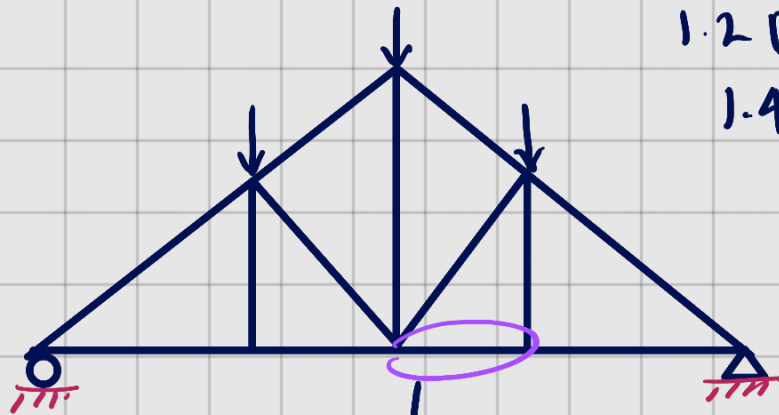


Recap:

Types of loads Dead, Live, snow, earthquake, wind



$$\left. \begin{array}{l} 1.2D + 1.6L \\ 1.4D \end{array} \right\}$$

$\rightarrow P_D, P_L$ (internal tensile forces)

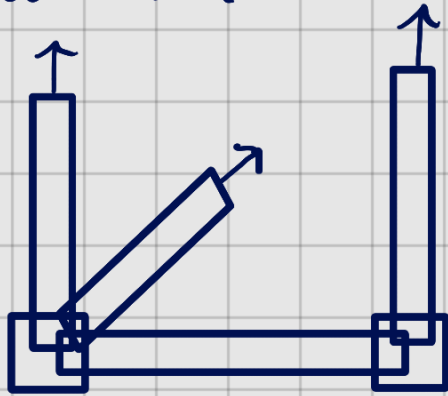
$$\underbrace{P_D = 15K, P_L = 20K}_{P_u}$$

$$P_u = \max \left\{ \begin{array}{l} 1.2P_D + 1.6P_L = 50K \\ 1.4D = 21K \end{array} \right. = 50K$$

$$P_u = 50K \leq \phi P_n, \quad P_n: \text{nominal strength/capacity}$$

ϕ : capacity factor

Zoom in:



Two failure modes:

1) gross yield

$$P_n = F_y \cdot A_g$$

gross area

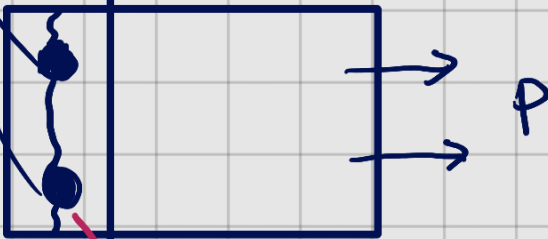
yield stress

2) Net Section Fracture

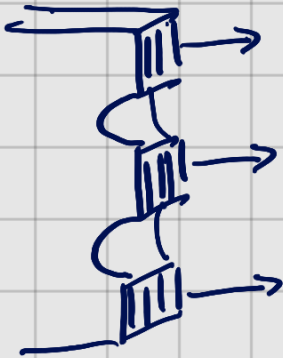
$$P_n = F_u \cdot A_{net}$$

$$A_{net} = (A_g - A_{holes})$$

Bolts at connections



reduced area



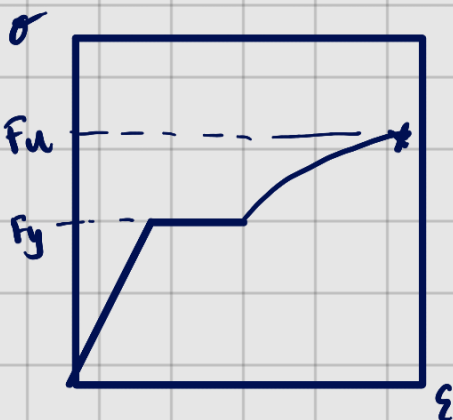
- net section fracture is more concerning because it can happen suddenly due to smaller area

- gross yield

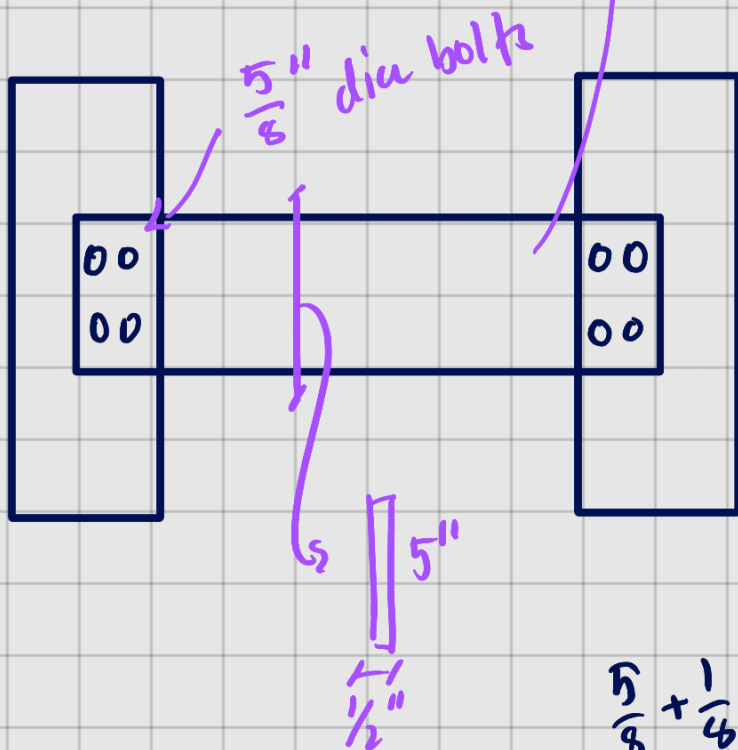
$$\phi = 0.9$$

- net section fracture

$$\phi = 0.75$$



$$P_u = 50 \text{ K}$$



Assume A36 steel

$$\begin{aligned} \rightarrow F_y &= 36 \text{ ksi} \\ F_u &= 58 \text{ ksi} \end{aligned}$$

Gross Yield

$$\begin{aligned} \rightarrow P_n &= 0.9 (36) (5 \times \frac{1}{2}) \\ &= \underline{81 \text{ K}} \end{aligned}$$

Net section Fracture

$$\begin{aligned} \rightarrow P_n &= 0.75 (58) \\ &\quad \text{in}^2 \left(\frac{1}{2} (5 - \frac{3}{4} \times 2) \right) \end{aligned}$$

$$\begin{aligned} &= 0.75 (58) (1.75) \\ &= \underline{76.125 \text{ K}} \end{aligned}$$

$$\frac{5}{8} + \frac{1}{4} = \frac{3}{4}$$

bolt tolerance

Member does not yield

for $P_u = 50 \text{ ksi}$ because

$$P_u \leq 81 \text{ K} \text{ and } P_u \leq 76.125 \text{ K}$$

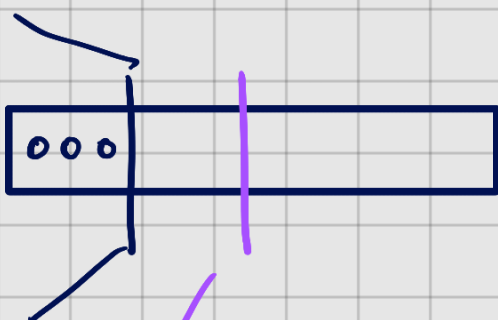
$$P_D = 35 \text{ K}, P_L = 15 \text{ K}$$

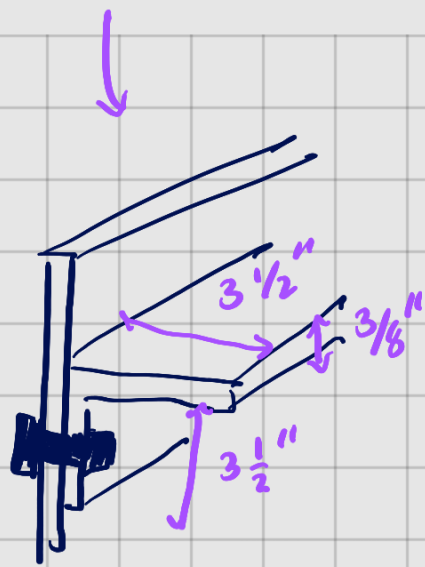
$$\text{A36, L } 3\frac{1}{2} \times 3\frac{1}{2} \times \frac{3}{8}$$

$$\Rightarrow P_u = \max \begin{cases} 1.2 P_D + 1.6 P_L \\ 1.4 P_D \end{cases} = 66 \text{ K}$$

$$\text{G.Y.} \Rightarrow 0.9 F_y A_g$$

$$\text{N.S.F.} \Rightarrow 0.75 F_u A_{\text{net}}$$





\Rightarrow G.Y.

$$\hookrightarrow P_n = 0.9(36)(2.5) = 81 \text{ K}$$

\Rightarrow N.S.F

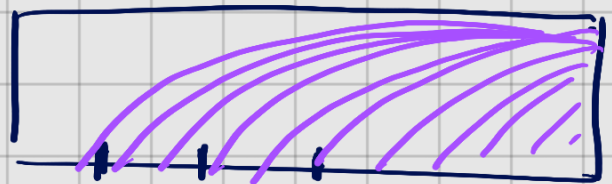
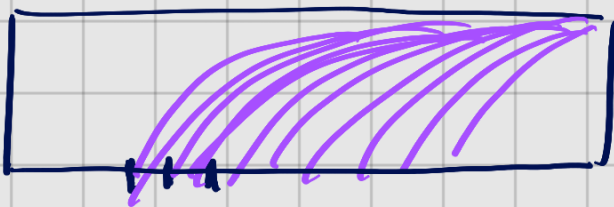
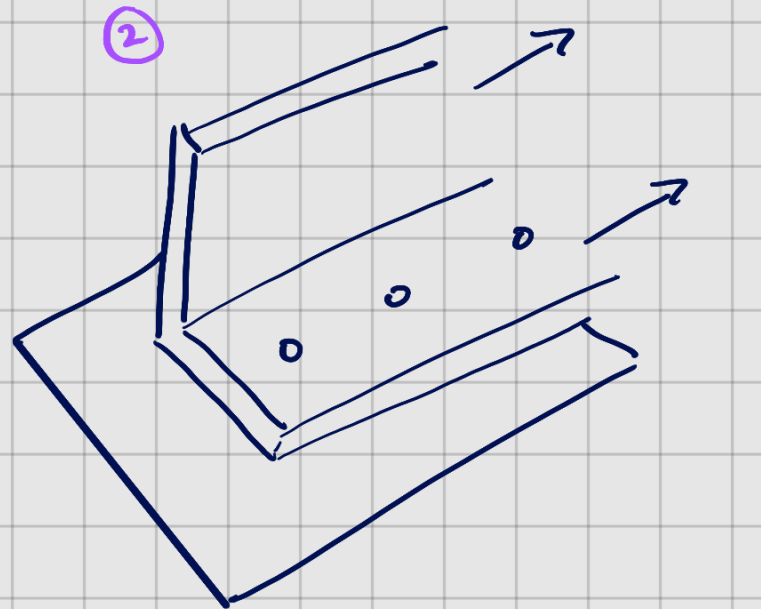
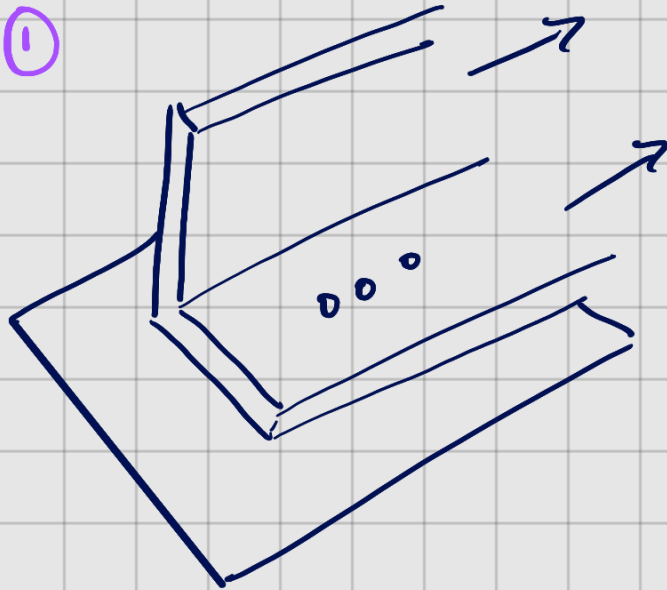
$$\hookrightarrow P_n = 0.75(58)\left(2.5 - \frac{3}{8}\right)$$

$$P_n = 92.44 \text{ K}$$

$A = 2.5 \text{ in}^2$ (from table)

$$P_n = 66 \text{ K} \leq 92.44 \text{ K},$$

$$P_n = 66 \text{ K} \leq 81 \text{ K}$$



- Shear - lag factor

\hookrightarrow N.S.F. $\Rightarrow P_n = 0.75 \times F_u \times A_e$ effective area

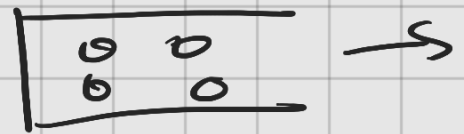
$\hookrightarrow A_e = U \cdot A_n$, U : shear-lag factor / connection efficiency factor

How to calculate U :

- longer connection, $U \uparrow$
- taller member cross-section, $U \downarrow$

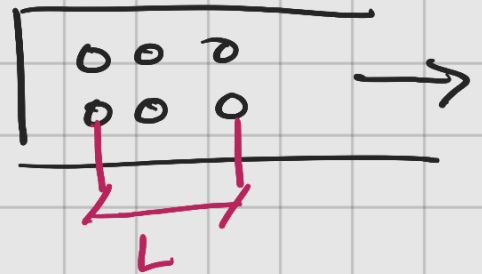
- if 2 bolt rows

$$\hookrightarrow U = 0.75$$



- if 3+ bolt rows

$$\hookrightarrow U = 1 - \frac{\bar{x}}{L} \leq 0.9$$



Use
 0.9
 if
 calculation
 > 0.9

\bar{x} is distance of bottom to centroid of cross-section



- if flat cross section

$$\hookrightarrow U = 1$$

