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1. Suppose wind is blowing over a hut which looks like a half cylinder of radius a and length L . The wind and pressure at far distances are U_∞ and p_∞ , respectively. Let the pressure inside the hut be p_∞ . Assuming the flow is ideal and can be modelled using the potential for flow past a cylinder without circulation, what is the expression for the upward force on the hut due to the difference in pressures? Assume the flow is two-dimensional.

[Complex potential for uniform flow past a cylinder is
 $w(z) = U_\infty \left(z + \frac{a^2}{z} \right)$; $z = re^{i\theta}$.

This gives, $\phi = U_\infty \left(r + \frac{a^2}{r} \right) \cos \theta$ & $\psi = U_\infty \left(r - \frac{a^2}{r} \right) \sin \theta$.

& vel. components: $u_r = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = U_\infty \left(1 - \frac{a^2}{r^2} \right) \cos \theta$
 & $u_\theta = -\frac{\partial \phi}{\partial r} = -U_\infty \left(1 + \frac{a^2}{r^2} \right) \sin \theta$.

On the surface $r = a$, $u_\theta = -U_\infty \left(1 + \frac{a^2}{a^2} \right) \sin \theta = -2U_\infty \sin \theta$. ①

This result for our case is valid for $0 \leq \theta \leq \pi$ (upper half)

From Bernoulli's eqn: ①

$$\frac{1}{2} \rho U_\infty^2 + p_\infty = \frac{1}{2} \rho U_\theta^2 + p(\theta) \Rightarrow p_\theta = p_\infty + \frac{1}{2} \rho (U_\infty^2 - U_\theta^2)$$

Putting $U_\theta = -2U_\infty \sin \theta \Rightarrow p_\theta = p_\infty + \frac{1}{2} \rho U_\infty^2 (1 - 4 \sin^2 \theta)$ ①

\therefore Upward force/length, $F_y = - \int_0^\pi p_\theta \sin \theta \, a \, d\theta$.

$$\begin{aligned} \Rightarrow F_y &= -a \int_0^\pi \left[p_\infty + \frac{1}{2} \rho U_\infty^2 (1 - 4 \sin^2 \theta) \right] \sin \theta \, d\theta \\ &= -a \left[p_\infty \int_0^\pi \sin \theta \, d\theta + \frac{1}{2} \rho U_\infty^2 \int_0^\pi \sin \theta \, d\theta - 2 \rho U_\infty^2 \int_0^\pi \sin^3 \theta \, d\theta \right] \end{aligned}$$

$$\int_0^\pi \sin \theta d\theta = 2; \quad \int_0^\pi \sin^3 \theta d\theta = \frac{4}{3}$$

$$\therefore F_y = -a \left[2p_a + \rho U_\infty^2 - \frac{8}{3} \rho U_\infty^2 \right]$$

$$= -a \left[2p_a - \frac{5}{3} \rho U_\infty^2 \right]$$

Note: pressure inside the hut is p_a . We only need net upward force due to outer pressure relative to inside.

$$\therefore F_y = -a \int_0^\pi (p_a - p_a) \sin \theta d\theta$$

$$= -a \int_0^\pi \frac{1}{2} \rho U_\infty^2 (1 - 4 \sin^3 \theta) \sin \theta d\theta$$

$$= -a \left[\frac{1}{2} \rho U_\infty^2 \cdot 2 - 2 \rho U_\infty^2 \cdot \frac{4}{3} \right] \quad (2)$$

$$= \frac{5}{3} a \rho U_\infty^2$$

ROLL NO : MS NAME :

[2+3]

1. For capillary waves with the dispersion relation:

$$\omega = \sqrt{k \left(g + \frac{\sigma k^3}{\rho} \right) \tanh(kH)}$$

where ρ is the liquid density and σ is the surface tension, determine the following:

- At what water depth H are the waves non-dispersive (wave speed c is independent of wavelength λ)?
- In deep water, if the gravitational effects are negligible, what is the relation between the group velocity c_g and the phase velocity c ?

$$\omega^2 = gk + \frac{\sigma}{\rho} k^3 \tanh(kH)$$

(a) Waves are non-dispersive when wave speed c is independent of wavelength λ (or wavenumber k)

$$\text{Phase speed } c = \frac{\omega}{k} \Rightarrow c^2 = \frac{\omega^2}{k^2} = \frac{g}{k} + \frac{\sigma}{\rho} k \tanh(kH)$$

$$\Rightarrow c^2 = g \frac{2\pi}{\lambda} + \frac{\sigma}{\rho} \left(\frac{2\pi}{\lambda} \right) \tanh\left(\frac{2\pi H}{\lambda} \right) \quad (1)$$

For non-dispersive: $\frac{dc}{d\lambda} = 0$ or $\frac{dc}{dH} = 0$.

Rather than solving for this, recall:

in shallow water $kH \ll 1 \Rightarrow \tanh(kH) \approx kH$

in deep water $kH \gg 1 \Rightarrow \tanh(kH) \approx 1$

$$\text{In shallow water, } \omega^2 \approx gk + \frac{\sigma}{\rho} k^3 \cdot kH \\ = gk + \frac{\sigma}{\rho} H k^4$$

\rightarrow still dispersive due to k^4 term.

For very shallow water & negligible surface

$$\text{tension } (\sigma = 0): \omega^2 = gk \Rightarrow c = \frac{\omega}{k} = \sqrt{gH}$$

\rightarrow non-dispersive

(1)

(b) In deep water, when gravity is negligible,

$$\omega^2 \approx \frac{\sigma}{\rho} k^3 \Rightarrow \omega = \sqrt{\frac{\sigma}{\rho}} k^{3/2} \quad (1)$$

$$c = \frac{\omega}{k} = \sqrt{\frac{\sigma}{\rho}} k^{1/2}$$

Group velocity, $c_g = \frac{d\omega}{dk} = \frac{3}{2} \sqrt{\frac{\sigma}{\rho}} k^{1/2} \quad (1)$

$$\therefore \frac{c_g}{c} = \frac{\frac{3}{2} \sqrt{\frac{\sigma}{\rho}} k^{1/2}}{\sqrt{\frac{\sigma}{\rho}} k^{1/2}} = \frac{3}{2}$$

$$c_g = \frac{3}{2} c \quad (1)$$

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1. Using the velocity field

$$u_r = U \cos \theta \left(1 - \frac{3a}{2r} + \frac{a^3}{2r^3} \right), \text{ and } u_\theta = -U \sin \theta \left(1 - \frac{3a}{4r} - \frac{a^3}{4r^3} \right)$$

and the pressure $p - p_\infty = -\frac{3\mu U \cos \theta}{2r^2}$, determine the drag on Stokes' sphere from the surface pressure and the viscous surface stresses σ_{rr} and $\sigma_{r\theta}$:

$$\sigma_{r\theta} = \mu \left(\frac{1}{r} \frac{\partial u_r}{\partial \theta} + \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r} \right), \text{ and } \sigma_{rr} = 2\mu \frac{\partial u_r}{\partial r}.$$

Component of drag force per unit area in the direction of uniform stream is :

$$[-p \cos \theta + \sigma_{rr} \cos \theta - \sigma_{r\theta} \sin \theta]_{r=a}$$

$$\sigma_{rr} = 2\mu \frac{\partial u_r}{\partial r} = 2\mu U \cos \theta \left[\frac{3a}{2r^2} - \frac{3a^3}{2r^4} \right] \quad (1)$$

$$\begin{aligned} \sigma_{r\theta} &= \mu \left[\frac{1}{r} \frac{\partial u_r}{\partial \theta} + \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r} \right] \\ &= \mu \left[\frac{1}{r} \frac{\partial}{\partial \theta} \left(U \cos \theta \left(1 - \frac{3a}{2r} + \frac{a^3}{2r^3} \right) \right) - U \sin \theta \left(\frac{3a}{4r^2} + \frac{3a^3}{4r^4} \right) \right. \\ &\quad \left. + U \frac{\sin \theta}{r} \left(1 - \frac{3a}{4r} - \frac{a^3}{4r^3} \right) \right] \end{aligned}$$

$$\begin{aligned} &= \mu \left[\frac{U \sin \theta}{r} \left\{ -1 + \frac{3a}{2r} - \frac{a^3}{2r^3} - \frac{3a}{4r} - \frac{3a^3}{4r^3} + 1 - \frac{3a}{4r} - \frac{a^3}{4r^3} \right\} \right] \\ &= -\frac{3\mu U a^3}{2r^4} \sin \theta \quad (2) \end{aligned}$$

$$\therefore (\sigma_{rr} \cos \theta - \sigma_{r\theta} \sin \theta) \Big|_{r=a} = 0 + \frac{3\mu U}{2a} \sin^2 \theta \quad (1)$$

Pressure contribution = $\frac{3\mu U}{2a} a^2 \theta$. (1)

$$\therefore [-p \cos \theta + \sigma_{rr} \cos \theta - \sigma_{r\theta} \sin \theta]_{r=a} = \frac{3\mu U}{2a} a^2 \theta + \frac{3\mu U}{2a} a^2 \sin \theta$$

$$= \frac{3\mu U}{2a}$$

\therefore Drag force = $\frac{3\mu U}{2a} \times 4\pi a^2 = 6\pi\mu a U$. (1)