

# Microbubble generation using fiber optic tips coated with nanoparticles

Reinher Pimentel-Domínguez, Juan Hernández-Cordero,\* and Roberto Zenit

Instituto de Investigaciones en Materiales, UNAM, A.P. 70-360 Circuito Exterior, Cd. Universitaria, México, D. F., 04510, México

\*[jhcordero@iim.unam.mx](mailto:jhcordero@iim.unam.mx)

**Abstract:** We show that fiber optic tips can be used as microbubble generators in liquid media. Using standard single-mode silica fibers incorporating nanoparticles (carbon nanoparticles and metallic powders), bubbles can be generated with low optical powers owing to the enhanced photothermal effects of the coating materials. We provide details about the hydrodynamic effects generated in the vicinity of the fiber tip during the coating process, bubble generation and growth. Flow visualization techniques show that thermal effects lead to bubble formation on the tip of the fibers, and coating optimization is crucial for optimal performance of the probes.

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## 1. Introduction

Optical fibers have been widely used for sensors and laser delivery in biomedical applications [1–3]. Laser surgery and noncontact manipulation of microparticles, as well as biological materials using optical traps, are two applications in which optical fibers have also played a key role [1, 4, 5]. Recently, laser delivery through optical fibers has shown to yield hydrodynamic effects that may be relevant for medical procedures involving water-saturated tissues [6]. In particular, it has been shown that moderate laser powers can lead to bubble formation and explosion resulting in tissue damage and degradation of the end surface of the delivery fiber [7]. In general, bubbles at the micron and nano-scale have attracted interest in scientific research and in industry because their properties are very different from those of macroscopic bubbles. Suitable methods for bubble generation and control at those scales are therefore of interest for a wide variety of applications.

Bubble generation on the tip of optical fibers immersed in liquid media has been demonstrated under different experimental conditions [7–9]. In contrast to continuous-wave (CW) laser-induced cavitation effects that can produce bubbles in liquids [10], bubble formation using optical fibers usually requires moderate laser power and does not rely on absorbing solutions. The mechanism for bubble formation is mainly driven by optical absorption in the vicinity of the fiber tip, which leads to thermal effects yielding gas-vapor bubbles. Fiber optic tips for micron-sized bubble generation have been based on metallic coatings as well as on carbon layers on the fiber end-face. While metallic coated fibers typically require elaborated fabrication methods and/or specialty fibers [8, 9], carbon coatings have been obtained upon placing a quartz fiber in contact with wood [6, 7]. The latter approach is simple and apparently reproducible enough so as to yield bubbles in water with laser powers ranging from 1 to 5 W. However, there are other methods upon which carbon coatings may be incorporated on the tips of optical fibers, thereby providing further options for developing fiber tips for microbubble generation.

In this paper we demonstrate a simple means to fabricate fiber optic tips for microbubble generation in liquids using a laser diode. The tips are based on standard single-mode silica fibers coated with carbon nanoparticles and metallic powders. Such materials provide enhanced optical absorption compared to metallic and carbon coatings, and the thermal effects required for bubble formation in liquids can be obtained with low laser power (tens of mW). Bubbles can be readily generated upon immersing the coated fibers in liquids such as water and methanol and their maximum size depends on the coating features. We provide details about the fabrication procedure of the probes and the hydrodynamic effects generated in the vicinity of the fiber tip during bubble generation and growth. Using flow visualization techniques we also show experimental evidence of the thermal effects leading to bubble formation on the tip of the fiber probes. The performance of the probes is demonstrated under different experimental conditions, showing that the coating process has a significant impact on the capabilities of the probes for bubble generation.

## 2. Fabrication of fiber tips and experiments

Nanoparticles can be readily incorporated onto optical fibers using a simple technique originally demonstrated with carbon nanotubes [11, 12]. This is based on immersing the tip of an optical fiber in a solution of nanotubes dispersed in ethanol and launching a laser beam through the waveguide. The output beam irradiating the solution generates thermophoresis and pressure gradients leading to deposition of the carbon nanotubes onto the fiber end-face. We have shown that this optically driven deposition technique can be also used with other materials such as graphite, iron and iron-graphite particles [13]. In addition, we have also verified that deposition occurs using either single- or multimode optical fibers.

The experimental setup used for optically driven deposition of materials onto optical fibers has been described previously [11–13]. As illustrated in Fig. 1(a), the main components

are a laser diode, an optical fiber for guiding the laser light and the nanostructures to be deposited on the fiber. The nanostructures are dissolved in a liquid that must be chosen so as to avoid optical absorption at the laser wavelength. In our experiments, the nanostructures were dissolved in ethanol and a CW fiber-coupled laser diode (Thorlabs, 975 nm, 300 mW max. output power) is used as the light source. The fiber tips are based on standard single-mode optical fiber (SMF-28e), which is used for laser guiding and as the deposition target. Prior to being immersed in the solution, the fibers are cleaved to obtain a flat end-face. The results shown in this paper were obtained using graphite nanoparticles, multi-walled carbon nanotubes (carbon >95%, O.D.  $\times$  L 6-9 nm  $\times$  5  $\mu$ m, Sigma-Aldrich, 724769), carbon nanopowder (<50 nm particle size, Sigma-Aldrich, 633100) and silver nanopowder (<100 nm particle size, Sigma-Aldrich, 576832).

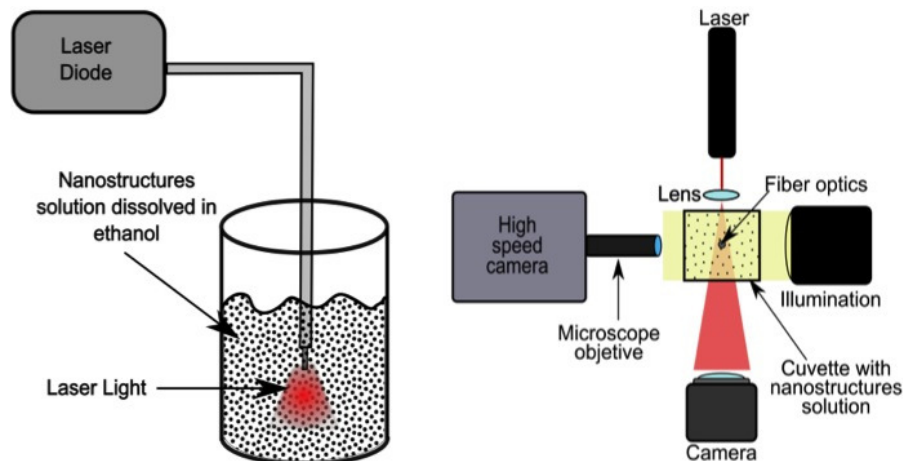


Fig. 1. (a) Experimental setup for nanoparticle deposition onto optical fibers. (b) Arrangement for visualization of bubble generation.

For visualizing bubble generation and growth, we used a high-speed camera (Redlike, 1108-0014) with a zoom-imaging lens (TECHSPEC® VZM, 1000i). The fiber tip was illuminated with a high intensity white LED spot lamp (Fig. 1(b)). Additionally, we used a shadowgraph system for monitoring thermal gradients around the location of the fiber end-faces. This included a laser light source (633 nm, 17 mW) and a microscope objective (0.55, 35X) for expanding the beam. Finally, a standard CCD camera was used for recording the shadowgraph images.

Deposition of nanoparticles is achieved after immersing the fibers in the liquid solution and turning the laser on. The time required for successful deposition on the fiber tip depends on the laser power as well as on the concentration and size of the nanoparticles. For our experiments, the nanoparticles were dissolved in ethanol using a concentration of 2.35 mg/ml for the silver nanoparticles and 0.235 mg/ml for the carbon nanotubes. All the solutions were sonicated for 10 minutes prior deposition. Three sets of tips were fabricated upon immersing the fibers during 30 seconds using three different power settings for the laser diode (57, 120 and 182 mW). Subsequent observations of the fiber end-faces with a scanning electron microscope (SEM) were also performed to verify the successful deposition of nanoparticles.

### 3. Hydrodynamic effects during nanoparticle deposition

The mechanisms leading to optically driven deposition of nanoparticles start when the laser diode is turned on. Laser light emerging from the optical fiber generates a gradient force driving the nanostructures towards the tip of the fiber [11, 12]; thus, flow patterns are induced. The fluid motion can thus be registered by means of the high-speed camera. Figure 2(a) shows a sequence of images that illustrate the initial motion of the nanoparticles, which is

altered once the laser diode is turned on. The flow pattern also shows some trajectories of the nanoparticles finishing on top of the fiber end-face.

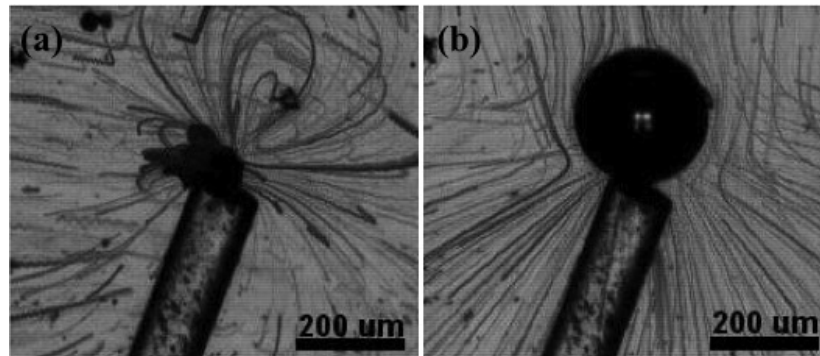


Fig. 2. Flow patterns obtained with the high-speed camera (1000 fps). The lines indicate the trajectories of the nanoparticles (graphite) after the laser diode is turned on ([Media 1](#)), and after the bubble is generated ([Media 2](#)). The laser diode output power was 2.9 mW and the core/cladding size of the fiber was 8/125  $\mu\text{m}$  (the gravity force points into the image).

Once deposition on the fiber end-face has been achieved, a micron-sized bubble is generated immediately after. Bubbles are usually generated at the tip of the fiber and they grow until reaching a maximum size. Once this is reached, the bubble detaches from the tip to float towards the surface and a new bubble is formed. Figure 2(b) shows the effect of bubble formation on the flow of nanoparticles; clearly, the bubble affects the hydrodynamics around the vicinity of the tip. In some cases, some nanoparticles and clusters can be trapped on the surface of the bubble, showing a similar effect to that previously reported for metallic-coated fiber tips [9].

#### 4. Thermal effects and bubble formation

Bubble formation in solutions with highly absorbing particles has been reported previously [14]. Laser absorption by the particles provides an extremely localized area over which thermal fluctuations lead to spontaneous formation of bubbles as a result of vaporization of the liquid. Further effects include convection around the heated nanoparticles, which in turn causes bubble migration towards regions of higher temperatures (i.e., thermophoresis). This provides a means for attracting bubbles towards heated particles and results in an effective bubble trapping mechanism estimated to be at least an order of magnitude more powerful than that possible with optical forces [14].

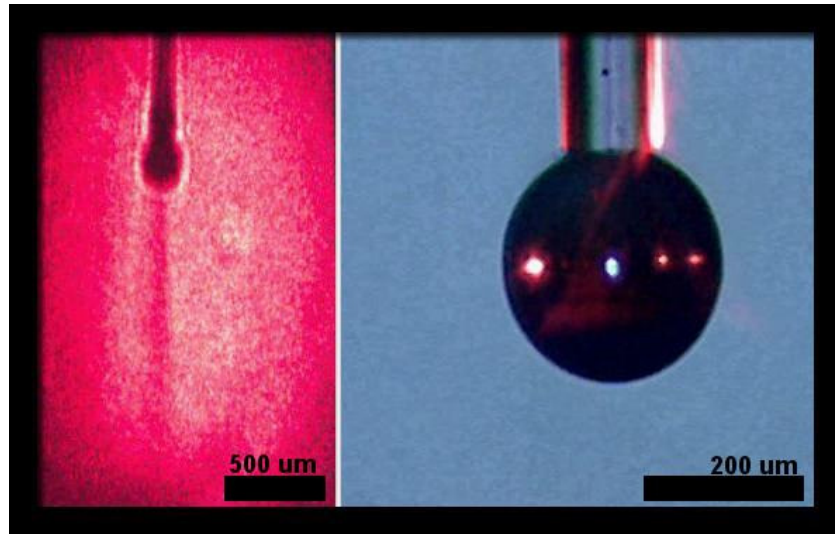


Fig. 3. Shadowgraph images (left) obtained during bubble growth (right). The fiber probe is coated with carbon nanotubes and immersed in clean methanol (optical power during deposition: 57.5 mW, laser diode output power: 180 mW). After reaching a maximum size, the bubble detaches from the probe and another bubble is formed immediately after ([Media 3](#)). In these experiments the gravity force points downwards (same direction as the fiber).

Using the shadowgraph setup we were able to obtain experimental evidence of the thermal effects associated with bubble formation. For these experiments, the nanoparticle coated fiber probes were immersed in clean methanol and/or water. Bubbles were readily generated once the laser diode was turned on, and refractive index changes in the vicinity of the fiber tip were evident in the shadowgraph image. As shown in Fig. 3, a bubble starts forming immediately after the laser diode is turned on and kept at a constant output power. The bubble reaches a maximum size and then detaches from the fiber tip; subsequently, another bubble starts growing and the process repeats itself. Similar effects were observed for the different nanoparticles used in our experiments, although the optical power required for bubble formation varied for each case.

The shadowgraph images show that thermal effects arise near the fiber tip owing to optical absorption of the nanostructures. This is consistent with previous observations of bubble formation in carbon nanotube clusters due to photothermal effects in optical tweezers experiments [14, 15]. In our case, clusters are formed on the tips of the fibers during deposition of the nanoparticles, thus providing a preferential site for optical absorption and hence bubble formation and growth. In the image sequence (Fig. 3), the intensity gradients observed around the bubble indicate that there are temperature gradients around the tip of the fiber. It is particularly interesting to note that, when the bubble detaches and a new one is formed, the temperature gradients in the vicinity of the tip are more pronounced. This is a clear indication that when the bubble is being formed, most of the thermal energy is being used to convert liquid into vapor (latent heat). As it is well known, this process is isothermal; therefore, weak temperature gradients are observed, as shown in [Media 3](#). When the bubble detaches, the heat is no longer used to transform liquid into vapor and a fast temperature change in the fluid is observed, again, as clearly shown in the image sequence.

Bubble growth and lifetime were evaluated for the different fiber tips. For each case, the optical power launched into the fiber was increased and the maximum size of the bubbles was measured from the video images. As seen in Fig. 4(a), each of the tested tips has a different bubble formation threshold, which depends on the optical power used for nanoparticle deposition. Above this power threshold, the bubbles grow to the same maximum size, although this also depends on the deposition conditions. The largest bubbles are obtained with

the tip fabricated using the lowest laser power (57.5 mW). For comparison, we also include data obtained using a fiber coated with silver nanoparticles, showing that bubbles can only be generated for a small range of optical power. Furthermore, the maximum size attained with this tip is smaller than those obtained with fibers coated with carbon nanostructures. Notice that in spite of using a larger concentration of silver nanoparticles in the solutions, only one of the tips effectively generated bubbles that could be useful for comparing with the carbon nanotube coated fibers. This seems to suggest that thermal effects due to optical absorption of the nanostructures play an important role during the deposition process.

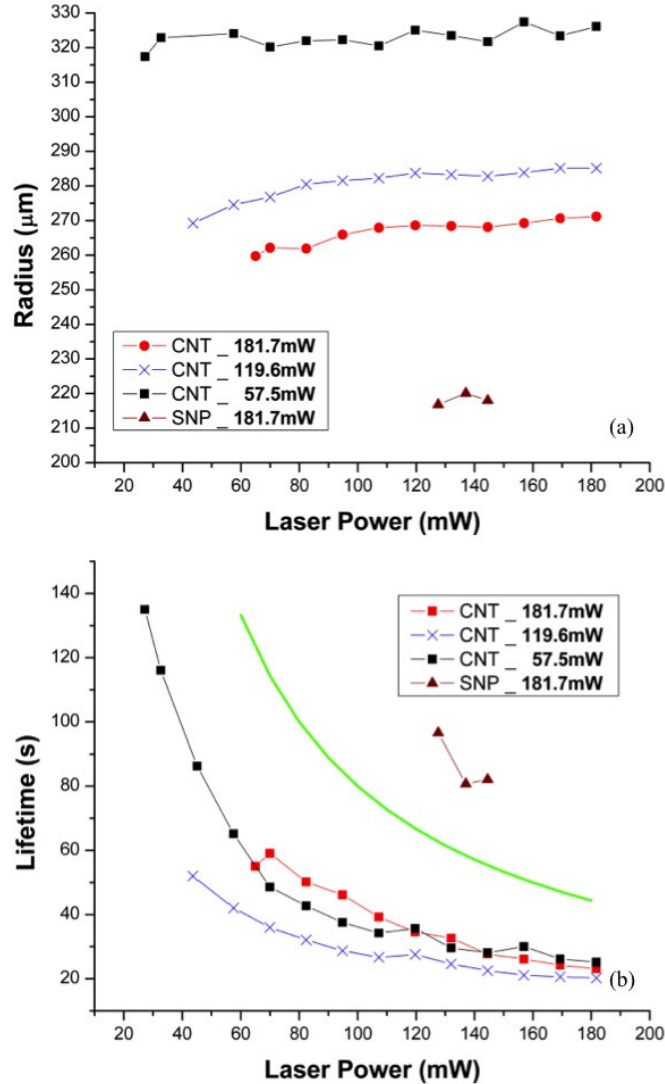


Fig. 4. Bubble size (a) and lifetime (b) for the different fiber tips fabricated for our experiments. Each fiber tip was fabricated using different optical powers for nanoparticle deposition (MWCNT-multi-wall carbon nanotubes, SNP-silver nanoparticles). Also shown in (b) is the lifetime as a function of energy as obtained from the force and mass balances (green line, see Eq. (8)).

The deposition conditions of the nanoparticles also affect the lifetime of the bubbles. We define the lifetime as the time taken for a bubble to reach its maximum size and detach from

the tip of the fiber. As seen in Fig. 4(b), the maximum lifetime is achieved with a tip fabricated with low optical powers during deposition. However, it is interesting to notice that regardless of the deposition conditions, the bubbles generated with carbon nanostructure coatings seem to reach a similar lifetime at higher laser diode powers. In contrast, the fibers with coatings based on silver nanoparticles show only a small variation in lifetime, albeit being smaller than those obtained with the carbon nanostructures.

Previous reports using carbon deposits on fibers have required a few watts of optical power for bubble generation [6]. In contrast, our coated tips can produce bubbles with optical powers as low as 20 mW, owing to the increased photothermal effects provided by the carbon nanotubes. Notice that our deposition technique does not yield a preferential alignment for the nanotubes and may favor clustering of nanoparticles on the fiber tips. Both, random orientation and clustering of carbon nanotubes have been pointed out as factors for the enhanced optical absorption observed in these materials [14–16]; thus, this may be a reason for the improved power efficiency observed with our fiber tips. Metallic coated fiber optic tips have shown to require even lower optical powers for bubble generation [9]; however, as pointed out earlier, their fabrication process involves more elaborated procedures than those required for depositing carbon nanoparticles on fiber optic end-faces.

The carbon nanotube coatings do not seem to degrade after bubbles detach from the fiber tip. Owing to the low optical powers used in our experiments, cavitation effects and explosion of the bubbles (as reported in [6]) are not apparent. A different scenario is obtained with silver nanoparticle coatings, which do degrade after generating one or two bubbles in subsequent experiments as observed in SEM images of the fiber tips. Nonetheless, further characterization of the fiber coatings is required in order to fully assess the lifetime of the fiber tips.

## 5. Discussion

The conditions for bubble detachment from the tip of the coated fiber can be estimated upon considering the forces acting upon the bubble. For a bubble of maximum radius  $R_{Bmax}$ , the balance between the buoyancy force and the “attachment” force yields:

$$\frac{4\pi}{3} R_{Bmax}^3 \rho_v g = \sigma (2\pi R_F) \quad (1)$$

where  $\rho_v$  is the density and  $g$  is the acceleration of gravity. The term on the right hand side involves the surface tension ( $\sigma$ ) and the wetted perimeter  $R_F$  represents the effective size of the area covered by nanoparticles onto which the bubble is being formed. Under these conditions, the maximum radius of the bubble is thus:

$$R_{Bmax}^3 = \frac{3}{2} \frac{\sigma}{\rho_v g} R_F \quad (2)$$

If  $R_F$  is independent of the laser power,  $R_{Bmax}$  should not show a dependence on it, as shown in Fig. 4(a). Notice also that features of the nanoparticle coating such as deposition quality and photothermal properties are also considered in  $R_F$ . This is also shown in Fig. 4(a), since  $R_{Bmax}$  indeed changes for different deposition conditions and different nanoparticles (i.e., different  $R_F$  values).

Let us consider now the bubble lifetime; the bubble is growing due to mass transfer from liquid to vapor as a result of heating. A simple mass balance for a bubble of radius  $R$ , volume  $V$  and constant density ( $\rho_v$ ) yields:

$$\dot{m} = \frac{1}{\rho_v} \frac{\partial V}{\partial t} = \frac{1}{\rho_v} \left( 4\pi R^2 \frac{\partial R}{\partial t} \right) \quad (3)$$



The mass flow rate can be calculated from the latent heat of the liquid ( $L$ ), which, from dimensional analysis, can be shown to be:

$$Q = mL \quad (4)$$

The power is then:

$$\dot{Q} = \dot{m} L \quad (5)$$

which can be combined with Eq. (3) to obtain:

$$\frac{1}{L} \dot{Q} = \frac{1}{\rho_v} \left( 4\pi R^2 \frac{\partial R}{\partial t} \right) \quad (6)$$

This shows that the bubble growth rate depends directly on the amount of power being injected into the system. Upon integrating Eq. (6), we can calculate the lifetime of the bubble ( $T$ ) assuming that the energy and the fluid properties ( $\rho_v$ ,  $L$ ) are constant. Thus:

$$T = \frac{4\pi}{3} \frac{L}{\rho_v} \frac{1}{\dot{Q}} R_{B\max}^3 \quad (7)$$

Further, using Eq. (2) we can obtain the lifetime as:

$$T = \frac{2\pi L \sigma R_F}{\rho_v^2 g} \frac{1}{\dot{Q}} \quad (8)$$

Notice that this expression states that bubble lifetime is inversely proportional to the energy injected to the system. This is what is shown in Fig. 4(b); thus, our assumptions are consistent with our experimental results. Also, as shown in the figure, the lifetime depends on  $R_F$ .

It is clear from our results that bubble features such as maximum size and lifetime depend on the coatings of the optical fibers. As demonstrated previously, deposition of the nanostructures depends on the optical power used during fabrication [11–13]. In general, low powers yield more uniform coatings on the fiber tips, thus providing a better surface for bubble formation and growth. This is confirmed in our results, since the threshold for bubble formation is smaller for the fiber tips fabricated with lower optical powers during deposition of the nanoparticles. Similarly, the simple models considered above show that an improved  $R_F$  (i.e., coating area) would yield larger bubbles. It is interesting to notice that bubbles smaller than the fiber diameter can remain attached to the tip, while larger bubbles always detach and float to the surface. Although the buoyancy force and other thermal effects in the vicinity of the bubble play an important role in the lifetime of the bubble [9], the fact that bubbles detach from the probes further suggests that the uniformity of the coating is also critical for holding the bubbles on the fiber. The large bubble lifetimes achieved with the tips fabricated at low optical powers seems to confirm this suggestion as well. Clearly, further experiments are required to optimize the coating process in order to fully exploit the photothermal effects generated in the fiber tips.

## Conclusions

We have demonstrated a simple technique for fabricating fiber optic tips for microbubble generation in liquids using low optical powers. The fiber tips are based on standard single-mode silica fibers incorporating carbon nanoparticles and metallic powders deposited on the fiber end-faces. Bubbles can be generated in different liquids using low optical powers owing to the enhanced photo-thermal effects of the nanoparticles used for coating the fibers. Our experiments show that microbubbles are generated through thermal effects arising from optical absorption by the nanostructures, thus leading to bubble formation on the tip of the



fibers. The maximum bubble size was shown to depend on the type and size of the coating, while the bubble lifetime was shown to depend inversely on the optical power. Although optimization of the coatings is still required, we have shown that standard single-mode optical fibers and carbon nanoparticles can be used as an enabling technology for localized heating generation. This might be of interest for biomedical applications.

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