
MEEN 432 –Automotive Engineering

Fall 2026

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Lecture 11: Transmission 1

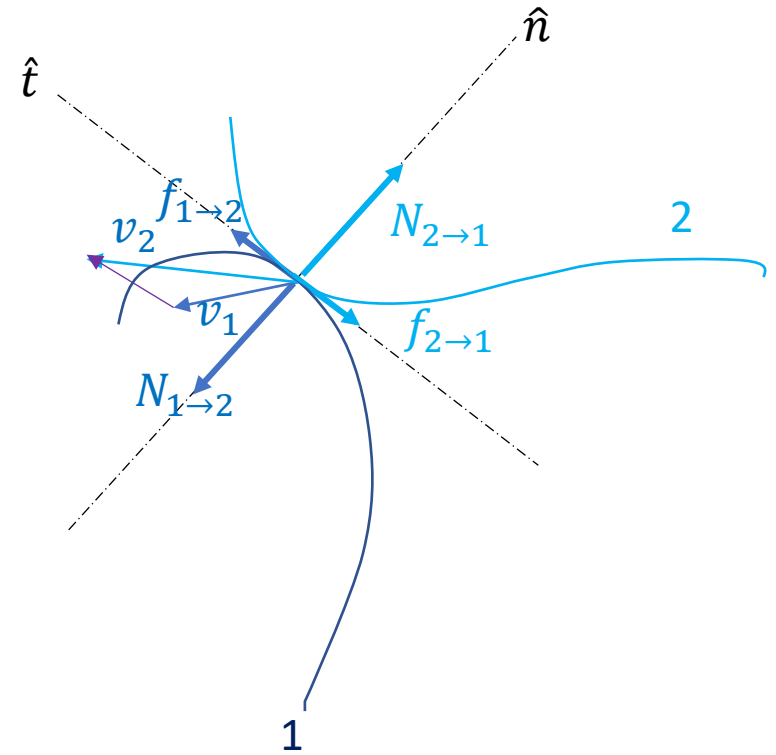
- Gears

Transmission

- The purpose of the transmission is to transmit power from one source of power to another
 - Delivered power is always mechanical in automotive systems, so there is a corresponding torque and angular speed (or force and linear speed):
 - $p_o = \tau_o \omega_o$
 - Input power could be either mechanical or electrical:
 - $p_i = \tau_i \omega_i$ or $p_e = i V$
- Mechanical Power Input to Mechanical Power Input is achieved through mechanical transmissions
 - A common mechanical transmission is composed of “gears”

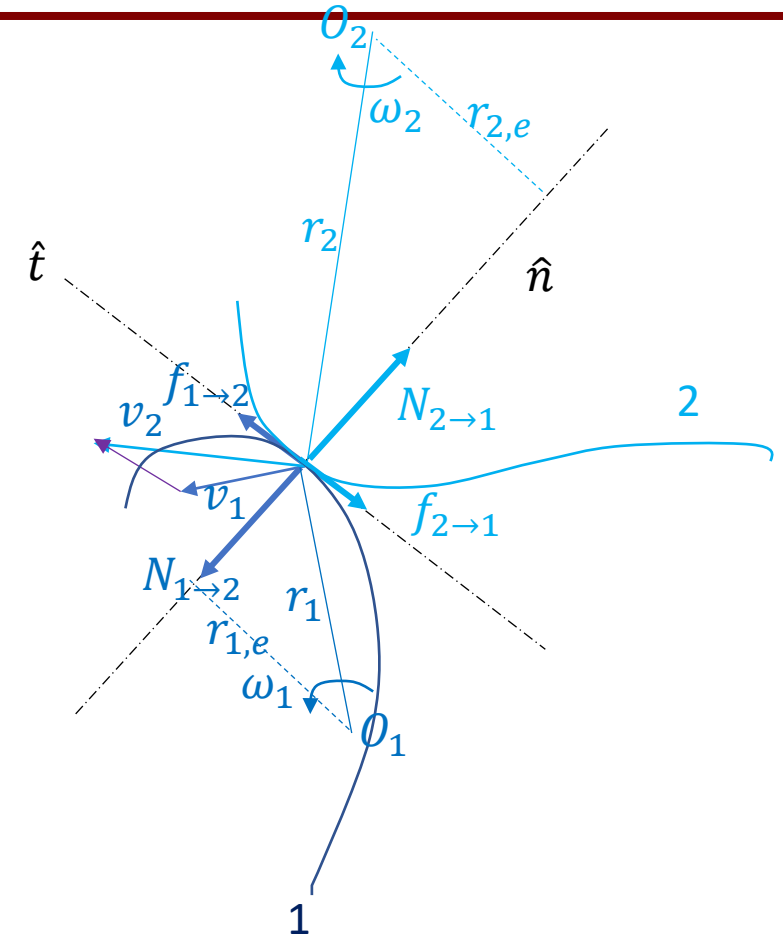
Contact force transmission

- When two surfaces contact each other to transmit force, we consider this a positive engagement
- The interaction force can be considered along two dimensions:
 - Normal to the surface
 - Tangential to the surface
- The tangential component of the force arises because of (and only if there is) friction at the surface
 - Relative motion at point of contact is possible
- The normal component of the force arises because the materials are sufficiently rigid and solid that both materials cannot exist at the same place at the same time!
 - Relative motion at point of contact is not possible without breaking contact
 - Action and Reaction: $N_{1 \rightarrow 2} = N_{2 \rightarrow 1}$ and $f_{1 \rightarrow 2} = f_{2 \rightarrow 1}$
- In general, we would like to design the contact profile so that useful power is transmitted along the normal, and sliding force is minimized by good surface finishes



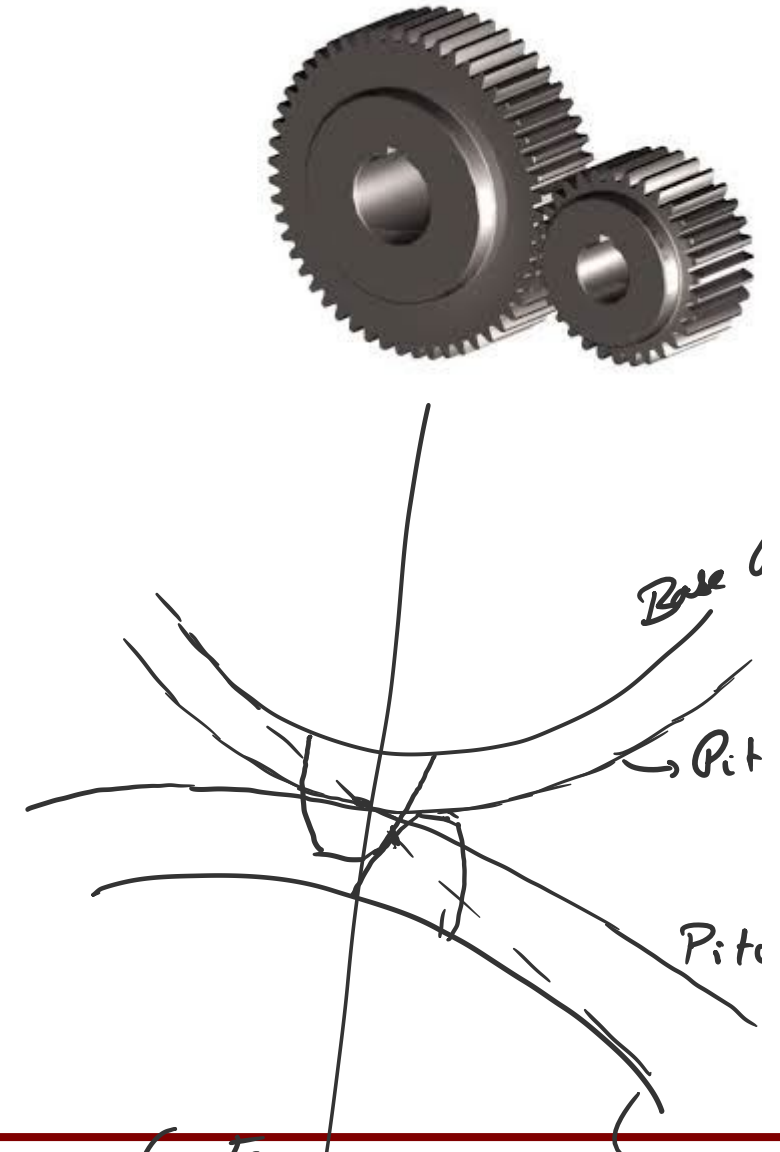
Contact force transmission

- Now consider that the two bodies 1 and 2 are rotating about centers of rotation at O_1 and O_2 , with angular velocities ω_1 and ω_2 respectively as shown
- Additionally let the distance from the center of rotation to the point of contact be r_1 and r_2 respectively
- Consider the case when there is no friction, i.e. $f_{1 \rightarrow 2} = f_{2 \rightarrow 1} = 0$
- Torque on each of the body is then:
 - $\tau_2 = \vec{r}_2 \times N_{2 \rightarrow 1}$ and $\tau_1 = \vec{r}_1 \times N_{1 \rightarrow 2}$
- Alternatively, we can consider the normal force acting tangential to two circles of effective radii $r_{1,e}$, $r_{2,e}$:
 - $\tau_2 = r_{2,e}N$ and $\tau_1 = r_{1,e}N$ with $N = |N_{2 \rightarrow 1}| = |N_{1 \rightarrow 2}|$
- Since relative velocity along normal is zero, we have:
 - $\omega_2 r_{2,e} = \omega_1 r_{1,e}$



Gears

- Gears transmit power through toothed wheels
 - Ideally at a constant ratio of speeds
- How to design a tooth profile such that a constant speed ratio be achieved?
 - This will be achieved if the Normal remains tangential to circles of radii of the desired ratio
 - An “involute” profile is an answer
 - The locus of a thread unwinding from a spooled roll!
- The Gears then behave like they are two “circles rolling on top of each other”!
 - These “effective” circles are called the “pitch circles”
- Dropping the “effective” subscripts we have:
 - $\omega_1 r_1 = \omega_2 r_2$
- Sometimes, pitch diameters are used:
 - $\omega_1 d_1 = \omega_2 d_2$



Simple Gear

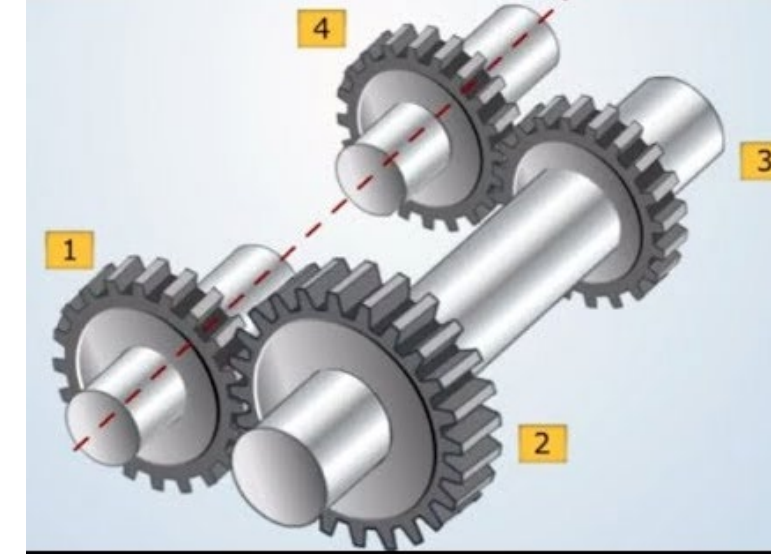
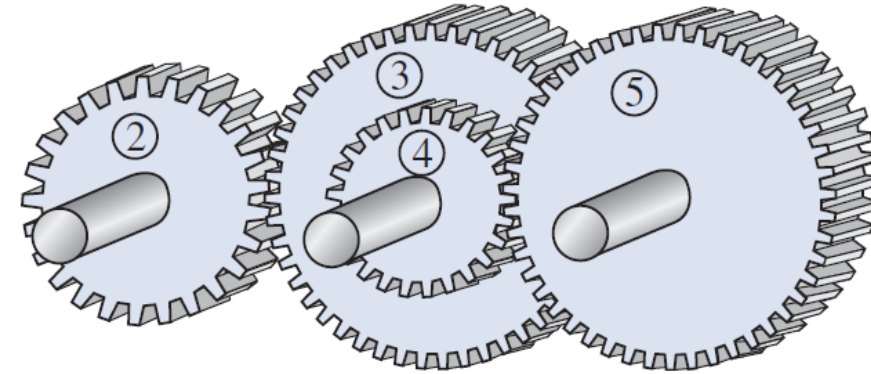
- Ratio of pitch circle diameters
- = Ratio of base circle diameters
- = ratio of number of teeth (assuming they all are equally sized)
- $\frac{\omega_1}{\omega_2} = \frac{d_2}{d_1} = \frac{N_2}{N_1} := G$
- G is used to define a “gear ratio”
 - The ratio of the speed of the input (upstream) shaft to the output (downstream) shaft
- What we have discussed is referred to as a “simple gear”

Power Flow through an “Ideal” Simple Gear

- An “ideal gear” is defined by the following assumptions:
 - Gear teeth surface have no friction
 - Gears have no inertia
- Then no energy can be stored or lost in a gear – so:
 - $p_1 = \tau_1 \omega_1 = p_2 = \tau_2 \omega_2$
 - Using the definition of gear ratio G :
 - $\tau_2 = \tau_1 \frac{\omega_1}{\omega_2} = \tau_1 G$
- The assumption of having no inertias also leads to the ideal gear being called the “kinematic gear”

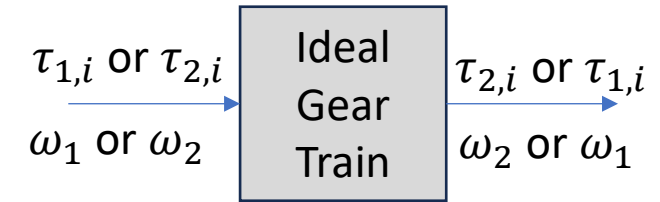
Combinations of gears – a gear train

- A simple gear is approximately characterized by one gear mesh
- Complex gears can be decomposed into a series of simple gears that are “kinematically attached” so the attachment shaft speeds are the same
- For example:
 - Top gear train: $\omega_3 = \omega_4$
 - Bottom gear train: $\omega_2 = \omega_3$
- Each simple gear decomposition follows its own speed relations
- Together the entire “gear train” can be considered as having one “effective” gear ratio
- Example:
 - Top gear train: $G := \frac{\omega_2}{\omega_5} = \frac{\omega_2 \omega_3}{\omega_3 \omega_5} = \frac{\omega_2 \omega_4}{\omega_3 \omega_5} = G_{23} G_{45}$
 - Bottom gear train: $G := \frac{\omega_1}{\omega_4} = \frac{\omega_1 \omega_2}{\omega_2 \omega_4} = \frac{\omega_1 \omega_3}{\omega_2 \omega_4} = G_{12} G_{34}$



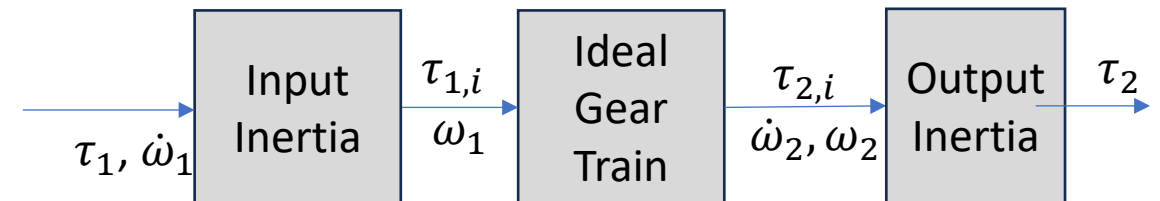
Gear Train Modeling

- An ideal gear train is modeled as a pure torque and speed ratio device, with two shafts 1 & 2



- $\tau_{2,i} = G \tau_{1,i}; \quad \omega_1 = G \omega_2$
 - Here the subscript “ i ” denotes an ideal gear train
- A (non-ideal) real gear train is modeled by partitioning the inertias of all rotating components and assigning them to the two shafts
- The inertias satisfy the standard equations of motion:

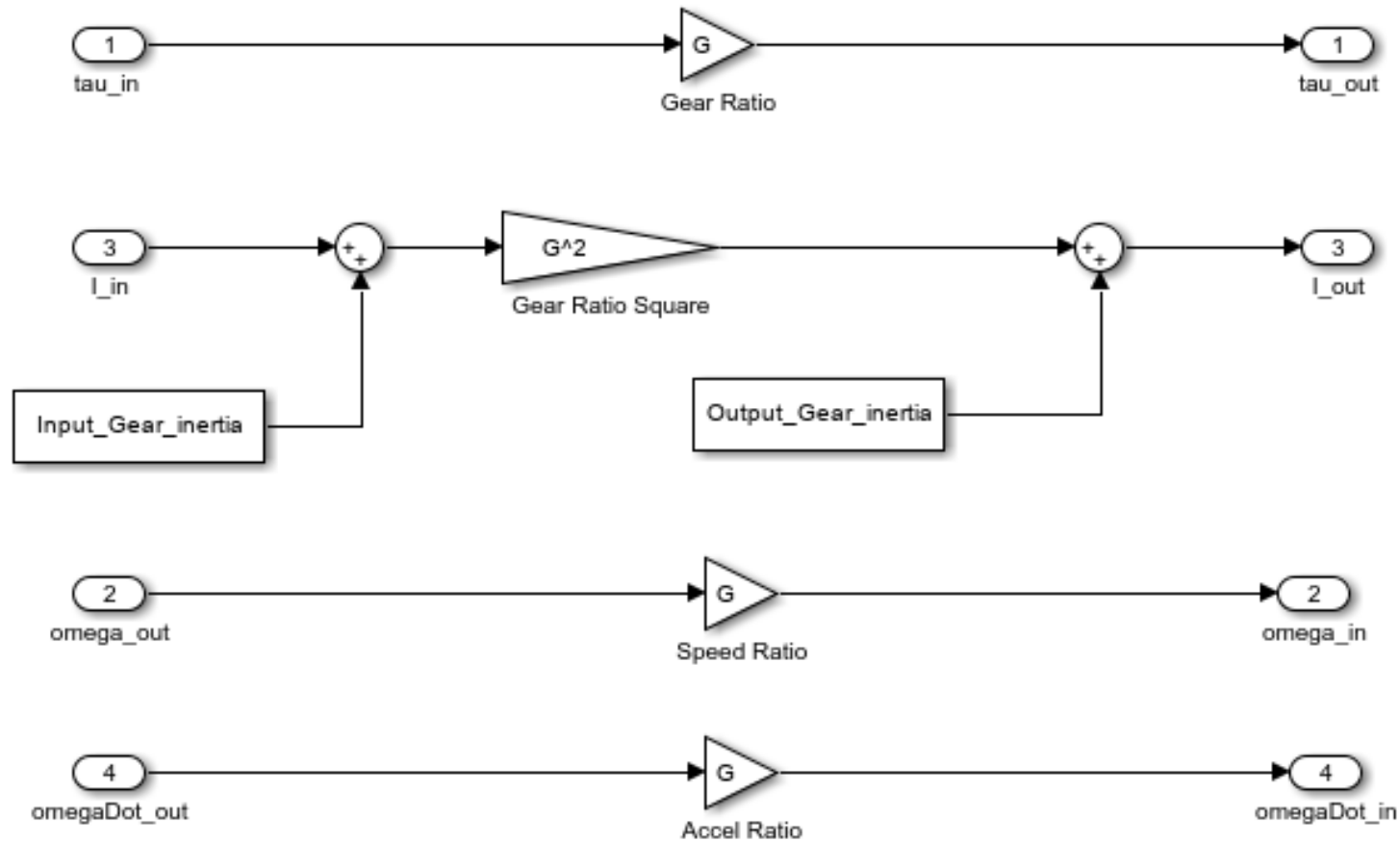
- $\tau_1 - \tau_{1,i} = I_1 \dot{\omega}_1 \quad \text{and} \quad \tau_{2,i} - \tau_2 = I_2 \dot{\omega}_2$



Gear Train Modeling

- Rewriting, we have:
 - $\tau_{1,i} = \tau_{2,i}/G$; $\tau_1 - \tau_{1,i} = I_1 \dot{\omega}_1$; and $\tau_{2,i} = \tau_2 + I_2 \dot{\omega}_2$
- Observing that $\dot{\omega}_1 = G \dot{\omega}_2$ we have:
 - $I_1 \dot{\omega}_1 = \tau_1 - \tau_{1,ideal} = \tau_1 - \frac{\tau_{2,ideal}}{G} = \tau_1 - \frac{1}{G} (I_2 \dot{\omega}_2 + \tau_2) = \tau_1 - \frac{1}{G} (I_2 \frac{\dot{\omega}_1}{G} + \tau_2)$
 - Or $\left(I_1 + \frac{I_2}{G^2}\right) \dot{\omega}_1 = \tau_1 - \frac{1}{G} \tau_2$
- Alternatively, we can also derive:
 - $(I_2 + I_1 G^2) \dot{\omega}_2 = G \tau_1 - \tau_2$
- Note the patterns that you have seen before:
 - The input shaft inertia appears squared by gear ratio when reflected on the output shaft

Gear Train Modeling – Implementation Example



Gear Losses

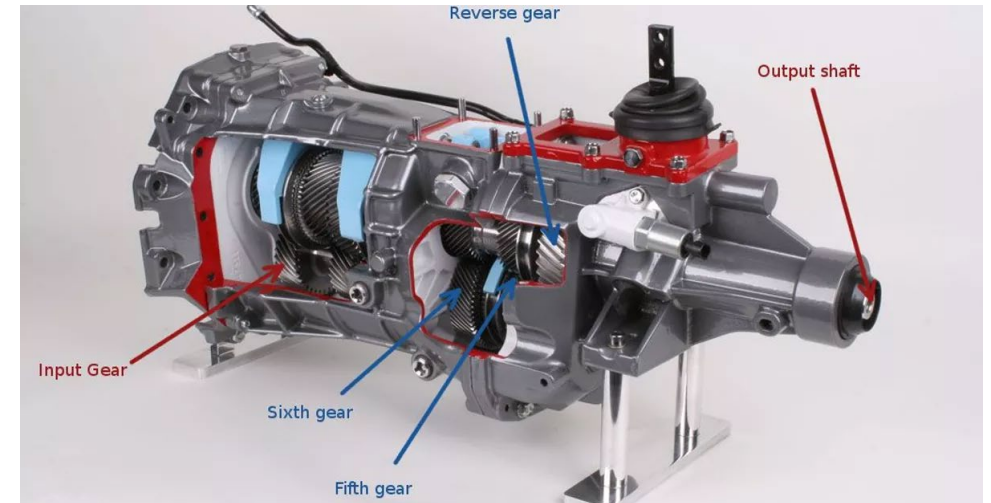
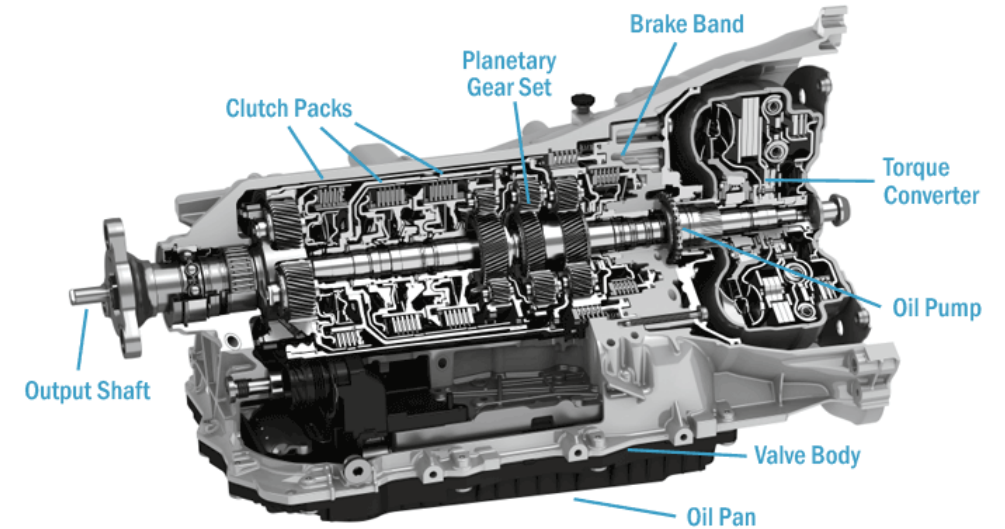
- In reality, there is friction (at the meshes)
 - The loss is characterized in many ways – example, a function of shaft speeds and transmitted torque
 - We will use a simple “Efficiency” η
- We will model gear losses external to the ratio transmission dynamics, and can be either done at the output or the input
 - $p_{loss} = |p_j| (1 - \eta)$ where $|p_1| > |p_2| \Rightarrow j = 1, \text{ else } 2$
 - Then we can write $p_2 = p_1 \eta^{\text{sgn } p_1}$
 - the signum function for negative power flow through the gear train.
 - Gear losses do not impact the kinematics, so we still have $\omega_1 = G \omega_2$
 - Thus: $\tau_2 \omega_2 = \tau_2 \frac{\omega_1}{G} = \tau_1 \omega_1 \eta^{\text{sgn } \tau_1 \omega_1}$
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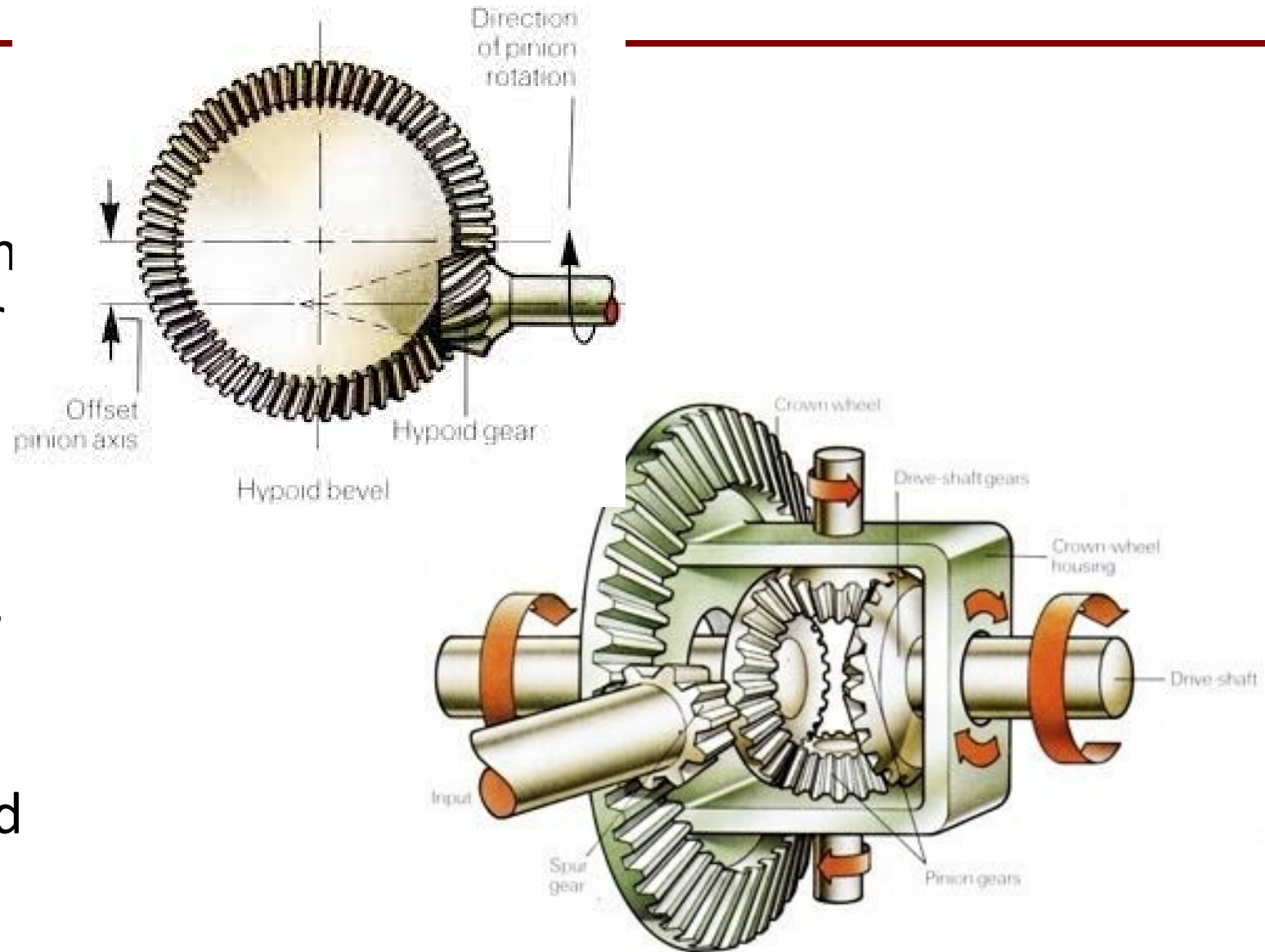
Automotive Transmission

- A typical vehicle transmission consists of multiple gear pairs that could be “selected” in an algorithmic way
 - “Clutches” used to selectively connect/disconnect shafts, and correspondingly which gear train is active
 - A “torque converter” or a “starting clutch” couples the engine with the gear train part of the transmission
- We will not discuss the design of a Transmission for this class scope
 - Instead a transmission will be characterized by its gear ratios (and corresponding input and output inertias, and efficiencies)
 - And we will assume that we can magically control the gear ratio by simply issuing a command
 - In reality, such command will lead a to coordinated actuation of multiple solenoids, which will in turn engage different clutches, to realize the gear change!



Final Drive

- Provides torque multiplication
- Changes direction of rotation (from longitudinal axis of car to along wheel shaft axes)
- Allows for differential rotation of wheels
 - Two-degree of freedom gears (planetary gears)
- For the class scope – just another gear train (with fixed gear ratio!)



Powertrain

- Now you know how to model everything about the longitudinal dynamics
 - Except the power plant – we will consider electric motors
- Components of the powertrain
 - Engine / Electric Motor
 - Transmission
 - Final Drive
 - Wheels
 - Brakes
 - Body
- Control capability (what can the driver (model) influence?)
 - Torque from Engine
 - Torque from Brake
 - Gear Cmd