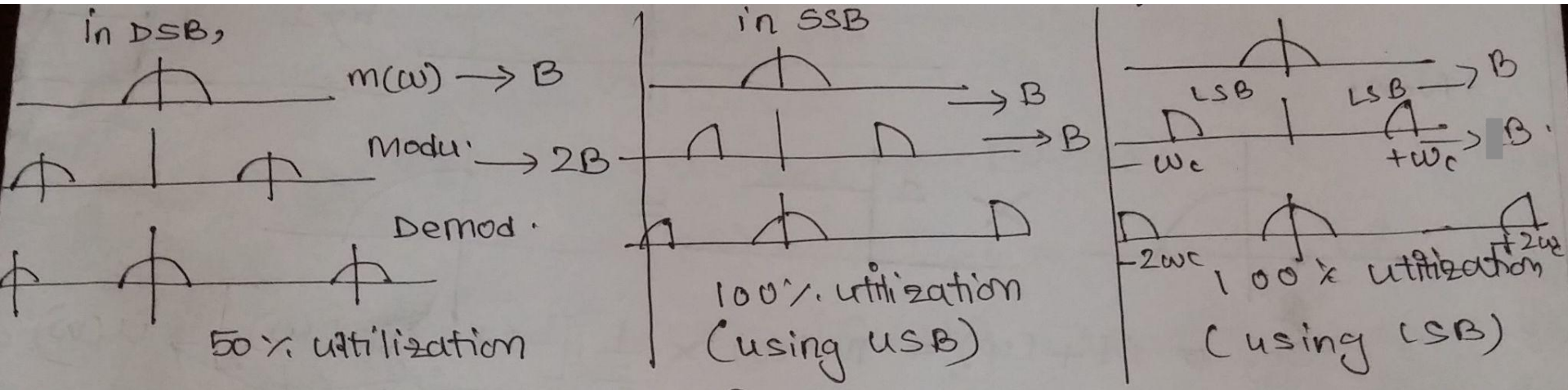

Lectures 6 & 7

Topics

- **SSB: Modulation**
- **SSB: Coherent and Envelope Detection**
- **Problems of SSB**
- **Drawing Spectrum of SSB**
- **Concept of VSB**

DSB vs SSB

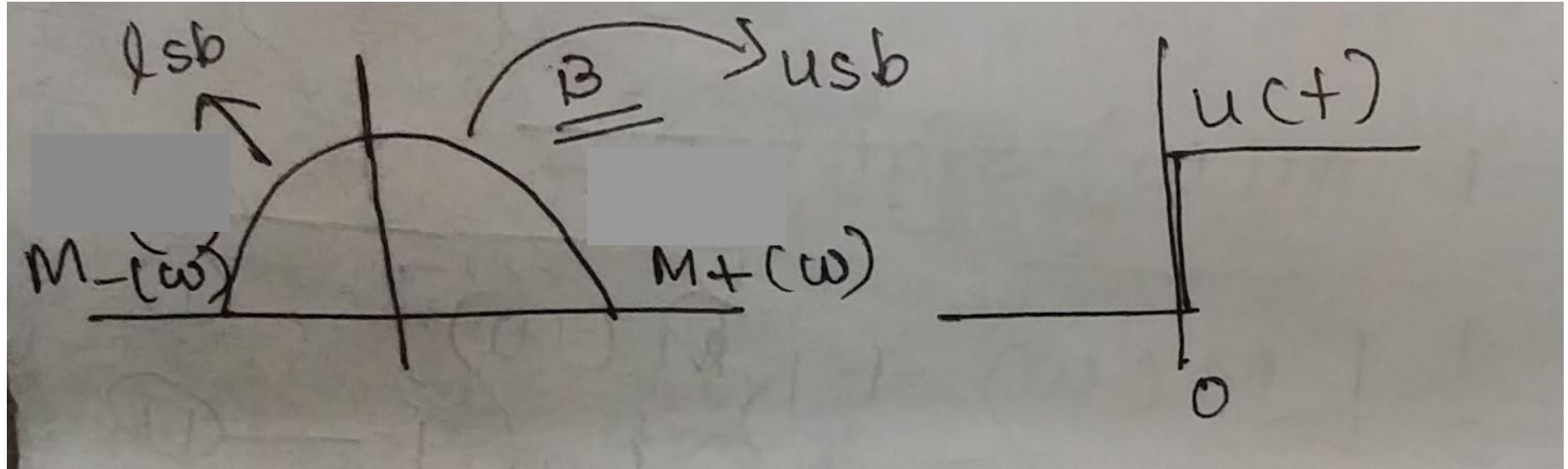
- In **DSB**, bandwidth utilization is **50%**
- In **SSB**, bandwidth utilization is **100%**



SSB

- In **SSB**, bandwidth utilization is **100%**
- **Full signal recovery** is possible from SSB
- **Cutoff** is done using a **filter**

SSB: Modulation



SSB: Modulation

$$M_+(w) = M(w) u(w)$$

$$M_-(w) = M(w) u(-w)$$

$m_+(t), m_-(t) \rightarrow$
inverse fourier transform

SSB: Modulation

*** Since amplitude spectra $|M_+(\omega)|$ and $|M_-(\omega)|$ are not even functions of ω , the signals $m_+(t)$ & $m_-(t)$ cannot be real \rightarrow they are complex.

& $M_+(\omega)$ & $M_-(\omega)$ are two halves of $M(\omega)$

So, $M_+(\omega)$ & $M_-(\omega) \rightarrow$ conjugates & $\left| \begin{array}{l} M(\omega) \\ = M_+(\omega) \\ + M_-(\omega) \end{array} \right.$
 $m_+(t)$ & $m_-(t) \rightarrow$ conjugates.

Also, $m_+(t) + m_-(t) = m(t)$

SSB: Modulation

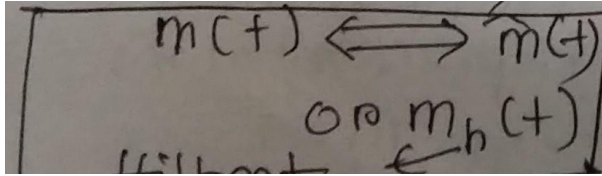
Now, $\Phi_{usb}(\omega) = M_+(\omega - \omega_c) + M_-(\omega + \omega_c)$

Taking Inverse Fourier Transform,

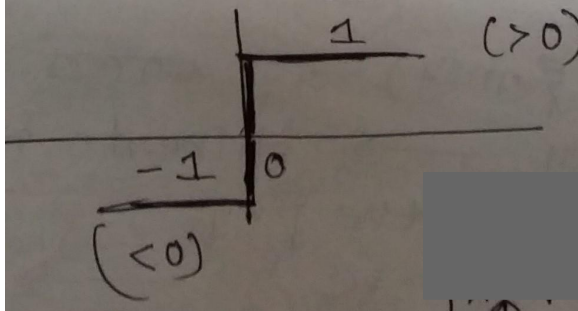
$$\phi_{usb}(t) = m_+(t) e^{j\omega_c t} + m_-(t) e^{-j\omega_c t}$$

$$\begin{aligned} m_+(t) &= \frac{1}{2} [m(t) + j\hat{m}(t)] \\ m_-(t) &= \frac{1}{2} [m(t) - j\hat{m}(t)] \end{aligned} \quad \left. \vphantom{\begin{aligned} m_+(t) &= \frac{1}{2} [m(t) + j\hat{m}(t)] \\ m_-(t) &= \frac{1}{2} [m(t) - j\hat{m}(t)] \end{aligned}} \right\} \begin{array}{l} \text{conjugate} \\ \text{form} \end{array}$$

SSB: Modulation

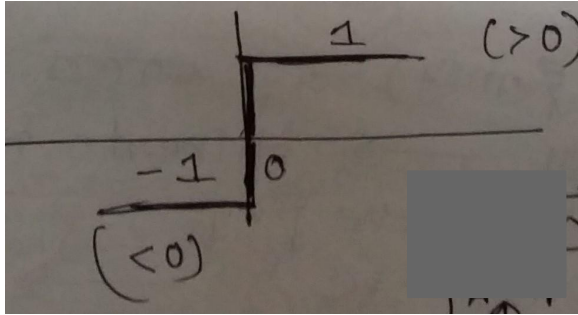

$$m(t) \longleftrightarrow \hat{m}(t) \text{ or } m_h(t)$$

Hilbert Transform



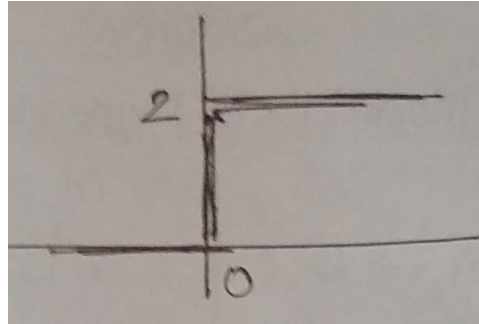
Signum Function

SSB: Modulation

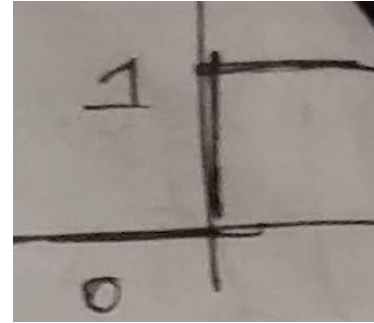


Signum Function

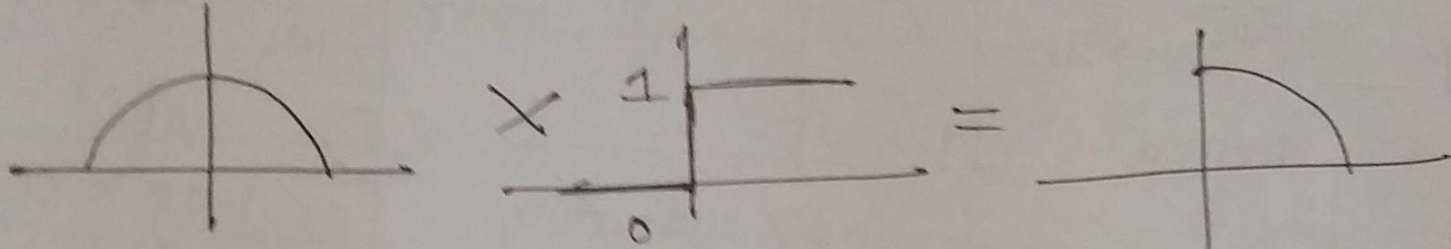
+1 ->



Divided
by 2 ->



SSB: Modulation



$$\text{So, } M + (\omega) = M(\omega) \times \frac{1}{2} [1 + \text{sign}(\omega)] \rightarrow U(\omega)$$

SSB: Modulation

$$\text{Now, } m_+(t) = \frac{1}{2} m(t) + j \frac{1}{2} \hat{m}(t)$$

$$M_+(\omega) = \frac{1}{2} M(\omega) + \frac{1}{2} M(\omega) \operatorname{sgn}(\omega) \quad \text{--- (A)}$$

$$\text{Now, } m_+(\omega) = \frac{1}{2} [M(\omega) + j \hat{M}(\omega)] \quad \text{--- (i)}$$

$$M_-(\omega) = \frac{1}{2} [M(\omega) - j \hat{M}(\omega)] \quad \text{--- (ii)}$$

$$\text{From (i), } j \hat{M}(\omega) = 2 M_+(\omega) - M(\omega)$$

$$= M(\omega) + M(\omega) \operatorname{sgn}(\omega) - M(\omega)$$

$$= M(\omega) \operatorname{sgn}(\omega)$$

(From A)

SSB: Modulation

$$\text{So, } j\hat{M}(\omega) = M(\omega)\text{sgn}(\omega)$$

$$\Rightarrow \hat{M}(\omega) = -jM(\omega)\text{sgn}(\omega) \quad \text{--- (iii)}$$



Inverse Fourier transform of $M(\omega)$ will yield $m(t)$

Inverse Fourier transform of $\hat{M}(\omega)$ will yield $\hat{m}(t)$

To invert the two together, we will use convolution operation



$$\hat{m}(t) = m(t) * \frac{2}{\pi}$$

from $\hat{M}(\omega)$

from $M(\omega)$

time domain representation
of $-j\text{sgn}(\omega)$

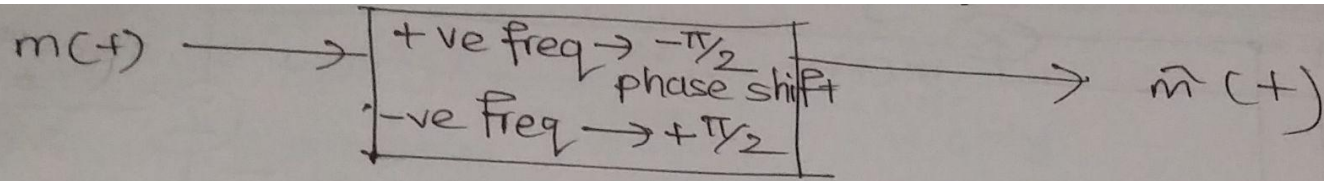
SSB: Modulation

*** Hilbert Transform is convolution of a signal $m(t)$ & $\frac{2}{\pi}$

+ve frequencies of the signal $\rightarrow -\pi/2$ phase shift

-ve frequencies of the signal $\rightarrow +\pi/2$ phase shift

SSB: Modulation

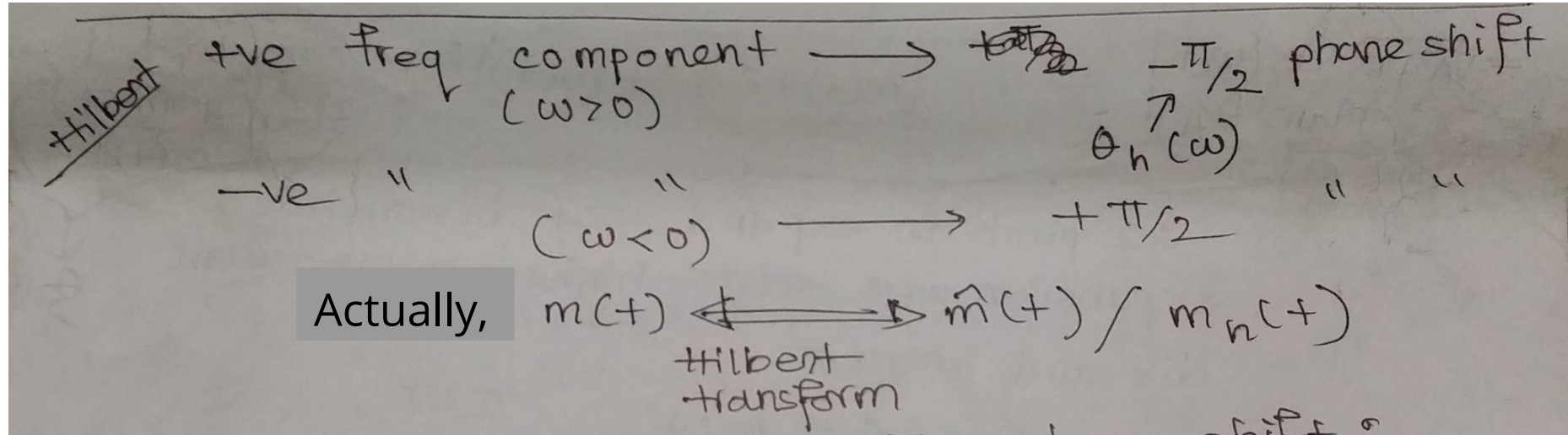


$$\begin{aligned}\text{So, } m_{\text{USB}}(\omega) &= m_+(\omega - \omega_c) + m_-(\omega - \omega_c) \\ &= m_+(t) e^{j\omega_c t} + m_-(t) e^{-j\omega_c t}\end{aligned}$$

$$\begin{aligned}2m_{\text{USB}}(\omega) &= [m(t) + j\hat{m}(t)] (\cos \omega_c t + j \sin \omega_c t) \\ &\quad + [m(t) - j\hat{m}(t)] (\cos \omega_c t - j \sin \omega_c t) \\ &= 2m(t) \cos \omega_c t + \underline{2\hat{m}(t) \sin \omega_c t}\end{aligned}$$

$$\text{So, } m_{\text{USB}}(\omega) = m(t) \cos \omega_c t + \underline{\hat{m}(t) \sin \omega_c t}$$

SSB: Modulation



SSB: Modulation

Hilbert Transform for cosine signal ->

Shifting cosine signal by $+\pi/2$ (for negative frequencies) or $-\pi/2$ (for positive frequencies) ->

Transmitting cosine signal with a phase delay of $-\pi/2$

SSB: Modulation

$$\begin{aligned} -\frac{\pi}{2} \text{ phase shift : } & \cos\left(\omega_c - \frac{\pi}{2}\right) \boxed{\text{+ve freq component}} \\ & \cos\left(-\omega_c - \frac{\pi}{2}\right) \boxed{\text{-ve freq comp.}} \\ & = \cos\left(\omega_c + \frac{\pi}{2}\right) \longrightarrow \text{so} \\ & \quad +\frac{\pi}{2} \text{ phase shift} \end{aligned}$$

SSB: Modulation

Example: $m(t) = \cos 100t$

$$\tilde{m}_n(t) = \cos(100t - \pi/2) = \sin 100t$$

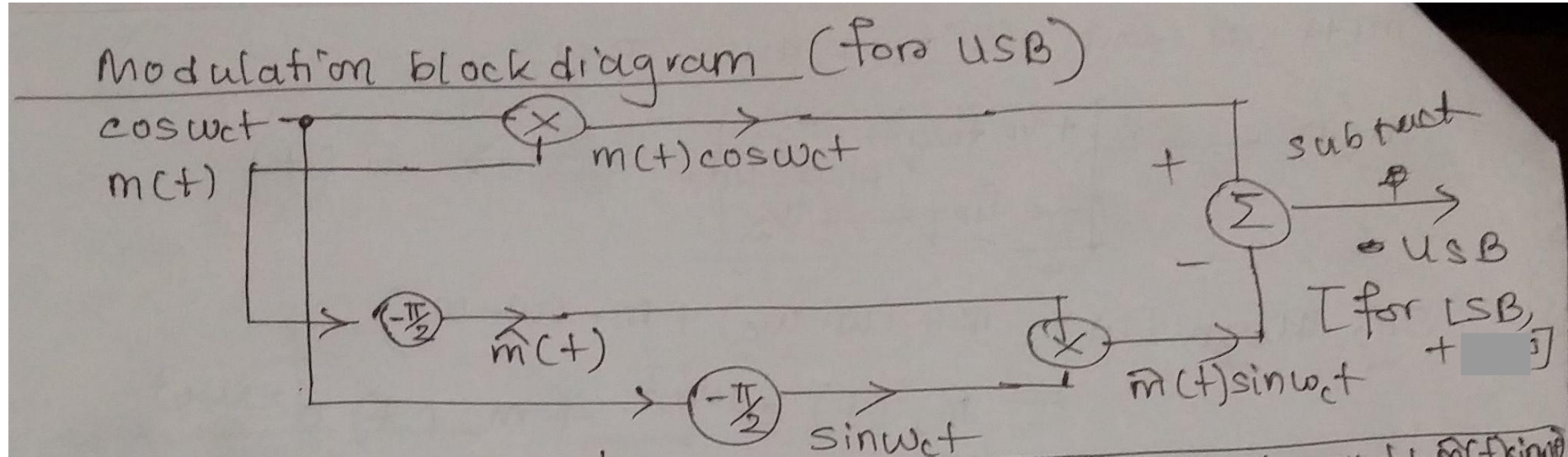
SSB: Modulation

$$* m_{LSB}(w) = m(t) \cos w_c t + \hat{m}(t) \sin w_c t$$

$$\text{so, } m_{SSB}(w) = m(t) \cos w_c t \pm \hat{m}(t) \sin w_c t$$

[+ \rightarrow LSB, - \rightarrow USB]

SSB: Modulation



SSB: Coherent Demodulation

$$\begin{aligned}\text{Demodulation (coherent)} &= [m(t)\cos\omega_c t + \hat{m}(t)\sin\omega_c t] \\ &\times \cos\omega_c t = \frac{1}{2} [m(t)(1 + \cos 2\omega_c t) - \hat{m}(t)\sin 2\omega_c t] \\ &= \frac{1}{2} m(t) + \underbrace{\quad}_{\text{filter out}}\end{aligned}$$

SSB-WC: Envelope Detection

transmit this signal $\rightarrow m(t) \cos \omega_c t - \hat{m}(t) \sin \omega_c t$

$$+ A \cos \omega_c t$$

$$= [m(t) + A] \cos \omega_c t - \hat{m}(t) \sin \omega_c t$$

$$= \sqrt{(m(t) + A)^2 + (\hat{m}(t))^2} \cos(\omega_c t + \underbrace{\tan^{-1} \frac{\hat{m}(t)}{m(t) + A}}_{\theta})$$

After expanding this part using binomial expansion and discarding higher order terms,

$$\approx A + m(t)$$

So, ultimately $\approx [A + m(t)] \cos(\omega_c t + \theta)$

SSB-WC: Condition for Envelope Detection

So, ultimately $\approx [A + m(t)] \cos(\omega_c t + \theta)$

In AM, condition: $A \geq |m(t)|$

SSB+WC: $A \gg |m(t)| \rightarrow$ the

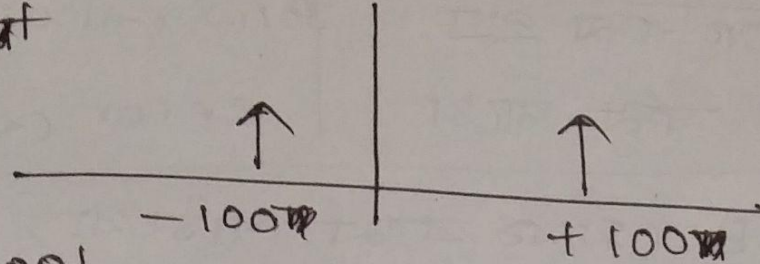
required amplitude is much larger than in AM
 \rightarrow so efficiency of SSB+WC is very low.

SSB: Problems

- In practice, it is often not feasible to sharply cut off double sideband to produce single sideband using filters
- It is not always possible to multiply a signal and its Hilbert transform -> since real signals have many components, it is not possible to transform each component -> approximation methods are used

Drawing Spectrum of SSB

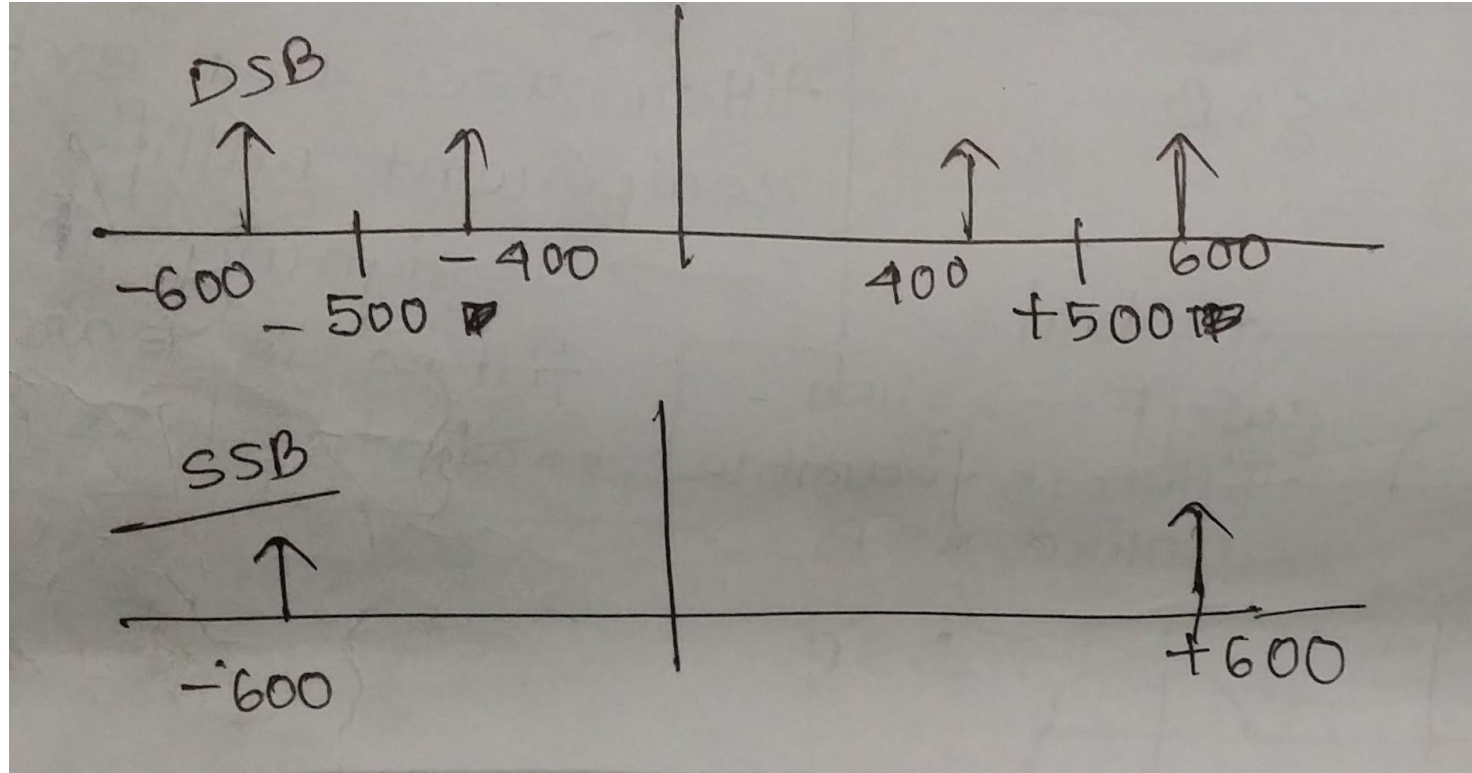
$$* m(t) = \cos 100t$$



$$* \text{carrier} = \cos 500t$$

$$\begin{aligned} * \text{So, transmitted signal} &= m(t) \cos \omega_c t - \hat{m}(t) \sin \omega_c t \\ &= \cos 100t \cos 500t \\ &\quad - \sin 100t \sin 500t \\ &= \cos(500t + 100t) = \cos 600t \end{aligned}$$

Drawing Spectrum of SSB



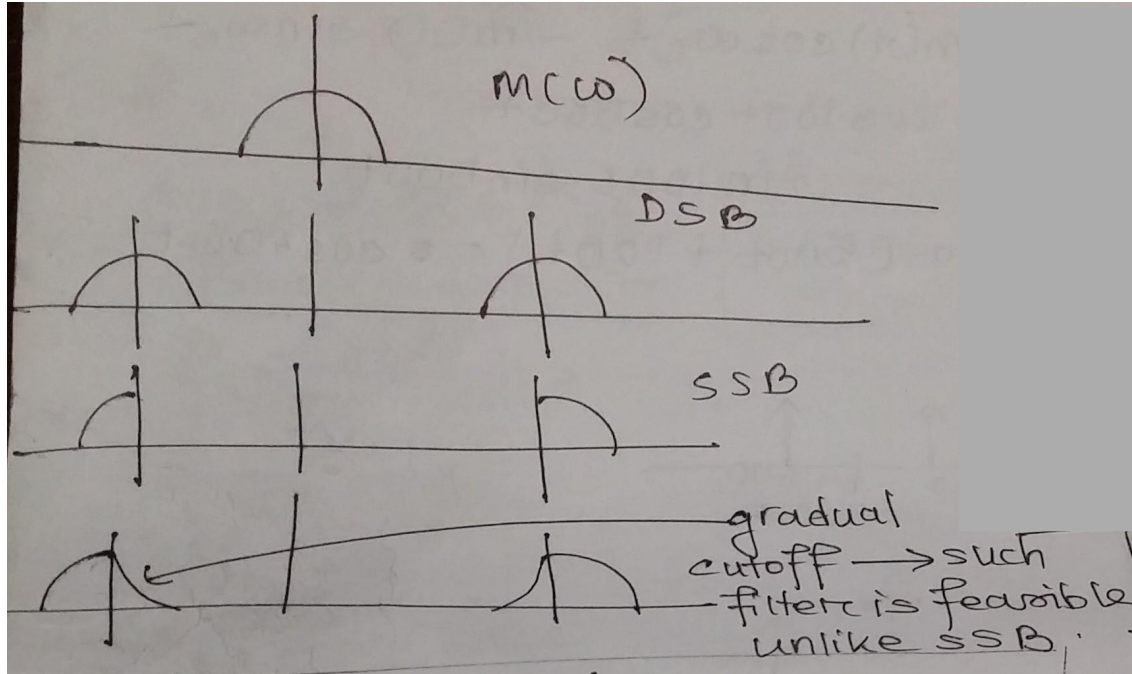
Pros and Cons of DSB and SSB

DSB: Less error-prone, but requires more bandwidth!

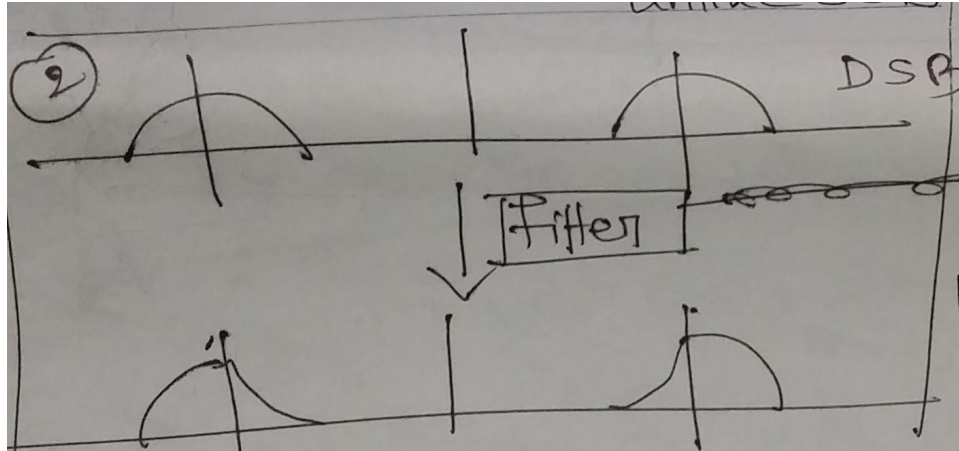
SSB: Requires less bandwidth, but more error-prone!

Concept of VSB (Vestigial Sideband): Sending more than SSB, but less than DSB!!

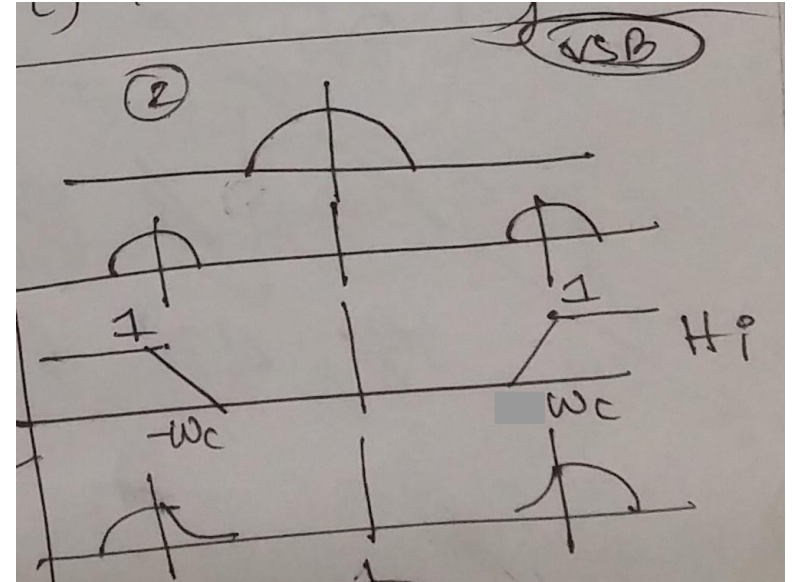
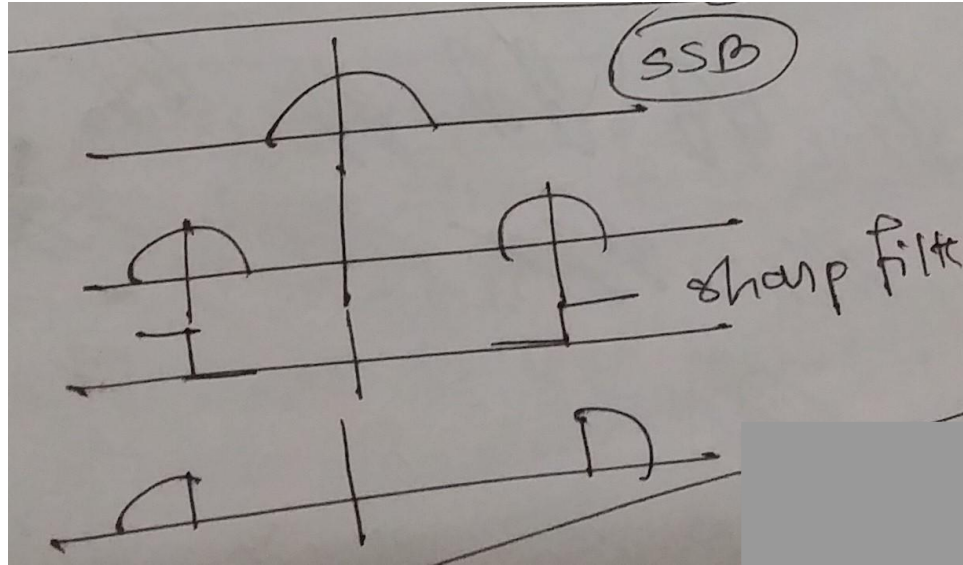
Concept of VSB



Concept of VSB



Concept of VSB



Concept of VSB: Problem with Demodulation

- During demodulation, the extra portion will overlap in the middle and become distorted ->
has to be nullified using an inverse filter
- Since designing an inverse filter is quite easy, data loss will not occur!