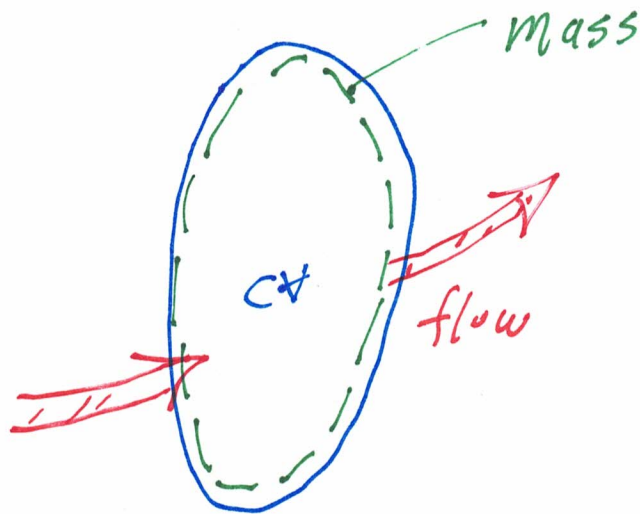


-1-

Class #9

Reynolds Transport Theorem

At instant
mass fills
CV



— CV
- - - mass

Φ any extensive property

mass
momentum

$\phi = \Phi / m$ intensive property

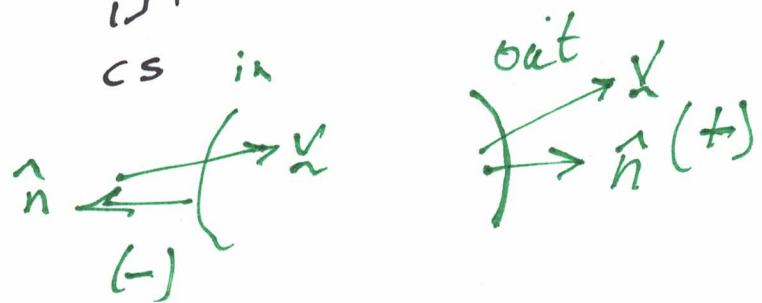
Net flow
of Φ out

$$\left. \frac{d\Phi}{dt} \right|_{\text{mass}} = \left. \frac{d\Phi}{dt} \right|_{\text{CV}} + \dot{\Phi}$$

$$\frac{d}{dt} \int_{\text{CV}} \rho \phi dV$$

Φ_{CV}

$$\int_{\text{CS}} \rho \phi (\mathbf{V} \cdot \mathbf{\hat{n}}) dA$$



1-aa

$$\Phi = m \quad \phi = \frac{\Phi}{m} = 1$$

$$\Phi = m \underline{V} \quad \phi = \frac{\Phi}{m} = \underline{V}$$

$$= \underline{G}$$

momentum

$$\left. \frac{d\Phi}{dt} \right|_{\text{mass}} = 0 = \frac{d}{dt} \int_{cv} \rho d\mathcal{V}$$

$$\Phi = \text{mass}$$

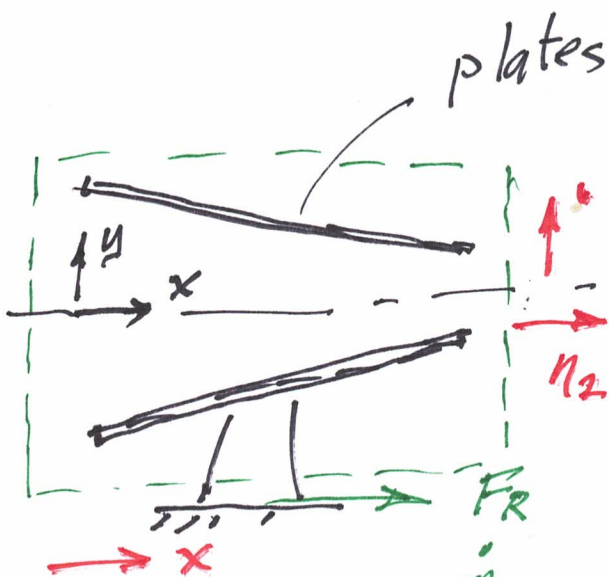
$$+ \int_{cs} \rho \underline{V} \cdot \underline{n} dA$$

$$\left. \frac{d\Phi}{dt} \right|_{\text{mass}} = \frac{d}{dt} m \underline{V} = m \underline{a} = \underline{\Sigma F}$$

$$\underline{\Sigma F} = \frac{d}{dt} \int_{cv} \rho \underline{V} d\mathcal{V} + \int_{cs} \rho \underline{V} (\underline{V} \cdot \underline{n}) dA$$

1-a Global Example

V



"Nozzle" W into paper

on stand

Inlet H_1, W
 know: density mass flow rate \dot{m}

$$V_{2x} = V_{20} \left(1 - \frac{y^2}{(H_2/2)^2} \right)$$

steady incomp.

$$V_{x1} = \text{const} = \frac{\dot{m}}{\rho W H_1}$$

$$\dot{m}_2 = \int_{CS} \rho (\underline{V} \cdot \underline{n}) dA = \rho W \int_{-H_2/2}^{+H_2/2} V_{2x} dy$$

$$= \frac{2}{3} V_{20} H_2 W \rho$$

$$\Sigma F = F_R = + \int \rho V_x (\underline{V} \cdot \underline{n}) dA$$

=

Find F_R

Force on nozzle



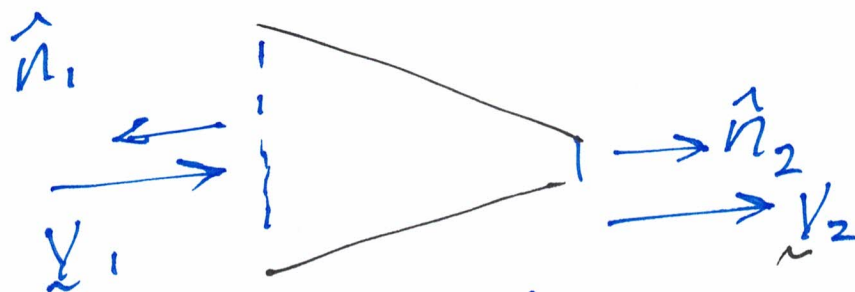
1-b

Nozzle Example (cont)

mass

$$0 = \frac{d}{dt} m_{cv} + \int \rho (\underline{V} \cdot \underline{n}) dA$$

$$0 = \underbrace{-\rho V_1 W H_1}_{\dot{m}} + \underbrace{\rho W \int_{-H/2}^{H/2} V_{20} \left(1 - \frac{y^2}{(H/2)^2}\right) dy}_{\frac{2}{3} H_2 W V_{20}}$$



$$V_{20} = \frac{3}{2} \frac{\dot{m}}{H_2 W \rho}$$

$$V_x = \frac{3}{2} \frac{\dot{m}}{\rho H_2 W} \left(1 - \frac{y^2}{(H/2)^2}\right)$$

1-6

x-momentum

$$\sum F = F_R = \frac{d}{dt} m \bar{u} \Big|_{CV} + \int \rho V_x (\underline{V} \cdot \underline{n}) dA$$

$$\textcircled{1} \quad n_1 = -\hat{e}_x$$

$$\hat{n} = \hat{e}_x$$

$$= - \rho \int_{-H/2}^{+H/2} V_{x1}^2 W dy + \rho \int_{-H/2}^{+H/2} V_{x2}^2 W dy$$

$\underbrace{\hspace{10em}}_{\text{at 1}}$
 $\underbrace{\hspace{10em}}_{\text{at 2}}$

: algebra

$$F_R = \frac{(6H_1 - 5H_2) \dot{m}^2}{5H_1 H_2 W \rho}$$

There is still a
force if $H_1 = H_2$
due to different
profiles

-2-

$$\int_{CS} \Rightarrow \int_{CV}$$

divergence
theorem

just math
changes volume \int
to surface \int

$$\int_{CS} \rho \phi (\underline{V} \cdot \underline{n}) dA = \int_{CV} \nabla \cdot (\rho \phi \underline{V}) dV$$

turn global continuity to one
volume \int

$$\int_{CV} \left[\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{V}) \right] dV = 0$$

$$0 = \frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} \rho V_x + \frac{\partial}{\partial y} \rho V_y$$

Differential
continuity

Incomp
steady

$\rho = \text{const}$
 $\partial \rho / \partial t = 0$

2-D

$$\boxed{\frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} = 0}$$

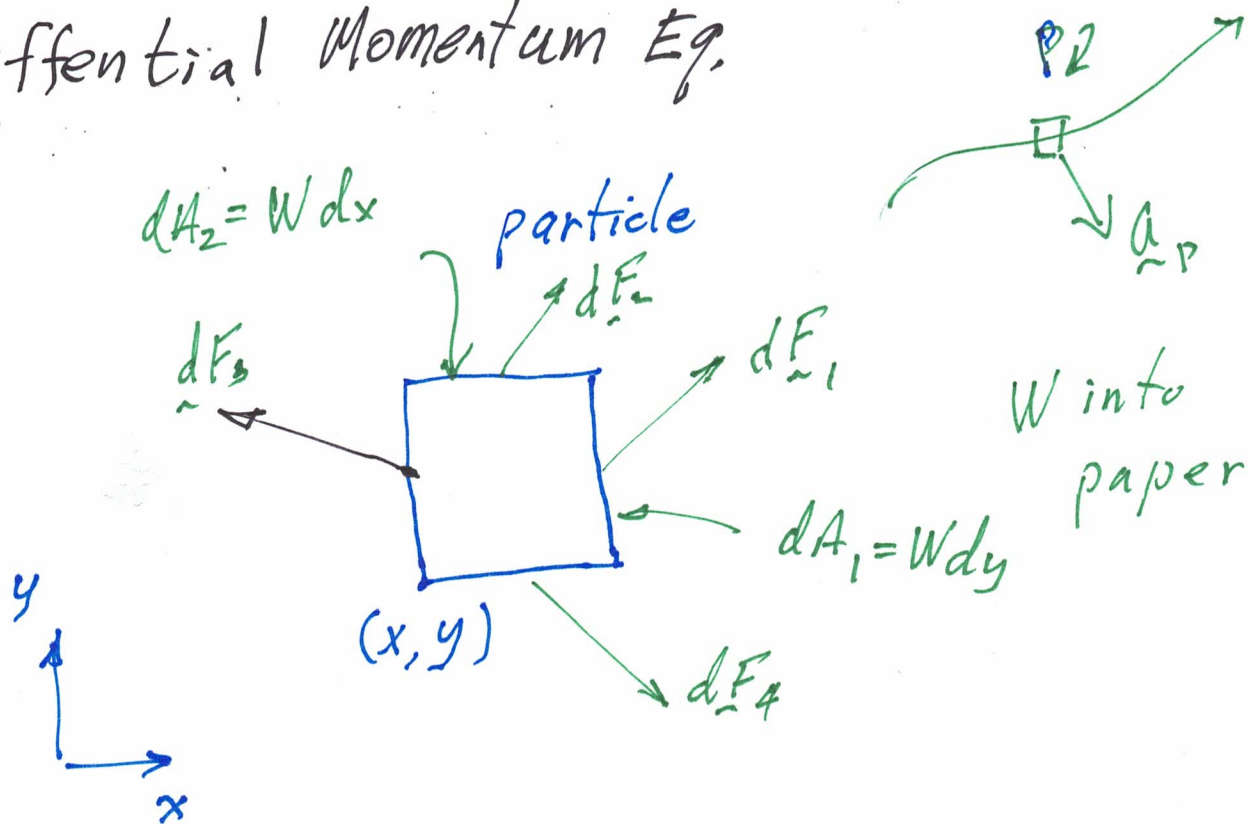
$$\underline{\nabla} \cdot \underline{V} = \text{div } \underline{V} = 0$$

-3-

Global Momentum Eq.

$$\sum \underline{F} = \frac{d}{dt} \int_V \rho \underline{V} dV + \int_{CS} \rho \underline{V} (\underline{V} \cdot \underline{n}) dA$$

Differential Momentum Eq.



$$m \underline{a}_p = \sum \underline{F} \quad \frac{1}{V} (m \underline{a}_p = \sum \underline{F})$$

$$\frac{m}{V} = \rho$$

$$\underline{a}_p = \frac{D\underline{V}}{Dt} = \frac{\partial \underline{V}}{\partial t} + \underline{V} \cdot \underline{\nabla} \underline{V}$$

-3a-

$$d\vec{F}_1 = \vec{t}_1 dA_1, \quad dA_1 = W dy$$

$$\vec{n}_1 = \hat{e}_x$$

$$\vec{t}_1 = \hat{e}_x \cdot \underline{\underline{\sigma}}$$

$$= \hat{e}_x \cdot (\sigma_{xx} \hat{e}_x \hat{e}_x + \sigma_{xy} \hat{e}_x \hat{e}_y + \sigma_{yx} \hat{e}_y \hat{e}_x + \sigma_{yy} \hat{e}_y \hat{e}_y)$$

$$= \sigma_{xx} \hat{e}_x + \sigma_{xy} \hat{e}_y$$

force on x-surface
area

in y-direction

$$\sigma_{xx}(x+dx) = \sigma_{xx}(x) + \frac{\partial \sigma_{xx}}{\partial x} dx$$

$$\sigma_{xx} = -p + \tau_{xx}$$

$$\sum (d\vec{F}_1 + d\vec{F}_2 + d\vec{F}_3 + d\vec{F}_4) =$$

$$\left(\frac{\partial \sigma_{xx}}{\partial x} dx \underbrace{W dy}_{dV} + \frac{\partial \sigma_{yx}}{\partial y} dy \underbrace{W dx}_{dV} \right) \hat{i}$$

$$m \vec{a} = \sum \vec{F}$$

$$\rho \vec{a} = \sum \vec{F} / V$$

36

surface/
Net force/volume

$$\left(\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{yx}}{\partial y} \right) \hat{e}_x$$

$$+ \left(\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} \right) \hat{e}_y$$

$$\sigma_{xx} = -p + \tau_{xx}$$

$$\sigma_{xy} = \tau_{xy}$$

etc.

total stress

$$\underline{\underline{\sigma}} = -p \underline{\underline{\delta}} + \underline{\underline{\tau}}$$

hydrostatic
pressure

$\underline{\underline{\tau}}$ deviatoric (extra)
stress

due to motion

3c X-Comp

$$\rho \frac{DV_x}{Dt} = -\frac{\partial p}{\partial x} + \frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y}$$

$$\rho \frac{DV_y}{Dt} = -\frac{\partial p}{\partial y} + \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} - \rho g$$

$$F_{\text{grav}} = -mg$$

$$\frac{F_{\text{grav}}}{\text{Vol}} = -\rho g$$

Any ~~the~~ flowing material

Newtonian fluid

$$\tau = \mu \dot{\gamma}$$

incompressible

$\mu = \text{viscosity}$

$$\tau_{xx} = 2\mu \frac{\partial V_x}{\partial x}$$

$$\tau_{xy} = \tau_{yx} = \mu \left(\frac{\partial V_x}{\partial y} + \frac{\partial V_y}{\partial x} \right)$$

$$\tau_{yy} = 2\mu \frac{\partial V_y}{\partial y} = -\tau_{xx}$$

2-D incomp

4-

recall:

$$a_x^p = \frac{DV_x}{Dt} = \frac{\partial V_x}{\partial t} + V_x \frac{\partial V_x}{\partial x} + V_y \frac{\partial V_x}{\partial y}$$

acceleration
following
particle

$$a_y^p = \frac{DV_y}{Dt} = \frac{\partial V_y}{\partial t} + V_x \frac{\partial V_y}{\partial x} + V_y \frac{\partial V_y}{\partial y}$$

$$\Sigma F_x / \mathcal{V} = -\frac{\partial p}{\partial x} + \frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y}$$

$$\Sigma F_x = m a_x^p$$

$$\Sigma F_x / \mathcal{V} = \rho a_x^p$$

-4a- Navier-Stokes Equation

$$\rho \left(\frac{\partial V_x}{\partial t} + \underbrace{V_x \frac{\partial V_x}{\partial x} + V_y \frac{\partial V_x}{\partial y}}_{\text{non-linear}} \right) = -\frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 V_x}{\partial x^2} + \frac{\partial^2 V_x}{\partial y^2} \right)$$

$$\rho \left(\frac{\partial V_y}{\partial t} + \underbrace{V_x \frac{\partial V_y}{\partial x} + V_y \frac{\partial V_y}{\partial y}}_{\text{non-linear}} \right) = -\frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 V_y}{\partial x^2} + \frac{\partial^2 V_y}{\partial y^2} \right) - \rho g$$

Cont $\frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} = 0$

$$\rho \frac{D \underline{V}}{Dt} = -\nabla p + \nabla \cdot \underline{\underline{\tau}} - \rho \underline{g} = -\underline{\underline{\nabla}} p + \underbrace{\underline{\underline{\nabla}} \cdot (\underline{\underline{\nabla}} \underline{V})}_{\underline{\underline{\nabla^2 V}}} - \rho \underline{g}$$

Boundary & Initial

1 IC

Conditions

2 BC's in
on x in y

(to be continued)

$$y = y_1(x)$$

$$V_x = \dots; V_y =$$

$$y = y_2(x)$$

$$V_x = \dots; V_y =$$

