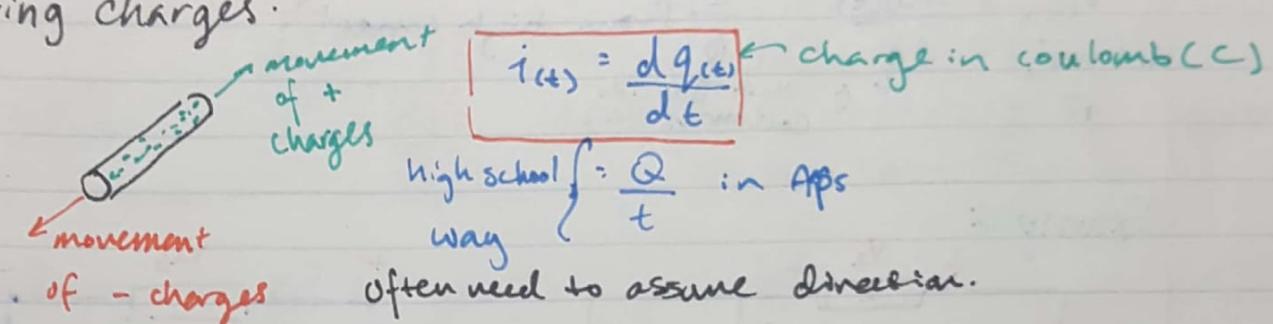


ECE 140

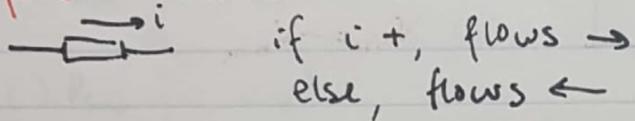
Current:

Jan 4, 2018

Moving charges.



Reference Direction:

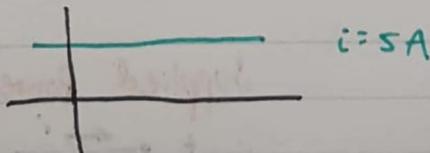


charge:

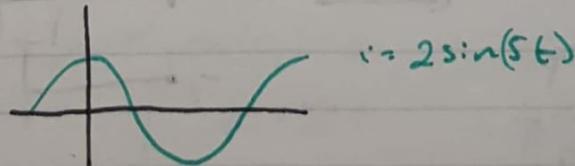
$$q(t) = q(t_0) + \int_{t_0}^t i(\tau) d\tau$$

Types of Current:

1) DC - constant wrt time.



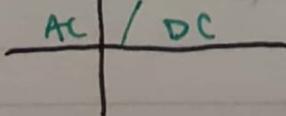
2) AC - Sinusoidal



3) Time Varying:

ANYTHING BUT $i = 5e^{-2t}$

AC / DC



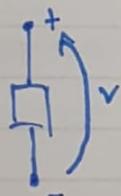
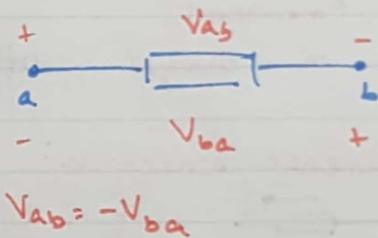
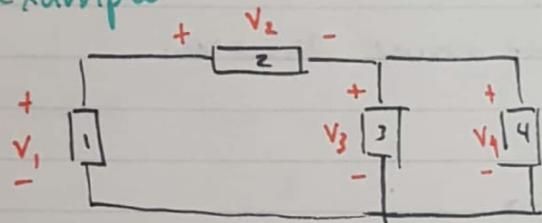
Voltage:

$$V(t) = \frac{dW(t)}{dq} \quad \begin{matrix} \leftarrow \text{Energy (J)} \\ \leftarrow \text{from high school} \end{matrix}$$

AKA emf,
PD

$$\leftarrow \begin{matrix} \text{charge in} \\ \text{Coulombs (C)} \end{matrix}$$

Example:



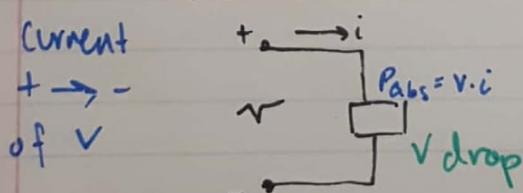
Also sometimes used.

Power:

$$P(t) = \frac{dW}{dt} \quad \begin{matrix} \leftarrow \text{J} \\ \uparrow \text{Watts} \end{matrix} = \frac{dW}{dq} \cdot \frac{dq}{dt} = V \cdot i$$

Jan 8, 2018

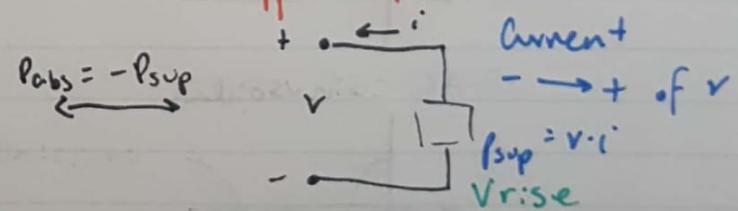
Absorbed Power:



Passive sign convention ↑
+ → i → -

If $P_{abs} > 0$, actually absorbed: <0 supplied.

Supplied Power:

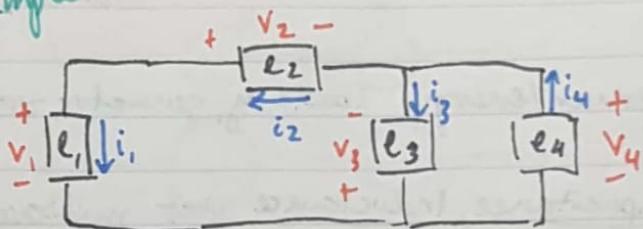


$$Psup = V \cdot i$$

$$V_{rise}$$

$$Current + - \rightarrow + \text{ of } V$$

Example:



$$\begin{aligned}i_1 &= i_2 = 5A & V_1 &= 8V \\i_3 &= -2A & V_2 &= -2V & V_4 &= 10V \\i_4 &= 3A & V_3 &= -10V\end{aligned}$$

a) Power for e_1 ? Not specified? Assume abs.

$$P_{abs} = V_1 i_1 = 40W +40, \text{ so actually abs.}$$

b) P_{abs} for e_2 ?

$$P_{abs} = -V_2 i_2 = 10W +10, \text{ so actually abs.}$$

c) P_{sup} for e_3 ?

$$P_{sup} = V_3 i_3 = 20W +20, \text{ so actually sup.}$$

d) P_{abs} for e_4 ?

$$P_{abs} = -V_4 i_4 = -30W -30, \text{ so actually sup.}$$

} concerned

Conservation of Power/Energy:

$$\sum P_{abs} = \sum P_{sup} \quad \sum P = 0$$

Energy:

$$w = w(t_2) - w(t_1) = \int_{t_1}^{t_2} p(\tau) d\tau \quad \left. \right\} \text{number}$$

Assume $t_1 = -\infty$, $w(t_1) = 0$.

$$w(t) = \int_{-\infty}^t p(\tau) d\tau \quad \left. \right\} \text{function of } t.$$

Circuit Elements:

Jan 9, 2018

1) Active:

↳ Generates power/energy (battery, generator, transistor)

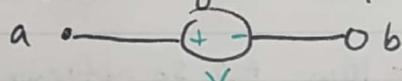
2) Passive:

↳ Resistance, Capacitance, Inductance (post midterm).

↳ Absorbs/stores energy.

3) Independent Voltage Source:

↳ Specific v. regardless of i. (Not constant, but independent)

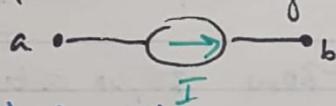


$$V_{ab} = V, \text{ no matter } i$$

I, V
independent
of each other

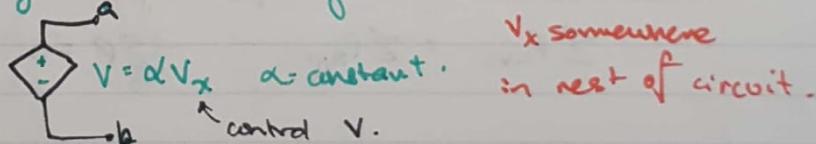
4) Independent Current Source:

↳ Specific current regardless of v. (" " "



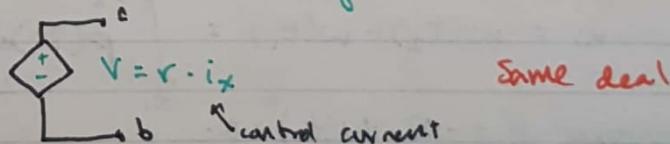
5) Dependent Sources:

a) Voltage-controlled Voltage Source:



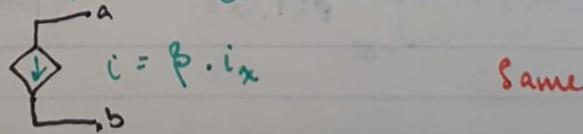
V_x somewhere
in rest of circuit.

b) Current-controlled Voltage Source:



Same deal

c) Current-controlled Current Source:



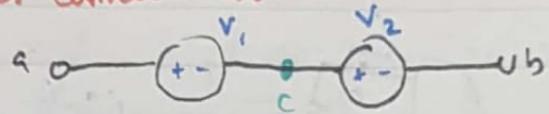
Same

d) Voltage-controlled Current Source:

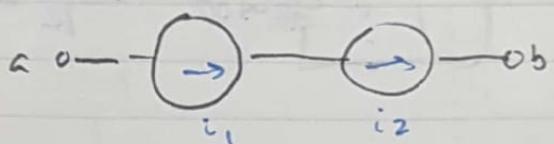


Same

Series Connection:

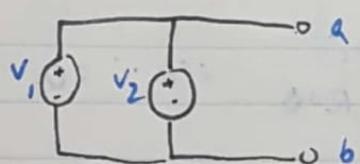


Only V_1, V_2 connected at C.



i_1 should = i_2 (else invalid)

Parallel Connection:



V_1 should = V_2
(else invalid)



valid

"Parallel" - Connected b/w same two nodes (a, b).

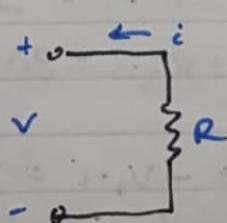
Resistance and Ohm's Law:

$$R \begin{array}{l} | \\ \downarrow i \\ | \\ V \end{array} \quad \boxed{V = R \cdot i} \quad R \geq 0$$

$$\hookrightarrow i = \frac{1}{R} \cdot V$$

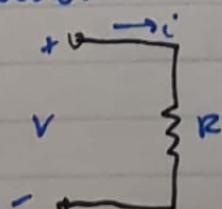
= $G \cdot V$ where G = conductance in Siemens (S or Ω^{-1})

Note:



$V = -R \cdot i$ for this
(watch for current direction)

Power:



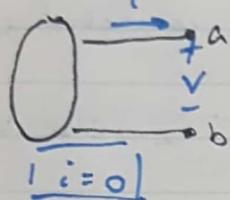
$$P_{abs} = V \cdot i$$

$$= R \cdot i^2$$

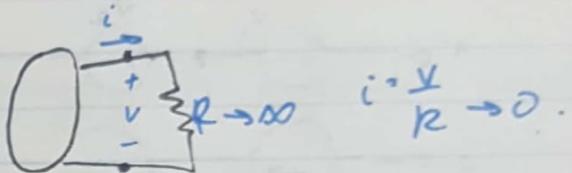
$$= \frac{V^2}{R}$$

$\left. \begin{array}{l} \geq 0 \text{ b/c of } ^2 \\ \text{Resistors always} \\ \text{absorb power.} \end{array} \right\}$

Open Circuit:

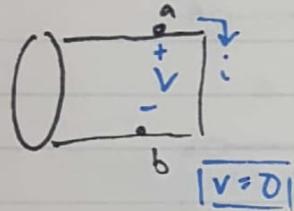


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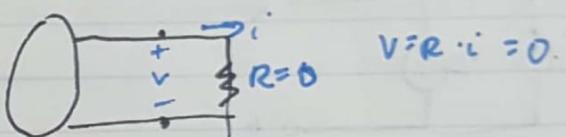


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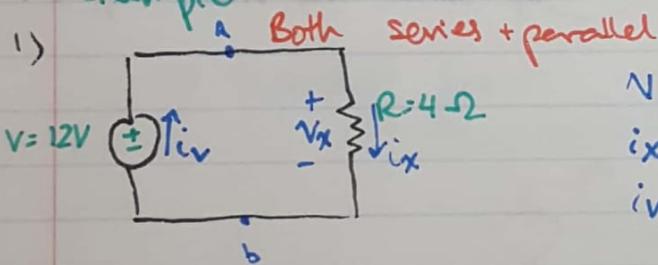
Short Circuit:



=



Example:

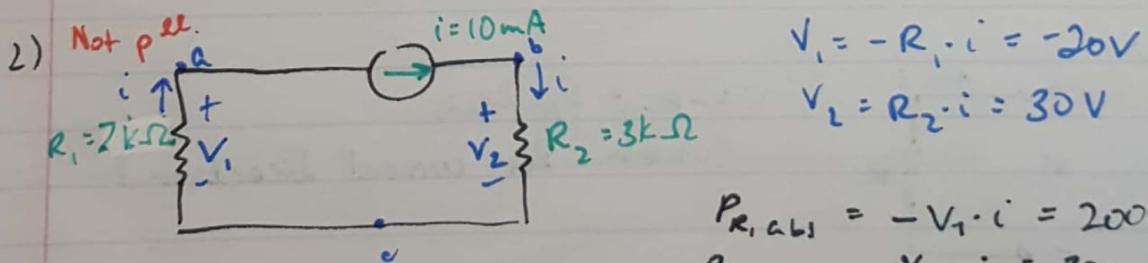


$$N_x = 12V \quad (-12V \text{ if } -+)$$

$$i_x = \frac{V_x}{R_x} = 3A$$

$$i_V = i_x = 3A.$$

$$P_{R,\text{abs}} = 12 \cdot 3 = 36W \text{ and } P_{r,\text{abs}} = -V \cdot i = -36W.$$



$$V_1 = -R_1 \cdot i = -20V$$

$$V_2 = R_2 \cdot i = 30V$$

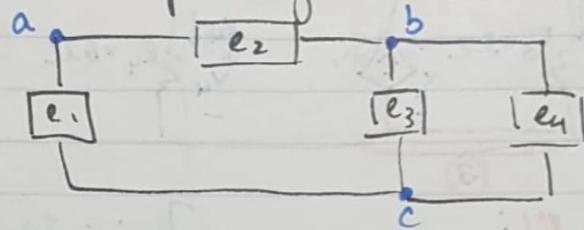
$$P_{R_1,\text{abs}} = -V_1 \cdot i = 200mW$$

$$P_{R_2,\text{abs}} = V_2 \cdot i = 300mW$$

Kirchhoff's Current Law (KCL):

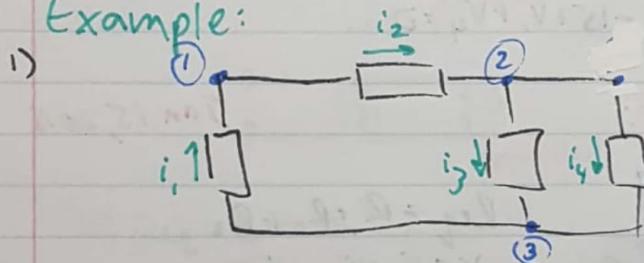
Jan 17, 2018

A node: pt or junction where 2+ elements connected.



KCL: sum of all currents at any node = 0.
 $\sum i_{in} = 0$ i enter = i leaving node.

Example:



$$\begin{aligned} 1) i_1 &= i_2 \\ 2) i_2 &= i_3 + i_4 \\ 3) i_3 + i_4 &= i_1 \end{aligned}$$

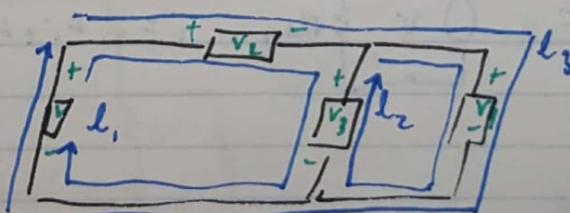
Note linear
independence/
dependence

N nodes give N-1 independent KCL eqn.

Kirchhoff's Voltage Law (KVL):

A loop: closed path where no element is encountered more than once.

mesh:
loop w/o any
loops instllit.

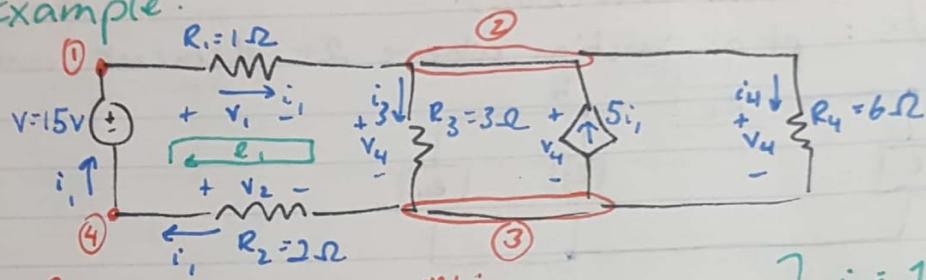


$$\begin{aligned} 1) V_1 &= V_2 + V_3 \\ 2) V_3 &= V_4 \\ 3) V_2 + V_4 &= V_1 \end{aligned}$$

KVL: sum of all voltages around any loop is 0.
 $\sum V_n = 0$ $V_{\text{drops}} = V_{\text{rises}}$

N meshes give N independent KVL eqn.

Example:



OL:

$$V_1 = R_1 i_1$$

$$V_2 = -R_2 i_1$$

$$V_3 = R_3 i_3$$

$$V_4 = R_4 i_4$$

KCL:

Only need node 2

$$i_1 + 5i_1 = i_3 + i_4$$

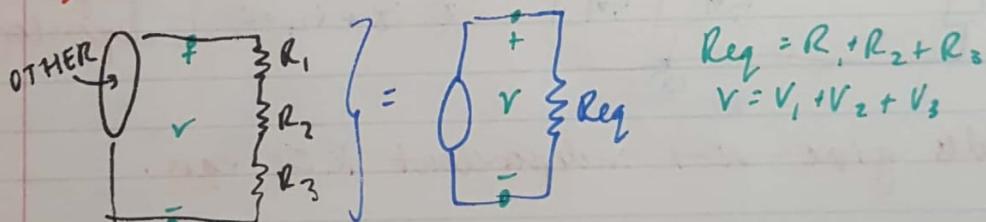
KVL: Only need V_1

$$-V_2 - 15 + V_1 + V_4 = 0$$

$$\left. \begin{array}{l} i_1 = 1A \\ i_4 = 2A \\ i_3 = 4A \end{array} \right. \quad \left. \begin{array}{l} V_1 = 1V \\ V_2 = -2V \\ V_4 = 12V \end{array} \right.$$

Equivalent Series Resistors:

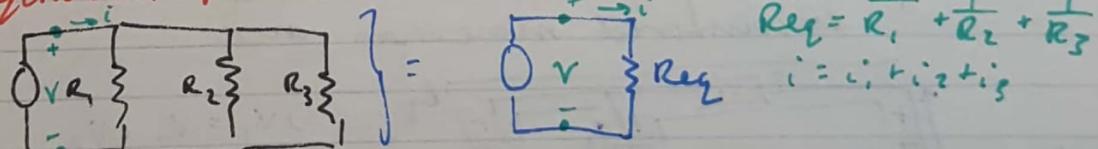
Jan 15, 2018



$$Req = R_1 + R_2 + R_3$$

$$V = V_1 + V_2 + V_3$$

Equivalent Parallel Resistors:

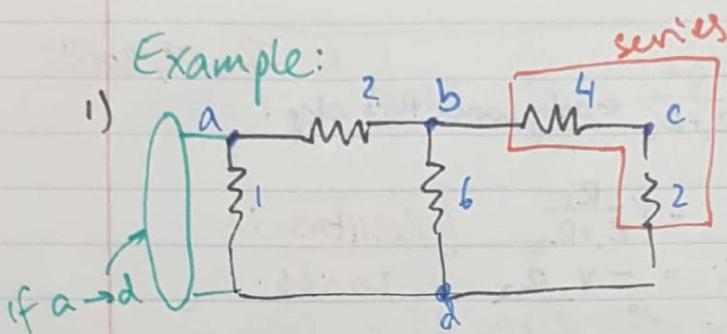


$$\frac{1}{Req} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}$$

$$i = i_1 + i_2 + i_3$$

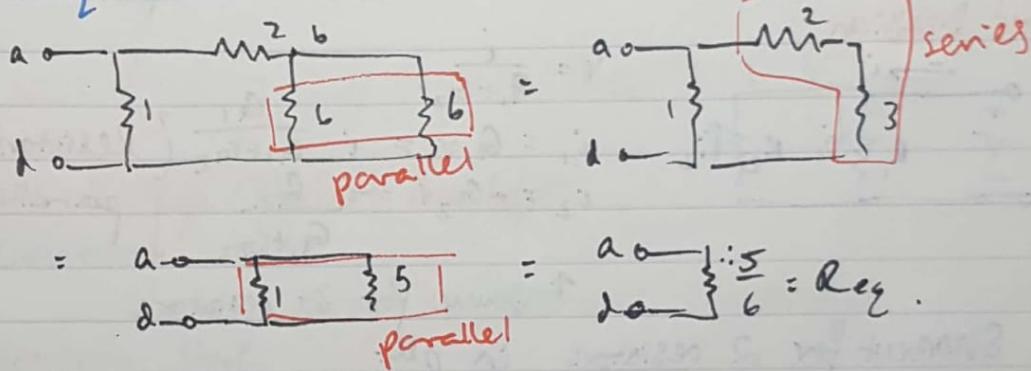
Note:

$$\left(\text{parallel branch} \right) R_1 = 0 \quad \Rightarrow \quad Req = 0$$

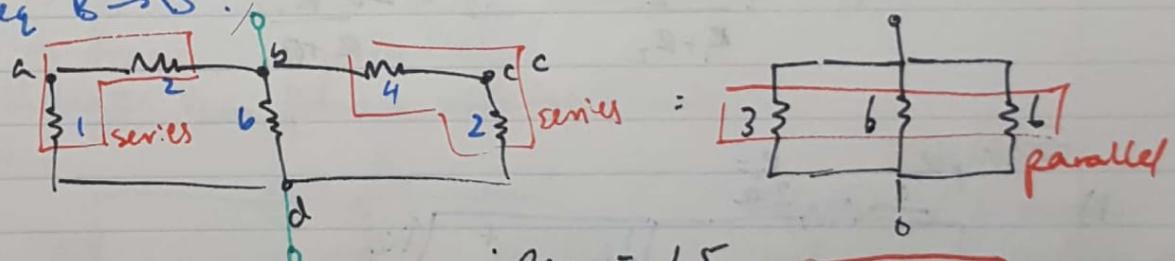


Should draw rest of circuit on left to show 1,2 not in series.
→ depends on nodes you want (a,d)

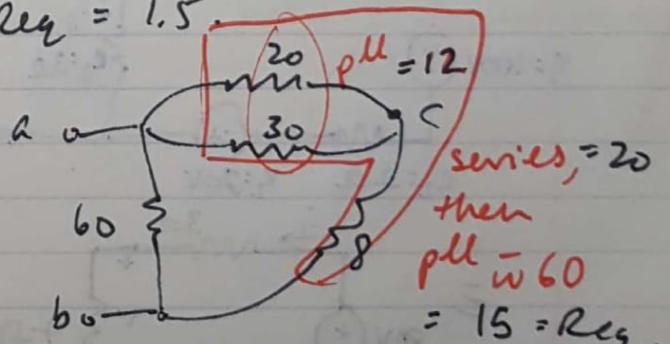
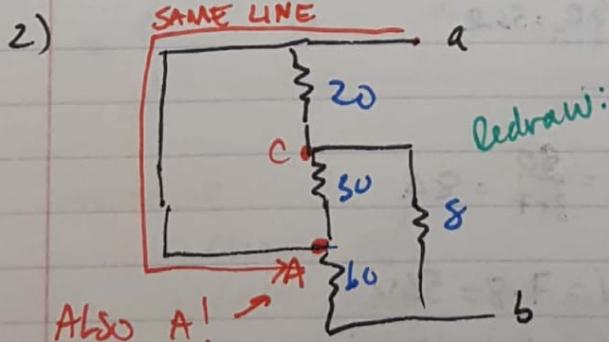
a) Req $A \rightarrow D$?



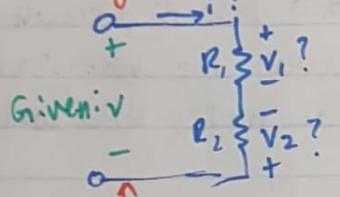
b) Req $B \rightarrow D$?



$$\therefore \text{Req.} = 1.5$$



Voltage Division:



Given: V

$$i = \frac{V}{R_1 + R_2} \quad \text{only solves this step.}$$

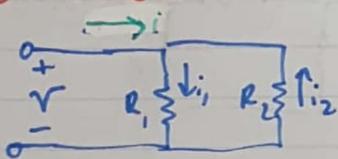
$$\begin{aligned} V_1 &= R_1 i = \frac{V R_1}{R_1 + R_2} \\ V_2 &= -R_2 i = -\frac{V R_2}{R_1 + R_2} \end{aligned} \quad \left. \begin{array}{l} \text{Resistors in} \\ \text{series.} \end{array} \right\}$$

based on $+V -$

same for 3+ resistors

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Current Division:



$$V = \frac{i}{G_1 + G_2}$$

$$\begin{aligned} i_1 &= G_1 V = i \frac{G_1}{G_1 + G_2} \\ i_2 &= -G_2 V = i \frac{G_2}{G_1 + G_2} \end{aligned} \quad \left. \begin{array}{l} \text{Resistors in} \\ \text{parallel} \end{array} \right\}$$

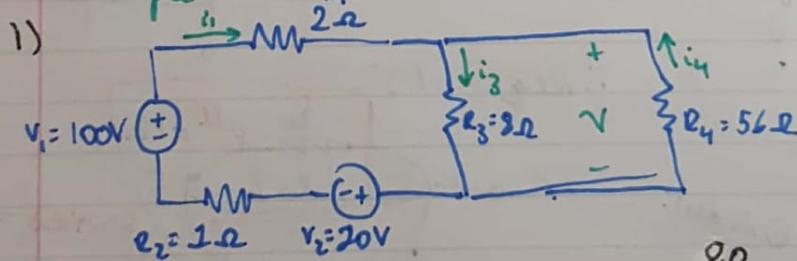
same for 3+ resistors

Shortcut for 2 resistors in par:

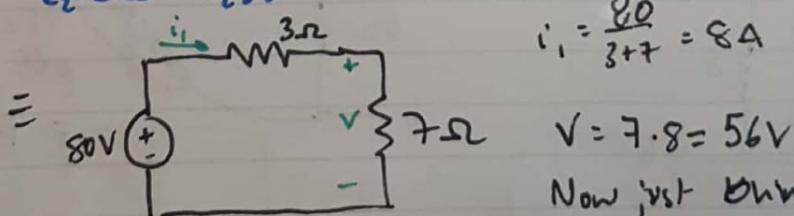
$$i_1 = i \frac{R_2}{R_1 + R_2}$$

$$i_2 = -i \frac{R_1}{R_1 + R_2}$$

Example:



$$i_1 = \frac{80}{3+7} = 8A$$

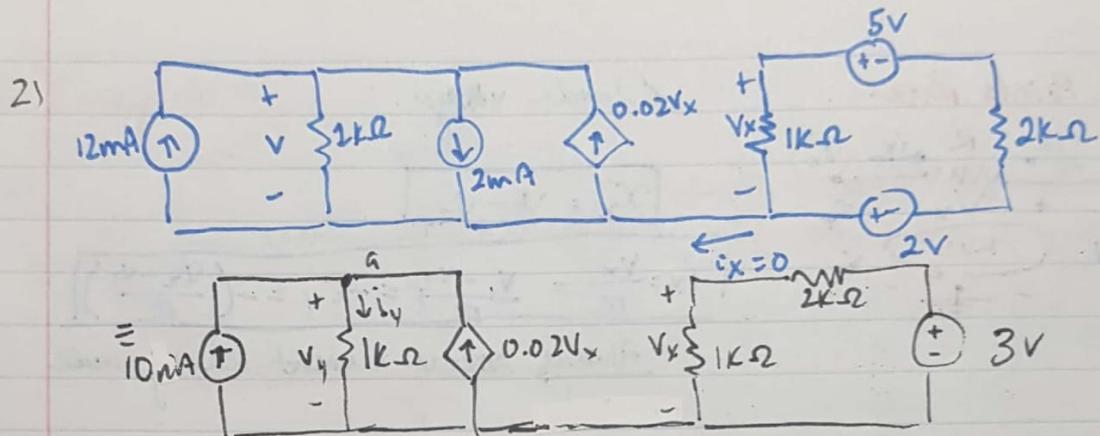


$$V = 7 \cdot 8 = 56V$$

Now, use Ohm's law.

$$\text{Or, CD: } i_3 = i_1 \frac{R_4}{R_3 + R_4}$$

$$i_4 = -\frac{i_1 \cdot R_3}{R_3 + R_4}$$



$$\text{By VD: } V_x = 3 \cdot \frac{1}{1+2} = 1V \text{ Then KCL } V_y = 3V$$

Node-Voltage (Nodal) Analysis:

Essential Node:

→ Node where 3+ elements connected

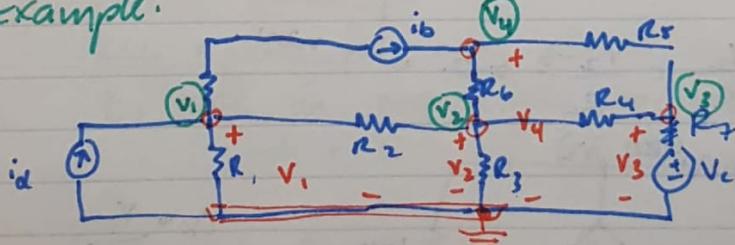
Reference Node:

→ One of essential nodes chosen arb. $\Rightarrow \frac{1}{R_1} = \frac{1}{R_2}$

→ Assumed 0 potential.

Node Voltage: V_{drop} from a node → ref. node.

Example:



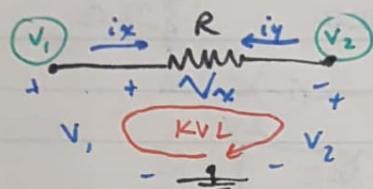
Jan 19, 2018

of node V's @ essential nodes = # of ind. eqns.
(4)

Procedure:

- 1) choose ref.
- 2) Label node voltages
- 3) Assign currents to branches (optional)
- 4) KCL at each non-ref essential node.
- 5) Ohm's law + KVL to get all I in terms of voltages.

Three Points Rule:



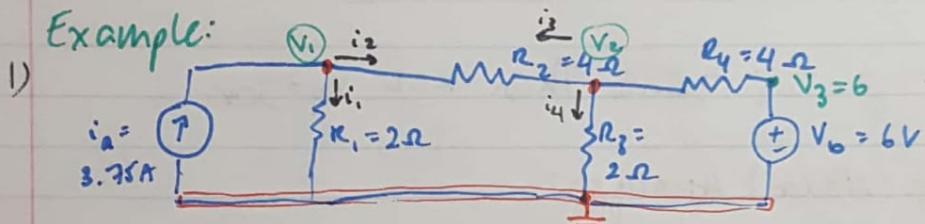
Node voltages.

$$V_x = V_1 - V_2$$

$$i_X = \frac{V_x}{R} = \frac{V_1 - V_2}{R} = -i_Y = -\left(\frac{V_2 - V_1}{R}\right)$$

Always assume current leaving node

Example:



$$KCL 1: 3.75 = i_1 + i_2$$

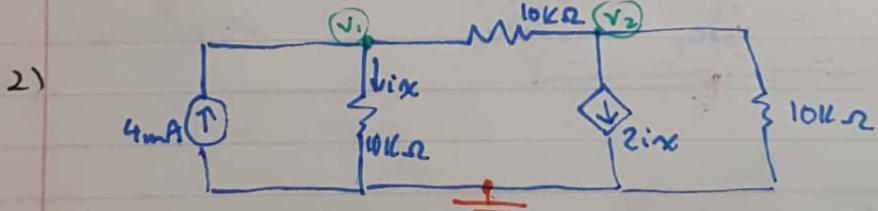
$$3pt \text{ rule: } i_1 + i_2 = -3.75 \quad \leftarrow \text{enter} = -ve, \text{leave} = +ve$$

$$\frac{V_1}{2} + \frac{V_2 - V_1}{4} = 3.75$$

$$0.75V_1 - 0.25V_2 = 3.75$$

KCL 2:

$$\frac{V_2 - V_1}{R_2} + \frac{V_2}{R_3} + \frac{V_2 - 6}{R_4} = 0$$



$$i_X = \frac{V_1}{10}$$

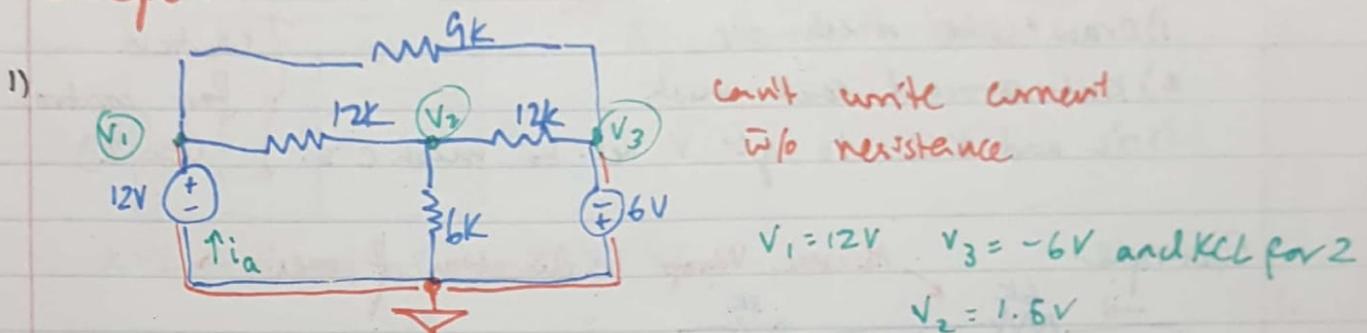
$$KCL 1: -4mA + \frac{V_1}{10k} + \frac{V_1 - V_2}{10k} = 0 \quad \leftarrow \text{Solve}$$

$$\frac{2}{10}V_1 - \frac{1}{10}V_2 = 4$$

$$KCL 2: \frac{V_2 - V_1}{10} + 2i_X + \frac{V_2}{10} = 0 \quad \leftarrow \begin{cases} V_1 = 16V \\ V_2 = -8V \end{cases}$$

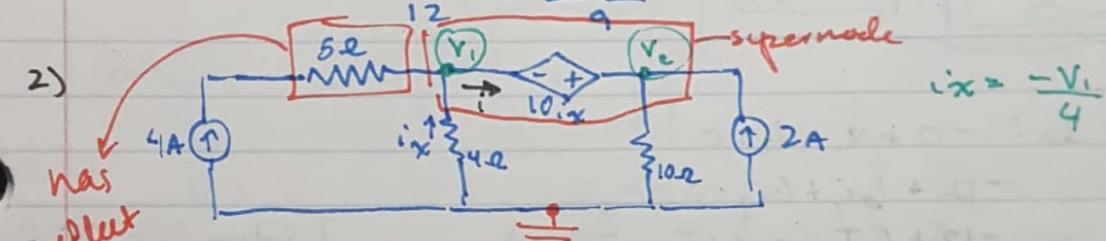
Exceptions:

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To get i_a , KCL V_1 :

$$i_a = \frac{V_1 - V_2}{12} + \frac{V_1 - V_3}{6} = 2.875 \text{ mA}$$



KCL 1: $-4 + \frac{V_1}{4} + i = 0 \quad \left\{ V_2 - V_1 = 10 \left(\frac{-V_1}{4} \right) \right.$. Now
 KCL 2: $-i + \frac{V_2}{10} - 2 = 0 \quad \left. \text{solve.} \right.$

Supernode Shortcut:

KCL applies for any closed surface.

Do KCL on supernode to avoid using i .

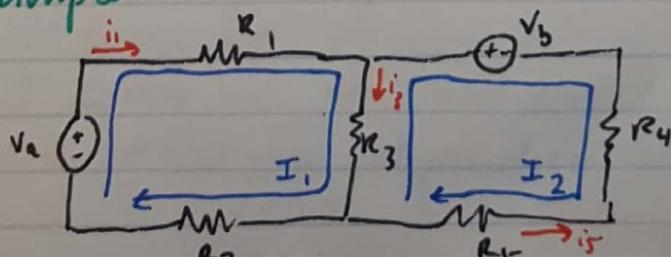
$$-4 + \frac{V_1}{4} + \frac{V_2}{10} - 2 = 0.$$

Mesh Current Analysis:

Jan 23, 2018

Mesh Current - Imaginary current, one direction + value.

Example:



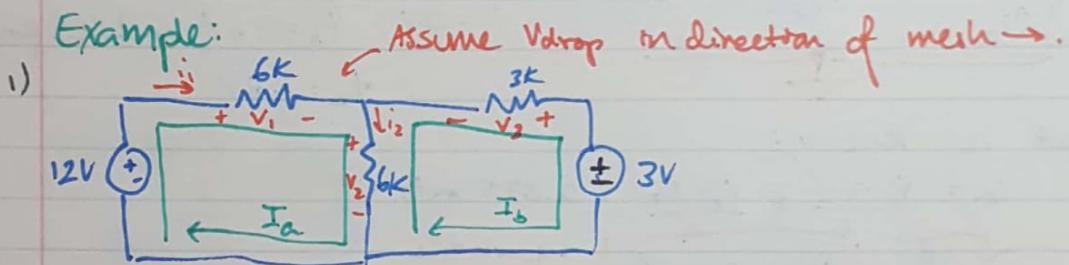
I_1, I_2 mesh currents
 $i_1 = I_1, \quad i_2 = I_1 - I_2, \quad i_3 = -I_2$ branch currents

Procedure:

- 1) Draw + label mesh a's
- 2) KVL around each mesh
- 3) O'L and KCL to get V rel. to mesh c's.

} Watch
for control
(ex 2)

Example:



$$\text{KVL } I_a: -12 + V_1 + V_2 = 0$$

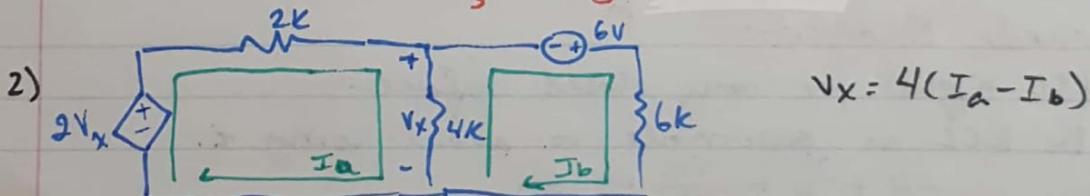
$$-12 + 6i_1 + 6i_2 = 0$$

$$-12 + 6I_a + 6(I_a - I_b) = 0$$

$$\text{KVL } I_b \text{ (short form): } 6(I_b - I_a) + 3I_b = -3 \quad \left. \begin{array}{l} \text{solve for } I_a = \frac{5}{4} \text{ mA} \\ I_b = \frac{1}{2} \text{ mA} \end{array} \right\}$$

Can solve either w/ I_b, I_a rex: $i_2 = I_a - I_b$

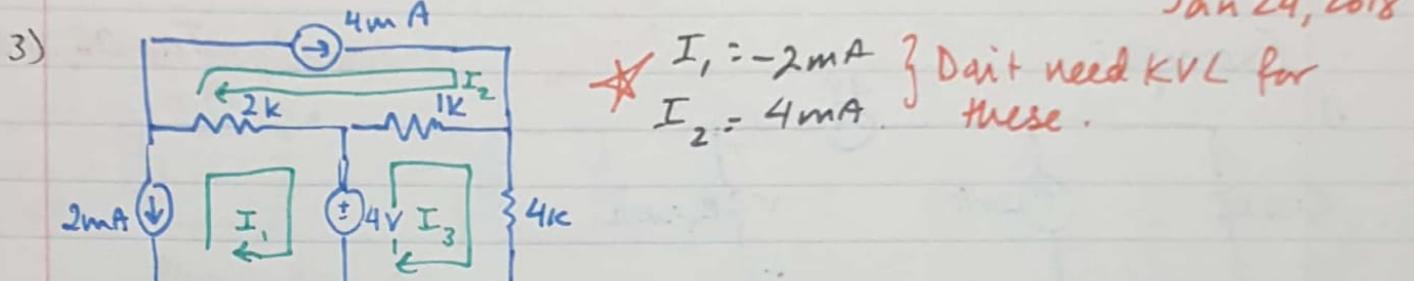
$$\Rightarrow V_3 = 3I_b$$



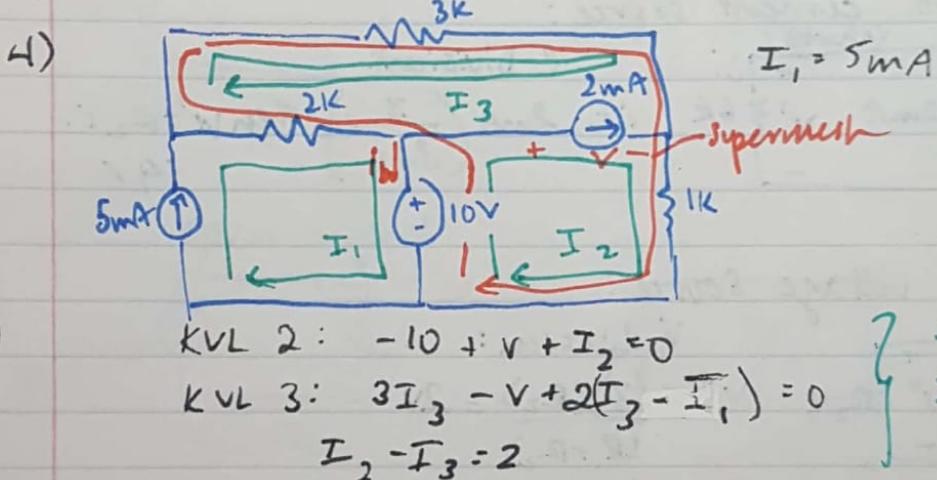
$$V_x = 4(I_a - I_b)$$

$$\text{KVL } I_a: -2V_x + 2I_a + V_x = 0 \quad \left. \begin{array}{l} \text{solve for } I_a = 6 \text{ mA} \\ I_b = 3 \text{ mA} \end{array} \right\}$$

$$\text{KVL } I_b: 4(I_b - I_a) - 6 + 6I_b = 0$$



$$\text{KVL 3: } -4 + (I_3 - I_2) + 4I_3$$



Supermesh Shortcut:

$$\text{KVL: } -10 + 2(I_3 - I_1) + 3V_3 + I_2 = 0 \quad (\text{KVL 2} + \text{KVL 3})$$

$i_b = I_1, -I_2 = 0 \Rightarrow$ removing this branch makes no diff.

Principle of Superposition:

CURRENT/VOLTAGE in a linear circuit can be found as the alg. sum of the indiv. contributions of each indep. source acting alone.

Deactivating Indep. Sources:

V source = 0 \Rightarrow short circuit.

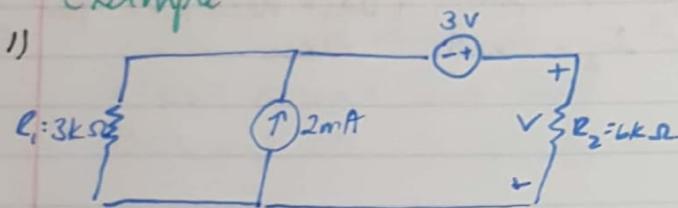
I source = 0 \Rightarrow open circuit.

*Not for dependent sources!!!

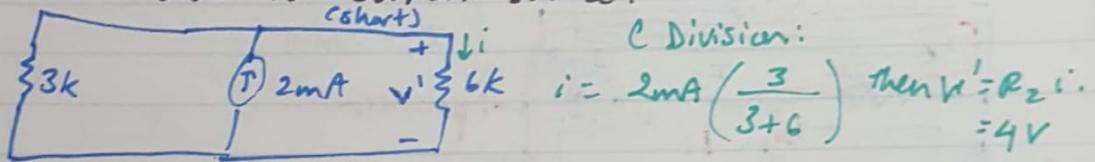
Jan 24, 2018

Example:

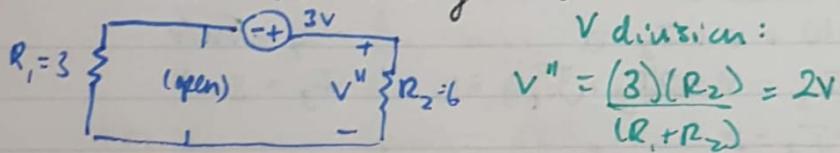
Jan 26, 2018



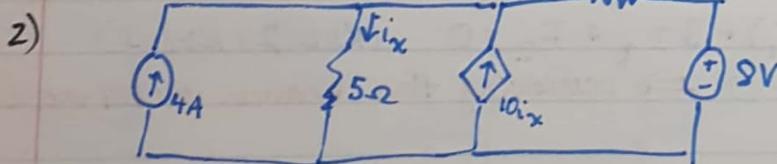
V' due to current source:



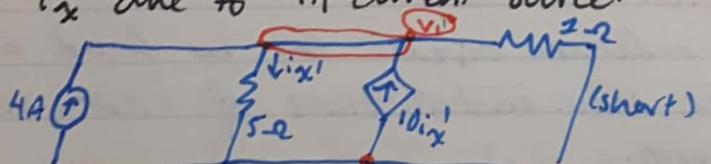
V'' due to voltage source:



By superposition, $V = V' + V'' = 6V$

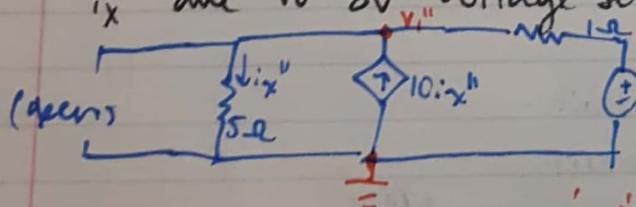


i_x' due to 4A current source:



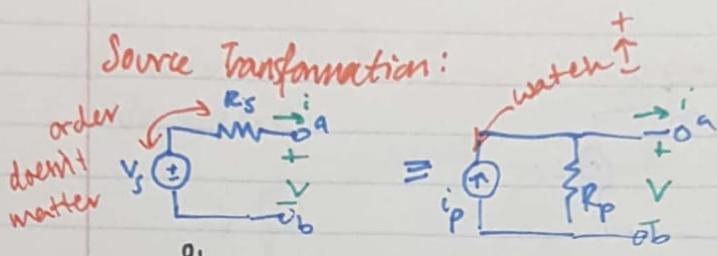
$$KCL V_1': -4 + \frac{V_1'}{5} - 10 \cdot \frac{V_1'}{5} + V_1' = 0$$
$$V_1' = -5V, i_x' = -1A$$

i_x'' due to 9V Voltage source:



$$KCL V_1'': \frac{V_1''}{5} - 10i_x'' + \frac{V_1'' - 8}{1} = 0$$
$$V_1'' = -10V, i_x'' = -2A$$

$\therefore i_x = i_x' + i_x'' = -3A$ by superposition.



Short circuit:

$i_{sc} = \frac{V_s}{R_s}$

i_p

R_p

$V=0$

$i_{sc} = i_p$

$$\left. \begin{aligned} &= i_p \\ &\quad \left. \begin{aligned} &i=0 \\ &V=0 \\ &R_p \end{aligned} \right. \\ &\quad \left. \begin{aligned} &i=0 \\ &V=0 \\ &R_p \end{aligned} \right. \end{aligned} \right\} \therefore i_p = \frac{V_s}{R_s}$$

Open circuit:

$V_{oc} = V_i$

i_p

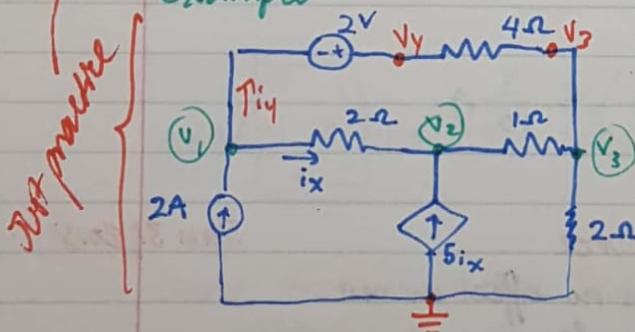
R_p

V_{oc}

$i=0$

$$\left. \begin{aligned} &= i_p \\ &\quad \left. \begin{aligned} &i=0 \\ &V=0 \\ &R_p \end{aligned} \right. \\ &\quad \left. \begin{aligned} &i=0 \\ &V=0 \\ &R_p \end{aligned} \right. \end{aligned} \right\} \therefore R_p = R_s$$

Example:



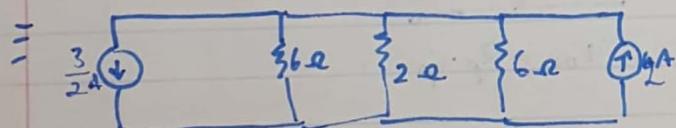
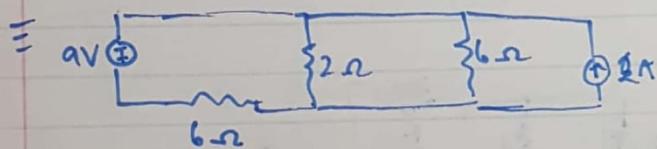
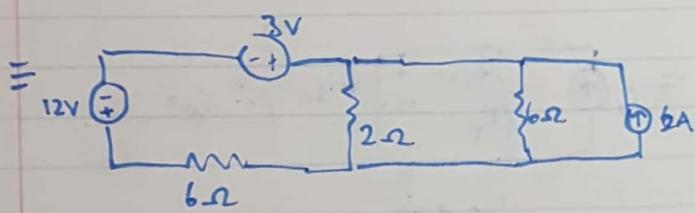
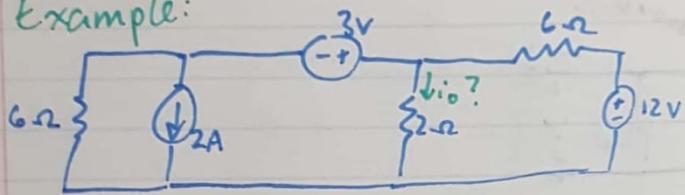
$$V_2 = 2 + V_1, \quad i_x = \frac{V_1 - V_2}{2}$$

$$KCL 1: -2 + \frac{V_1 - V_2}{2} + \frac{V_1 + 2 - V_3}{4} = 0$$

$$KCL 2: -5i_x + V_2 - V_3 - i_x = 0$$

$$KLL 3: \frac{V_3}{2} + V_3 - V_2 + \frac{V_3 - V_1 - 2}{4} = 0$$

Example:

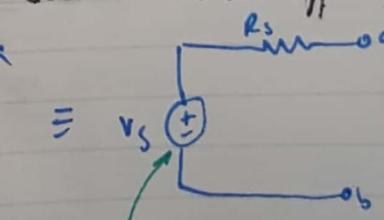
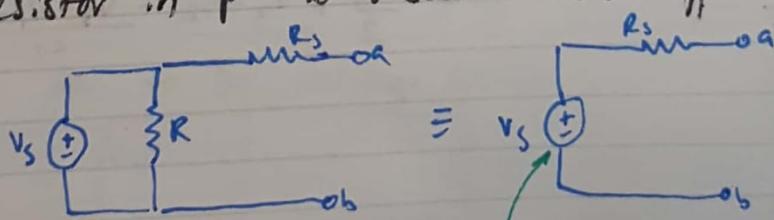


$$= \frac{1}{2}A \uparrow \quad \frac{3}{5}A \downarrow \quad \text{c' division: } i_o = \frac{1}{2} \left(\frac{3}{5} \right) = \frac{3}{10} A$$

Resistor in \parallel w Voltage source

Resistor in \parallel w V source has no effect on rest.

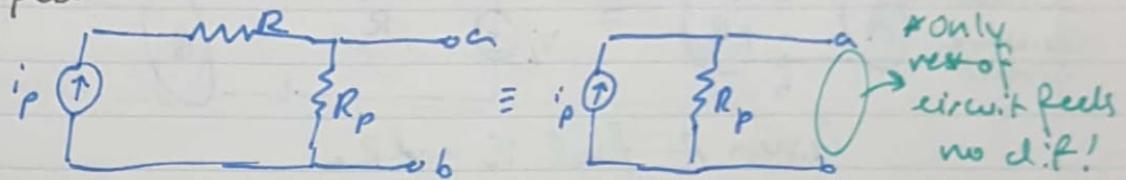
Jan 31, 2018



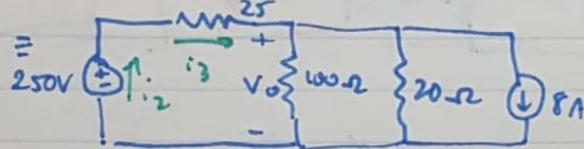
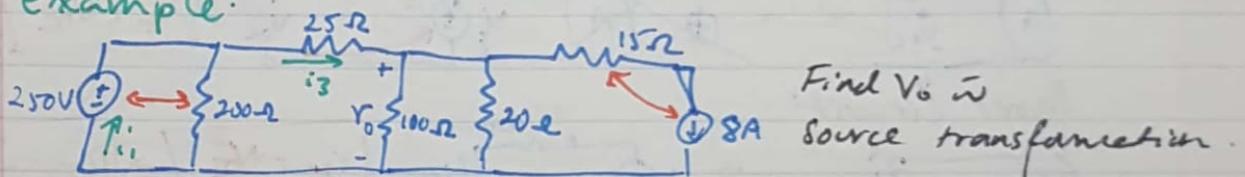
* has dif
current, but rest of circuit has no dif.

Resistor in Series with Current Source:

No effect

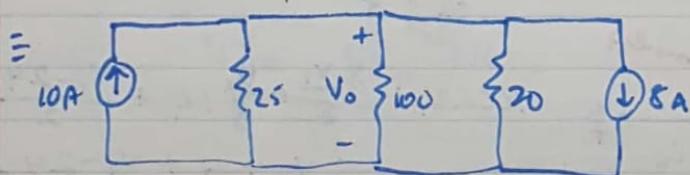


Example:



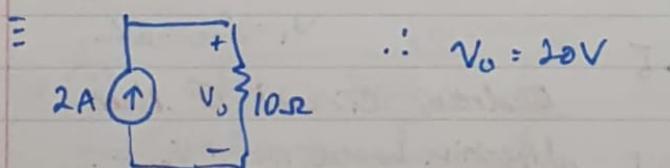
Now, source transformation.

$$i_1 \neq i_2 !!!!$$



$$i_3 = \frac{250 - 20}{25}$$

$$i_1 = i_3 + \frac{250}{200}$$

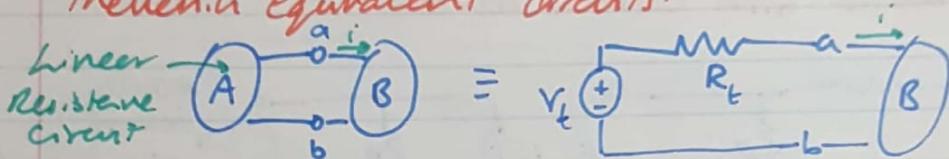


$$\therefore V_o = 20V$$

Source Transformation Can't always be used:

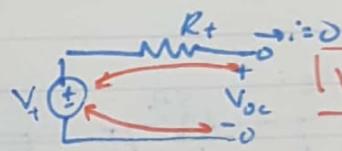
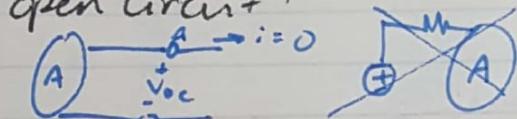
→ When there's no V_{source} in series w/ R or C_{some} in parallel w/ R.

Thevenin Equivalent circuit:



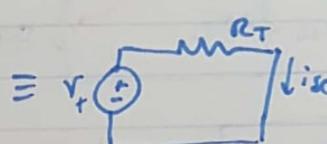
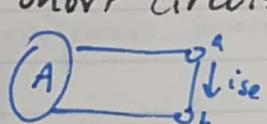
Given A, find V_T and R_T

open circuit +:



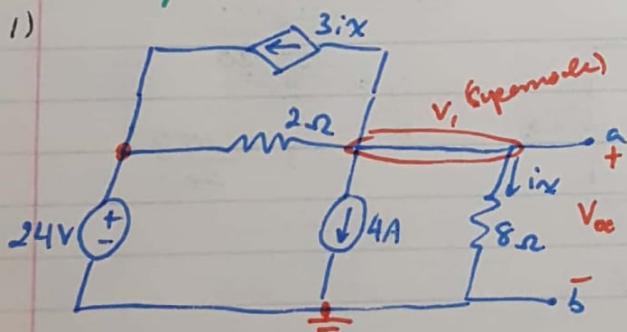
$$V_T = V_{oc}$$

Short circuit:



$$i_{sc} = \frac{V_1}{R_T} \Rightarrow R_T = \frac{V_{oc}}{i_{sc}}$$

Example:



$$i_X = \frac{V_1}{8}$$

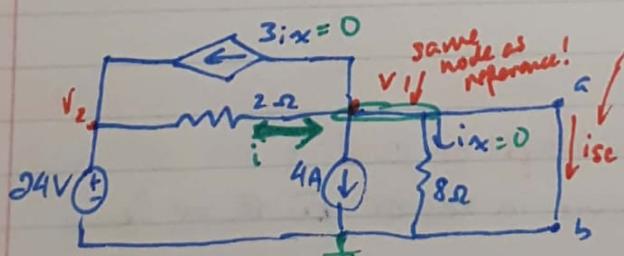
$$\text{KCL } V_1: \frac{3V_1}{8} + \frac{V_1}{8} + 4 + \frac{V_1 - 24}{2} = 0$$

$$\frac{1}{2}V_1 + 4 + \frac{V_1 - 24}{2} = 0$$

$$V_1 = V_{oc} = 8V$$

Redraw circuit in short.

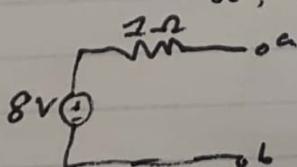
direction based on + V_{oc} -.



$$i_{sc} = \frac{V_2 - V_1}{2} \quad \text{But } V_1 = 0 \quad \text{(short).}$$

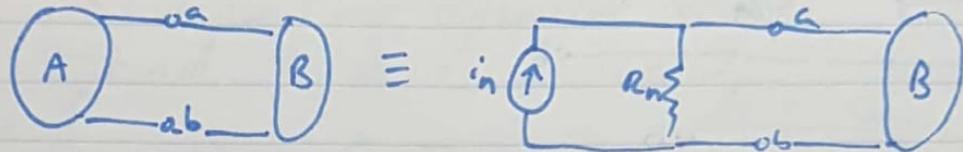
$$\text{KCL } 0: i_{sc} = i - 4 - 0 - 0 \quad i_{sc} = 8A$$

$$\text{Now, } R_T = 1\Omega$$

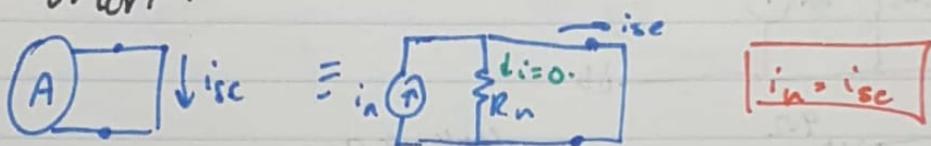


Norton Equivalent Circuit:

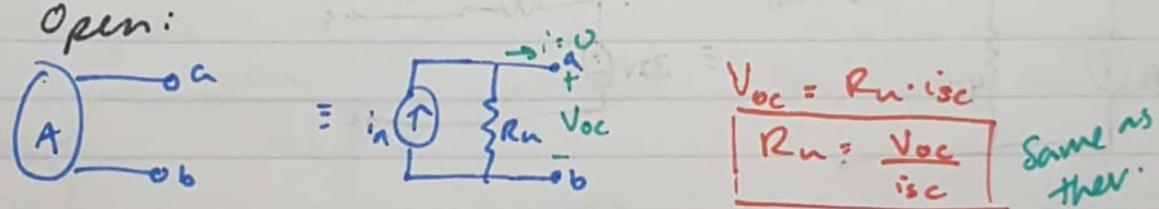
Feb 2, 2018.



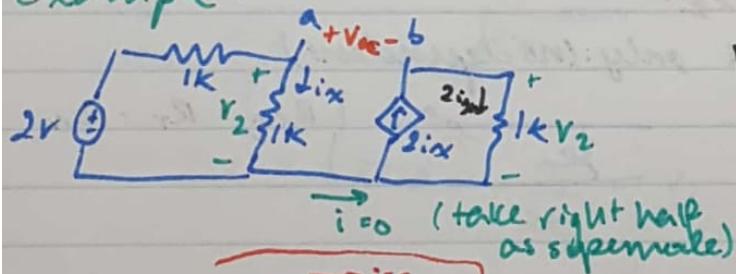
Short:



Open:



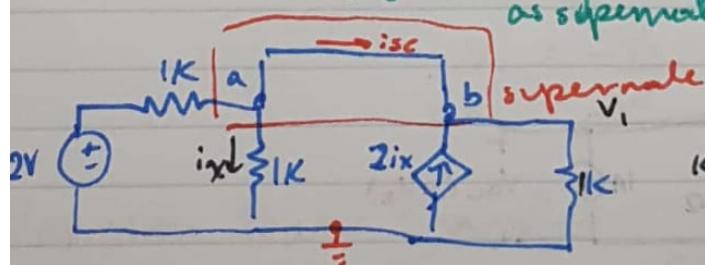
Example:



$$V_1 = \frac{(2)(1)}{2} = 1V \quad (\text{V'division})$$

$$i_x = \frac{1V}{1k} = 1mA \quad \therefore V_{oc} = V_1 - V_2$$

$$V_2 = (1k)(2i_x) = 2V = -1V$$

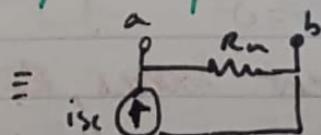


$$i_{sc} = \frac{V_1}{1} = V_1$$

$$\text{KCL at } V_1: \frac{V_1 - 2}{1} + \frac{V_1}{1} - 2\frac{V_1}{1} + \frac{V_1}{1} = 0$$

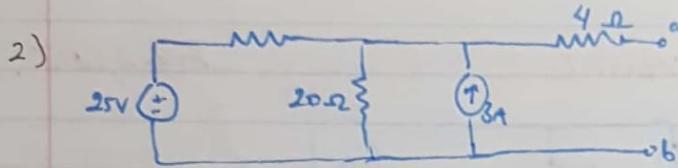
$$V_1 = 2V$$

$$\text{KCL: } i_{sc} = \frac{2 - V_1}{1} - \frac{V_1}{1} = -2mA \Rightarrow R_n = \frac{-1}{-2mA} = 0.5k\Omega$$

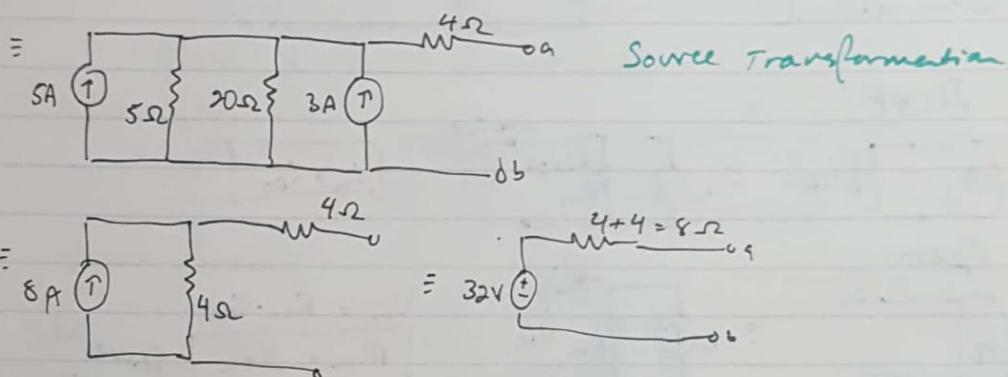


Modterm:

↳ up to some transformation

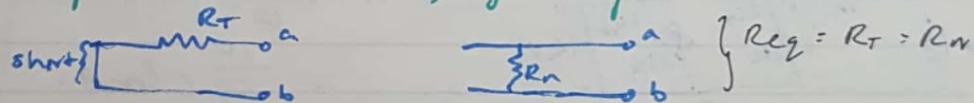


Feb 4, 2018

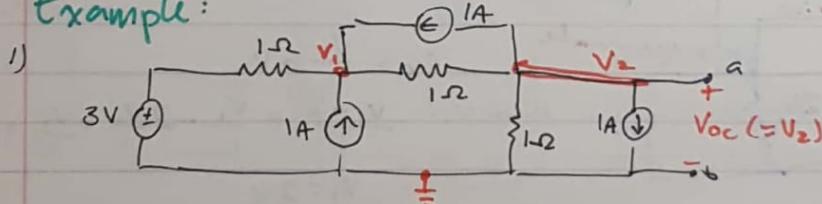


Finding R_T or R_N with Req :

→ Independent sources only. (no dependent).



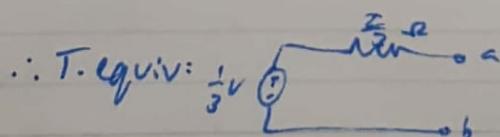
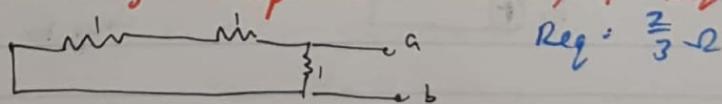
Example:



$$KCL 1: -1 - 1 + \frac{V_1 - 3}{1} + \frac{V_1 - V_2}{1} = 0 \quad \left\{ V_{oc} = V_2 = \frac{1}{3}V \right.$$

$$KCL 2: 1 + 1 + V_2 + \frac{V_2 - V_1}{1} = 0$$

Since only independent sources, $R_T = Req$. Deactivate sources.

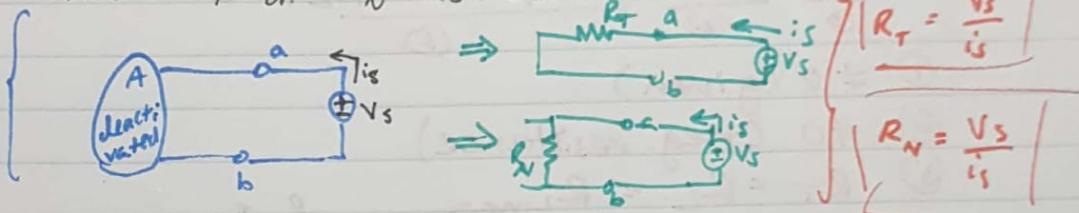


Finding R_T or R_N with External Sources:

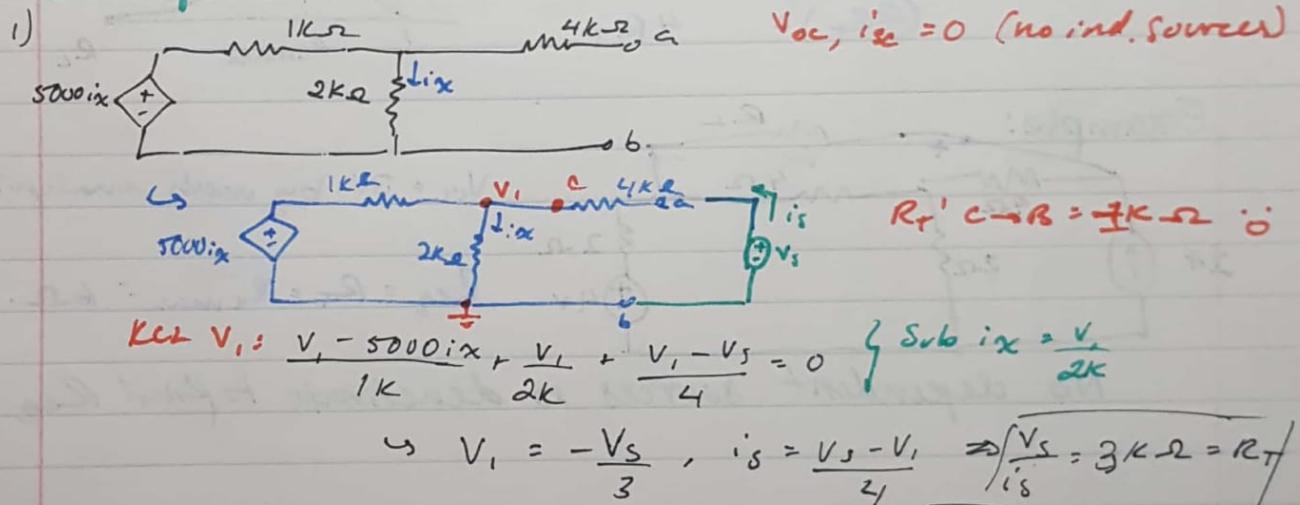
→ Independent/dependent source.

→ Find V_T or i_N as usual.

Can also do $\oplus i_s$, then find V_S

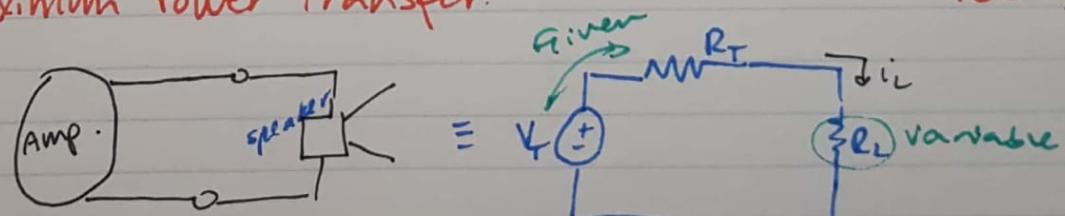


Example:



Maximum Power Transfer:

Feb 6, 2018



Given A , find R_L for max power

$$i_L = \frac{V_T}{R_T + R_L}$$

$$P_L = R_L \left(\frac{V_T}{R_T + R_L} \right)^2$$

& R_L variable, derive wrt R_L .

$$\frac{dP_L}{dR_L} = \frac{V_T^2(R_T + R_L)^2 - R_L V_T^2 2(R_T + R_L)}{(R_T + R_L)^4} = 0$$

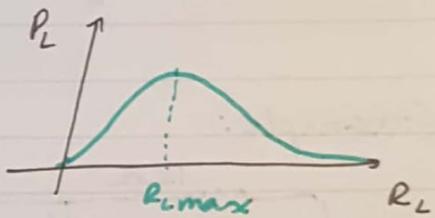
$$\Rightarrow \frac{V_T^2(R_T + R_L)}{①} \left[\frac{(R_T + R_L) - 2R_L}{②} \right] = 0 \quad ③$$

① $\neq 0$ (given)

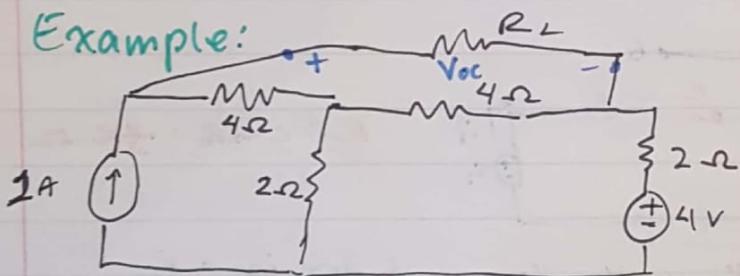
② $\neq 0$ (neg. resistance)

③ $R_T = R_L = R_{L\max}$

$$\text{So, } P_{L\max} = \frac{R_T V_T^2}{(2R_T)^2} = \frac{V_T^2}{4R_T}$$



Example:



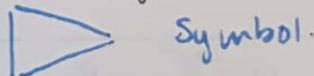
$V_{oc} = 3V$ by mesh analysis.

$R_{eq} = R_T = R_{L\max} = 6\Omega$.

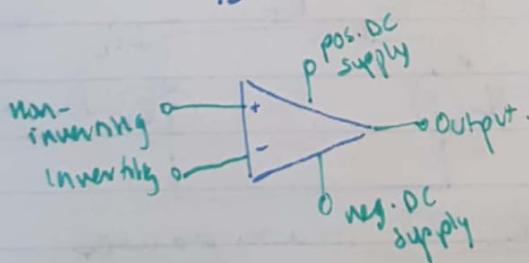
No dependent sources, so deactivate to find R_{eq} .

Operational Amplifier:

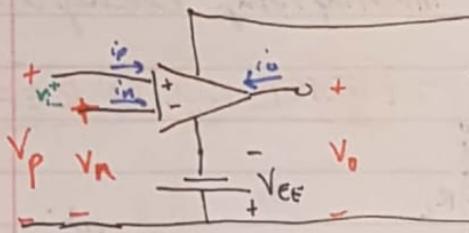
- Amplification, Integration, Addition/Subtraction, Differentiation, non-linear.



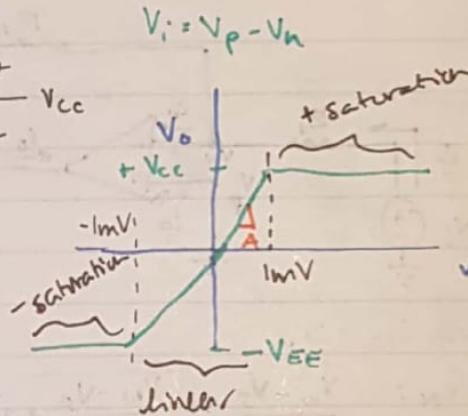
Symbol.



Example:



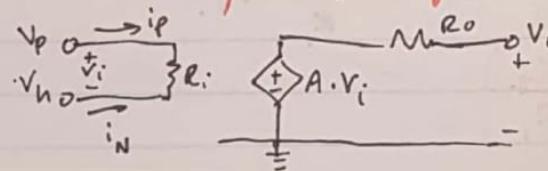
$$V_i \approx 0, V_p \approx V_N.$$



(Assume
 $V_{CC} = V_{EE} = 10V$)

$A = \text{Slope (GmPf)}$,
Open-circuit
voltage gain.
If $A = 10^4$

Linear Model for Op-Amps:

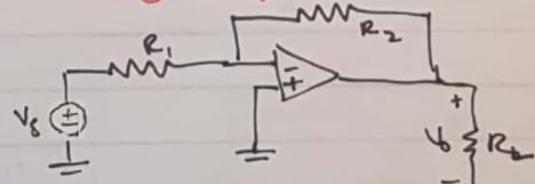


$R_i = \text{inp resistance}$

$$= 10^5 - 10^{12} \Omega \quad A = 10^4 - 10^8$$

$R_o = \text{out resistance} \quad R_i, A \gg R_o$
 $= 1 - 150 \Omega$

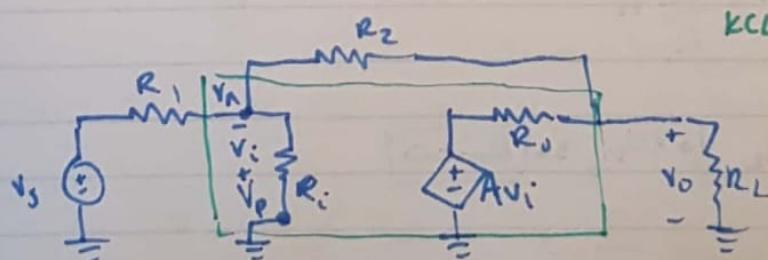
Inverting Amplifier:



$$\text{KCL } V_N: \frac{V_N - V_S}{R_1} + \frac{V_N - V_O}{R_2} = 0$$

$$\text{KCL } V_O: \frac{V_O - A V_I}{R_o} + \frac{V_O - V_N}{R_2} + \frac{V_O}{R_L} = 0$$

$$\text{where } V_I = V_p - V_N = -V_N$$



If $R_i = 1k\Omega$, $R_2 = 5$, $R_L = 1$, $R_o = 10^8 \Omega$, $R_1 = 50\Omega$, $A = 10^5$, then:

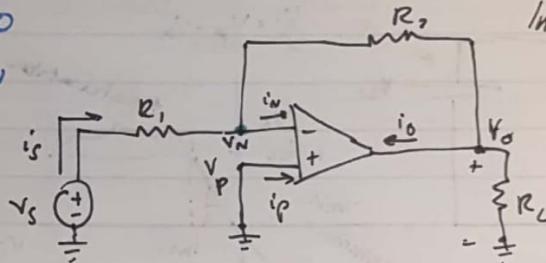
Complicated to solve: $V_o \approx -5V_s$

$$\text{Voltage Gain } A_v \approx -5. = \frac{V_o}{V_s}$$

Ideal Model:

$$i_p = i_N = 0$$
$$V_P = V_N$$

Start KCL
at inputs.



$$V_P = 0 \Rightarrow V_N = 0.$$

$$\text{KCL } V_N: \frac{V_N - V_s}{R_1} + \frac{V_N - V_o}{R_2} + i_N = 0$$

$$\frac{-V_s}{R_1} + \frac{-V_o}{R_2} = 0 \Rightarrow V_o = \frac{-R_2}{R_1} V_s.$$

$$(V_{\text{gain}} = \frac{V_o}{V_s} = -\frac{R_2}{R_1})$$

Inverting Amp example.

| NEVER KCL @ REF! |

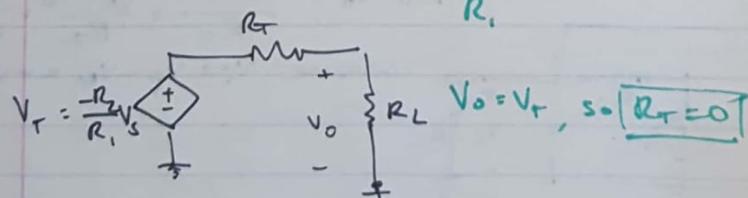
some answer
as linear model
independent
of R_L

Input Resistance:

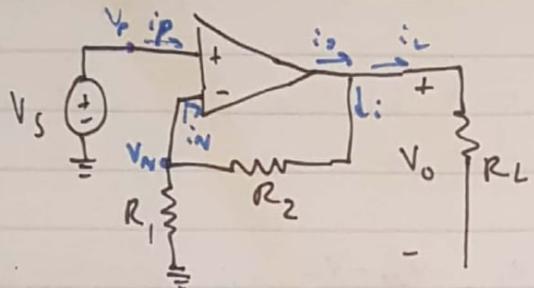
$$R_{\text{in}} = \frac{V_s}{i_s}, i_s = \frac{V_s - V_N}{R_1} = \frac{V_s}{R_1}. \quad | \because R_{\text{in}} = R_1 |$$

Output Resistance:

$$R_{\text{out}} = R_T \quad V_{\text{oc}} = -\frac{R_2}{R_1} V_s$$



Non-Inverting Amplifier:



$$V_p = V_s = V_N$$

$$KCL \text{ at } V_N: \frac{V_N}{R_1} + \frac{V_N - V_o}{R_2} + i_N = 0$$

$$\frac{V_s}{R_1} + \frac{V_s - V_o}{R_2} = 0$$

$$R_2 V_s = R_1 V_o - R_1 V_s$$

$$V_o = \left(\frac{R_2 + R_1}{R_1} \right) V_s$$

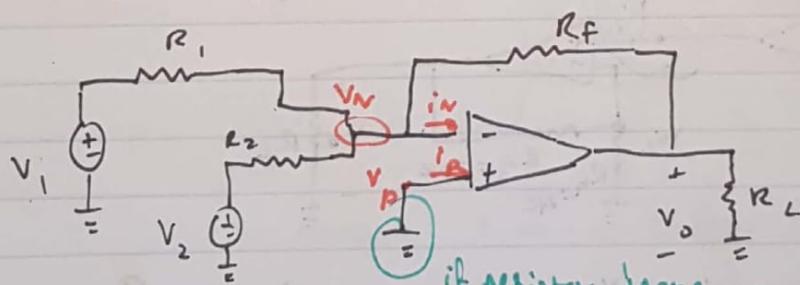
$$R_{in} = \frac{V_s}{i_s} = \frac{V_s}{i_p} \quad | \infty \quad | R_{out} = 0$$

$$\rightarrow P_{sup} = 0, \text{ so } P_L = \frac{V_o^2}{R_L} \quad \text{Gained power: } \frac{P_L}{P_s} = \infty$$

$$\rightarrow i_o = i + i_L = \frac{V_o - V_s}{R_2} + \frac{V_o}{R_L}$$

Summing Amp:

March 3, 2018



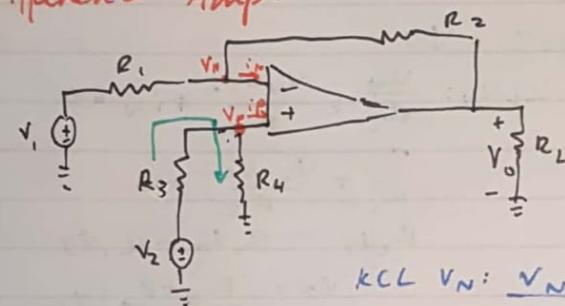
$$V_p = V_N = 0 \text{ (Collected).}$$

if no resistor here, no diff: $i_p = 0$.

$$KCL \text{ at } V_N: \frac{V_N - V_1}{R_1} + \frac{V_N - V_2}{R_2} + \frac{V_N - V_o}{R_f} + i_N = 0$$

$$V_o = - \left(\frac{R_f}{R_1} V_1 + \frac{R_f}{R_2} V_2 \right) \quad \left\{ \begin{array}{l} \text{hence the} \\ \text{name.} \end{array} \right.$$

Difference Amp:



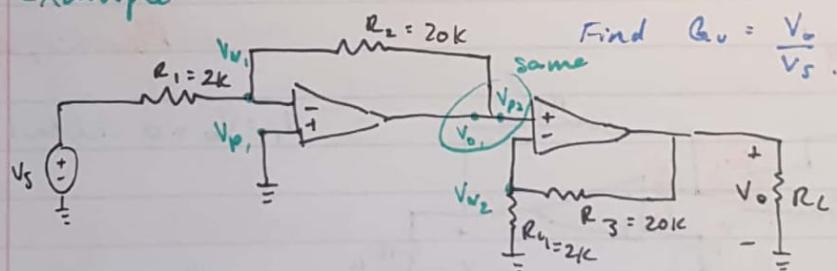
ideal as well ($i_p = i_n = 0, V_p = V_N$)

$$KCL \text{ at } V_N: \frac{V_N - V_1}{R_1} + \frac{V_N - V_O}{R_2} + i_N = 0$$

$$V_O = \left(\frac{R_2}{R_1} + 1 \right) V_N - \frac{R_2}{R_1} V_1 \quad \text{Since } i_p = 0, R_3, R_4 \text{ in "series"} \\ V_p = \frac{R_4}{R_3 + R_4} \cdot V_2 = V_N$$

$$= \frac{R_2}{R_1} \left[\left(1 + \frac{R_1}{R_2} \right) V_2 - V_1 \right] \quad \left\{ \begin{array}{l} \text{If } \frac{R_1}{R_2} = \frac{R_3}{R_4} : V_O = \frac{R_2}{R_1} (V_2 - V_1) \\ \end{array} \right.$$

Example:



$$\text{Find } G_V = \frac{V_O}{V_S}$$

$$KCL \text{ at } V_{N1}: \frac{V_{N1} - V_S}{R_1} + \frac{V_{N1} - V_{O1}}{R_2} + i_{N1} = 0 \Rightarrow V_{O1} = - \frac{R_2}{R_1} V_S = V_{P2} \cdot V_{N2}$$

$$KCL \text{ at } V_{N2}: \frac{V_{N2}}{R_4} + \frac{V_{N2} - V_O}{R_3} + i_{N2} = 0 \Rightarrow V_O = \left(\frac{R_3}{R_4} + 1 \right) V_{N2}$$

$$G_V = \frac{V_O}{V_S} = \left(\frac{R_3}{R_4} + 1 \right) \left(- \frac{R_2}{R_1} V_S \right)$$

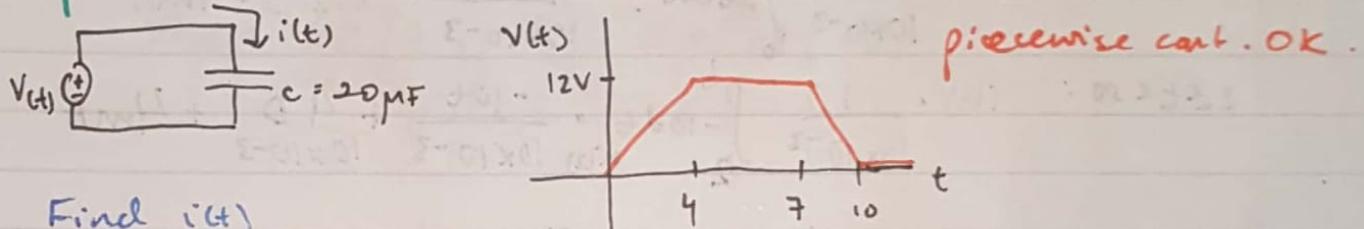
Capacitors:

Mar 5, 2018

$$q(t) = C V(t) \Rightarrow i(t) = \frac{C dV(t)}{dt} \Rightarrow V(t) = \int_{t_0}^t \frac{i(t_s) dt}{C} + V(t_0)$$

- 1) If $V(t)$ constant, $i=0$. (open circuit)
- 2) $\frac{dV(t)}{dt}$ must be defined (continuous V fun)

Example:



Find $i(t)$

$$0 \leq t \leq 4: i(t) = 20 \cdot 3 = 60 \mu\text{A}$$

$$4 < t \leq 7: i(t) = 0$$

$$10 \geq t > 7: i(t) = -80 \mu\text{A}$$

$$t > 10: i(t) = 0$$

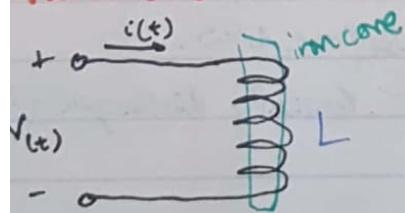
Power: $V(t) \cdot i(t) = \boxed{C \cdot V(t) \frac{dV(t)}{dt}}$

Energy: $\frac{dw}{dt} = p(t) \Rightarrow \boxed{w = \frac{1}{2} C [V^2(t_2) - V^2(t_1)]} = \frac{1}{2} C \cdot V^2(t)$

Assume $t_1 \rightarrow -\infty \Rightarrow V(t_1) = 0 \Rightarrow t_2 = t$

Inductors:

Mar 6, 2018



Ideal Model:

$$V(t) = L \frac{di(t)}{dt} \quad L \text{ in } \frac{\text{V} \cdot \text{s}}{\text{A}} \text{ (Henry's)}$$

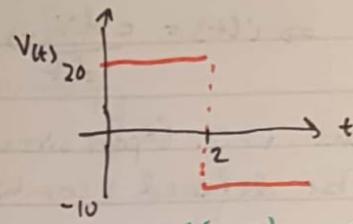
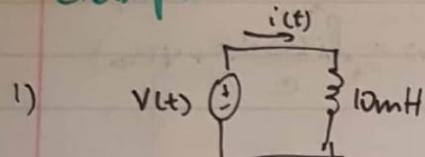
$$i(t) = \frac{1}{L} \int_{t_0}^t V(t) dt + i(t_0)$$

- 1) If $i(t)$ constant, $V=0$ (short circuit)

- 2) $\frac{di(t)}{dt}$ must be defined (continuous i fun)

$$W(t) = \frac{1}{2} L i(t)^2 \quad P(t) = L \cdot i(t) \frac{di(t)}{dt}$$

Example:

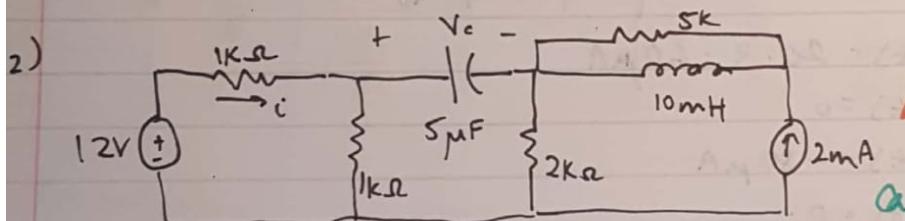


Find $i(t)$, $\omega(t)$
where $i(0^-) = 0$

$i(t)$ must be continuous, so $i(x^-) = i(x^+) = i(x)$

$$0 \leq t < 2: i(t) = \frac{1}{10 \times 10^{-3}} \int_0^t 20 dt + 0 = \frac{20t}{10 \times 10^{-3}} \quad i(2^-) = 4 \text{ mA}$$

$$2 \leq t < \infty: i(t) = \frac{1}{10 \times 10^{-3}} \int_2^t -10 dt + i(2^-) = \frac{-10t}{10 \times 10^{-3}} + \frac{i(2^-)}{10 \times 10^{-3}} + 4 \text{ mA}$$



Find i , $V_C(t)$, $\omega(t)$, $\dot{\omega}(t)$
left for a long time.

$\text{Cap} \Rightarrow \text{open}$. $\text{Ind} \Rightarrow \text{short}$.

Inductor Relations:

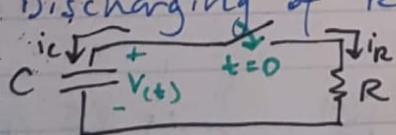
$$\begin{aligned} L_{\text{series}} &= L_1 + L_2 + L_3 \\ L_{\text{parallel}} &= \frac{1}{\frac{1}{L_1} + \frac{1}{L_2} + \frac{1}{L_3}} \end{aligned}$$

} Conductors switched.

Mar 7, 2018

Transient Analysis:

Discharging of RC circuit:



C charged to V_i before $t=0$.

RC = time const = T . Basically discharged after $5T$

↳ Rule of thumb

$$V(0^-) = V_i = V(0)$$

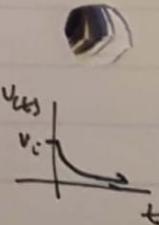
For $t \geq 0$:

$$i_C + i_R = 0 \rightarrow R \frac{dV}{dt} + V_{C(t)} = 0 \rightarrow V_{C(t)} = K e^{-st}$$

$$C \frac{dV_{C(t)}}{dt} + \frac{V_{C(t)}}{R} = 0 \quad \text{Dif. eqn.}$$

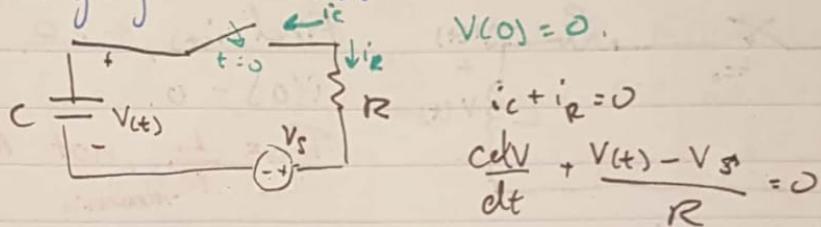
$$RCKse^{-st} + K e^{-st} = 0$$

$$s = -\frac{1}{RC}, K = V_i \quad \therefore V_{C(t)} = V_i e^{-\frac{1}{RC}t}$$



Charging Re Circuit:

Mar 9, 2018



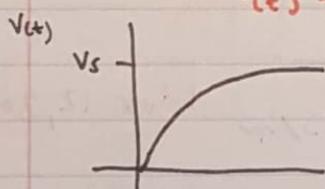
$$RC \frac{dV}{dt} + V_c(t) = V_s \Rightarrow \text{Assume } V_c(t) = K_1 e^{st} + K_2$$

$$\text{Then } RC [K_1 s e^{st}] + K_1 e^{st} + K_2 = V_s.$$

$$(RCs + 1)(K_1 e^{st}) + K_2 = 0 + V_s$$

$$s = -\frac{1}{RC} \quad \text{and} \quad K_2 = V_s$$

$$V_c(t) = K_1 e^{-t/RC} + V_s \Rightarrow = \underbrace{-V_s e^{-t/RC}}_{\text{transient}} + \underbrace{V_s}_{\text{steady-state}}$$

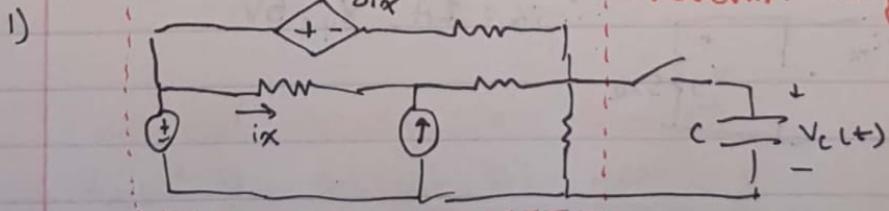


$V_c(5T) \approx V_s$ } Shortcut: C behaves as O.C., so
 $i_R = 0 \Rightarrow V_R = 0 \Rightarrow V_{c5T} = V_s$ steady state

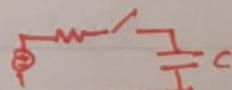
General Formula:

$$V_c(t) = \underbrace{V_c(\infty)}_{\text{Steady state}} + \left[\underbrace{V_c(t_0)}_{\text{Given/Find}} - V_c(\infty) \right] e^{-(t-t_0)/\tau}$$

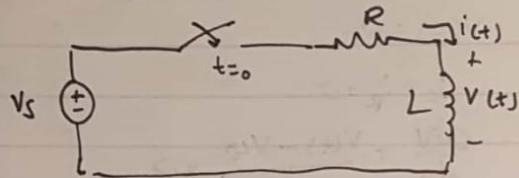
Example:



Thevenin to get



RL circuit:



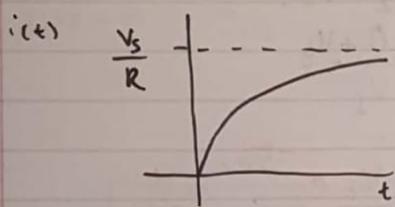
Find $i_{(t)}, t > 0$.

$$i(0) = 0.$$

$$\tau = \frac{L}{R}, \text{ not } RC \text{ here.}$$

$$R \cdot i_{(t)} + L \frac{di}{dt} = V_s$$

$$\frac{L}{R} \frac{di}{dt} + i_{(t)} = \frac{V_s}{R} \quad \left\{ \begin{array}{l} i_{(t)} = -\frac{V_s}{R} e^{-t/\tau} + \frac{V_s}{R} \\ V_{(t)} = L \frac{di_{(t)}}{dt} \end{array} \right.$$

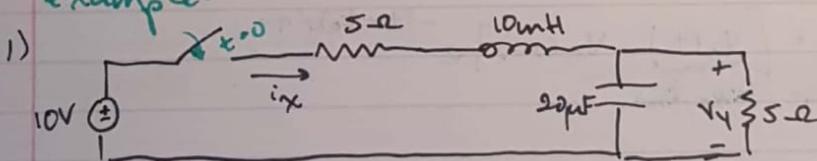


$$\begin{aligned} V_{(t)} &= L \frac{di_{(t)}}{dt} \\ &= L \left[0 - \frac{V_s}{R} \left(-\frac{1}{\tau} \right) e^{-t/\tau} \right] \\ &= V_s e^{-t/\tau} \end{aligned}$$

Generalization:

$$i_r(t) = i_r(\infty) + [i_r(t_0) - i_r(\infty)] e^{-(t-t_0)/\tau} \quad \text{Mar 12, 2018}$$

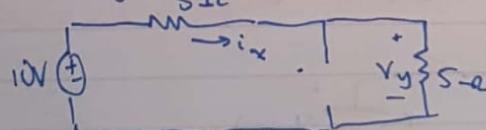
Example:



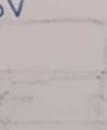
$t \gg 0$, find i_x, V_y .

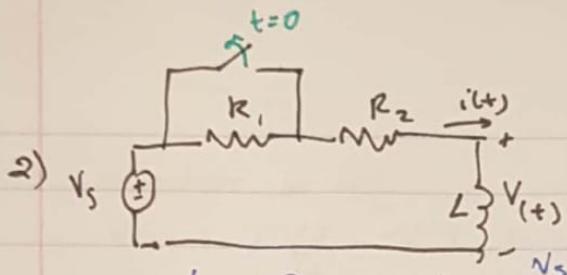
$\rightarrow \gg 0 \Rightarrow$ steady state
 $> 0 \Rightarrow$ transient

Steady state:

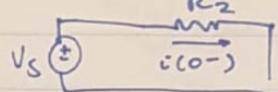


$$\therefore i_x = 1A, V_y = 5V$$





$$t_0 = 0, \quad i_L(0) = \frac{V_s}{R_1 + R_2}, \text{ since S.S. at } t=0^-.$$



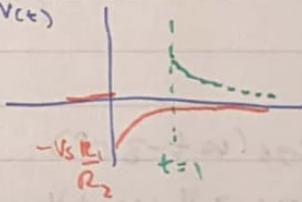
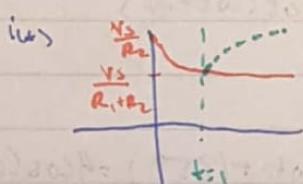
Switch closed for long time. opened at $t=0$. Find $i_{(t)}$, $V_{(t)}$ for $t \geq 0$.

$$\tau = \frac{L}{R_T} = \frac{L}{R_1 + R_2}$$

$$i_L(\infty) = \frac{V_s}{R_1 + R_2} \quad (\text{S.S. with switch open})$$

$$\therefore i_L(t) = \frac{V_s}{R_1 + R_2} + \left[\frac{V_s}{R_2} - \frac{V_s}{R_1 + R_2} \right] e^{-(t-0)/\tau} \quad \textcircled{1}$$

$$V(t) = L \frac{di(t)}{dt} = L \left[-\frac{1}{\tau} \left(\frac{V_s}{R_2} - \frac{V_s}{R_1 + R_2} \right) e^{-t/\tau} \right]$$



If switch closed at $t=1$, graph is same until $t=1$.

\rightarrow Then $t_0 = 1$, and use eqn. find $i(1^-)$ with $\textcircled{1}$.

$$\rightarrow \tau \text{ becomes } \frac{L}{R_2}$$

Complex Numbers:

$$j = \sqrt{-1} \quad z = x + jy = r e^{j\theta} = r \angle \theta = r(\cos \theta + j \sin \theta)$$

$$r = \sqrt{x^2 + y^2} \quad \theta = \tan^{-1}\left(\frac{y}{x}\right)$$

Mar 14, 2018

Sinusoidal Steady-State Analysis:

$$V(t) = V_m \cos(\omega t + \phi) \quad -\infty < t < \infty$$

\hookrightarrow max value/magnitude. \rightarrow Any freq. rad/s.

$$\text{Period } T = \frac{2\pi}{\omega} \text{ (rad/s)}$$

Some identities:

$$\sin \theta = \cos(\theta - \frac{\pi}{2})$$

$$-\sin \theta = \cos(\theta + \frac{\pi}{2})$$

$$-\cos \theta = \cos(\theta + \frac{\pi}{2})$$

Example:

$$1) V(t) = 3 \sin(20t + 30^\circ) \quad 3 = V_m, \omega = 20, \theta = -60^\circ \\ = 3 \cos(20t - 60^\circ)$$

Phasors:

$\tilde{V} = V_m e^{j\theta}$ is the phasor for $V_{ct} = V_m \cos(\omega t + \theta)$

Example:

$$1) V_1(t) = 3 \cos(\omega t - 30^\circ) \quad V_2(t) = 4 \sin(\omega t + 135^\circ) = 4 \cos(\omega t + 45^\circ)$$

$$\begin{aligned} & V_1(t) \rightarrow V_1(t) + V_2(t) \\ & \tilde{V}_1 = 3e^{-j30^\circ} \quad \tilde{V}_2 = 4e^{j45^\circ} \\ & = 3(\cos(-30) + j\sin(-30)) = 4(\cos 45 + j\sin 45) \\ & = 2.598 - 1.5j \quad = 2.828 + 2.828j \\ & \tilde{V} = \tilde{V}_1 + \tilde{V}_2 = \text{_____} \cdot \tan^{-1}(\frac{y}{x}) \text{ to get } \theta \cdot \sqrt{x^2+y^2} = r. \\ & V_{ct} = 5.586 \cos(\omega t + 13.75^\circ) \end{aligned}$$

Get in
c.N. rectangular form.

Current AC:

$$i(t) = I_m \cos(\omega t + \theta_i)$$

$$V(t) = R \cdot i(t)$$

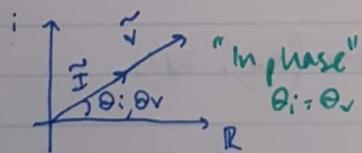
$$\tilde{I} = I_m e^{j\theta_i}$$

$$\tilde{V} = V_m e^{j\theta_v} = R \tilde{I}$$

Mar 19, 2018

$$V_m = R I_m$$

$$\theta_v = \theta_i$$



Inductors in AC:

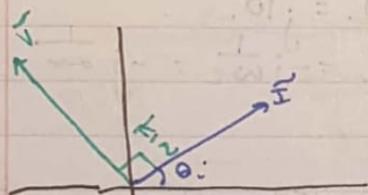
$$V(t) = L \frac{di}{dt} = -L I_m \omega \sin(\omega t + \theta_i)$$

$$= \underbrace{\omega L I_m}_{\text{peak voltage}} \cos(\omega t + \theta_i + \frac{\pi}{2})$$

$$\tilde{V} = \omega L I_m e^{j(\theta_i + \frac{\pi}{2})} = j\omega L \tilde{I} \quad (\text{e}^{j\frac{\pi}{2}} \cdot j)$$

$$\tilde{V} = z_L \tilde{I}$$

Inductor impedance $z_L = j\omega L$



\tilde{V} "leads" by $\frac{\pi}{2}$.
 \tilde{I} "lags" by $\frac{\pi}{2}$

Capacitors in AC:

$$i(t) = \frac{dv}{dt} \quad \tilde{I} = j\omega c \tilde{V} \Rightarrow \tilde{V} = \frac{1}{j\omega c} \tilde{I} = -j \frac{1}{\omega c}$$

capacitor impedance $= -j \frac{1}{\omega c} = z_c$

$$V_m = \frac{1}{\omega c} I_m$$

$$\theta_v = \theta_i - \frac{\pi}{2}$$

General Impedance:

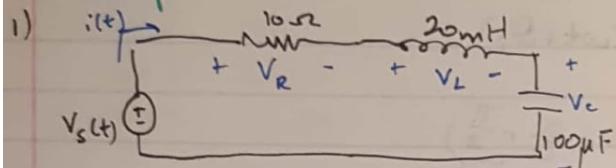
$$z = \underline{\frac{R}{\text{resistance}}} + j \underline{\text{reactance}} \quad Y = \frac{1}{z} = \underline{\frac{G}{\text{conductance}}} + j \underline{\text{B}} \text{ susceptibility}$$

$$\rightarrow \text{KCL: } \sum \tilde{I}_n = 0. \quad \text{KVL: } \sum \tilde{V}_n = 0$$

$$\rightarrow \text{Series: } z_1 + z_2 = z_{eq}$$

$$\leftrightarrow \text{Parallel: } z_1 \parallel z_2 = z_{eq} = \frac{1}{\frac{1}{z_1} + \frac{1}{z_2}}$$

Example:

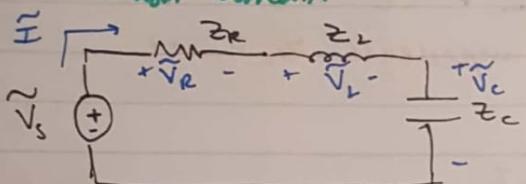


Mar 20, 2018

$$V_s(t) = 20 \cos(500t + 15^\circ)$$

Find $i(t)$, $V_R(t)$, $V_L(t)$, $V_C(t)$

Phasor Domain:



$$\tilde{V}_s = 20 e^{j15^\circ}$$
$$Z_R = R = 10 \Omega$$
$$Z_L = j\omega L = j10$$
$$Z_C = \frac{1}{j\omega C} = -j\frac{1}{\omega C} = -j20$$

$$\text{KVL: } \tilde{V}_R + \tilde{V}_L + \tilde{V}_C = \tilde{V}_s$$
$$\tilde{I}(Z_R + Z_L + Z_C) = \tilde{V}_s$$
$$\tilde{I} = \frac{20 \angle 15^\circ}{10 + j10 - j20} = \frac{20 e^{j15^\circ}}{\sqrt{10^2 + 10^2} \tan^{-1}(-\frac{10}{10})} = \frac{20 e^{j15^\circ}}{10\sqrt{2} e^{j-45^\circ}} = \sqrt{2} e^{j60^\circ}$$
$$\therefore I(t) = \sqrt{2} \cos(500t + 60^\circ)$$

$$\therefore V_R(t) = R \cdot i(t) = 10\sqrt{2} \cos(500t + 60^\circ)$$
$$\tilde{V}_L = (j\omega L) \tilde{I} = (10j)(\sqrt{2} e^{j60^\circ})$$
$$= (10e^{j90^\circ})(\sqrt{2} e^{j60^\circ}) = 10\sqrt{2} e^{j150^\circ}$$
$$\therefore V_L(t) = 10\sqrt{2} \cos(500t + 150^\circ)$$
$$\tilde{V}_C = Z_C \tilde{I} = (20e^{j-90^\circ})(\sqrt{2} e^{j60^\circ})$$
$$V_C(t) = 20\sqrt{2} \cos(500t - 30^\circ)$$

If $C = 200 \mu\text{F}$:

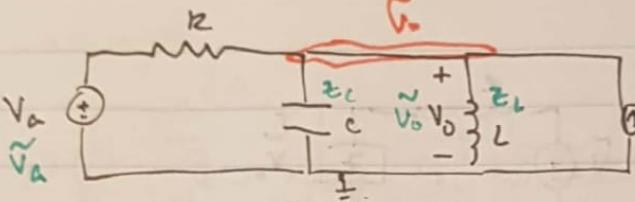
$$Z_C = -j10, \text{ then } Z_{eq} = 10$$
$$\rightarrow \tilde{I} = 2\sqrt{15}^\circ \text{ and } \tilde{V}_L + \tilde{V}_R = 0$$

When is $Z_L + Z_C = 0$?

$$Z_C = -Z_L$$

$$\omega^2 = \frac{1}{LC}$$

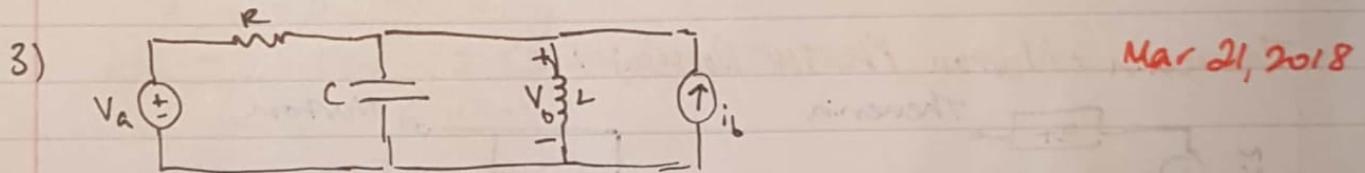
$$\omega = \frac{1}{\sqrt{LC}}$$

2) 

$V_a = 2 \cos(1000t + 30^\circ)$ Find V_o .
 $i_b = \cos(1000t - 45^\circ)$
 $R = 4\Omega$ $C = 450\mu F$ $L = 2mH$

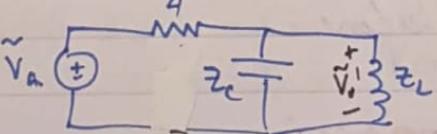
$\tilde{V}_a = 2e^{j30^\circ}$ $\tilde{I}_b = e^{-45j}$ $z_c = -j\frac{1}{\omega C} = -j4$ $z_L = j\omega L = j2$

KVL: $\frac{\tilde{V}_o - \tilde{V}_a}{R} + \frac{\tilde{V}_o}{j4} + \frac{\tilde{V}_o}{j2} - \tilde{I}_b = 0$ Solve for $V_o = 3.5 \cos(1000t + 23^\circ)$



Same example, but $V_a = 2 \cos(1000t + 30^\circ)$, $i_b = \cos(2000t - 45^\circ)$
 Different freq. Use superposition.

$V_o'(t)$ due to V_a :

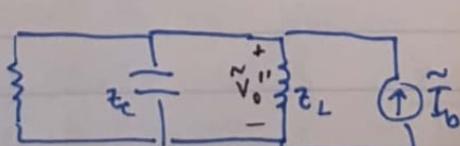


$\tilde{V}_a = 2 \angle 30^\circ$
 $z_c = -j\frac{1}{\omega C} = -j4$
 $z_L = j\omega L = j2$

$\tilde{V}_o' = \frac{\tilde{V}_a z_L}{z_c + z_L} = j4$

V division: $\tilde{V}_o' = \tilde{V}_a \left(\frac{z_c}{z_{eq} + z_c} \right) = \sqrt{2} \cos(1000t + 75^\circ)$

$V_o''(t)$ due to i_b :



$\tilde{I}_b = \frac{1}{L} \angle -45^\circ$
 $z_c = -j2$
 $z_L = j4$ changed.

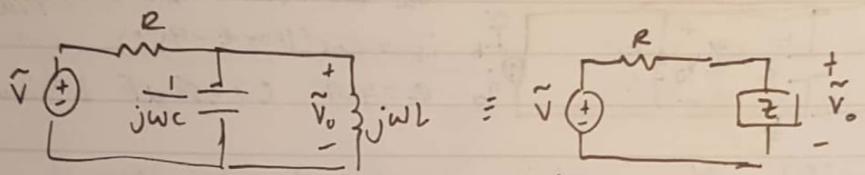
$z_{eq} = 4 // z_c // z_L$

$V_o''(t) = z_{eq} \cdot \tilde{I}_b$

$\therefore V_o''(t) = z_{eq} \tilde{I}_b =$

$\therefore V_o(t) = V_o'(t) + V_o''(t) = \sqrt{2} \cos(1000t + 75^\circ) + 2\sqrt{2} \cos(2000t - 90^\circ)$
 (can't combine).

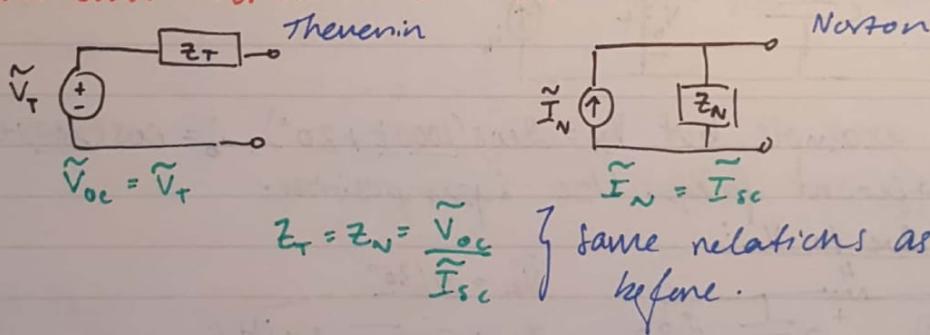
Remark:



$$Z = \frac{1}{jwC} \parallel jwL = \frac{jwC}{j(wL - \frac{1}{wC})}$$

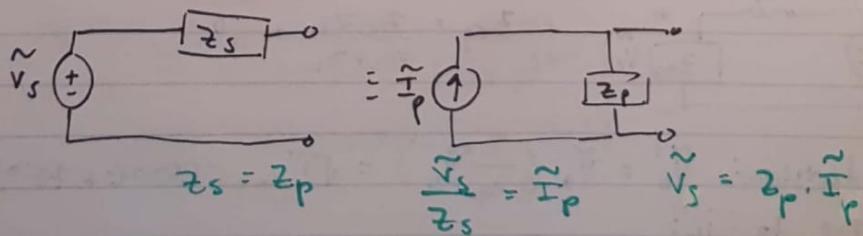
If $wL = \frac{1}{wC} \Rightarrow w = \sqrt{\frac{1}{LC}}$, $Z = \infty$ (open circuit) $\tilde{V}_o = \tilde{V}$ (parallel resonances).

Thevenin + Norton Phasor Domain:



$$Z_T = Z_N = \frac{\tilde{V}_{oc}}{\tilde{I}_{sc}} \quad \left. \begin{array}{l} \text{same relations as} \\ \text{before.} \end{array} \right\}$$

Source Transformation Phasor Domain:

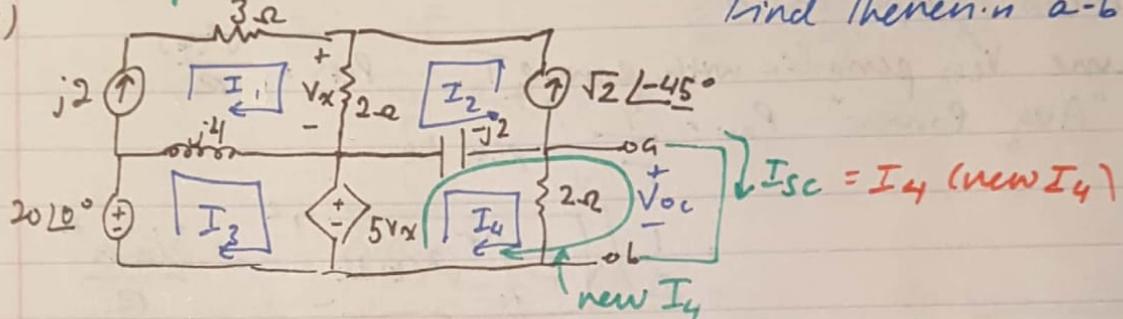


$$Z_s = Z_p \quad \frac{\tilde{V}_s}{Z_s} = \tilde{I}_p \quad \tilde{V}_s = Z_p \cdot \tilde{I}_p$$

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Example:

1) Find Theneen in a-b.



$$I_1 = j2 = 2 \angle 90^\circ$$

$$V_x = 2 \cdot (I_1 + I_2) = 2 \cdot (1+j) = 2\sqrt{2} \angle 45^\circ$$

$$I_2 = \sqrt{2} \angle -45^\circ = 1-j$$

$$\text{KVL } I_4: -5V_x - j2 \cdot (I_2 + I_4) + 2I_4 = 0$$

$$\rightarrow I_4 = 6 \angle 90^\circ$$

$$\therefore V_{oc} = 2 \cdot I_4 = 12 \angle 90^\circ$$

To find I_{sc} , get short + adjust I_4 .

I_1, I_2, V_x unchanged.

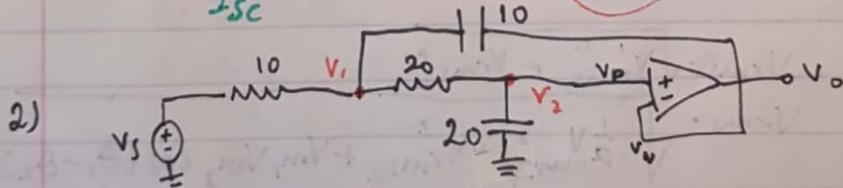
$$\text{KVL } I_4: -5V_x - j2(I_2 + I_4) = 0$$

$$\rightarrow I_4 = I_{sc} = \frac{V_x}{j2} = \frac{V_x}{\sqrt{2}} \angle 135^\circ$$

$$Z_{th} = R - j \frac{1}{\omega C}$$

$$Z_{th} = \frac{V_{oc}}{I_{sc}} = \sqrt{2} \angle -45^\circ = 1-j$$

capacitive, since $-j$.



$$V_{follower}: V_o = V_2$$

$$\text{Find } V_o \text{ given } V_s = 12 \cos(\omega t)$$

Convert to time domain.

$$\left. \begin{array}{l} C_1 \cdot 10 \mu F = -j20 \\ C_1 \cdot 2 \mu F = -j10 \end{array} \right\} \quad \left. \begin{array}{l} \frac{V_1 - V_s}{10} + \frac{V_1 - V_2}{20} + \frac{V_1 - V_o}{-j20} = 0 \quad (1) \\ \frac{V_2 - V_1}{20} + \frac{V_2 - V_o}{-j10} = 0 \quad (2) \end{array} \right\} \quad V_o = 4 \angle -90^\circ$$

AC Power:

Root mean square value:

Assume $V(t)$ periodic with period T . $P(t) = \frac{V^2(t)}{R}$

$$\text{"Avg Power"} P_{av} = \frac{1}{T} \int_0^T P(t) dt$$

$$= \frac{1}{R} \left[\underbrace{\frac{1}{T} \int_0^T V^2(t) dt}_{\text{RMS VALUE}} \right]^2 = \frac{V_{rms}^2}{R}$$

$$\therefore V_{rms} = \sqrt{\frac{1}{T} \int_0^T V^2(t) dt}$$

RMS Value for Sinusoidal:

$$T = \frac{2\pi}{\omega} \quad V(t) = V_m \cos(\omega t + \theta)$$

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$$V_{rms} = \sqrt{\frac{\omega}{2\pi} \int_0^{\frac{2\pi}{\omega}} V_m^2 \cos^2(\omega t + \theta) dt}$$

$$\boxed{V_{rms} = \frac{V_m}{\sqrt{2}}} \quad \boxed{I_{rms} = \frac{I_m}{\sqrt{2}}}$$

If $V_{ac} = V_1(t) + V_2(t)$:

$$1) \text{ If } \omega_1 \neq \omega_2 : V_{rms} = \sqrt{V_{rms_1}^2 + V_{rms_2}^2}$$

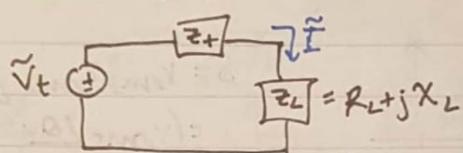
$$2) \text{ If } \omega_1 = \omega_2 : V_{rms} = \sqrt{V_{rms_1}^2 + V_{rms_2}^2 + V_{rms_1} V_{rms_2} \cos(\theta_1 - \theta_2)}$$

→ Don't use 2. Convert to one sinusoid w/ phasors.

If $V(t) = \text{constant}$?

$$V_{rms} = V_{dc} \text{ (same as function)}$$

AC Max Power:



$$P_{avg} = I_{rms}^2 \cdot |Z_L|$$

$$P_{max} = \frac{|V_t|^2}{8R_T}$$

where $|Z_L| = |Z_T|$
 $R_L = R_T$
 $X_L = -X_T$

If $Z_L = R_L$, then ...
 $Z_L = |Z_t| = \sqrt{R_t^2 + X_t^2}$
 for max power.

AC Power: Let $V = V_{rms} \cos(\omega t + \theta_v - \theta_i)$, $I = I_{rms} \cos(\omega t)$.

Instantaneous power:

$$P(t) = V_{rms} \cdot I_{rms} \cos(\theta_v - \theta_i)$$

$$= P - P_{constant} + Q \sin(2\omega t)$$

Active (Real) Power:

$$P = \frac{1}{2} V_{rms} I_{rms} \cos(\theta_v - \theta_i)$$

$$= V_{rms} I_{rms} \cos(\theta_v - \theta_i)$$

Avg Power:

$$P_{av} = P$$

Reactive Power:

$$Q = V_{rms} I_{rms} \sin(\theta_v - \theta_i)$$

Power Factor:

$$P_f = \cos(\theta_v - \theta_i)$$

$$P = V_{rms} I_{rms} P_f$$

Inductors:

$$\cos(\theta_v - \theta_i) = \cos 90^\circ = 0 \quad \left\{ \begin{array}{l} P = 0 \\ Q = +V_{rms} \cdot I_{rms} \end{array} \right.$$

$$\sin(\theta_v - \theta_i) = \sin 90^\circ = 1 \quad \left\{ \begin{array}{l} P = 0 \\ Q = +V_{rms} \cdot I_{rms} = \frac{V_{rms}^2}{wL} = I_{rms}^2 wL \end{array} \right.$$

Capacitors:

$$\cos(\theta_v - \theta_i) = \cos -90^\circ = 0 \quad \left\{ \begin{array}{l} P = 0 \\ Q = -V_{rms} \cdot I_{rms} \end{array} \right.$$

$$\sin(\theta_v - \theta_i) = \sin -90^\circ = -1 \quad \left\{ \begin{array}{l} P = 0 \\ Q = -V_{rms} \cdot I_{rms} = -\frac{I_{rms}^2}{wC} = -wC V_{rms}^2 \end{array} \right.$$

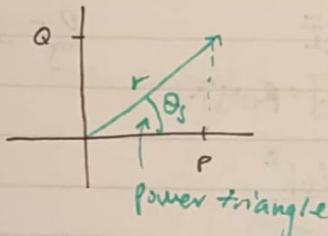
Mar 28, 2015

Complex Power:

$$S = P + jQ$$

$$\begin{aligned} S &= \sqrt{P^2 + Q^2} \angle \tan^{-1}\left(\frac{Q}{P}\right) \\ &= \sqrt{P^2 + Q^2} \angle (\theta_v - \theta_i) \\ &= V_{rms} I_{rms} \angle (\theta_v - \theta_i) \end{aligned}$$

$$V_{rms} \cdot I_{rms} = |S| = \sqrt{P^2 + Q^2} = \text{Apparent Power.}$$



$$\begin{aligned} S &= V_{rms} I_{rms} \angle (\theta_v - \theta_i) \\ &= (V_{rms} \angle \theta_v) (I_{rms} \angle -\theta_i) \\ \tilde{V} &= \tilde{V}_{rms} \quad \tilde{I} = \tilde{I}_{rms} = \frac{\tilde{S}}{\sqrt{2}} \\ | \quad | \\ \therefore S &= \tilde{V}_{rms} \cdot \tilde{I}_{rms} \\ &= \frac{1}{2} \tilde{V} \tilde{I} \end{aligned}$$

Units of Power:

Active: P — Watt (W)

Reactive: Q — Volt·Ampere Reactive (VAR)

Complex: S — Volt·Ampere (VA)

Apparent: $|S|$ — Volt·Ampere (VA)

Power for Impedance:

$$S = Z \cdot \tilde{I}_{rms} \cdot \tilde{I}_{rms} = \frac{R I_{rms}^2}{P} + j \frac{X I_{rms}^2}{Q}$$

Apr 2, 2018

Power Triangle for Impedance:

$Q > 0 \Rightarrow$ Inductor

$Q < 0 \Rightarrow$ Capacitor

$Q = 0 \Rightarrow$ Resistor

Power Factor:

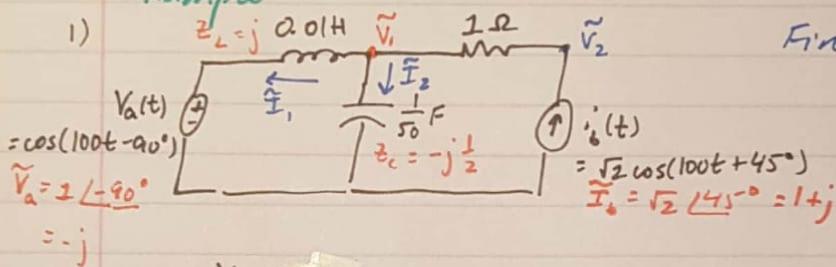
1) Pf lagging —

→ \tilde{I} lags \tilde{V} (inductor) and $Q > 0$

2) Pf leading —

→ \tilde{I} leads \tilde{V} (capacitor) and $Q < 0$

Example:



Find P, Q for every element.

$$\frac{V_1 + j}{j} + \frac{V_1}{-j\frac{1}{2}} = \sqrt{2} \angle 45^\circ = 1+j \Rightarrow \boxed{V_1 = 1 \angle 0^\circ}$$

$$\tilde{V}_2 = 2+j \quad \text{and} \quad \tilde{I}_1 = \sqrt{2} \angle -45^\circ = 1+j \quad \text{and} \quad \tilde{I}_2 = 2j$$

Power for \tilde{V}_a :

$$P = \left(\frac{1}{\sqrt{2}}\right) \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \cos(-90^\circ + 45^\circ) = \frac{1}{2} W$$

$$Q = \left(\frac{1}{\sqrt{2}}\right) \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \sin(-90^\circ + 45^\circ) = -\frac{1}{2} \text{ VAR}$$

Power for \tilde{I}_b :

$$(need -\tilde{I}_b) = -1-j \quad P = \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \cos(26.57 - (-135)) = -\frac{3}{2} W$$

$$= \sqrt{2} \angle 45 - 180^\circ \quad Q = \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \sin(26.57 - (-135)) = \frac{1}{2} \text{ VAR}$$

Power for L:

$$P = 0 W$$

$$V_L = \sqrt{2} \angle 45^\circ \quad Q = \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \sin(45 - (-45)) = 1 \text{ VAR} = \omega L I_{rms}^2$$

Power for C:

$$P = 0 W$$

$$Q = \left(\frac{1}{\sqrt{2}}\right) \left(\frac{\sqrt{2}}{\sqrt{2}}\right) \sin(0 - 90^\circ) = -1 \text{ VAR} = -\frac{1}{\omega C} I_{rms}^2$$

Power for R:

$$P = RI_{rms}^2 = 2 W$$

$$Q = 0$$

$$\boxed{P = Q = 0}$$