# Exercise 2b: Model-based control of the ABB IRB 120

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October 30, 2018

## Abstract

In this exercise you will learn how to implement control algorithms focused on model-based control schemes. A MATLAB visualization of the robot arm is provided. You will implement controllers which require a motion reference in the joint-space as well as in the operational-space. Finally, you will learn how to implement a hybrid force and motion operational space controller. The partially implemented MATLAB scripts, as well as the visualizer, are available at http://www.rsl.ethz.ch/education-students/lectures/robotdynamics.html.



Figure 1: The ABB IRW 120 robot arm.

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## 1 Introduction

The robot arm and the dynamic properties are shown in Figure 2. The kinematic and dynamic parameters are given and can be loaded using the provided MATLAB scripts. To initialize your workspace, run the init\_workspace.m script. To start the visualizer, run the loadviz.m script.

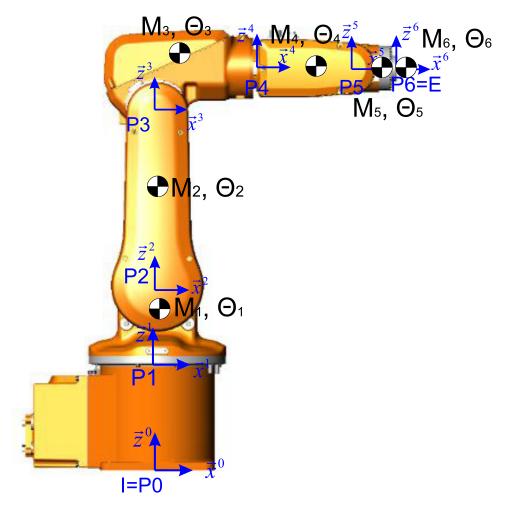


Figure 2: ABB IRB 120 with coordinate systems and joints

# 2 Model-based control

In this section you will write three controllers which use of the dynamic model of the arm to perform motion and force tracking tasks. The template files can be found in the problems/ directory. Each controller comes with its own Simulink model, which is stored under problems/simulink\_models/. To test each of your controllers, open the corresponding model and start the simulation.

## 2.1 Joint space control

#### Exercise 2.1

In this exercise you will implement a controller which compensates for the gravitational terms. Additionally, the controller should track a desired joint-space configuration and provide damping which is proportional to the measured joint velocities. Use the provided Simulink block scheme abb\_pd\_g.mdl to test your controller. What behavior would you expect for various initial conditions?

```
function [ tau ] = control_pd_g( q_des, q, q_dot )
   % CONTROL_PD_G Joint space PD controller with gravity compensation.
2
   % q_des -> a vector R^n of desired joint angles.
4
   % q ---> a vector R^n of measured joint angles.
  % q_dot -> a vector in R^n of measured joint velocities
   % Here the controller response is mainly inertia dependent
   % so the gains have to be tuned joint-wise
   kp = 0; % TODO
12
   kd = 0; % TODO
13
   \$ The control action has a gravity compensation term, as well as a PD
  % feedback action which depends on the current state and the desired
15
  % configuration.
17
   tau = zeros(6,1); % TODO
18
  end
19
```

## 2.2 Inverse dynamics control

## Exercise 2.2

In this exercise you will implement a controller which uses an operational-space inverse dynamics algorithm, i.e. a controller which compensates the entire dynamics and tracks a desired motion in the operational-space. Use the provided Simulink model stored in abb\_inv\_dyn.mdl. To simplify the way the desired orientation is defined, the Simulink block provides a way to define a set of Euler Angles XYZ, which will be converted to a rotation matrix in the control law script file.

```
function [ tau ] = control_inv_dyn(I_r_IE_des, eul_IE_des, q, q_dot)
            % CONTROL_INV_DYN Operational—space inverse dynamics controller ...
  2
                          with a PD
           % stabilizing feedback term.
  4
          % I_r_IE_des \longrightarrow a vector in R^3 which describes the desired ...
  5
                         position of the
                         end-effector w.r.t. the inertial frame expressed in the ...
                          inertial frame.
            % eul_IE_des —> a set of Euler Angles XYZ which describe the desired
           % end-effector orientation w.r.t. the inertial frame.
          % q \longrightarrow a vector in R^n of measured joint angles
           % q_dot -> a vector in R^n of measured joint velocities
 10
          % Set the joint-space control gains.
          kp = 0; % TODO
13
           kd = 0; % TODO
         % Find jacobians, positions and orientation based on the current
            % measurements.
18 I_{J_e} = I
19 I_dJ_e = I_dJe_fun_solution(q, q_dot);
```

```
20 T_IE = T_IE_fun_solution(q);
I_r = T_I = (1:3, 4);
22 C_IE = T_IE(1:3, 1:3);
23
   % Define error orientation using the rotational vector ...
^{24}
       parameterization.
25  C_IE_des = eulAngXyzToRotMat(eul_IE_des);
26 C_err = C_IE_des*C_IE';
27  orientation_error = rotMatToRotVec_solution(C_err);
_{\rm 29} % Define the pose error.
30 chi_err = [I_r_IE_des - I_r_Ie;
31
              orientation_error];
32
   % PD law, the orientation feedback is a torque around error ...
33
       rotation axis
  % proportional to the error angle.
34
35 tau = zeros(6, 1); % TODO
36
37
   end
```

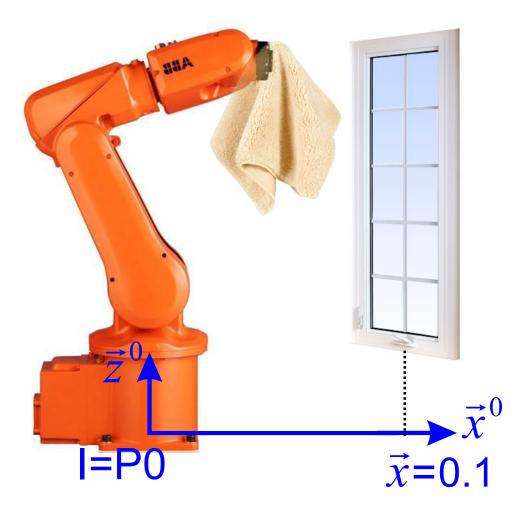


Figure 3: Robot arm cleaning a window

## 2.3 Hybrid force and motion control

## Exercise 2.3

We now want to implement a controller which is able to control both motion and force in orthogonal directions by the use of appropriate selection matrices. As shown in Fig. 3, there is a window at x=0.1m. Your task is to write a controller that wipes the window. This controller applies a constant force on the wall in x-axis and follows a trajectory defined on y-z plane. To do this, you should use the equations of motion projected to the operational-space. Use the provided Simulink model abb\_op\_space\_hybrid.mdl, which also implements the reaction force exerted by the window on the end-effector.

```
1 function [ tau ] = control_op_space_hybrid( I_r_IE_des, eul_IE_des, ...
                 q, dq, I_F_E_x )
      % CONTROL_OP_SPACE_HYBRID Operational—space inverse dynamics controller
       % with a PD stabilizing feedback term and a desired end-effector force.
 3
 4
       % I_r_IE_des \longrightarrow a vector in R^3 which describes the desired ...
                 position of the
                 end-effector w.r.t. the inertial frame expressed in the ...
                 inertial frame.
        % \ \text{eul_IE\_des} \longrightarrow \text{a set of Euler Angles XYZ which describe the desired}
       % end-effector orientation w.r.t. the inertial frame.
       % q \longrightarrow a \ \text{vector in R^n of measured joint positions}
       % q_{dot} \longrightarrow a \ vector \ in \ R^n \ of \ measured \ joint \ velocities
        % I_F_E_x \longrightarrow a scalar value which describes a desired force in the x
                direction
12
       % Design the control gains
14
15 kp = 0; % TODO
 16 kd = 0; % TODO
17
       % Desired end-effector force
18
      I_F_E = [I_F_E_x, 0.0, 0.0, 0.0, 0.0, 0.0]';
20
{\tt 21}~ % Find jacobians, positions and orientation
22   I_Je = I_Je_fun_solution(q);
       I_dJ_e = I_dJ_e_fun_solution(q, dq);
        T_{IE} = T
_{25} I_r_IE = T_IE(1:3, 4);
26 \quad C_{-}IE = T_{-}IE (1:3, 1:3);
27
      % Define error orientation using the rotational vector ...
28
                parameterization.
       C_IE_des = eulAngXyzToRotMat(eul_IE_des);
30 C_err = C_IE_des*C_IE';
31 orientation_error = rotMatToRotVec_solution(C_err);
32
33 % Define the pose error.
34 chi_err = [I_r_IE_des - I_r_IE;
35
                                 orientation_error];
36
      % Project the joint-space dynamics to the operational space
38
       % TODO
       % lambda = ... ;
39
40 % mu = ...;
       % p = ...;
41
      % Define the motion and force selection matrices.
43
44 % TODO
       % Sm = ...;
       % Sf = ... ;
46
47
```

```
48 % Design a controller which implements the operational—space inverse
49 % dynamics and exerts a desired force.
50 tau = zeros(6,1); % TODO
51
52 end
```