018SI01).	1.580(35)
$^{168}\text{Os} \rightarrow ^{164}\text{W}$	$Q_\alpha = 5815.6(27)$ . $\% \alpha = 43(4)$ , $T_{1/2} = 2.1 \text{ s}$ (1), $I_\alpha = 97(3)$ (2018SI01).	1.5642(59)
$^{168}\text{Pt} \rightarrow ^{164}\text{Os}$	$Q_\alpha = 6990(3)$ . $\% \alpha = 99.3(7)$ , $T_{1/2} = 2.02 \text{ ms}$ (10), $I_\alpha = 100$ (2018SI01).	1.5568(29)
$^{170}\text{Os} \rightarrow ^{166}\text{W}$	$Q_\alpha = 5536.9(27)$ . $\% \alpha = 9.5(10)$ , $T_{1/2} = 7.37 \text{ s}$ (18) (2018BA41). $I_\alpha = 97(3)$ (2008BA14).	1.5611(60)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{170}\text{Pt} \rightarrow ^{166}\text{Os}$	$Q_\alpha = 6707(3)$ . $\% \alpha = 98(2)$ (2018BA41). $T_{1/2} = 13.93 \text{ ms}$ (24), $I_\alpha = 100$ (2008BA14).	1.5636(19)
$^{170}\text{Hg} \rightarrow ^{166}\text{Pt}$	$Q_\alpha = 7773(30)$ . $\% \alpha = 100$ , $T_{1/2} = 0.08 \text{ ms}$ (+40-4) (2019HI06). $I_\alpha = 100$ . $Q_\alpha$ : From 2019HI06, based on $E_\alpha = 7590 \text{ keV}$ (30).	1.526(64)
$^{172}\text{Os} \rightarrow ^{168}\text{W}$	$Q_\alpha = 5224(7)$ . $\% \alpha = 1.4(3)$ (2004GOZZ). $T_{1/2} = 19.2 \text{ s}$ (9) (1995HI02). $I_\alpha = 95(5)$ (2010BA27).	1.583 (13)
$^{172}\text{Pt} \rightarrow ^{168}\text{Os}$	$Q_\alpha = 6463(4)$ . $\% \alpha = 94(6)$ (2004GOZZ). $T_{1/2} = 97.5 \text{ ms}$ (13). $I_\alpha = 98(2)$ (2010BA27). $T_{1/2}$ : WA of $97.6 \text{ ms}$ (13) (2003DA06), $104 \text{ ms}$ (7) (2002RO17) and $96 \text{ ms}$ (3) (1996PA01).	1.5578(40)
$^{172}\text{Hg} \rightarrow ^{168}\text{Pt}$	$Q_\alpha = 7524(6)$ . $T_{1/2} = 231 \mu\text{s}$ (9) (2009SA27). $\% \alpha = 100$ , $I_\alpha = 99.3(7)$ (2010BA27).	1.5567(30)
$^{174}\text{Hf} \rightarrow ^{170}\text{Yb}$	$Q_\alpha = 2449.5(23)$ (2017Wa10). $T_{1/2} = 7.0 \times 10^{16} \text{ y}$ (12) (2020CA15). The value of $E_\alpha$ is not given in 2020CA15. $\% \alpha = 100$ , $I_\alpha = 100$ (2018BA41). $Q_\alpha = 2559(31)$ (from $E_\alpha = 2500(30) \text{ keV}$ ) and $T_{1/2} = 2.0 \times 10^{15} \text{ y}$ (4) from 1961MA05 gives radius parameter of $1.552(51) \text{ fm}$ , but these data are not used here as the half-life is about 35 times shorter than in 2020CA15, and the deduced $Q_\alpha$ is not in good agreement with the value recommended in 2017WA10.	1.4833(91)
$^{174}\text{Os} \rightarrow ^{170}\text{W}$	$Q_\alpha = 4871(10)$ . $T_{1/2} = 44 \text{ s}$ (5). $\% \alpha = 0.020(10)$ , $I_\alpha = 100$ (2018BA41). $T_{1/2}$ : WA of $45 \text{ s}$ (5) (1973BE67) and $42 \text{ s}$ (6) (1972BE89).	1.540(34)
$^{174}\text{Pt} \rightarrow ^{170}\text{Os}$	$Q_\alpha = 6183(3)$ . $T_{1/2} = 0.868 \text{ s}$ (9). $\% \alpha = 75(4)$ , $I_{\alpha 1} = 99.5(5)$ , $I_{\alpha 2} < 1$ (2018BA41). $T_{1/2}$ : WA of $0.7 \text{ s}$ (2) (1966SI08), $0.80 \text{ s}$ (5) (1981DE22), $0.90 \text{ s}$ (1) (1982EN03), $0.890 \text{ s}$ (20) (1996PA01), $0.857 \text{ s}$ (5) (2004GOZZ) and $0.93 \text{ s}$ (3) (2014PE02).	1.5551(32)
$^{174}\text{Hg} \rightarrow ^{170}\text{Pt}$	$Q_\alpha = 7233(6)$ . $T_{1/2} = 1.9 \text{ ms}$ (+4-3), $\% \alpha = 99.7(3)$ , $I_\alpha = 100$ (2018BA41).	1.548(12)
$^{176}\text{Pt} \rightarrow ^{172}\text{Os}$	$Q_\alpha = 5885.1(21)$ . $\% \alpha = 40(3)$ . $T_{1/2} = 6.33 \text{ s}$ (15) (1973GA08). $I_{\alpha 1} = 99.74(13)$ , $I_{\alpha 2} = 0.26(13)$ (1979HA10). $\% \alpha$ : WA of $42(4)$ (1996PA01), $38(3)$ (1979HA10) and $42(4)$ (1970HA18).	1.5597(42)
$^{176}\text{Hg} \rightarrow ^{172}\text{Pt}$	$Q_\alpha = 6897(6)$ . $\% \alpha = 91(9)$ . $T_{1/2} = 20.8 \text{ ms}$ (20). $I_\alpha = 100$ (ENSDF updates private communication 2018). $T_{1/2}$ : Weighted average of $20 \text{ ms}$ (3) (2009AN20), $22 \text{ ms}$ (1) (2004GOZZ); uncertainty is taken as doubled in averaging procedure so that it is not weighted by more than 50%, $20 \text{ ms}$ (2) (2002RO17), $21 \text{ ms}$ (3) (2001JU09, 1998MU25), $20 \text{ ms}$ (3) (1999TO11) and $21 \text{ ms}$ (4) (1999PO09). The value $18 \text{ ms}$ (10) (1996PA01) is not considered because of its comparatively large uncertainty. $\% \alpha$ : 1999PO09 give $\% \alpha = 94(12)$ , which has been adjusted here to $91(9)$ as the maximum alpha branch cannot exceed 100%.	1.5457(75)
$^{178}\text{Pt} \rightarrow ^{174}\text{Os}$	$Q_\alpha = 5573.0(22)$ . $\% \alpha = 7.7(3)$ (2009AC01). $T_{1/2} = 20.8 \text{ s}$ (8). $I_{\alpha 1} = 96.7(4)$ , $I_{\alpha 2} = 3.3(4)$ (2019HAAA). $T_{1/2}$ : WA of $20 \text{ s}$ (1) (2000KO16), $22 \text{ s}$ (2) (1993ME13), $21 \text{ s}$ (1) (1982BO04), $19 \text{ s}$ (2) (1970HA18), $21.2 \text{ s}$ (8) (1968DE01) and $21.3 \text{ s}$ (15) (1966SI08).	1.5708(31)
$^{178}\text{Hg} \rightarrow ^{174}\text{Pt}$	$Q_\alpha = 6577.3(30)$ . $\% \alpha = 89(4)$ (2012VE04). $T_{1/2} = 266.6 \text{ ms}$ (23). $I_\alpha = 98(2)$ (1999BR24). $T_{1/2}$ : WA of $283 \text{ ms}$ (23) (2004GOZZ), $269 \text{ ms}$ (3) (2002RO17), $262 \text{ ms}$ (4) (200KO01), $287 \text{ ms}$ (23) (1996PA01), $250 \text{ ms}$ (25) (1991SE01), $260 \text{ ms}$ (30) (1979HA10) and $260 \text{ ms}$ (30) (1976HOZD).	1.5409(29)
$^{178}\text{Pb} \rightarrow ^{174}\text{Hg}$	$Q_\alpha = 7790(14)$ . $\% \alpha = 100$ (2009AC01). $T_{1/2} = 0.21 \text{ ms}$ (+21-8), $I_\alpha = 100$ (2016BA60).	1.545(35)
$^{180}\text{Pt} \rightarrow ^{176}\text{Os}$	$Q_\alpha = 5277(5)$ . $T_{1/2} = 56 \text{ s}$ (3) (2015MC03). $\% \alpha = 0.52(5)$ (2020CU02). $I_{\alpha 1} = 97.8(2)$ , $I_{\alpha 2} = 2.2(2)$ (2019CUBB). $Q_\alpha$ : From 2020CU02, based on $E_\alpha = 5160(5) \text{ keV}$ (30)	1.5468(62)
$^{180}\text{Hg} \rightarrow ^{176}\text{Pt}$	$Q_\alpha = 6258.5(24)$ . $\% \alpha = 48(2)$ , $T_{1/2} = 2.59 \text{ s}$ (1) (2015MC03). $I_{\alpha 1} = 99.87(3)$ , $I_{\alpha 2} = 5.4 \times 10^{-2}(9)$ , $I_{\alpha 3} = 7.9 \times 10^{-2}$ (2006BA16).	1.5324(24)
$^{180}\text{Pb} \rightarrow ^{176}\text{Hg}$	$Q_\alpha = 7419(5)$ . $\% \alpha = 100$ , $T_{1/2} = 4.1 \text{ ms}$ (3) (2015MC03). $I_\alpha > 96$ (2006BA16). $I_\alpha$ : $98(2)$ used to deduce radius parameter.	1.5184(43)
$^{182}\text{Pt} \rightarrow ^{178}\text{Os}$	$Q_\alpha = 4951(5)$ . $\% \alpha = 0.038(2)$ , $T_{1/2} = 2.67 \text{ min}$ (12) (2015SI18). $I_\alpha = 91(9)$ (2009AC01).	1.5539(68)
$^{182}\text{Hg} \rightarrow ^{178}\text{Pt}$	$Q_\alpha = 5996(5)$ . $\% \alpha = 13.8(9)$ , $T_{1/2} = 10.83 \text{ s}$ (6) (2015SI18). $I_{\alpha 1} = 99.2(1)$ , $I_{\alpha 2} = 0.57(10)$ , $I_{\alpha 3} = 0.24(6)$ (2009AC01). $I_{\alpha 1}$ : Uncertainty deduced by authors using values of $I_{\alpha 2}$ and $I_{\alpha 3}$ .	1.5176(41)
$^{182}\text{Pb} \rightarrow ^{178}\text{Hg}$	$Q_\alpha = 7066(6)$ . $\% \alpha = 99(1)$ (2015SI18). $T_{1/2} = 59 \text{ ms}$ (6). $I_\alpha = 94(6)$ (1998AK04). $T_{1/2}$ : WA of $55 \text{ ms}$ (5) (1999TO11) and $68 \text{ ms}$ (7) (2000JE09).	1.5093(64)
$^{184}\text{Pt} \rightarrow ^{180}\text{Os}$	$Q_\alpha = 4599(8)$ . $\% \alpha = 0.0017(7)$ , $T_{1/2} = 17.3 \text{ min}$ (2), $I_\alpha = 94(6)$ (2015MC03).	1.542(27)
$^{184}\text{Hg} \rightarrow ^{180}\text{Pt}$	$Q_\alpha = 5662(4)$ . $\% \alpha = 1.26(20)$ , $T_{1/2} = 30.87 \text{ s}$ (26), $I_{\alpha 1} = 99.44(10)$ , $I_{\alpha 2} = 0.40(8)$ , $I_{\alpha 3} = 0.16(3)$ (2015MC03).	1.5120(81)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{184}\text{Pb} \rightarrow ^{180}\text{Hg}$	$Q_\alpha = 6774(3)$ . $\% \alpha = 80(15)$ , $T_{1/2} = 490 \text{ ms}$ (25) (2015MC03). $I_\alpha = 91(9)$ (1998AK04).	1.504(11)
$^{186}\text{Os} \rightarrow ^{182}\text{W}$	$Q_\alpha = 2821.2(9)$ . $\% \alpha = 100$ , $T_{1/2} = 2.0 \times 10^{15} \text{ y}$ (11), $I_\alpha = 97.5(25)$ (2015SI18).	1.486(29)
$^{186}\text{Pt} \rightarrow ^{182}\text{Os}$	$Q_\alpha = 4320(18)$ . $T_{1/2} = 2.08 \text{ h}$ (5). $\% \alpha = 0.00018(10)$ , $I_\alpha = 94(6)$ (2015SI18). $T_{1/2}$ : WA of $2.10 \text{ h}$ (5) (1991BE25), $2.0 \text{ h}$ (1) (1972FI12) and $2.0 \text{ h}$ (2) (1963GR08). $\% \alpha$ : $\approx 0.00014\%$ was deduced by 1963GR08 by assuming that neighboring mass nuclei were produced in equal quantities and their reported branching is estimated to be correct within a factor of 2. Therefore, the probable branching i.e. $\% \alpha = 0.00014$ , $0.00028$ and $0.00007$ gives radius parameters as $r_0 = 1.518 \text{ fm}$ , $r_0 = 1.574 \text{ fm}$ , $r_0 = 1.485 \text{ fm}$ , respectively (2015SI18). The adopted value of $\% \alpha$ is $0.00018(10)$ .	1.536(30)
$^{186}\text{Hg} \rightarrow ^{182}\text{Pt}$	$Q_\alpha = 5204(10)$ . $\% \alpha = 0.016(5)$ , $T_{1/2} = 1.38 \text{ min}$ (6), $I_\alpha = 94(6)$ (2015SI18).	1.500(17)
$^{186}\text{Pb} \rightarrow ^{182}\text{Hg}$	$Q_\alpha = 6470(6)$ . $\% \alpha = 40(8)$ , $T_{1/2} = 4.82 \text{ s}$ (3), $I_{\alpha_1} = 99.6(2)$ , $I_{\alpha_2} = 0.20(5)$ , $I_{\alpha_3} < 0.16$ (2015SI18).	1.486(10)
$^{186}\text{Po} \rightarrow ^{182}\text{Pb}$	$Q_\alpha = 8501(14)$ . $\% \alpha \approx 100$ (2015SI18). $T_{1/2} = 28 \text{ } \mu\text{s}$ (+16-6) (2013AN13). $I_\alpha = 100$ .	1.488(19)
$^{188}\text{Pt} \rightarrow ^{184}\text{Os}$	$Q_\alpha = 4007(5)$ . $T_{1/2} = 10.2 \text{ d}$ (3). $\% \alpha = 2.6 \times 10^{-5}(3)$ , $I_\alpha = 95(5)$ (2010BA05). $T_{1/2}$ : WA of $10.5 \text{ d}$ (10) (1963KA17), $10.2 \text{ d}$ (3) (1963GR08), $10.0 \text{ d}$ (3) (1955SM42) and $10.3 \text{ d}$ (4) (1954NA25).	1.4648(74)
$^{188}\text{Hg} \rightarrow ^{184}\text{Pt}$	$Q_\alpha = 4707(16)$ . $\% \alpha = 3.7 \times 10^{-5}(8)$ , $T_{1/2} = 3.25 \text{ min}$ (15) (2018KO15). $I_\alpha = 96(4)$ (2010BA05).	1.480(15)
$^{188}\text{Pb} \rightarrow ^{184}\text{Hg}$	$Q_\alpha = 6109(3)$ . $\% \alpha = 8.5(5)$ , $T_{1/2} = 25.5 \text{ s}$ (1) (2018KO15). $I_{\alpha_1} = 99(1)$ , $I_{\alpha_2} = 0.095$ , $I_{\alpha_3} \approx 1$ (2010BA05).	1.4885(32)
$^{188}\text{Po} \rightarrow ^{184}\text{Pb}$	$Q_\alpha = 8082(15)$ . $T_{1/2} = 275 \text{ } \mu\text{s}$ (30) (2003VA16). $\% \alpha \approx 100$ , $I_{\alpha_1} = 80(4)$ , $I_{\alpha_2} = 20(4)$ (2010BA05).	1.4868(76)
$^{190}\text{Pt} \rightarrow ^{186}\text{Os}$	$Q_\alpha = 3268.6(6)$ . $T_{1/2} = 4.97 \times 10^{11} \text{ y}$ (16) (2017BR04). $\% \alpha = 100$ , $I_\alpha = 100$ (2003BA44).	1.4651(16)
$^{190}\text{Pb} \rightarrow ^{186}\text{Hg}$	$Q_\alpha = 5698(5)$ . $\% \alpha = 0.40(4)$ , $T_{1/2} = 71 \text{ s}$ (1), $I_{\alpha_1} = 99.90(2)$ , $I_{\alpha_2} = 0.084(15)$ , $I_{\alpha_3} = 0.014(6)$ (2003BA44). $I_{\alpha_1}$ : Uncertainty deduced by authors using values of $I_{\alpha_2}$ and $I_{\alpha_3}$ .	1.4923(55)
$^{190}\text{Po} \rightarrow ^{186}\text{Pb}$	$Q_\alpha = 7693(7)$ . $T_{1/2} = 2.46 \text{ ms}$ (5). $\% \alpha = 100$ , $I_{\alpha_1} = 96.4(4)$ , $I_{\alpha_2} = 3.3(4)$ , $I_{\alpha_3} = 0.3(1)$ (2003BA44). $T_{1/2}$ : WA of $2.5 \text{ ms}$ (1) (2003VA05), $2.45 \text{ ms}$ (5) (2000AN14, 2001AN07) and $2.53 \text{ ms}$ (33) (1999AN22).	1.5114(26)
$^{192}\text{Pb} \rightarrow ^{188}\text{Hg}$	$Q_\alpha = 5221(5)$ . $\% \alpha = 0.0059(10)$ . $T_{1/2} = 3.5 \text{ min}$ (1) (2012BA36). $I_\alpha = 100$ (2018KO15). $\% \alpha$ : WA of $0.0057(10)$ (1979TO06) and $0.0061(11)$ (1992WA14).	1.5005(86)
$^{192}\text{Po} \rightarrow ^{188}\text{Pb}$	$Q_\alpha = 7320(3)$ . $\% \alpha = 99.5(5)$ , $T_{1/2} = 32.2 \text{ ms}$ (3) (2012BA36). $I_{\alpha_1} = 98.57(15)$ , $I_{\alpha_2} = 1.43(15)$ (2018KO15).	1.5137(13)
$^{194}\text{Pb} \rightarrow ^{190}\text{Hg}$	$Q_\alpha = 4738(17)$ . $\% \alpha = 7.3 \times 10^{-6}(29)$ , $T_{1/2} = 10.7 \text{ min}$ (6) (2006SI17). $I_\alpha = 99.9(1)$ (2003SI05).	1.437(24)
$^{194}\text{Po} \rightarrow ^{190}\text{Pb}$	$Q_\alpha = 6987(3)$ . $\% \alpha = 93(7)$ (1993WA04). $T_{1/2} = 0.392 \text{ s}$ (4) (2006SI17). $I_{\alpha_1} = 99.71(6)$ , $I_{\alpha_2} = 0.24(3)$ . $I_{\alpha_3} = 0.05(5)$ (2003SI05).	1.5113(39)
$^{194}\text{Rn} \rightarrow ^{190}\text{Po}$	$Q_\alpha = 7862(10)$ . $T_{1/2} = 0.78 \text{ ms}$ (16) (2006AN36). $\% \alpha = 100$ , $I_\alpha = 100$ (ENSDF updates Jan.-2014).	1.590(11)
$^{196}\text{Po} \rightarrow ^{192}\text{Pb}$	$Q_\alpha = 6658.1(24)$ . $\% \alpha = 94(5)$ , $T_{1/2} = 5.60 \text{ s}$ (8), $I_{\alpha_1} = 99.978$ , $I_{\alpha_2} = 0.022$ , $I_{\alpha_3} < 0.0065$ (2012BA36).	1.5126(28)
$^{196}\text{Rn} \rightarrow ^{192}\text{Po}$	$Q_\alpha = 7617(9)$ . $T_{1/2} = 4.4 \text{ ms}$ (+13-9) (2001KE06). $\% \alpha = 99.80(20)$ , $I_\alpha = 100$ (2012BA36).	1.585(15)
$^{198}\text{Po} \rightarrow ^{194}\text{Pb}$	$Q_\alpha = 6309.7(14)$ . $\% \alpha = 57(2)$ , $T_{1/2} = 1.760 \text{ min}$ (24) (2016HU04). $I_{\alpha_1} = 99.9987(3)$ , $I_{\alpha_2} = 0.00133(24)$ (2006SI17).	1.4962(19)
$^{198}\text{Rn} \rightarrow ^{194}\text{Po}$	$Q_\alpha = 7349(4)$ . $T_{1/2} = 65 \text{ ms}$ (3) (2016HU04). $\% \alpha = 99.4(6)$ , $I_{\alpha_1} = 99.93(2)$ , $I_{\alpha_2} = 0.07(2)$ (2006SI17).	1.5455(27)
$^{200}\text{Po} \rightarrow ^{196}\text{Pb}$	$Q_\alpha = 5981.6(18)$ . $\% \alpha = 11.1(3)$ (2007KO42). $T_{1/2} = 11.5 \text{ min}$ (1), $I_\alpha = 100$ (2007HU13).	1.4803(16)
$^{200}\text{Rn} \rightarrow ^{196}\text{Po}$	$Q_\alpha = 7043.4(21)$ . $\% \alpha = 91(9)$ , $T_{1/2} = 1.03 \text{ s}$ (+20-11) (2007KO42). $I_{\alpha_1} = 99.986(3)$ , $I_{\alpha_2} = 0.006(2)$ , $I_{\alpha_3} = 0.0081(7)$ (1998AK04).	1.5205(93)
$^{202}\text{Po} \rightarrow ^{198}\text{Pb}$	$Q_\alpha = 5701.0(17)$ . $\% \alpha = 1.92(7)$ , $T_{1/2} = 44.6 \text{ min}$ (4), $I_\alpha = 100$ (2016HU04).	1.4720(20)
$^{202}\text{Rn} \rightarrow ^{198}\text{Po}$	$Q_\alpha = 6773.8(18)$ . $\% \alpha = 78(8)$ , $T_{1/2} = 9.7 \text{ s}$ (1), $I_{\alpha_1} = 99.9982(6)$ , $I_{\alpha_2} < 0.018$ , $I_{\alpha_3} = 0.0018(6)$ (2016HU04).	1.5106(49)
$^{202}\text{Ra} \rightarrow ^{198}\text{Rn}$	$Q_\alpha = 7880(7)$ . $T_{1/2} = 3.8 \text{ ms}$ (+13-8) (2014KA23). $\% \alpha = 100$ , $I_\alpha = 100$ (2016HU04).	1.573(15)
$^{204}\text{Po} \rightarrow ^{200}\text{Pb}$	$Q_\alpha = 5484.9(14)$ . $\% \alpha = 0.67(3)$ , $T_{1/2} = 3.519 \text{ h}$ (12) (2010CH02). $I_\alpha = 100$ (2007KO42).	1.4625(22)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{204}\text{Rn} \rightarrow ^{200}\text{Po}$	$Q_\alpha = 6546.7(18)$ . $\% \alpha = 72.4(9)$ , $T_{1/2} = 74.5 \text{ s}$ (14) (2010CH02). $I_\alpha = 100$ (2007KO42).	1.5026(13)
$^{204}\text{Ra} \rightarrow ^{200}\text{Rn}$	$Q_\alpha = 7637(7)$ . $\% \alpha = 100$ (2010CH02). $T_{1/2} = 54 \text{ ms}$ (+19-11) (2005UU02). $I_\alpha = 100$ (2007KO42).	1.525(14)
$^{206}\text{Po} \rightarrow ^{202}\text{Pb}$	$Q_\alpha = 5327.0(13)$ . $\% \alpha = 5.45(5)$ , $T_{1/2} = 8.8 \text{ d}$ (1) (2008KO21). $I_\alpha = 100$ (2008ZH05).	1.4547(10)
$^{206}\text{Rn} \rightarrow ^{202}\text{Po}$	$Q_\alpha = 6383.7(16)$ . $\% \alpha = 62(3)$ , $T_{1/2} = 5.67 \text{ min}$ (17) (2008KO21). $I_\alpha = 100$ (2008ZH05).	1.4917(27)
$^{206}\text{Ra} \rightarrow ^{202}\text{Rn}$	$Q_\alpha = 7415(4)$ . $\% \alpha = 99.3(7)$ . $T_{1/2} = 0.24 \text{ s}$ (2) (2008KO21). $I_\alpha = 100$ (2008ZH05). $\% \alpha$ : Based on theoretical $T_{1/2}(\alpha) = 0.20 \text{ s}$ and $T_{1/2}(\beta^+) = 11.93 \text{ (s)}$ , which gives $\% \epsilon + \% \beta^+ \approx 1.5$ (2019MO01) or $\% \alpha = 99.3(7)$ .	1.5287(42)
$^{208}\text{Po} \rightarrow ^{204}\text{Pb}$	$Q_\alpha = 5215.4(13)$ . $\% \alpha = 99.9960(4)$ (2007MA45). $T_{1/2} = 2.898 \text{ y}$ (2), $I_{\alpha_1} = 99.99976(7)$ , $I_{\alpha_2} = 0.00024(7)$ (2010CH02).	1.42967(74)
$^{208}\text{Rn} \rightarrow ^{204}\text{Po}$	$Q_\alpha = 6260.7(17)$ . $\% \alpha = 62(7)$ , $T_{1/2} = 24.35 \text{ min}$ (14), $I_{\alpha_1} = 99.953(4)$ , $I_{\alpha_2} = 0.047(4)$ (2010CH02).	1.4755(52)
$^{208}\text{Ra} \rightarrow ^{204}\text{Rn}$	$Q_\alpha = 7273(5)$ . $T_{1/2} = 1.110 \text{ s}$ (45) (2010HE25). $\% \alpha = 95(5)$ , $I_\alpha = 100$ (2010CH02). $T_{1/2}$ : 1.1 s (+21-5) and 0.41 s (+75-16) (2015MA37) are not considered due to comparatively large uncertainties.	1.5029(36)
$^{210}\text{Pb} \rightarrow ^{206}\text{Hg}$	$Q_\alpha = 3792(20)$ . $\% \alpha = 1.9 \times 10^{-6}(4)$ , $T_{1/2} = 22.20 \text{ y}$ (22) (2014BA41). $I_\alpha = 100$ (2008KO21).	1.449(21)
$^{210}\text{Po} \rightarrow ^{206}\text{Pb}$	$Q_\alpha = 5407.53(7)$ . $\% \alpha = 100$ , $T_{1/2} = 138.376 \text{ d}$ (14) (2014BA41). $I_{\alpha_1} = 99.99885(9)$ , $I_{\alpha_2} = 0.00115(9)$ (2018SH12). $T_{1/2}$ : Uncertainty of 0.002 d quoted in 2014BA41 evaluation increased to 0.014 d, as per guidelines for half-life evaluations for ENSDF, accepted at the 2015 NSDD meeting. $T_{1/2} = 138.43 \text{ d}$ (21) (2015ZH41) and 140.6 d (15) (2014PO01) are imprecise, thus not considered here. $I_{\alpha_1}$ : Uncertainty is deduced by authors using values of $I_{\alpha_2}$ .	1.408790(38)
$^{210}\text{Rn} \rightarrow ^{206}\text{Po}$	$Q_\alpha = 6159.0(22)$ . $\% \alpha = 96(1)$ , $T_{1/2} = 2.4 \text{ h}$ (1) (2014BA41). $I_{\alpha_1} = 99.9944(3)$ , $I_{\alpha_2} = 0.0056(3)$ (2008KO21).	1.4568(22)
$^{210}\text{Ra} \rightarrow ^{206}\text{Rn}$	$Q_\alpha = 7151(3)$ . $\% \alpha = 95(5)$ . $T_{1/2} = 3.9 \text{ s}$ (1). $I_{\alpha_1} = 99.97$ , $I_{\alpha_2} = 0.03$ (2008KO21). $T_{1/2}$ : WA of 3.8 s (2) (1967VA22), 3.6 s (2) (1968LO15) and 4.0 s (1) (2008HA12). $T_{1/2}$ : 6.6 ms (+317-30) and 1.4 s (+67-6) (2015MA37) are not considered due to comparatively large uncertainties. $\% \alpha$ : Based on theoretical $T_{1/2}(\alpha) = 3.7 \text{ s}$ and $T_{1/2}(\beta) = 68.9 \text{ (s)}$ , which gives $\% \beta = 5\%$ (2019MO01) and allowing 100% uncertainty gives $\% \beta < 10\%$ or $\% \alpha = 95(5)$ .	1.4861(29)
$^{210}\text{Th} \rightarrow ^{206}\text{Ra}$	$Q_\alpha = 8069(6)$ . $T_{1/2} = 16.0 \text{ ms}$ (36) (2010HE25). $\% \alpha \approx 100$ , $I_\alpha = 100$ (2008KO21).	1.507(11)
$^{212}\text{Po} \rightarrow ^{208}\text{Pb}$	$Q_\alpha = 8954.20(11)$ . $T_{1/2} = 0.2956 \mu\text{s}$ (10). $\% \alpha = 100$ , $I_\alpha = 100$ (2007MA45). $T_{1/2}$ : WA of 0.2939 $\mu\text{s}$ (12) (2017AP03), 0.309 $\mu\text{s}$ (11) (1981BO29), 0.296 $\mu\text{s}$ (2) (1975SA06), 0.304 $\mu\text{s}$ (8) (1972MC29), 0.305 $\mu\text{s}$ (5) (1963AS02), 0.304 $\mu\text{s}$ (4) (1949BU09), 0.2947 $\mu\text{s}$ (10) (2013BE31) and 0.299 $\mu\text{s}$ (2) (2010AS03).	1.52177(18)
$^{212}\text{Rn} \rightarrow ^{208}\text{Po}$	$Q_\alpha = 6385.1(26)$ . $\% \alpha = 100$ , $T_{1/2} = 23.9 \text{ min}$ (12), $I_{\alpha_1} = 99.950(5)$ , $I_{\alpha_2} = 0.050(5)$ (2007MA45).	1.4343(25)
$^{212}\text{Ra} \rightarrow ^{208}\text{Rn}$	$Q_\alpha = 7031.7(17)$ . $\% \alpha = 94(6)$ . $T_{1/2} = 13.0 \text{ s}$ (2), $I_{\alpha_1} = 99.95$ , $I_{\alpha_2} = 0.05$ (2007MA45). $T_{1/2}$ : 9.9 s (+46-24) (2014YA19) is not considered due to comparatively large uncertainty. $\% \alpha$ : Based on theoretical $T_{1/2}(\alpha) = 2.9 \text{ s}$ and $T_{1/2}(\beta) > 100 \text{ (s)}$ , which gives $\% \beta < 3\%$ (2019MO01) but using experimental $T_{1/2}(\alpha) = 13.0 \text{ s}$ gives $\% \beta < 12\%$ or $\% \alpha = 94(6)$ .	1.4718(31)
$^{212}\text{Th} \rightarrow ^{208}\text{Ra}$	$Q_\alpha = 7958(5)$ . $T_{1/2} = 31.7 \text{ ms}$ (13) (ENSDF updates Dec.-2015). $\% \alpha = 99.7(3)$ , $I_\alpha = 98.8(12)$ (2007MA45). $T_{1/2}$ : 22 ms (+22-7) and 28 ms (+51-11) (2015MA37) are not considered due to comparatively large uncertainties.	1.5058(26)
$^{214}\text{Po} \rightarrow ^{210}\text{Pb}$	$Q_\alpha = 7833.54(6)$ . $T_{1/2} = 163.47 \mu\text{s}$ (4). $\% \alpha = 100$ , $I_{\alpha_1} = 99.9895(6)$ , $I_{\alpha_2} = 0.0104(6)$ , $I_{\alpha_3} = 6 \times 10^{-5}(2)$ (2014BA41). $T_{1/2}$ : WA of 163.46 $\mu\text{s}$ (4) (2016AL28), 163.58 $\mu\text{s}$ (31) (2013BE31) and 164.2 $\mu\text{s}$ (6) (2012SU11). The values 169.5 $\mu\text{s}$ (94) (2015AL27) and 163.8 $\mu\text{s}$ (30) (2013BE20) are imprecise, thus not considered here.	1.539616(24)
$^{214}\text{Rn} \rightarrow ^{210}\text{Po}$	$Q_\alpha = 9208(9)$ . $T_{1/2} = 259 \text{ ns}$ (3) (2019PA45). $\% \alpha = 100$ , $I_\alpha = 99.95(5)$ (2014BA41). $T_{1/2}$ : 0.27 s (2) (1970VA13) is not considered due to comparatively large uncertainty.	1.5340(25)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{214}\text{Ra} \rightarrow ^{210}\text{Rn}$	$Q_\alpha = 7272.6(26)$ . $\% \alpha = 99.941(4)$ (2009WU02). $T_{1/2} = 2.44$ s (4). $I\alpha_1 = 99.84(3)$ , $I\alpha_2 = 0.16(3)$ (2014BA41). $T_{1/2}$ : WA of 2.36 s (6) (2015KH09) and 2.46 s (3) (1973BE33).	1.4557(12)
$^{214}\text{Th} \rightarrow ^{210}\text{Ra}$	$Q_\alpha = 7827(5)$ . $\% \alpha = 99.90(10)$ , $T_{1/2} = 87$ ms (10) (2014BA41). $I\alpha = 99.5(5)$ (1998AK04). $T_{1/2}$ : 68 ms (+93–25) and 67 ms (+322–31) (2015MA37) are not considered due to comparatively large uncertainties.	1.4986(56)
$^{216}\text{Po} \rightarrow ^{212}\text{Pb}$	$Q_\alpha = 6906.4(5)$ . $\% \alpha = 100$ , $T_{1/2} = 144.0$ ms (6) (2017NA22). $I\alpha_1 = 99.9981(3)$ , $I\alpha_2 = 0.0019(3)$ (2005BR03). $T_{1/2}$ : 136 ms (6) (2018BA44), 175 ms (+13–11) (2012BE14), 144 ms (8) (2003DA24) and 145 ms (2) (1963DI05) are not considered due to comparatively large uncertainties.	1.54117(28)
$^{216}\text{Rn} \rightarrow ^{212}\text{Po}$	$Q_\alpha = 8197(6)$ . $\% \alpha = 100$ , $T_{1/2} = 45$ $\mu$ s (5) (2007WU02). $I\alpha = 99.6(4)$ (2005BR03).	1.5658(59)
$^{216}\text{Ra} \rightarrow ^{212}\text{Rn}$	$Q_\alpha = 9526(8)$ . $\% \alpha = 100$ (2007WU02). $T_{1/2} = 172$ ns (10). $I\alpha = 99.97(3)$ (2005BR03). $T_{1/2}$ : WA of 161 ns (11) (2019PA45) and 182 ns (10) (1973NO09).	1.5433(36)
$^{216}\text{Th} \rightarrow ^{212}\text{Ra}$	$Q_\alpha = 8072(4)$ . $\% \alpha = 100$ , $T_{1/2} = 26.0$ ms (2) (2007WU02). $I\alpha_1 = 99.6(1)$ , $I\alpha_2 = 0.4(1)$ (2005KU31). $T_{1/2}$ : 29 ms (+13–7) (2014YA19) is not considered due to comparatively large uncertainty.	1.4695(14)
$^{216}\text{U} \rightarrow ^{212}\text{Th}$	$Q_\alpha = 8531(26)$ . $T_{1/2} = 4.7$ ms (+47–16) (2015MA37). $\% \alpha = 100$ , $I\alpha = 100$ (ENSDF updates Dec.-2015). $T_{1/2}$ : 3.8 ms (+88–32) (2015DE22) is not considered due to comparatively large uncertainty.	1.486(33)
$^{218}\text{Po} \rightarrow ^{214}\text{Pb}$	$Q_\alpha = 6114.75(9)$ . $T_{1/2} = 3.098$ min (12) (2006JA03). $\% \alpha = 99.980(2)$ , $I\alpha_1 = 99.9989(11)$ , $I\alpha_2 = 0.0011$ (ENSDF updates Feb.-2015).	1.53788(19)
$^{218}\text{Rn} \rightarrow ^{214}\text{Po}$	$Q_\alpha = 7262.5(19)$ . $T_{1/2} = 33.75$ ms (15) (2012SU11). $\% \alpha = 100$ , $I\alpha_1 = 99.87(1)$ , $I\alpha_2 = 0.127(10)$ (2009WU02).	1.56062(74)
$^{218}\text{Ra} \rightarrow ^{214}\text{Rn}$	$Q_\alpha = 8540(4)$ . $\% \alpha = 99.88(6)$ (2019PA45). $T_{1/2} = 25.91$ $\mu$ s (14). $I\alpha = 99.5$ (5) (2009WU02). $T_{1/2}$ : WA of 25.99 $\mu$ s (10) (2019PA45), 25.2 $\mu$ s (3) (2001Ku07), 26 $\mu$ s (2) (1992WI14) and 25.6 $\mu$ s (11) (1986TO02). $Q_\alpha$ : WA of $Q_\alpha = 8538$ keV (4) based on $E_\alpha = 8810$ keV (13) (2019PA45), $Q_\alpha = 8546$ keV (6) based on $E_\alpha = 8385$ keV (10) (1970VA13) and $Q_\alpha = 8392$ keV (8) (1970TO07).	1.5655(13)
$^{218}\text{Th} \rightarrow ^{214}\text{Ra}$	$Q_\alpha = 9849(9)$ . $\% \alpha = 100$ (2006JA03). $T_{1/2} = 122$ ns (5). $I\alpha = 100$ (2009WU02). $T_{1/2}$ : NRM WA of 169 ns (+73–40) (2018BR13), 160 ns (40) (2015KH09), 96 ns (7) (1973NO09, 1973HI06), 122 ns (8) (1973HA32) and 125 ns (5) (1982CH29). The NRM method is preferred, as in 2019SI39 evaluation, because regular weighted average gives reduced $\chi^2$ of 3.7 as compared to critical $\chi^2 = 2.4$ .	1.5487(30)
$^{218}\text{U} \rightarrow ^{214}\text{Th}$	$Q_\alpha = 8775(9)$ . $T_{1/2} = 0.51$ ms (+17–10) (2006JA03). $\% \alpha = 100$ , $I\alpha = 100$ (2009WU02). $T_{1/2}$ : 1.15 s (+158–42) (2015MA37) is not considered due to comparatively large uncertainty.	1.512(14)
$^{220}\text{Rn} \rightarrow ^{216}\text{Po}$	$Q_\alpha = 6404.74(10)$ . $\% \alpha = 100$ , $T_{1/2} = 55.6$ s (1) (2011BR05). $I\alpha_1 = 99.886(17)$ , $I\alpha_2 = 0.114(17)$ (2007WU02). $T_{1/2}$ : The values 58 s (4) (2018BA44) and 64 s (+19–12) (2012BE14) are imprecise, thus not considered here.	1.55548(10)
$^{220}\text{Ra} \rightarrow ^{216}\text{Rn}$	$Q_\alpha = 7592(6)$ . $\% \alpha = 100$ , $T_{1/2} = 18$ ms (2) (2011BR05). $I\alpha_1 = 99.0(4)$ , $I\alpha_2 = 1.0(4)$ (2007WU02). $I\alpha$ : $3^rd$ alpha branch is also reported in 2007WU02, not considered here because of its highly tentative nature.	1.5539(57)
$^{220}\text{Th} \rightarrow ^{216}\text{Ra}$	$Q_\alpha = 8973(13)$ . $T_{1/2} = 10.2$ $\mu$ s (4). $\% \alpha = 100$ (2011BR05). $I\alpha = 99.3(7)$ (2007WU02). $T_{1/2}$ : WA of 10.4 $\mu$ s (4) (2019PA45) and 9.7 $\mu$ s (6) (1973HA32). $Q_\alpha$ : Based on $E_\alpha = 8810$ keV (13) obtained from WA of $E_\alpha = 8818$ keV (13) (2019PA45) and $E_\alpha = 8790$ keV (30) (1973HA32).	1.6051(43)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{222}\text{Rn} \rightarrow ^{218}\text{Po}$	$Q_\alpha = 5590.4(3)$ . $T_{1/2} = 3.8222$ d (9). $\% \alpha = 100$ , $I_{\alpha_1} = 99.92(1)$ , $I_{\alpha_2} = 0.078(1)$ , $I_{\alpha_3} \approx 0.0005$ (2006JA03). $T_{1/2}$ : WA of 3.82146 d (85) (2015BE07, quoted uncertainty of 0.00017 d increased to 0.00085 d, to have a maximum relative weight of 50%); 3.8195 d (30) (2004SC04, reanalysis of 2004SC04 data by 2018PO01 gave 3.825 d (5)); 3.8224 d (18) (1995CO34); 3.82351 d (170) (1972BU33, quoted uncertainty of 0.00034 d increased to 0.00170 d as in 1990HO28 evaluation); 3.83 d (3) (1958SH69); 3.82290 d (170) (1956MA64, quoted uncertainty of 0.00027 d increased to 0.00170 d as in 1990HO28); 3.825 d (5) (1956RO31, quoted uncertainty of 0.004 d increased to 0.005 d as in 1990HO28); 3.825 d (6) (1955TO07,1951TO25, quoted uncertainty of 0.005 d increased to 0.006 d as in 1990HO28); 3.823 d (3) (1924CU01, quoted uncertainty of 0.002 d increased to 0.003 d as in 1990HO28) and 3.825 d (4) (1923BO01).	1.54863(17)
$^{222}\text{Ra} \rightarrow ^{218}\text{Rn}$	$Q_\alpha = 6678(4)$ . $T_{1/2} = 33.6$ s (4) (2012PO13). $\% \alpha = 100$ , $I_{\alpha_1} = 96.9(1)$ , $I_{\alpha_2} = 3.05(5)$ , $I_{\alpha_3} = 0.0041(1)$ , $I_{\alpha_4} = 0.0041(2)$ , $I_{\alpha_5} = 0.0042(1)$ (2006JA03).	1.5492 (18)
$^{222}\text{Th} \rightarrow ^{218}\text{Ra}$	$Q_\alpha = 8127(5)$ . $\% \alpha = 100$ (2011SI24). $T_{1/2} = 1.964$ ms (2), $I_{\alpha_1} = 98.16(5)$ , $I_{\alpha_2} = 1.81(1)$ , $I_{\alpha_3} = 1.8 \times 10^{-2}(3)$ , $I_{\alpha_4} = 1.4 \times 10^{-2}(4)$ (2016PA28).	1.5571(17)
$^{222}\text{U} \rightarrow ^{218}\text{Th}$	$Q_\alpha = 9480(50)$ . $\% \alpha = 100$ , $T_{1/2} = 4.7$ $\mu$ s (7) (2015KH09). $I_\alpha = 100$ . $Q_\alpha$ : Based on $E_\alpha = 9.31$ MeV (5) (2015KH09).	1.529(15)
$^{224}\text{Ra} \rightarrow ^{220}\text{Rn}$	$Q_\alpha = 5788.92(15)$ . $\% \alpha = 100$ , $T_{1/2} = 3.6319$ d (23) (2015SI19). $I_{\alpha_1} = 94.92(5)$ , $I_{\alpha_2} = 5.06(5)$ , $I_{\alpha_3} = 0.0071$ , $I_{\alpha_4} = 0.0076(11)$ , $I_{\alpha_5} = 0.0030(5)$ (2011BR05).	1.542177(86)
$^{224}\text{Th} \rightarrow ^{220}\text{Ra}$	$Q_\alpha = 7299(6)$ . $\% \alpha = 100$ , $T_{1/2} = 1.04$ s (2) (2015SI19). $I_{\alpha_1} = 79(2)$ , $I_{\alpha_2} = 19(2)$ , $I_{\alpha_3} = 1.2(4)$ , $I_{\alpha_4} = 0.3(1)$ (2011BR05).	1.5385(27)
$^{224}\text{U} \rightarrow ^{220}\text{Th}$	$Q_\alpha = 8628(7)$ . $\% \alpha = 100$ (2015SI19). $T_{1/2} = 396$ $\mu$ s (17), $I_{\alpha_1} = 96.6(8)$ , $I_{\alpha_2} = 3.4(8)$ (ENSDF updates Nov.-2014).	1.5514(30)
$^{226}\text{Ra} \rightarrow ^{222}\text{Rn}$	$Q_\alpha = 4870.70(25)$ . $\% \alpha = 100$ , $T_{1/2} = 1600$ y (7) (2011SI24). $I_{\alpha_1} = 94.07$ (1), $I_{\alpha_2} = 5.93$ (1), $I_{\alpha_3} = 0.0059(15)$ (2017MA22). $I_{\alpha_4} = 0.0010(1)$ , $I_{\alpha_5} = 0.00027(5)$ (2011SI24).	1.53945(26)
$^{226}\text{Th} \rightarrow ^{222}\text{Ra}$	$Q_\alpha = 6452.5(10)$ . $\% \alpha = 100$ (2011SI24). $T_{1/2} = 30.83$ min (1). $I_{\alpha_1} = 75.39(10)$ , $I_{\alpha_2} = 22.93(9)$ , $I_{\alpha_3} = 1.266(7)$ , $I_{\alpha_4} = 0.181(4)$ , $I_{\alpha_5} = 0.230$ (5) (2012MA30). $I_{\alpha_6} = 0.00023(2)$ , $I_{\alpha_7} = 0.00034(4)$ , $I_{\alpha_8} = 0.00017(4)$ (2011SI24). $T_{1/2}$ : WA of 30.70 min (3) (2012PO13), 30.57 min (10) (1987MI10) and 30.83 min (1) (1995KO54).	1.53749(45)
$^{226}\text{U} \rightarrow ^{222}\text{Th}$	$Q_\alpha = 7701(4)$ . $T_{1/2} = 267$ ms (9). $\% \alpha = 100$ , $I_{\alpha_1} = 85(5)$ , $I_{\alpha_2} = 15(5)$ (2011SI24). $T_{1/2}$ : WA of 258 ms (13) (2002CAZZ), 260 ms (20) (2001KU07), 281 ms (9) (2000HE17), 260 ms (10) (1999GR28, 1998GR19) and 200 ms (50) (1990AN22). $I_{\alpha_1}$ : 2001Ku07 give $I_{\alpha_1} = 85(11)$ , which has been adjusted here as 85(5) from $I_{\alpha_1} = 100 - I_{\alpha_2}$ .	1.5394(34)
$^{228}\text{Th} \rightarrow ^{224}\text{Ra}$	$Q_\alpha = 5520.15(22)$ . $\% \alpha = 100$ , $T_{1/2} = 1.9125$ y (9), $I_{\alpha_1} = 73.4(5)$ , $I_{\alpha_2} = 26.0(10)$ , $I_{\alpha_3} = 0.408(14)$ , $I_{\alpha_4} = 0.218(8)$ , $I_{\alpha_5} = 0.036(6)$ , $I_{\alpha_6} = 1.0 \times 10^{-5}(3)$ , $I_{\alpha_7} = 2.4 \times 10^{-5}(5)$ , $I_{\alpha_8} = 1.7 \times 10^{-5}(3)$ , $I_{\alpha_9} \approx 4.6 \times 10^{-6}$ (2015SI19).	1.53389(32)
$^{228}\text{U} \rightarrow ^{224}\text{Th}$	$Q_\alpha = 6804(10)$ . $\% \alpha = 97.5(25)$ , $T_{1/2} = 9.1$ min (2), $I_{\alpha_1} = 70(4)$ , $I_{\alpha_2} = 29(4)$ , $I_{\alpha_3} = 0.66(11)$ , $I_{\alpha_4} = 0.56(20)$ (2015SI19). $I_\alpha$ : $I_{\alpha_3}$ and $I_{\alpha_4}$ branches are questionable.	1.5237(51)
$^{228}\text{Pu} \rightarrow ^{224}\text{U}$	$Q_\alpha = 7940(18)$ . $\% \alpha = 100$ , $T_{1/2} = 1.1$ s (+20-5) (2015SI19). $I_\alpha = 100$ (1998AK04).	1.480(42)
$^{230}\text{Th} \rightarrow ^{226}\text{Ra}$	$Q_\alpha = 4769.9(15)$ . $\% \alpha = 100$ , $T_{1/2} = 7.54 \times 10^4$ y (3) (2012BR12). $I_{\alpha_1} = 76.3(3)$ , $I_{\alpha_2} = 23.4(1)$ , $I_{\alpha_3} = 0.151(12)$ , $I_{\alpha_4} = 0.030(15)$ , $I_{\alpha_5} = 9.7 \times 10^{-4}(13)$ , $I_{\alpha_6} = 8.0 \times 10^{-6}$ (20), $I_{\alpha_7} = 1.03 \times 10^{-5}(22)$ , $I_{\alpha_8} \approx 3.4 \times 10^{-6}$ , $I_{\alpha_9} = 1.4 \times 10^{-6}$ (1998AK04).	1.5332 (11)
$^{230}\text{U} \rightarrow ^{226}\text{Th}$	$Q_\alpha = 5992.5(5)$ . $\% \alpha = 100$ , $T_{1/2} = 20.23$ d (2) (2012BR12). $I_{\alpha_1} = 67.40(23)$ , $I_{\alpha_2} = 31.95(22)$ , $I_{\alpha_3} = 0.38(9)$ , $I_{\alpha_4} = 0.26(9)$ , $I_{\alpha_5} = 0.013(1)$ (2012MA30). $I_{\alpha_6} = 0.00054(5)$ , $I_{\alpha_7} \approx 0.0001$ , $I_{\alpha_8} \approx 0.00007$ , $I_{\alpha_9} \approx 0.00025$ , $I_{\alpha_{10}} \approx 0.00030$ , $I_{\alpha_{11}} \approx 0.000069$ (1998AK04).	1.53197(29)
$^{230}\text{Pu} \rightarrow ^{226}\text{U}$	$Q_\alpha = 7181(7)$ . $\% \alpha = 100$ , $T_{1/2} = 102$ s (10) (2012BR12). $I_{\alpha_1} = 81(4)$ , $I_{\alpha_2} = 19(4)$ . (ENSDF updates March-2014).	1.5375(56)
$^{232}\text{Th} \rightarrow ^{228}\text{Ra}$	$Q_\alpha = 4081.6(14)$ . $\% \alpha = 100$ , $T_{1/2} = 1.40 \times 10^{10}$ y (1), $I_{\alpha_1} = 78.2(13)$ , $I_{\alpha_2} = 21.7(13)$ , $I_{\alpha_3} = 0.069(13)$ (2014AB04).	1.5370(14)
$^{232}\text{U} \rightarrow ^{228}\text{Th}$	$Q_\alpha = 5413.63(9)$ . $\% \alpha = 100$ , $T_{1/2} = 68.9$ y (4), $I_{\alpha_1} = 68.15(23)$ , $I_{\alpha_2} = 31.55(23)$ , $I_{\alpha_3} = 0.30(2)$ , $I_{\alpha_4} = 0.00616(8)$ , $I_{\alpha_5} = 5.1 \times 10^{-5}(5)$ , $I_{\alpha_6} = 4.8 \times 10^{-5}(4)$ , $I_{\alpha_7} = 5.6 \times 10^{-5}(3)$ , $I_{\alpha_8} = 2.1 \times 10^{-5}(2)$ , $I_{\alpha_9} = 3.9 \times 10^{-6}(9)$ (2014AB04).	1.52885(29)
$^{232}\text{Pu} \rightarrow ^{228}\text{U}$	$Q_\alpha = 6716(10)$ . $\% \alpha = 11(9)$ (1952OR03, 1973JA06). $T_{1/2} = 33.8$ min (7) (2006BR19). $I_{\alpha_1} = 67(5)$ , $I_{\alpha_2} = 33(5)$ (2014AB04).	1.487(50)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{234}\text{U} \rightarrow ^{230}\text{Th}$	$Q_\alpha = 4857.5(7)$ . $\% \alpha = 100$ , $T_{1/2} = 2.455 \times 10^5$ y (6), $I_{\alpha 1} = 71.38(16)$ , $I_{\alpha 2} = 28.42(9)$ , $I_{\alpha 3} = 0.20(1)$ , $I_{\alpha 4} = 4 \times 10^{-5}(1)$ , $I_{\alpha 5} = 2.6 \times 10^{-5}(9)$ , $I_{\alpha 6} \approx 0.7 \times 10^{-5}$ (2012BR12).	1.52224(49)
$^{234}\text{Pu} \rightarrow ^{230}\text{U}$	$Q_\alpha = 6310(5)$ . $\% \alpha = 6(3)$ , $T_{1/2} = 8.8$ h (1), $I_{\alpha 1} = 68$ , $I_{\alpha 2} = 32$ , $I_{\alpha 3} = 0.4$ (2012BR12). $I_{\alpha 1,2}$ : Authors assigned 50% uncertainty to $I_{\alpha 2}$ i.e. 32(16), which gives $I_{\alpha 1} = 68(16)$ and used these values for the calculations of radius parameter.	1.518(27)
$^{236}\text{U} \rightarrow ^{232}\text{Th}$	$Q_\alpha = 4572.9(9)$ . $\% \alpha = 100$ , $T_{1/2} = 2.342 \times 10^7$ y (4) (2006BR19). $I_{\alpha 1} = 74.20(5)$ , $I_{\alpha 2} = 25.68(5)$ , $I_{\alpha 3} = 0.123(5)$ (2014MA14)	1.52595(66)
$^{236}\text{Pu} \rightarrow ^{232}\text{U}$	$Q_\alpha = 5867.15(8)$ . $\% \alpha = 100$ , $T_{1/2} = 2.858$ y (8), $I_{\alpha 1} = 69.1(3)$ , $I_{\alpha 2} = 30.8(3)$ , $I_{\alpha 3} = 0.23$ , $I_{\alpha 4} = 1.85 \times 10^{-3}$ , $I_{\alpha 5} = 1.3 \times 10^{-5}$ (2), $I_{\alpha 6} = 2.6 \times 10^{-4}(1)$ , $I_{\alpha 7} = 5.8 \times 10^{-4}(10)$ , $I_{\alpha 8} = 1.3 \times 10^{-5}(1)$ , $I_{\alpha 9} = 2.46 \times 10^{-6}$ , $I_{\alpha 10} = 6 \times 10^{-7}$ , $I_{\alpha 11} = 1.21 \times 10^{-5}(6)$ , $I_{\alpha 12} = 1.33 \times 10^{-5}$ , $I_{\alpha 13} = 1.53 \times 10^{-5}$ (2006BR19).	1.51022(22)
$^{238}\text{U} \rightarrow ^{234}\text{Th}$	$Q_\alpha = 4269.9(21)$ . $\% \alpha = 100$ , $T_{1/2} = 4.468 \times 10^9$ y (6) (2004SC03). $I_{\alpha 1} = 77.01(10)$ , $I_{\alpha 2} = 22.92(10)$ , $I_{\alpha 3} = 0.068(10)$ (2014PO02). $T_{1/2}$ : 4.456 $\times 10^9$ y (21) (2018PA45) is a preliminary result, thus not considered here.	1.5350(17)
$^{238}\text{Pu} \rightarrow ^{234}\text{U}$	$Q_\alpha = 5593.27(19)$ . $\% \alpha = 100$ , $T_{1/2} = 87.7$ y (1) (2015BR06). $I_{\alpha 1} = 70.91(10)$ , $I_{\alpha 2} = 28.98(10)$ , $I_{\alpha 3} = 0.105(5)$ , $I_{\alpha 4} = 0.0030(1)$ , $I_{\alpha 5} = 6.8 \times 10^{-6}(4)$ , $I_{\alpha 6} = 2.2 \times 10^{-5}$ , $I_{\alpha 7} = 5 \times 10^{-5}$ , $I_{\alpha 8} = 0.9 \times 10^{-7}(4)$ , $I_{\alpha 9} = 5.93 \times 10^{-6}(23)$ , $I_{\alpha 10} = 1.2 \times 10^{-5}$ , $I_{\alpha 11} = 2.5 \times 10^{-7}(8)$ , $I_{\alpha 12} \leq 1.3 \times 10^{-7}$ , $I_{\alpha 13} = 1.2 \times 10^{-6}(2)$ , $I_{\alpha 14} \approx 1.1 \times 10^{-6}$ (2007BR04).	1.50745(13)
$^{238}\text{Cm} \rightarrow ^{234}\text{Pu}$	$Q_\alpha = 6670(10)$ . $\% \alpha = 3.84$ (18), $T_{1/2} = 2.2$ h (4) (2015BR06). $I_{\alpha 1} = 69.5(8)$ , $I_{\alpha 2} = 30.5(8)$ (2007BR04).	1.4805(90)
$^{240}\text{Pu} \rightarrow ^{236}\text{U}$	$Q_\alpha = 5255.82(14)$ . $\% \alpha = 100$ , $T_{1/2} = 6561$ y (7) (2008SI25). $I_{\alpha 1} = 72.70(7)$ , $I_{\alpha 2} = 27.21(7)$ , $I_{\alpha 3} = 0.085(4)$ , $I_{\alpha 4} = 0.00097(9)$ , $I_{\alpha 5} = 1.72 \times 10^{-6}(7)$ , $I_{\alpha 6} = 0.000032$ (5) (2010SI30). $I_{\alpha 7} = 1.3 \times 10^{-8}(7)$ , $I_{\alpha 8} = 5.9 \times 10^{-7}(7)$ , $I_{\alpha 9} < 1 \times 10^{-7}$ , $I_{\alpha 10} < 5 \times 10^{-8}$ , $I_{\alpha 11} < 5 \times 10^{-8}$ (2006BR20).	1.51631(11)
$^{240}\text{Cm} \rightarrow ^{236}\text{Pu}$	$Q_\alpha = 6397.8(6)$ . $\% \alpha > 99.5$ , $T_{1/2} = 27$ d (1) (2008SI25). $I_{\alpha 1} = 71.1(8)$ , $I_{\alpha 2} = 28.9(8)$ , $I_{\alpha 3} = 0.052$ , $I_{\alpha 4} = 0.014$ (2006BR20). $\% \alpha$ : Given as $> 99.5$ in 2008SI25 but authors used 99.75(25) to conserve total alpha branching.	1.4947(17)
$^{240}\text{Cf} \rightarrow ^{236}\text{Cm}$	$Q_\alpha = 7711(4)$ . $\% \alpha = 98.5(23)$ (2010KH06). $T_{1/2} = 0.96$ min (15) (2008SI25). $I_{\alpha 1} = 68(3)$ , $I_{\alpha 2} = 32(3)$ (2006BR20).	1.5027(72)
$^{242}\text{Pu} \rightarrow ^{238}\text{U}$	$Q_\alpha = 4984.2(10)$ . $T_{1/2} = 3.75 \times 10^5$ y (2) (1989HO24). $\% \alpha = 100$ , $I_{\alpha 1} = 76.5(6)$ , $I_{\alpha 2} = 23.4(6)$ , $I_{\alpha 3} = 0.0304(14)$ , $I_{\alpha 4} = 6.20 \times 10^{-4}(3)$ (2015BR06).	1.51448(75)
$^{242}\text{Cm} \rightarrow ^{238}\text{Pu}$	$Q_\alpha = 6215.63(8)$ . $T_{1/2} = 162.84$ d (7). $\% \alpha = 100$ , $I_{\alpha 1} = 74.08(7)$ , $I_{\alpha 2} = 25.92(6)$ , $I_{\alpha 3} = 0.035(2)$ , $I_{\alpha 4} = 0.0046(5)$ , $I_{\alpha 5} = 2 \times 10^{-5}$ , $I_{\alpha 6} = 2.5 \times 10^{-4}(5)$ , $I_{\alpha 7} = 1.26 \times 10^{-5}(24)$ , $I_{\alpha 8} = 2.2 \times 10^{-7}(3)$ , $I_{\alpha 9} = 3.6 \times 10^{-5}(7)$ , $I_{\alpha 10} = 1.13 \times 10^{-6}(21)$ , $I_{\alpha 11} = 1.7 \times 10^{-6}(4)$ , $I_{\alpha 12} \leq 2 \times 10^{-7}$ , $I_{\alpha 13} = 3.7 \times 10^{-6}(8)$ , $I_{\alpha 14} = 3.1 \times 10^{-7}(8)$ , $I_{\alpha 15} = 5.5 \times 10^{-7}(15)$ , $I_{\alpha 16} = 5.2 \times 10^{-7}(15)$ (2015BR06). $T_{1/2}$ : WA of 162.5 d (20) (1950HA14), 162.46 d (27) (1954GL37), 163.0 d (18) (1954HU32), 163.2 d (2) (1975KE02), 163.1 d (4) (1965FL02), 162.76 d (4) (1977DI04), 163.02 d (11) (1979CH41), 161.35 d (10) (1981US03), 163.00 d (11) (1982AG02) and 163.0 d (2) (1984WI14) is obtained by omitting 161.35(10) (1981US03) as an outlier and inflating the uncertainty in 1977DI04 to 0.06 to bring its weight down to 50%.	1.501258(57)
$^{242}\text{Cf} \rightarrow ^{238}\text{Cm}$	$Q_\alpha = 7517(4)$ . $\% \alpha = 61(3)$ (2011VE03). $T_{1/2} = 3.7$ min (5) (2002AK06). $I_{\alpha 1} \approx 80$ , $I_{\alpha 2} \approx 20$ (2015BR06). $I_{\alpha 1,2}$ : Authors assigned 50% uncertainty to $I_{\alpha 2}$ i.e. 17(9), which gives $I_{\alpha 1} = 83(9)$ and used these values for the calculations of radius parameter.	1.4986(78)
$^{244}\text{Pu} \rightarrow ^{240}\text{U}$	$Q_\alpha = 4665.6(10)$ . $\% \alpha = 99.877(6)$ , $T_{1/2} = 8.13 \times 10^7$ y (3) (2017NE10). $I_{\alpha 1} = 80.6(8)$ , $I_{\alpha 2} = 19.4(8)$ (2008SI25).	1.50549(82)
$^{244}\text{Cm} \rightarrow ^{240}\text{Pu}$	$Q_\alpha = 5901.60(3)$ . $\% \alpha = 100$ , $T_{1/2} = 18.11$ y (3) (2017NE10). $I_{\alpha 1} = 76.9(1)$ , $I_{\alpha 2} = 23.1(1)$ , $I_{\alpha 3} = 0.0204(15)$ , $I_{\alpha 4} = 0.00352(18)$ , $I_{\alpha 5} = 4 \times 10^{-5}$ , $I_{\alpha 6} = 5.6 \times 10^{-5}(5)$ , $I_{\alpha 7} = 4 \times 10^{-6}(3)$ , $I_{\alpha 8} = 1.49 \times 10^{-4}(16)$ , $I_{\alpha 9} = 5.0 \times 10^{-5}(5)$ (2008SI25).	1.498180(88)
$^{244}\text{Cf} \rightarrow ^{240}\text{Cm}$	$Q_\alpha = 7329.0(18)$ . $\% \alpha = 75(6)$ , $T_{1/2} = 19.3$ min (12) (2018KO05). $I_{\alpha 1} = 75(8)$ , $I_{\alpha 2} = 25(8)$ (2008SI25). $\% \alpha$ : 75(+12-6) is used in the calculation of radius parameter as reported alpha branching is somewhat higher than 75%(6) (2018KO05).	1.498(60)
$^{246}\text{Cm} \rightarrow ^{242}\text{Pu}$	$Q_\alpha = 5475.1(9)$ . $\% \alpha = 99.97385(7)$ , $T_{1/2} = 4706$ y (40) (2011BR11). $I_{\alpha 1} = 79.08(22)$ , $I_{\alpha 2} = 20.9(4)$ , $I_{\alpha 3} = 0.020(2)$ (2007KO01).	1.49412(62)
$^{246}\text{Cf} \rightarrow ^{242}\text{Cm}$	$Q_\alpha = 6861.6(10)$ . $\% \alpha = 100$ , $T_{1/2} = 35.7$ h (5) (2011BR11). $I_{\alpha 1} = 79.3(10)$ , $I_{\alpha 2} = 20.6(10)$ , $I_{\alpha 3} = 0.15(2)$ , $I_{\alpha 4} \approx 0.016$ (2002AK06).	1.49528(88)



Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{246}\text{Fm} \rightarrow ^{242}\text{Cf}$	$Q_\alpha = 8377(8)$ . $\% \alpha = 93.2(6)$ , $T_{1/2} = 1.54$ s (4) (2011BR11). $I_{\alpha_1} = 80(20)$ , $I_{\alpha_2} = 20(20)$ (2002AK06). $r_0$ : Calculated radius parameter is based on systematically deduced $I_\alpha$ values.	1.506(12)
$^{248}\text{Cm} \rightarrow ^{244}\text{Pu}$	$Q_\alpha = 5161.81(25)$ . $\% \alpha = 91.61(16)$ , $T_{1/2} = 3.48 \times 10^5$ y (6), $I_{\alpha_1} = 81.89(41)$ , $I_{\alpha_2} = 18.03(19)$ , $I_{\alpha_3} = 0.076(12)$ , $I_{\alpha_4} \leq 0.01$ (2017NE10).	1.49627(74)
$^{248}\text{Cf} \rightarrow ^{244}\text{Cm}$	$Q_\alpha = 6361(5)$ . $\% \alpha = 99.9971$ (3), $T_{1/2} = 333.5$ d (28), $I_{\alpha_1} = 80.0(10)$ , $I_{\alpha_2} = 19.6(10)$ , $I_{\alpha_3} = 0.4(2)$ (2017NE10).	1.4851(24)
$^{248}\text{Fm} \rightarrow ^{244}\text{Cf}$	$Q_\alpha = 7995(8)$ . $\% \alpha = 95(5)$ . $T_{1/2} = 34.5$ s (12), $I_{\alpha_1} = 80(10)$ , $I_{\alpha_2} = 20(10)$ (2017NE10). $I_{\alpha_{1,2}}$ : Uncertainties assumed as 10 units.	1.4945(65)
$^{250}\text{Cf} \rightarrow ^{246}\text{Cm}$	$Q_\alpha = 6128.51(19)$ . $\% \alpha = 100$ , $T_{1/2} = 13.08(9)$ y, $I_{\alpha_1} = 82.60(11)$ , $I_{\alpha_2} = 17.11(11)$ , $I_{\alpha_3} = 0.283(15)$ , $I_{\alpha_4} = 0.007(2)$ (2011BR11).	1.48260(30)
$^{250}\text{Fm} \rightarrow ^{246}\text{Cf}$	$Q_\alpha = 7557(8)$ . $\% \alpha > 90$ , $T_{1/2} = 30$ min (2), $I_{\alpha_1} = 83(3)$ , $I_{\alpha_2} = 17(3)$ (2011BR11). $\% \alpha$ : Authors used $\% \alpha = 95(5)$ in the calculations of radius parameter.	1.4789 (48)
$^{252}\text{Cf} \rightarrow ^{248}\text{Cm}$	$Q_\alpha = 6216.95(4)$ . $\% \alpha = 96.908(8)$ , $T_{1/2} = 2.645$ y (8), $I_{\alpha_1} = 84.1(4)$ , $I_{\alpha_2} = 15.0(9)$ , $I_{\alpha_3} = 0.25(12)$ , $I_{\alpha_4} = 0.0020$ , $I_{\alpha_5} \approx 6 \times 10^{-5}$ (2014MA86).	1.50113(23)
$^{252}\text{Fm} \rightarrow ^{248}\text{Cf}$	$Q_\alpha = 7152.7(20)$ . $\% \alpha = 99.9977(2)$ (2005NI22). $T_{1/2} = 25.39$ h (4), $I_{\alpha_1} = 84.0(5)$ , $I_{\alpha_2} = 15.0(2)$ , $I_{\alpha_3} = 0.97(4)$ , $I_{\alpha_4} = 0.023(5)$ (2014MA86).	1.46703(81)
$^{252}\text{No} \rightarrow ^{248}\text{Fm}$	$Q_\alpha = 8549(5)$ . $T_{1/2} = 2.46$ s (2). $\% \alpha = 67.8(19)$ , $I_{\alpha_1} \approx 75$ , $I_{\alpha_2} \approx 25$ (2014MA86). $T_{1/2}$ : WA of 2.44 s (4) (2001OG08), 2.46 s (5) (2006LE29), 2.42 s (6) (2007SU19), 2.47 s (2) (2011GA19) and 2.43 s (13) (2012SU22). $I_{\alpha_{1,2}}$ : Authors assigned 50% uncertainty to $I_{\alpha_2}$ i.e. 25(13), which gives $I_{\alpha_1} = 75(13)$ and used these values for the calculations of radius parameter.	1.4787(75)
$^{254}\text{Cf} \rightarrow ^{250}\text{Cm}$	$Q_\alpha = 5927(5)$ . $\% \alpha = 0.31(16)$ (1968BE21). $T_{1/2} = 60.5$ d (2) (1963PH01). $I_{\alpha_1} = 83(1)$ , $I_{\alpha_2} = 17(2)$ (2001AK11).	1.517(24)
$^{254}\text{Fm} \rightarrow ^{250}\text{Cf}$	$Q_\alpha = 7307.5(19)$ . $T_{1/2} = 3.240$ h (2) (1967FI03). $\% \alpha = 99.9408$ (3) (2019SI11). $I_{\alpha_1} = 85.0(5)$ , $I_{\alpha_2} = 14.2(3)$ , $I_{\alpha_3} = 0.82(6)$ , $I_{\alpha_4} = 0.0066(8)$ (2001AK11).	1.48871(75)
$^{254}\text{No} \rightarrow ^{250}\text{Fm}$	$Q_\alpha = 8226(8)$ . $\% \alpha = 90$ (4) (1988TU07). $T_{1/2} = 51.2$ s (4) (2006HE19). $I_{\alpha_1} = 86(2)$ , $I_{\alpha_2} = 14$ (2) (1998AK04).	1.4672(33)
$^{256}\text{Fm} \rightarrow ^{252}\text{Cf}$	$Q_\alpha = 7027(5)$ . $\% \alpha = 8.1(3)$ , $T_{1/2} = 157.1$ min (13) (2017SI08). $I_{\alpha_1} = 85(5)$ , $I_{\alpha_2} = 15(3)$ (2005NI22). $r_0$ : Calculated radius parameter is based on systematically deduced $I_\alpha$ values.	1.4989(35)
$^{256}\text{No} \rightarrow ^{252}\text{Fm}$	$Q_\alpha = 8582(5)$ . $\% \alpha = 99.47(6)$ , $T_{1/2} = 2.91$ s (5) (2017SI08). $I_{\alpha_1} = 87(2)$ , $I_{\alpha_2} = 13(2)$ (2005NI22).	1.4762(19)
$^{256}\text{Rf} \rightarrow ^{252}\text{No}$	$Q_\alpha = 8926(15)$ . $\% \alpha = 0.32(17)$ , $T_{1/2} = 6.67$ ms (10) (2017SI08). $I_\alpha \approx 100$ (1997HE29). $I_\alpha$ : Only one alpha branch has been reported by 1997HE29. Based on systematics, 2005NI22 suggested 84(4)% branch to g.s. and 16(4)% to the first $2^+$ state, which gives $r_0 = 1.459(25)$ .	1.466(26)
$^{258}\text{Rf} \rightarrow ^{254}\text{No}$	$Q_\alpha = 9190(30)$ . $\% \alpha = 4.9(16)$ , $T_{1/2} = 12.0$ ms (12) (2017SI20). $I_\alpha = 85(15)$ (2019SI11). $I_\alpha$ : 15(15)% is tentatively assigned to the alpha branch to the first $2^+$ state in $^{254}\text{No}$ , based on observation of one event in 2008GA08. $r_0$ : 1.476(17) if 100% branch to the g.s. and none to the excited states.	1.470(18)
$^{260}\text{Sg} \rightarrow ^{256}\text{Rf}$	$Q_\alpha = 9901(10)$ . $\% \alpha = 29(3)$ , $T_{1/2} = 4.95$ ms (33), $I_{\alpha_1} = 83(10)$ , $I_{\alpha_2} = 17(10)$ (2017SI08).	1.4562(75)
$^{264}\text{Hs} \rightarrow ^{260}\text{Sg}$	$Q_\alpha = 10591(20)$ . $\% \alpha = 83(17)$ , $T_{1/2} = 0.61$ ms (+47-19) (2011SA41). $I_\alpha = 100$ . $\% \alpha$ : 83(17) is based on 5 alpha decay events observed in 2011Sa41 and 1 event for fission.	1.485(24)
$^{266}\text{Hs} \rightarrow ^{262}\text{Sg}$	$Q_\alpha = 10346(16)$ . $\% \alpha = 76(9)$ , $T_{1/2} = 2.97$ ms (+78-51) (2012AC04). $I_\alpha = 100$ .	1.481(12)
$^{268}\text{Hs} \rightarrow ^{264}\text{Sg}$	$Q_\alpha = 9623(16)$ . $\% \alpha = 100$ . $T_{1/2} = 0.38$ s (+180-17) (2010NI14). $I_\alpha = 100$ .	1.458(48)
$^{270}\text{Ds} \rightarrow ^{266}\text{Hs}$	$Q_\alpha = 11117(28)$ . $\% \alpha = 100$ (2019SI12). $T_{1/2} = 0.20$ ms (+7-4) (2012AC04). $I_\alpha = 100$ .	1.472(12)
$^{270}\text{Hs} \rightarrow ^{266}\text{Sg}$	$Q_\alpha = 9070(40)$ , $\% \alpha = 75(25)$ , $T_{1/2} = 7.6$ s (+49-22) (2013OG03). $I_\alpha = 100$ .	1.471(27)
$^{286}\text{Fl} \rightarrow ^{282}\text{Cn}$	$Q_\alpha = 10370(30)$ . $\% \alpha = 60(11)$ (2017OG01). $T_{1/2} = 166$ ms (+40-27) (2016HO09). $I_\alpha = 100$ .	1.441(15)
$^{288}\text{Fl} \rightarrow ^{284}\text{Cn}$	$Q_\alpha = 10072(13)$ . $\% \alpha = 100$ , $T_{1/2} = 0.64$ s (+14-10) (2016HO09). $I_\alpha = 100$ .	1.476(10)
$^{290}\text{Lv} \rightarrow ^{286}\text{Fl}$	$Q_\alpha = 11000(70)$ . $\% \alpha = 100$ (2016HO09). $T_{1/2} = 8.3$ ms (+35-19) (2017OG01). $I_\alpha = 100$ .	1.486(28)
$^{292}\text{Lv} \rightarrow ^{288}\text{Fl}$	$Q_\alpha = 10774(15)$ . $\% \alpha = 100$ , $T_{1/2} = 12.8$ ms (+70-33) (2016HO09). $I_\alpha = 100$ .	1.516(18)

Continuation of Table II		
Alpha Decay	Input Parameters	$r_0$ (fm)
$^{294}\text{Og} \rightarrow ^{290}\text{Lv}$	$Q_\alpha = 11860(30)$ . $\% \alpha = 100$ (2016HO09). $T_{1/2} = 0.58 \text{ ms}$ (+44-18) (2018BR13). $I\alpha = 100$ . $Q_\alpha$ : Based on $E_\alpha = 11700 \text{ keV}$ (30) (2018BR13).	1.461(24)

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