



1 | Setup

The ball launcher problem involves an energetic optimization to figure, given the situation as shown in the above image, the parameters h_o and θ_o that would best create a maximum launch distance x_f .

In this problem, we will define the axis such that the "lower-left" corner of the wood block (corner sharing x value of the starting position of the marble, but on the "ground") as $(-w, 0)$, where w is the width of the wooden block. Therefore, we derive the x -value of the location of the launch of the projectile as $x = 0$. We define the direction towards which the marble is launching as positive- x , so as the marble rolls, its position's x value increases. We will define the location of the marble before starting as positive y , and as the marble decreases in height, its position's y value decreases.

We define the start of the experiment as time t_0 , the moment the marble leaves the track and travels as a projectile as t_1 , and the end — in the moment when the marble hits the ground — as t_f . We will call the marble m_0 .

2 | Figuring the Velocity at t_1

In order to expedite the process of derivation, we will leverage an energetic argument instead of that of kinematics for figuring the velocity at launch. The change-in-height that m_0 experiences before t_1 is $\Delta h = H - h_0$. Therefore, the potential energy expenditure is $\Delta PE_{grav} = mg\Delta h = m_0g(H - h_0)$. Assuming that the marble starts out with 0 kinetic energy, we deduct that, at the moment of it finishing its descent, it will possess kinetic energy $KE = 0 + m_0g(H - h_0) = m_0g(H - h_0)$.

For this derivation, for now, we ignore $KE_{rotational}$, hence, we could roughly deduct the statement that $KE_{translational} \approx m_0g(H - h_0)$.

Creating this statement, we could deduct a statement that we could leverage to solve for the velocity at t_1 named \vec{v}_0 .

$$m_0g(H - h_0) = \frac{1}{2}m_0\vec{v}_0^2 \quad (1)$$

$$g(H - h_0) = \frac{1}{2}\vec{v}_0^2 \quad (2)$$

$$2g(H - h_0) = \vec{v}_0^2 \quad (3)$$

$$\vec{v}_0 = \sqrt{2g(H - h_0)} \quad (4)$$

This velocity vector could be easily split into its two constituent parts. Namely:

$$\begin{cases} v_{0x} = \sqrt{2g(H - h_0)}\cos(\theta_0) \\ v_{0y} = \sqrt{2g(H - h_0)}\sin(\theta_0) \end{cases}$$

3 | Figuring the Maximum Possible Travel Distance

Here, we devise an function for x_f w.r.t. v_{0y} , v_{0x} , h_0 , m_0 .

3.1 | Setup for Kinematics

We first will leverage the parametric equations for position in kinematics in order to ultimately result in a function for x_f .

$$\begin{cases} x(t) = \frac{1}{2}a_{0x}t^2 + v_{0x}t + x_0 \\ y(t) = \frac{1}{2}a_{0y}t^2 + v_{0y}t + y_0 \end{cases}$$

Given the situation of our problem, we could modify the pair as follows:

$$\begin{cases} x(t) = v_{0x}t \\ y(t) = \frac{-1}{2}gt^2 + v_{0y}t + h_0 \end{cases}$$

as...

- there are no acceleration in the x-direction at the point of launch
- the only acceleration in the y-direction is that due to gravity
- the start x-position of the marble at launch is, as defined above, $x = 0$
- the start y-position of the marble at launch is, as defined above, $y = h_0$

3.2 | Solving for $\frac{dx_f}{d\theta_0}$

We need to maximize $\frac{dx_f}{d\theta_0}$ as one out of two components to optimize for. Once we figure that value, we then supply the corresponding maximum value then optimize again for $\frac{h_0}{d\theta_0}$. The position equations above could be leveraged to figure a value for x_f .

3.2.1 | Setup for Solution

We first create a set of equations modeling the location of the marble at t_f .

$$\begin{cases} x(t_f) = x_f = v_{0x}t_f = t_f\sqrt{2g(H-h_0)}\cos(\theta_0) \\ y(t_f) = 0 = \frac{-1}{2}gt_f^2 + v_{0y}t_f + h_0 = \frac{-1}{2}gt_f^2 + t_f\sqrt{2g(H-h_0)}\sin(\theta_0) + h_0 \end{cases}$$

We first solve for t_f , and supply it to the first equation.

$$t_f = \frac{x_f}{\sqrt{2g(H-h_0)}\cos(\theta_0)} \quad (5)$$

Finally, we substitute the definition of t_f into $y(t_f)$.

$$y(t_f) = 0 = \frac{-1}{2}g\left(\frac{x_f}{\sqrt{2g(H-h_0)}\cos(\theta_0)}\right)^2 + \frac{x_f}{\sqrt{2g(H-h_0)}\cos(\theta_0)}\sqrt{2g(H-h_0)}\sin(\theta_0) + h_0 \quad (6)$$

We will now proceed to simplify the expression further

$$0 = \frac{-1}{4}\frac{-x_f^2}{(H-h_0)\cos^2(\theta_0)} + x_f\tan(\theta_0) + h_0 \quad (7)$$

$$= \frac{-1}{4}\frac{-x_f^2}{(H-h_0)}\cos^{-2}(\theta_0) + x_f\tan(\theta_0) + h_0 \quad (8)$$

$$= \frac{-1}{4}\frac{-1}{(H-h_0)}x_f^2\cos^{-2}(\theta_0) + x_f\tan(\theta_0) + h_0 \quad (9)$$

3.2.2 | Finding $\frac{dx_f}{d\theta_0}$

We leverage implicit differentiation to figure a value for $\frac{dx_f}{d\theta_0}$. We set x_f as a differentiable function, and h_0 and H as both constants.

$$0 = \frac{-1}{4} \frac{-1}{(H - h_0)} x_f^2 \cos^{-2}(\theta_0) + x_f \tan(\theta_0) + h_0 \quad (10)$$

$$\Rightarrow \frac{d}{d\theta_0} 0 = \frac{d}{d\theta_0} \left(\frac{-1}{4} \frac{-1}{(H - h_0)} x_f^2 \cos^{-2}(\theta_0) + x_f \tan(\theta_0) + h_0 \right) \quad (11)$$

$$\Rightarrow 0 = \frac{-1}{4} \frac{-1}{(H - h_0)} \frac{d}{d\theta_0} x_f^2 \cos^{-2}(\theta_0) + \frac{d}{d\theta_0} x_f \tan(\theta_0) + \frac{d}{d\theta_0} h_0 \quad (12)$$

$$\Rightarrow 0 = \frac{-1}{4} \frac{-1}{(H - h_0)} \left(\left(\frac{d}{d\theta_0} x_f^2 \right) \cos^{-2}(\theta_0) + x_f^2 \left(\frac{d}{d\theta_0} \cos^{-2}(\theta_0) \right) \right) + \quad (13)$$

$$\left(\left(\frac{d}{d\theta_0} x_f \right) \tan(\theta_0) + \left(\frac{d}{d\theta_0} \tan(\theta_0) \right) x_f \right) + 0 \quad (14)$$

$$\Rightarrow 0 = \frac{-1}{4} \frac{-1}{(H - h_0)} \left((2x_f \frac{dx_f}{d\theta_0}) \cos^{-2}(\theta_0) + x_f^2 (2 \cos^{-3}(\theta_0) \sin(\theta_0)) \right) + \quad (15)$$

$$\left(\left(\frac{d}{d\theta_0} x_f \right) \tan(\theta_0) + \left(\frac{d}{d\theta_0} \tan(\theta_0) \right) x_f \right) \quad (16)$$

$$(17)$$