Chapter 4 : Flow Of Incompressible Fluids In Conduit And Thin Layers

<u>Important Terms ⇒</u>

- ★ Friction factor: Ratio of wall shear stress to the product the density and velocity head.
- ★ Hydraulically Smooth: When further smoothening brings about no further reduction in the friction factor for a given Reynolds number.
- ★ Moody Diagram : 1. Log-log plot of friction factor vs Reynolds number.
 - 2. The frictional characteristics of round pipes(both smooth and rough) are summarized by a friction factor chart.
- ★ Vena Contracta: The cross-section of minimum area at which the jet changes from a contraction to an expansion is called vena contracta.
- ★ Couette Flow: It is the flow of a viscous fluid in the space between two surfaces, one of which is moving tangentially relative to the other. The relative motion of the surfaces imposes a shear stress on the fluid and induces flow.

Important Formulas ⇒

1. SHEAR-STRESS DISTRIBUTION IN A CYLINDRICAL TUBE:

$$\frac{dp}{dL} + \frac{2\tau}{r} = 0 \qquad \qquad \frac{\tau_w}{r_w} = \frac{\tau}{r}$$

2. RELATION BETWEEN SKIN FRICTION AND WALL SHEAR:

$$h_{fs} = \frac{2}{\rho} \frac{\tau_w}{r_w} \Delta L = \frac{4}{\rho} \frac{\tau_w}{D} \Delta L$$

3. Friction Factor:

$$f \equiv \frac{\tau_w}{\rho \, \overline{V}^2 / 2g_c} = \frac{2g_c \tau_w}{\rho \, \overline{V}^2}$$

4. RELATIONS BETWEEN SKIN-FRICTION PARAMETERS:

$$h_{fs} = \frac{2}{\rho} \frac{\tau_w}{r_w} \Delta L = \frac{\Delta p_s}{\rho} = 4f \frac{\Delta L}{D} \frac{\bar{V}^2}{2g_c}$$

$$f = \frac{\Delta p_s \, g_c D}{2\Delta \, L \rho \, \bar{V}^2}$$

5. LAMINAR FLOW OF NEWTONIAN FLUIDS:

$$u = \frac{\tau_w g_c}{2r_w \mu} (r_w^2 - r^2)$$
 $\frac{u}{u_{\text{max}}} = 1 - \left(\frac{r}{r_w}\right)^2$

6. Average Velocity:

$$\bar{V} = \frac{\tau_w g_c}{r_w^3 \mu} \int_0^{r_w} (r_w^2 - r^2) r \, dr = \frac{\tau_w g_c r_w}{4\mu} \qquad \frac{\bar{V}}{u_{\text{max}}} = 0.5$$

HAGEN-POISEUILLE EQUATION: Main use is in the experimental measurement of viscosity by measuring pressure drop and volumetric flow rate.

$$\Delta p_s = \frac{32 \ \Delta L \ \overline{V} \mu}{g_c D^2} \qquad \qquad f = \frac{16 \ \mu}{D \overline{V} \rho} = \frac{16}{N_{\rm Re}}$$

8. Velocity Distribution for Turbulent Flow:

$$u^* \equiv \bar{V} \sqrt{\frac{f}{2}} = \sqrt{\frac{\tau_w g_c}{\rho}}$$

$$u^+ \equiv \frac{u}{u^*}$$

$$y^+ \equiv \frac{y u^* \rho}{\mu} = \frac{y}{\mu} \sqrt{\tau_w g_c \rho}$$

where $u^* = friction velocity$

 u^+ = velocity quotient, dimensionless

 y^+ = distance, dimensionless

y =distance from wall of tube

9. UNIVERSAL VELOCITY-DISTRIBUTION EQUATIONS:

• Viscous sublayer:
$$u^+ = y^+$$

• Buffer layer :
$$u^+ = 5.00 \ln y^+ - 3.05$$

• Turbulent layer :
$$u^+ = 2.5 \ln y^+ + 5.5$$

for the viscous sublayer: $y^+ < 5$ for the buffer zone: $5 < y^+ < 30$ for the turbulent core: $30 < y^+$

10. Average velocity:

$$\overline{V} = \frac{5v^2}{r_w^2 u^*} \int_0^{y_c^+} \left(0.4u_c^+ + \ln \frac{y^+}{y_c^+} \right) (y_c^+ - y^+) \, dy^+ \qquad \qquad \frac{\overline{V}}{u_{\text{max}}} = \frac{1}{1 + (3.75\sqrt{f/2})}$$

11. Von-Karman equation:

$$\frac{1}{\sqrt{f/2}} = 2.5 \ln \left(N_{\text{Re}} \sqrt{\frac{f}{8}} \right) + 1.75$$

12. Hydraulic Radius:

$$r_H \equiv \frac{S}{L_p}$$

where S = cross-sectional area of channel $L_p = \text{perimeter}$ of channel in contact with fluid

13. Darcy-Weisbach equation :

$$h_{fs} = \frac{2}{\rho} \frac{\tau_w}{r_w} \Delta L = \frac{\Delta p_s}{\rho} = 4f \frac{\Delta L}{D} \frac{\bar{V}^2}{2g_c}$$