# Documentation for Differential Forms Summer Project

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# Abstract In this report we describe in details the constructions, theory, codings and results of the Python differential forms project obtained during the Summer Internship 2021 $\dots$

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# 1-Forms Graphical Representation

#### 1.1 Geometry of stack vectors

#### 1.1.1 Translations needed to define stack vectors and arrowheads

Stack vectors are covariant vectors, defined by planar sheets (lines, when working in 2D) perpendicular to arrows of the contravariant vector. The density of these planes, is determined by magnitude of the vector field at each point in space. These stack vectors, being covariant, correspond to differential forms, while arrow vectors (being contravariant) correspond to vector fields.

In python, these stack sheets have to be defined from the magnitude and direction of the input, based on x and y components of the 1-from.

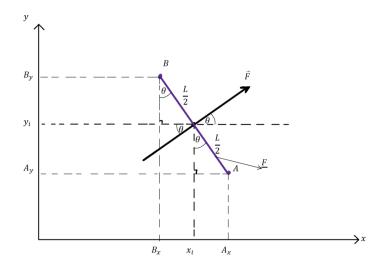


Figure 1.1: Sketch presenting the Geometrical arguments needed to define stack sheets, based on field magnitude and direction(indicated well by an arrow vector as shown)

For  $x_i$  and  $y_i$  marking the  $i^{th}$  considered position in the field, with its corresponding angle to the x-axis (ccw). Technically, points A and B as well as  $\theta$  and  $\vec{F}$  depend on the position in space that is considered, therefore, should include the subscript, 'i'. This was not added

for figure clarity.

The stack, shown in purple, is perpendicular to  $\vec{F}$  with end points A and B separated by distance L (in the code, defined as a fraction of graph scale).

From these, through simple geometry, one obtains the following equations:

$$\begin{split} A_{x} &= x + \left(\frac{L}{2}\right) \sin(\theta) \,, \\ A_{y} &= y - \left(\frac{L}{2}\right) \cos(\theta) \,, \\ B_{x} &= x - \left(\frac{L}{2}\right) \sin(\theta) \,, \\ B_{y} &= y + \left(\frac{L}{2}\right) \cos(\theta) \,, \end{split} \tag{1.1}$$

describing the positions of points A and B in terms of their Cartesian components. These also function generally as operations that displace a point on the vector in the direction perpendicular to the arrow, by a corresponding length - here by  $\frac{L}{2}$ .

To then displace the stack sheet by distance d in the direction parallel to the arrow as shown in Figure 1.2,

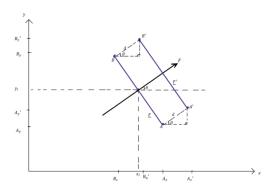


Figure 1.2: Sketch presenting the geometrical arguments needed to displace stack sheets in the direction parallel to the vector field direction at that point, (again - represented by an arrow)

we use the following translation equations:

$$A'_{x} = A_{x} + d\cos(\theta),$$

$$A'_{y} = A_{y} + d\sin(\theta),$$

$$B'_{x} = B_{x} + d\cos(\theta),$$

$$B'_{y} = B_{y} + d\sin(\theta),$$

$$(1.2)$$

which again function as general operations for such parallel displacements by any distance d, from the centre.

To define the arrowhead on that stack vector, both translation operations, eqs. (1.1, 5.2), need to be used to obatin points to be connected as shown on the figure below

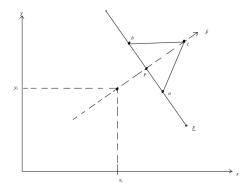


Figure 1.3: Sketch presenting the geometrical arguments needed to define the arrowhead on each stack vector)

$$\begin{split} P_i &= \left(x_i + \frac{L_s}{2}\cos(\theta_i), \ y_i + \frac{L_s}{2}\sin(\theta_i)\right) \\ a_i &= \left(P_{x,i} + \frac{L_s}{w_{head}}\sin(\theta_i), \ P_{y,i} - \frac{L_s}{w_{head}}\cos(\theta_i)\right) \\ b_i &= \left(P_{x,i} - \frac{L_s}{w_{head}}\sin(\theta_i), \ P_{y,i} + \frac{L_s}{w_{head}}\cos(\theta_i)\right) \\ c_i &= \left(x_i + \frac{L_s}{h_{head}}\cos(\theta_i), \ y_i + \frac{L_s}{h_{head}}\sin(\theta_i)\right) \end{split}$$

In these equations, variables are defined as shown on the above figure.  $L_s$  is the maximum thickness of the stack, parallel to the direction of the considered vector field,  $w_{\text{head}}$  is the width of the base of the arrowhead that rests on the last stack, and  $h_{\text{head}}$  is the height of the arrowhead parallel to the vector field direction.

Note that each has also been assigned a subscript i which does not appear on the figure. This is only done as these coordinates depend on the point in space that is currently being considered. Also note, that for a single sheet in the stack, the initial displacement from (x, y) to P must be omitted.

#### 1.1.2 General from of stack sheet positions, for any number of sheets

In the code, it was important to define the displacements of each stack sheet, form the middle position of the arrow vector, at each point in the field. Positioning of sheets depends on the magnitude of the vector field at that point in space. The larger the magnitude, the higher the sheet density. As the spread of the sheets is limited to a pre-defined maximum (on the plot, not physically), this increase in density corresponds to more stack sheets being present.

One way of plotting these, such that all sheets are equally-spaced is to consider odd and even number of stacks separately. We define them by displacing stack sheets along the arrow by certain lengths (as per the equations above) from the middle position (the considered position in the field).

For **odd number of stack sheets**, the following pattern was noticed:

For 1 sheet: no displacing is needed  $\Rightarrow \pm 0$ 

For 3 sheets: none, and ends of the stack  $\Rightarrow \pm 0$  and  $\pm \frac{1}{2}$   $\longrightarrow$  technically  $\pm \frac{1}{2} \cdot L_s$  For 5 sheets: none, ends, and points equally between  $\Rightarrow \pm 0$ ,  $\pm \frac{1}{2}$  and  $\pm \frac{1}{4}$  For 7 sheets:  $\Rightarrow \pm 0$ ,  $\pm \frac{1}{2}$ ,  $\pm \frac{2}{6}$  and  $\pm \frac{1}{6}$   $\longrightarrow$  At this point, note that  $\frac{3}{6} = \frac{1}{2}$  (obvious but important) For 9 sheets:  $\Rightarrow \pm 0$ ,  $\pm \frac{1}{2}$ ,  $\pm \frac{3}{8}$ ,  $\pm \frac{1}{4}$  and  $\pm \frac{1}{8}$   $\longrightarrow$  Again,  $\frac{1}{4} = \frac{2}{8}$  and  $\frac{1}{2} = \frac{4}{8}$  For 11 sheets:  $\Rightarrow \pm 0$ ,  $\pm \frac{1}{2}$ ,  $\pm \frac{4}{10}$ ,  $\pm \frac{3}{10}$ ,  $\pm \frac{2}{10}$  and  $\pm \frac{1}{10}$ 

These display the following recursion:

The displacement along the arrow as a fraction of total stack length L<sub>s</sub>, of the s<sup>th</sup> sheet, when drawing n stack sheets overall, for odd n is:

$$\pm \frac{s}{(n-1)}$$
,

where we require the fractional displacement (from the middle position) to not exceed half of the total length therefore:

$$1 < s < \frac{1}{2} (n-1)$$
.

For even number of stack sheets this pattern emerges:

2 sheets: $\Rightarrow \pm \frac{1}{2}$ 

4 sheets: $\Rightarrow \pm \frac{1}{2}$  and  $\pm \frac{1}{6}$ 6 sheets: $\Rightarrow \pm \frac{1}{2}$ ,  $\pm \frac{3}{10}$  and  $\pm \frac{1}{10} \longrightarrow$  Note again that  $\frac{1}{2} = \frac{5}{10}$ .

From here on continue with those not reduced fractions:

8 sheets:  $\Rightarrow \pm \frac{1}{14}, \pm \frac{3}{14}, \pm \frac{5}{14} \text{ and } \pm \frac{7}{14}$ 10 sheets:  $\Rightarrow \pm \frac{1}{18}, \pm \frac{3}{18}, \pm \frac{5}{18}, \pm \frac{7}{18} \text{ and } \pm \frac{9}{18}$ 

These display the following recursion:

The displacement along the arrow as a fraction of total stack length of the sth sheet, when drawing n stack sheets overall, for even n is:

$$\pm \frac{2s+1}{2(n-1)}$$
,

where we require the fractional displacement to not exceed half of the total length therefore:

$$1 < s < \frac{1}{2} (n-2)$$
.

Alternatively, each can be defined separately, manually, if a small amount of sheets is needed.

#### variables in stack plot code 1.1.3

This has been implemented in code. The parameters for this are as follows:

- L is the length of the positive x and y axes,
- pt\_den is the number of points along each axis,
- a is a linear scaling of the field,
- u is the vector field x-component, v is the vector field y-component  $\longrightarrow$  Alternatively: Fr is the radial component and Ftheta is the angular component
- orientation is a sting that defines how the arrows pivot,
- scale is a linear scale on the quiver plot arrows,
- delta is the extra length along the axis to show, past the defined grid, full emerging arrows from border points,
- fract is the fraction of graph length equal to stack sheet in direction perpendicular to arrow,
- s\_max is the maximum number of stacks to use,
- sheet\_L is the length of stack perp. to arrow,
- s\_L is the maximum length of stack sheet parallel to arrow,
- w\_head is the width of the arrowhead base as the fraction of the stack sheet length perpendicular to the arrow,
- h\_head is the length of the arrowhead parallel to the arrow, as the fraction of the total stack size parallel to the arrow,

#### 1.2 Initial GUI of the quiver and stack plot

#### 1.2.1 Explaining user defined functions in the GUI code

**parity**: this function takes an input of an integer and returns True (1) is it is even and False (0) when it is odd. It is useful when defining stack sheets as displacements from the middle position, as the formulas are different for even and odd number of sheets per stack.

**G**: it takes three inputs  $\Rightarrow$  s: the recursion of sheet displacing from the middle position (which pair is being completed), n: how many sheets are to plotted in total and c: which is the **bool** value from the parity function

**stack\_plot**: takes the following inputs:

- xg and yg: the grid of points to be used when plotting the field
- ax: the axis to plot on
- u and v: the x- and y-components of the vector field to be plotted

- s\_max: maximum number of sheets to plot, changes how dense the plot appears
- L: changes the size of axis (in both x and y equally, from origin)
- pt\_den: defines the number of points on each axis that create the grid
- fract: defines the size of the stack sheet (as a square) as a fraction of total graph size
- arrows (optional, default=True): Bool variable, defines if arrows should be plotted on top of the stacks (when True), or if only stacks are to be plotted (when False)
- orientation (optional, default='mid'): sets the pivoting point of the arrows about that grid point that they are defined at.
- scale (optional, default=1): Linearly scales the arrows in the quiver plot
- w\_head (optional, default=8): sets the fraction that defines the width of the arrowhead at its base (on the stack), from the total size of the stack.
- h\_head (optional, default=4): Sets the fraction that defines the height of the arrowhead parallel to the vector field magnitude at that point, from the total size of the stack.

**on\_key\_press**: Function that tracks mouse key presses, needed for the 'Matplotlib' toolbar to function

**format\_eq**: Takes a single string, converts all variables in it that are common in vector field equations, and turns them into things that python can understand. Returns the corrected string. Might be worth noting that many functions are untouched, because, to avoid issues in string replacements in compound function names, we use functions as defined by the NumPy library by importing them directly. This way the user can input their expressions in the standard, consistent, NumPy format (without the initial module name calling). The only input in our code that does not follow the NumPy format is are the exponentials, these are to be input in terms of a base e, therefore, for example: either  $e^{**}(x)$  or  $e^{\hat{}}(y)$  (both are accepted), but not exp(x). This distinction is drawn because of how Sympy simplifies powers, if there exists only one argument in the power, it removes the bracket, which breaks when is input into NumPy.

**eq\_to\_comps**: Takes the two strings given by the user (equations for the field in the x and y directions) as well as the x and y grids. Uses the above function (format\_eq) to make the string 'python readable'. If one or more of the strings does not contain x or y, it defines an array of ones and multiplies by the given constant. This is done for the component to be over all points along the grid and for shapes to match. Otherwise, it evaluates the given equation and returns the vector field components u and v in the usual way.

**vect\_type\_response**: Responds to changes in Radio-buttons that set the type of field to be plotted (arrow, stacks or both). Takes in a value from the Radio-buttons corresponding to the chosen field type. It clear the current plot. Checks which button has been selected and uses ax.quiver and previously user defined stack\_plot to create the updated graph. It then updates it on the GUI by using canvas.draw() for the canvas being defined on the main window, in its own frame. Returns no variables.

**PLOT**\_response: Responds to the 'PLOT' button being pressed. Updates the axis scaling, point density, maximum number of sheets per stack, linear scaling (' $\alpha$ ') and the new field components. Takes in no input. collects all needed variables by the '.get()' method of Tk-inter objects. After running, it plots the new specified field, with the new parameters as a stack only plot and changes the status of the Radio-buttons to one again be - stacks only (therefore for tensor (same variable name as in VFA java code) to equal 0)

**custom\_btn\_response**: when the button called 'customise' is pressed, this function responds by opening a new ('optimisation settings') window, in which features can be customised. It includes entry boxes where the user can input new values for parameters such as 'fract', 'w\_head' and 'h\_head' (described previously). These are initially filled with current values, changing them and pressing 'SUBMIT ALL' updates the plot.

**custom\_submission**: Responds to the 'SUBMIT ALL' in the new 'optimisation settings' window. When the button is pressed, the input values are globally saved. The current axis are cleared, a new plot is constructed as per the new specifications and it is displayed on the 'canvas' of the correct frame. The updated plot is initially only a stack plot, therefore the radio-buttons are returned to the original position of 'stacks'. The new window is then closed.

# **Differential Forms Calculus**

# 2.1 Mathematically: 2-forms from 1-forms, exterior derivative (on $\mathbb{R}^m$ )

The code includes a script that calculates 2–forms from a given 1–form in a specified number of dimensions. It requires input of the 1–form components respectively to their elemental 1–form (in code: string\_x, string\_y, etc.), variable arrays (in code: x, y etc.) as well as grids (in code: xg, yg, etc.) of these and a list of symbols for each variable used in the equations (coords). The code, so far, has to be changed manually to include the change of all given components from **string** type to **sympy.core.mul.Mul**. The number of used dimensions has to also be input as an integer ('m' in the code). The variable, 'expressions' has to also be appended with the correct number of components.

Python cycles over the components and the given symbols for variables, differentiating each. To improve efficiency, the derivatives have not been completed when components are to be differentiated with respect to their corresponding elementary 1-form (these go to zero). The results are saved into an  $(m \times m)$  array called 'ext\_ds'. The array is of data type 'object', as it must store strings of arbitrary length in each of its components. It stores all the found derivatives, with components changing along the rows, and variables changing along the columns. Each derivative expression is also changed into a string, This is done to append needed prefixes onto them and to later use them with the eval() function, such as brackets and negatives. Minus sings (strings) are then appended to the upper right hand-side of the matrix. This is done to correct for the elementary 2-forms being in the wrong order.

This, completed, array is then taken through loops that extract the components of each elementary 2–form. These components are symmetrical elements, therefore extracting them includes taking elements with the same i and j, switched in the coordinates. A 'pair' variable is introduced to keep track of how many times the loop extracted a pair of 2-form components and merged them. As only 2-forms are being calculated, there is always 2 components being extracted toward one elementary 2–form (including zeros as components) The number that this variable reaches is the number of components of a 2–form on  $\mathbb{R}^m$ , which was found to be given by triangular numbers. Resulting pairs are stored in an array of 1 column and a number of rows determined by the triangular number of di-

mensionality. This array is called 'result', and stores objects (it must consist of strings of varying lengths for each element). Each time a new pair is being considered, the element from 'result' is cleared to exclude the initial 'NoneType' variable present. When appending the components, it is checked that if one or more of them evaluated to zero, they are not appended. The result is printed, as a vector, whose rows correspond to different 2–form elements. The order is as follows: For m=3:

$$dx \wedge dy$$
,  $dx \wedge dz$ ,  $dy \wedge dz$ .

For m=4 these become:

$$dx \wedge dy$$
,  $dx \wedge dz$ ,  $dy \wedge dz$ ,  $dx \wedge dw$ ,  $dy \wedge dw$ ,  $dz \wedge dw$ ,

etc.

These follow the component pairs as they appear in the lower-right of the matrix (ext\_ds), in order that follows each line, until the main diagonal. It can be clearly visualised on the example of the 2-form on  $\mathbb{R}^4$  as follows:

$$\begin{pmatrix} 0 & dy \wedge dx & dz \wedge dx & dw \wedge dx \\ dx \wedge dy & 0 & dz \wedge dy & dw \wedge dy \\ dx \wedge dz & dy \wedge dz & 0 & dw \wedge dz \\ dx \wedge dw & dy \wedge dw & dz \wedge dw & 0 \end{pmatrix}$$

$$(2.1)$$

Each component of the outcome ('result') is then formatted in such a way as to be understood by python's eval() function and the evaluation of each is saved into a variable called 'form.2'. This has to be composed of m dimensional arrays, one for each elemental 2-form component (given by the triangular numbers from the used dimensions 'm').

#### **IMPORTANT - CONVENTION**

There exists a convention on  $\mathbb{R}^3$  which allows for simple matching of 2-forms to unit vectors used in vector calculus. By this convention, the elemental 2-forms used are not as stated above  $(dx \land dy, dx \land dz, dy \land dz)$ , but instead, are given by:  $dx \land dy, dz \land dx, dy \land dz$ . This allows for use of the standard Cartesian coordinates with the simple rule that the 2-forms correspond to unit vectors. This convention was not followed in this code, as it is irrational to use it in m > 3, and it was established that it shadows an important aspect of differential forms. Wedge products are not defined in extra dimensions (in a way that a curl is defined in a direction the filed does not occupy, perpendicular to it). Wedge products have their orientation defined through the axial sense (clockwise and counter-clockwise). This means that their wedge product does not occupy extra dimensions. This can only be clearly retained, as used in higher dimensions, when the convention on  $\mathbb{R}^3$  is abandoned. This is exactly what is done in the code. This code gives the 2-forms defined through clockwise (negative) and counter-clockwise (positive) orientations.

### 1-Forms Calculus

#### 3.1 Inset Plots

#### 3.1.1 Derivative Window

Selecting the 'Derivative Plot' radiobutton (top right frame) allows the user to display a small grid showing the local derivative of the field by clicking the vector field (top left frame) at the point of interest. The derivative field plots according to the 'tensor' variable (i.e. if the vector field is currently plotting with stacks/arrows, the derivative field will also.)

The radiobutton variable 'click\_option' is a tk IntVar and is converted to an integer in the response function 'click\_option\_handler'. 'click\_option' is then used to determine the required click control in the function 'on\_key\_press': if the 'Derivative Plot' radiobutton is selected, clicking calls 'deriv\_calc' which creates the plots. The feature is disabled by selecting the 'Tools' radiobutton ('Tools' option refers to the improved functionality of the matplotlib toolbar i.e. for zooming or panning.) Note: this method still needs work as the toolbar tools still function when 'Tools' is not selected.

The 'deriv\_calc' function takes the x, y data click coordinates, the pixel click coordinates to create an inset axis ('deriv\_inset\_ax') centred at the user's selected point. The parameters which determine the axis properties are:

- dpd: point density of the derivative plot (user sets via drop down menu)
- d\_length: size of the inset axis (user sets via drop down menu)
- d\_range: x and y distance from the chosen plot point over which the derivative is taken (user varies using zoom slider)
- d\_scale: scaling of the arrows in the derivative plot (user varies using zoom slider)

The plot is generated by creating new x and y meshgrids (dxg, dyg) with centres at the click data point. Previously mentioned 'eq\_to\_comps' is then called with the user defined components 'string\_x' and 'string\_y' to generate a local field 'u1' and 'v1'. The derivative is taken by subtracting the components of the central grid element from every element in the array, leaving du1 and dv1. The 'if' statement checks whether to plot with ar-

rows/stacks/both. To plot the stacks, the 'stack\_plot' function is called with changed input grids and axis to plot based on the internal parameters of the inset plot. The if/continue statement is entered this time, to prevent stacks plotting at the central grid position (as the derivative field is always zero there). Finally, the inset axis is displayed on the canvas using 'canvas.draw'.

#### 3.1.2 Zoom Window and Zoom Slider

The zoom window plots the local vector field components 'u1' and 'v1' on the 'dxg' and 'dyg' meshgrid arrays, in the same fashion as for the derivative. The zoom slider value is used in 'deriv\_calc' to decrease 'd\_range' and increase 'd\_scale' such that the plot shown takes vectors from a much smaller region of the field and makes sure they are sized appropriately. The effect of this can be seen when zooming in on a region of the plot sufficiently, such that a constant field is displayed. As for the derivative feature, low magnifications no longer produce a viable representation of the derivative field, but upon zooming the user can see the derivative field emerge (which tends to a linear field at high magnification).

#### 3.1.3 Divergence and Curl Windows

The divergence and curl plots are generated using an analytical method. The 'jacobian' function takes the string component entries from the entry boxes in the 'Field Input Frame' and calculates the Jacobian matrix using sympy partial differentiation. The resulting matrix is evaluated at the click coordinates (x\_m, y\_m) giving:

$$J = \begin{pmatrix} \frac{\partial u}{\partial x} & \frac{\partial u}{\partial y} \\ \frac{\partial v}{\partial x} & \frac{\partial v}{\partial y} \end{pmatrix}_{(x_m, y_m)}$$
(3.1)

For these plots, the 'dxg' and 'dyg' meshgrids must be centred on zero, rather than on the click coords used for the deriv and zoom plots (the first if statement in 'deriv\_calc' accounts for this.) The component equations of the divergence and curl fields are then calculated:

$$u_{\text{div}} = \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}\right)_{(x_m, y_m)} \Delta x \quad v_{\text{div}} = \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}\right)_{(x_m, y_m)} \Delta y \tag{3.2}$$

$$u_{\text{curl}} = \left(\frac{\partial u}{\partial y} - \frac{\partial v}{\partial x}\right)_{(x_{m}, y_{m})} \Delta y \quad v_{\text{curl}} = -\left(\frac{\partial u}{\partial y} - \frac{\partial v}{\partial x}\right)_{(x_{m}, y_{m})} \Delta x \tag{3.3}$$

In this notation,  $\Delta x$  and  $\Delta y$  represent displacements within the inset axis. As a result, positive curl is shown by a linear field with counter-clockwise flow and negative by a clockwise flow, as would be given by the right hand rule. Additionally, the divergence and curl plots use scaling that matches the field, which ensures that the magnitude of the vectors varies appropriately.

#### 3.2 Line Integrals

#### 3.2.1 Lines

Upon selecting the 'line integrals' tab, with the polygons drop down selection, the user can draw lines on the plot by clicking to mark the successive start and end points as required. The users click coordinates are stored in a list (LI\_coord). The function 'line\_int\_poly' takes the two most recent entries in the list of coordinates and finds the approximate line integral using the following method:

- Small displacements along the line in the x and y directions are calculated based on the last two entries in LI\_coord (coords of points a and b) and the chosen number of intervals along the line, N.  $dx = \frac{1}{N}(b_x a_x)$ ,  $dy = \frac{1}{N}(b_y a_y)$
- A 2xN array 'intervals' is created and stores the coordinates of the points along the line which will be used in the final calculation. This is achieved using a for loop; intervals $(x_k) = a_x + kdx$ , intervals $(y_k) = a_y + kdy$
- Next the vector field components must be evaluated at each of the interval points along the line. These components are stored in the 2xN array 'uv\_store'.
- The line integral is approximated by summing the products of the small displacements dx and dy with the respective vector field components at each interval point. Since the displacements are the same along the straight line, the sum is simplified to:

$$\int_{a}^{b} \vec{F} \cdot d\vec{l} \approx \sum_{k=0}^{N-1} \vec{F}(x_{k}, y_{k}) \cdot d\vec{l}(x_{k}, y_{k}) = dx \sum_{k=0}^{N-1} F_{x}(x_{k}, y_{k}) + dy \sum_{k=0}^{N-1} F_{y}(x_{k}, y_{k})$$
(3.4)

Here,  $\vec{F} = F_x \hat{i} + F_y \hat{j}$ ,  $\vec{dl} = dx \hat{i} + dy \hat{j}$  and  $(x_k, y_k)$  denotes the coordinates of the  $k^{th}$  interval point along the line. Each successive line integral is added to the total and displayed in a GUI label. The reset button clears the plot, the list of coordinates and the total, allowing the user to start from scratch.

This function operates not only over single starlight lines but also joins them head-to-tail to create polygonal shapes by accessing previous mouse click coordinates from LI\_coord. The polygons can be closed by clicking near **any** previously clicked point. This is coded by defining these coordinates as equal when the distance between them is smaller than a selected interval 'ctol'. Which is set to be 0.1 (in axis units).

This function also plots a square grid to aid the user in drawing rectangles on the plot, without the need for an additional function to draw squares. This grid is removed when any other option is selected.

#### 3.2.2 Circles

Selecting the circles drop down option will allow the user to plot circles on the vector field, updating the position and radius (user selected by entry box) upon every click. Circles are centred on click location. The user is also allowed to select the orientation of the integral by use of a button. This button displays the currently used orientation, and changes when it is clicked (between 'cw' and 'ccw'). To redo the calculation with the newly selected orientation, the plot has to once again be clicked.

The main difference from the calculation of straight line integrals is that the displacement vectors are no longer constant, as they will be tangent to the circle at each interval point. The method is as follows:

- Define the small displacements dx and dy (arrays) for the N interval points using  $dx_k = -A\sin(kdt)$  and  $dy_k = A\cos(kdt)$  (changed to negations using an if-else statement, depending on chosen orientation). dt is a small angle increment and is stored as an array in the code (linspace from 0 to  $2\pi$  with N points.) A, the magnitude of the displacement vector is chosen to be the length of the circumference swept out by each angle increment,  $A = \frac{2\pi R}{N}$ .
- Calculate the coordinates of interval points: intervals( $x_k$ ) =  $x_m$ + $A\cos(kdt)$ , intervals( $y_k$ ) =  $y_m$  +  $A\sin(kdt)$ . ( $x_m, y_m$ ) are the coordinates of the users click.
- Evaluate the vector components at each interval point as before.
- Find the total line integral using:

$$\oint_{\mathbf{k}} \vec{F} \cdot d\vec{l} \approx \sum_{k=0}^{N-1} F_{x}(x_{k}, y_{k}) dx_{k} + \sum_{k=0}^{N-1} F_{y}(x_{k}, y_{k}) dy_{k}$$
 (3.5)

#### 3.2.3 1-D "Flux"

The flux through a closed surface is given by the expression:

$$\oint \vec{F} \cdot d\vec{A} \tag{3.6}$$

In the 2D plane in which we are plotting the vector fields and taking integrals, we modify this definition such that the surface normal infinitesimal vectors dA are normal to the curve drawn by the user at each interval point,  $dA = dx_{norm}i + dy_{norm}j$ . For the circular curves, these vectors are radial, pointing away from the centre and are calculated at each interval point by:  $dx_{norm} = A\cos(kdt)$ ,  $dy_{norm} = A\sin(kdt)$ . Apart from this difference, the total flux through the curve is evaluated in the same way as for the line integral and the orientation of the curve (whether it is drawn clockwise or counter-clockwise) is not important. As for the polygon feature, where the user may draw a shape manually, the orientation of the drawn curve is important. The chosen method to ensure that the normal vectors point outward from the enclosed area of the curve is as follows:

• Initially define the normal vectors as the small displacement vectors (see section 3.2.1 'Lines') rotated by  $\frac{\pi}{2}$  radians **clockwise** (cw). For example, if a line is drawn to go vertically upwards,

$$\vec{dl} = dx\vec{i} + dy\vec{j} = 0\vec{i} + dy\vec{j}$$
$$\vec{dA} = dx_{norm}\vec{i} + dy_{norm}\vec{j} = dy\vec{i} + 0\vec{j}$$

More generally, the transformation is described by

$$dx_{norm} = dy$$

$$dy_{norm} = -dx$$

• Using this, the flux for each line (flux\_inc in the code) is found by:

$$dy \sum_{k=0}^{N-1} F_x(x_k, y_k) - dx \sum_{k=0}^{N-1} F_y(x_k, y_k)$$

and upon each line being drawn, the total 'flux' is updated adding each increment flux\_inc.

- When the program detects the user has closed the curve they are drawing, the signed area of the curve is calculated using the function 'calc\_area'. The function uses the 'shoelace formula' which effectively calculates the area of each triangle making up the polygon defined with vertices given by successive user clicks. If the area returned is positive, the polygon was drawn in a ccw direction, and if negative, cw.
- By rotating dl cw at every interval point, the vectors are correctly pointing outwards if the curve is drawn ccw, so no change is needed and flux is a true value. Whereas if the curve was drawn cw, the vectors are pointing in towards the enclosed area and the computed result is negative what it should be. Thus, the result is multiplied by -1 in this case.

#### 3.2.4 Stokes Theorem and Divergence Theorem

Examining the expression for Stokes theorem (Green's theorem as we are working in 2D),

$$\int_{S} (\nabla \times \vec{F}) \cdot d\vec{A} = \int_{S} (\nabla \times \vec{F}) \cdot \vec{k} dA = \oint_{C} \vec{F} \cdot d\vec{l}$$
(3.7)

we can see that the scalar curl (z component of the curl) at the centre point of the curve C with enclosed surface S can be approximated for small areas using:

$$\int_{S} (\nabla \times \vec{F}) \cdot \vec{k} dA \approx (\nabla \times \vec{F}) \cdot \vec{k} Area \approx \oint_{C} \vec{F} \cdot \vec{dl}$$
(3.8)

$$(\nabla \times \vec{\mathsf{F}}) \cdot \vec{\mathsf{k}} \approx \frac{\oint_{\mathsf{C}} \vec{\mathsf{F}} \cdot d\hat{\mathsf{l}}}{\mathsf{Area}} \tag{3.9}$$

So, an approximation for the local curl can be approximated as 'ratio' in the program by taking a circle line integral centred at the point of interest and decreasing the radius using

the entry box until the value converges. Similarly this can be done for the divergence by looking at the flux to area ratio. For linear fields, the respective ratios should always show the curl and divergence, since taking first order derivatives of linear expressions will give constant values (will add more on this later).

#### 3.2.5 Showflux

# 2-Forms Graphical Representation

# **4.1** Non-unique graphical representations of 2-forms on $\mathbb{R}^2$

#### 4.1.1 Blocks and stacks

Two alternative ways of representing 2–forms have initially been considered. Both of which were later established to be not the right approach. These are still discussed here, for record and, as it is believed to give good insight into problems that arise when attempting this task. The first, simpler method considers the 2–form magnitude at different points in space and represents them as squares, whose size is determined by the magnitude, and whose colour shows the orientation, obtained by the sign of the 2–form at that point. This method has been dubbed as plotting 2–forms through 'Blocks'.

The plotting of these is completed by defining rectangular patches, provided by the matplotlib library. The size of each rectangle is defined in terms of a fraction of a user defined total (customisable) and depends on the relative, unitary magnitude of the 2–form, with respect to its maximum value over the defined region.

Due to the simple approach of this method, no coding complications occur. The 2-forms are simply represented. However, they do not clearly show the most important characteristics of 2-forms. They, by requirement: have gaps between them, will overlap if magnitudes are large enough and in no way graphically represent the idea of 2-forms being elemental areas through which integration can be completed.

A graphically clearer way of representing 2-forms is through the superposition of stacks from elemental 1-forms. This process includes finding expressions for fields in the x and in the y directions such that the desired 2-form is being represented. These are then plotted using the x field for stacks in the x-direction and the y field for stacks only in the y-direction.

The result forms a grid that covers the defined region with squares, whose inside is dissected into further sections (separately in the x and in the y directions), depending on the 2–form magnitude at that position. More dissections occur inside, depending on which component of the 2–form is dominant at that position. This dominating is defined through the expressions of 1-forms that are being superposed.

This approach clearly presents all characteristics of 2-forms. The region is covered, no

overlap is allowed and it can be seen how integration over such areas can yield known results. Another characteristic which, through this, can be reproduced is merging of 2–form 'tubes' on  $\mathbb{R}^3$ , which we will return to later.

However, there exist major issues with this approach (which will also be explained in more details in the coming subsections). These include the above-mentioned processes of finding 1–forms that reproduce the desired 2–form. This has been attempted through two approaches, un-doing the exterior derivative, or through undoing a wedge product. Both of which give the desired 2–form in terms of component 1–forms.

#### **4.1.2** 2-forms on $\mathbb{R}^2$ through the exterior derivative

One way to obtain a 2–form from component 1–forms is to ask the user for a 1–form and compute the exterior derivative of it. This way, both are known, the 2-form and the 1-form that it originated from. To complete the above mentioned process, the input 1–forms can be differentiated (as in the Jacobian) and the skew-symmetric parts can be taken (these are the components that form the resulting 2–form). These components can then be plotted as stacks in the x-direction (differential of the dx component w.r.t y) and in the y-direction (differential of the dy component w.r.t x). However, there exists a problem with this procedure, and that is, the non-uniqueness of the result. Many 1-forms may become the same 2-form upon the exterior derivative, due to cancellations occurring between  $dx \wedge dy$ and dy  $\wedge$  dx components. This means that, the graphical representation of a given 2-form will vary, depending on its origin. Which should clearly not be the case, as the 2–form should be its own, separate, object, defined uniquely in space. The cancellations could be solved if code was written that would scan the two resulting equations for any cancelling or merging components and delete or distribute them (respectively). This would be difficult and is not needed. This is because this process will still make the 2-form not unique, it will simply be another representation. There also exists a much simpler method, which we will come back to.

A method of excluding such cancellations was found and implemented such that given 2–forms yield identical representations. This was done through, first obtaining the mathematical expression of the 2–form through the exterior derivative as described previously. The result was then simplified by changing it to a 'SymPy' expression and using the 'simplify' function. Once this was completed, the 2–form was split into two, equal elements,  $dx \wedge dy$  and  $dy \wedge dx$ , which determine the derivatives of 1–form components that can be used to plot stacks as described previously. Once again however, this was established not to be fully functional. The issue now was, the splitting of the 2–form is also not unique, it is arbitrary. Any splitting will work, so long as the components return the same 2–form when merged (by inverting the elementary 2–form and adding).

#### **4.1.3** 2–forms on $\mathbb{R}^2$ through the wedge product

There exists yet another way of defining 2–forms through stacks that represent 1–forms. This includes splitting the 2–form into components, not into  $dx \wedge dy$  and  $dy \wedge dx$  that are understood to originate from the exterior derivative, but into  $f(x,y)dx \wedge g(x,y)dy$ , where the 2–form is  $f(x,y)g(x,y)dx \wedge dy$ . This yields another issue. Similarly to the last

considered method, the splitting of the 2-form into a wedge product of two 1-form is not unique. Again, as above for the previous method, it is also possible here to let the user input two 1-forms to wedge together into a 2-form, but once again, this may also include cancellations or merges between components, which make the 2-form not unique.

#### 4.1.4 Lessons learnt

To conclude, any graphical representation of 2–form that is built by superposing two 1–form stackings will be different for different combinations of 1–forms (that algebraically produce the same 2–form). This can be simply put as "the algebraic and the geometric representations don't commute", that is:

let  $\alpha$ ,  $\beta \in \wedge^1(\mathbb{R}^2)$ ,  $\omega \in \wedge^2(\mathbb{R}^2)$  such that  $\alpha \in A$   $\beta = \omega$ , where A represents the algebraic operation (in our examples  $A = \wedge$ ) and let G be the geometric operation, then

$$\left. \begin{array}{l} G(\alpha \ A \ \beta) = G(\omega) \\ G(\alpha \ A \ \beta) = (G(\alpha) \ G(A) \ G(\beta)) \end{array} \right\} \rightarrow G(\omega) \neq (G(\alpha) \ G(A) \ G(\beta)),$$

where in the first line A acted first, and in the second line G acted first. The one secret here that we probably 'misunderstood' is G(A) or G(A). So, what is the geometric analogue of wedging? In the examples mentioned we applied the wedge geometrically as superposition of vertical stacks (say  $G(\alpha)$ ) and horizontal stacks (say  $G(\beta)$ ). If our interpretation is correct, then what was found is fundamental. As clear and intuitive as this method seems to be for graphically representing 2–forms, it does not provide a unique way of doing so. In fact, given a 2–form, all the graphical representation that starts from 1–forms stackings are related by coordinate transformation. To present this idea more clearly, let's look at the more rigorous proof of the above stated non-uniqueness which arises through splitting the 2–form.

#### **4.1.5** Proof of the non-uniqueness of 2-forms

I will add this soon ... (Moustafa)

#### **4.1.6** Initial 2–form representation as stacks in code

Due to the fact that unique representations could not be deduced. The code we produced initially allowed the user to choose, what representation they would like to see.

User-supplied 2-forms were being plotted as stacks by splitting the expression into two components  $dx \wedge dy$  and  $dy \wedge dx$ . The splitting of the expression was set by the user via the 'set splitting' button (by default splitting occurs into two equal halves). These have then been plotted as previously stated, one as the x component and the other as the y component. This plotting was done via a function ('form\_2\_components\_plot') which is very

similar in operation to stack\_plot. The new function however, also uses the end 2–form expression, evaluates it numerically, finds its sign and depending on this, colours the stacks (it is still used in the end version of the code). It was chosen to colour via the convention that grey signifies zero magnitude at that position, red represents positive (axially ccw) 2–form magnitude and blue stands for negative (axially cw) magnitude. Because 2–form areas must fill space, this function includes a variable that sets the minimum number of stacks ('s\_min') to two. This way, full squares are always being displayed and then dissected depending on magnitude, but will not become open areas. Also, to avoid the same issue, the size of stacks (initially set by the user as a customisation option) is now calculated from the chosen number of points along each axis automatically to fill space (this occurs when tabs are opened and when the number of points is changed). The equation by which this is done is the following:

$$d = \frac{2}{n-1} \tag{4.1}$$

for the stack size d and the number of points along the axis n.

2-forms from the exterior derivative were plotted by a similar process as above, with the initial addition of finding the mathematical expression of the 2-form and simplifying it (as has been described above) by the find\_2\_form function. Once the 2-form was found, it was input into the entry box for 2-forms and was highlighted in light green to show what is currently being displayed (as opposed to other options including the supplied 1-forms). This process of highlighting is still used in the end resulting code.

2-forms through the wedge product is (same as in the end resulting code) completed by first asking the user to input two 1-forms that are to be wedged together, in terms of their components in dx and dy (other on  $\mathbb{R}^3$ ). This is done by displaying a new window for these inputs after the 'wedge' button is pressed. Once these are submitted this extra window is closed, although its entries are saved and display again when it is re-opened. The inputs are simplified by briefly passing them into 'SymPy' expressions. The components of these inputs were then calculated using the previously described 'eq\_to\_comps'. The 2-form was found by concatenating strings of input in such a way as to result in the correct 2-form. This was also simplified in the same way and displayed in the 2-form entry box, which, once again, light up to a light green. The plotting of superposing stacks was then completed by using the stack\_plot function with disabled arrowheads.

Mathematically, given  $w_1 = f(x,y)dx + g(x,y)dy$  and  $w_2 = h(x,y)dx + m(x,y)dy$ . The 2–form on  $\mathbb{R}^2$ ,  $\alpha$ , must be made up of:

```
\alpha = w_1 \wedge w_2 = f(x,y)dx \wedge m(x,y)dy + h(x,y)dy \wedge g(x,y)dx= f(x,y)m(x,y)dx \wedge dy + h(x,y)g(x,y)dx \wedge dy= (f(x,y)m(x,y) - g(x,y)h(x,y))dx \wedge dy
```

which is used to be found by and plotted as stacks when an if condition was satisfied, stating that none of the entries were zero. Currently, this is still being used, to find the 2–form mathematically. Two rectangular stacks with the scaling factor were accounted to by giving similar colours to the vertical and horizontal stacks (red and green). After the first rectangular stacks were added the second group either sat on top of the first (in which case scaling contribution was zero) or sat in some gaps, hence increasing the density as result of its scaling function. If any of the coefficient functions (f, g, h or m) were zero, the stacking reduced to one function together with its elemental 2–form  $dx \wedge dy$ , these were executed in the 'elif' options under the if statement. This code, although it did not use splitting, and included cancellations was also incorrect. This was because, the 2–form did not fill space, its x and y contributions were implied by density of long vertical and horizontal lines that span many stacks etc.

#### 4.1.7 2-form representation as blocks in code

The simpler method was also implemented to show the comparison between the locally detailed, non-unique (stacks) and locally undefined, global, unique (blocks). Despite the fact that we have now established that blocks are not the best representation, an option to plot them was still implemented to highlight the difference between unique and non-unique representation methods. This was more simply implemented by defining the above described process of plotting blocks in a single function and calling it with the appropriate 2–form whenever necessary. The option as to which should be used was given to the user through radio buttons, however, when stacks was selected, a message box displayed, warning the user of the non-uniqueness of the result and its dependancy of their splitting choice.

#### **4.2** Correct 2-form on $\mathbb{R}^2$ representation

A unique, locally detailed, space filling representation of 2–forms has been found. This is the representation currently used by the code. It continues the idea of representing 2–forms as superposition of stacks, however, no longer as a superposition of two separate 1–forms. The way it is currently done is through using the 2–form scaling function to stack each unit square  $dx \wedge dy$  depending on their positions in space. This means that the starting point in stacking is the 2–form itself and not the constituting 1–forms which renders this stacking representation of each 2–form unique. Evidently, this is equivalent to equally splitting the 2–form in the previous representation, but without having to make any choice on how to "geometrize" the  $\wedge$ . Thus it was established that this representation is fulfilling.

The reason for that statement is the following. The 2-form, to be correctly represented must contain information about oriented areas, and how their number varies in space. It was originally thought that the information about such variation must be included in the dominant component (x or y of the 2-form, at that position). However, this can also be more simply represented by looking at variation in the number of areas at neighbouring positions.

The current method of plotting relies on constructing a space filling, square gird and dissecting each square (equally in the x and y) depending on the 2-form magnitude at that position. This guarantees uniqueness as the magnitude is well defined, and it continues to display the variation, when the grid is fine enough and s\_max value is chosen to be sufficient. The splitting ambiguity can be thought of as confusion by attempting to split these squares not by the 2-form alone, but by considering extra information - dominance of the dx or dy component. This information is not contained in the resulting 2–form, and therefore, of-course it cannot be reliably, clearly represented. The problem can (on some level) be compared to being given an area to draw (the 2-form) and saying that this cannot be done because the shape was not given (1-forms). Yes, the shape will not be known, but it is arbitrary and is not contained in the asked task (of drawing an area, the 2-form). In this analogy, our method can be compared to responding to such a task by drawing many small squares whose total area matches that given area. The task has been accomplished, and it can easily be seen how these can distribute over space to different shapes. We draw squares, not rectangles in x and y, but the variation over these can easily be seen by the number of these squares over the region changing.

It may also be noted that this idea was sparked by the problem of cancellations, which was found to be the case of correct arithmetic, but incorrect geometry. Mathematically, the components will cancel to give the same 2-form, however, when attempting to display the 2-form in terms of 1-forms this cancellation will not be geometrically valid. Hence, the 2-form can always (mathematically) be found as two 1-forms, however, to represent it graphically, we must abandon this approach. Surely it is correct, but it is not necessary to represent 2-forms. All that is needed is the 2-form itself.

This has been implemented by simply removing options to plot blocks and to choose splitting factors, instead, the 2–form was simply plotted by the same function as previously, half in the  $\mathfrak u$  and half in the  $\mathfrak v$ .

# 2-Forms Calculus

#### 5.1 Interior derivative acting on 2-forms

The code includes the option to calculate the interior derivative of a 2–form (and a 1–form) on  $\mathbb{R}^2$ . *Note: it has not yet been generalised to*  $\mathbb{R}^3$ . After pressing the button ('interior derivative'), a new window displays, which asks the user to chose which option to evaluate with. The interior derivative can be applied to a 2–form only, or to a 2–form and 1–from simultaneously. Once the option is chosen, it asks the user for a vector field to do the calculation with respect to in terms of the x and y components. The two windows are then shut.

To complete the interior derivative of the 2-form, the code takes given inputs (2-form and 'background' vector field), formats and simplifies them (as before) and calculates the resulting 1-form by the standard procedure (thanks to linearity of the interior derivative):

$$\iota_{\vec{\mathfrak{u}}}(\omega) = \mathfrak{f}\mathfrak{u}_1 d\mathfrak{y} - \mathfrak{f}\mathfrak{u}_2 d\mathfrak{x} \tag{5.1}$$

where  $\omega = \mathrm{fdx} \wedge \mathrm{dy}$ ,  $\vec{\mathrm{u}} = \mathrm{u_1} \mathrm{dx} + \mathrm{u_2} \mathrm{dy}$  and  $\mathrm{f}$ ,  $\mathrm{u_1}$  and  $\mathrm{u_2}$  are scalar functions on  $\mathbb{R}^2$ . This is found numerically and as a string, to be able to plot it, and to be able to display it to the user. This resulting 1–form is put into entries for 1–form components and the boxes are coloured into light green to show that these are currently displayed. The result is plotted using the 'form\_2\_components\_plot' function with  $\mathrm{u}$  and  $\mathrm{v}$  given by the expression as shown above. This function is used as opposed to 'stack\_plot', as it also includes colouring of stacks, depending on the sign of the original 2–form at that location. This process is specified in the 'Int\_deriv\_2\_form' function. This is called when the selected option is '2-form only' by the 'Int\_deriv\_22\_form' function.

To complete the interior derivative of the 2-form and the 1-form a similar process is completed, but the 1-form is also taken into account. The 1-form calculation is completed by a function called 'Int\_deriv\_1\_form'. The two functions are separate in order to be able to more easily call their combinations when user wished to use both, or each one separately. This function completes a similar process to the above described (for 2-forms) however, it is based on a different equation, as follows:

$$\iota_{\vec{\mathbf{u}}}(\omega) = \mathsf{f}_{\mathsf{x}} \mathsf{u}_1 + \mathsf{f}_{\mathsf{y}} \mathsf{u}_2 \tag{5.2}$$

where  $\omega = f_x dx + f_y dy$  and  $\vec{u}$  is as defined previously. The result is a zero form (scalar function), which can be most easily represented via its contours. Because in the GUI, there exists no entry box for a zero from, the result of that is displayed underneath the 1–form entry box in red, as a Tkinter label.

When the two require being computed together, both functions are called with appropriate canvas preparation by the function 'Int\_deriv\_21\_form'. This finds the result of the 2-form, which returns a vector field, which 'sits on top of' the computed 1-form. This can visualised as a vector field lying on a scalar function landscape.

These functions are called by a response to the PLOT button in the window where the user defines the background vector field. Depending on which option was selected in the previous window ('2-form only' or 'both'), The plot button binds to different functions and hence responds appropriately.

#### 5.2 Hodge

NOT IMPLEMENTED YET

# **Differential Forms on** $\mathbb{R}^3$

# **6.1** Representing 2-forms on $\mathbb{R}^3$

On  $\mathbb{R}^3$ , 1-forms are parallel, two dimensional sheets, perpendicular to the elemental 1-form. 2-forms can thus be represented as intersections of such sheets, forming tubes, which define elemental, oriented areas that are the 2-form. This is very difficult to show on a solid, rotating grid of many, small intersecting sheets, therefore a different approach has been used. The code lets the user inspect planes though a three dimensional cube by selecting the viewing axis and the depth into the solid. This, visually, gives the same looking 2-forms. This is because the viewer is slicing through the tubes at a selected height.

As the sheets are defined by stacks which run perpendicular to their corresponding direction, if any component of the viewed 2-form was in the direction of the axis along which the viewer is looking, the tubes would not be pointing in their direction and thus would be closed. Therefore:

- Viewing from the z axis, only the 2-form components in  $dx \wedge dy$  would be apparent
- Viewing from the y axis, only the 2-form components in  $dx \wedge dz$  would be apparent
- Viewing from the x axis, only the 2-form components in dy  $\land$  dz would be apparent

The process of calculating and plotting these is similar to the previously defined process used in plotting two forms on  $\mathbb{R}^2$  (the new, corrected one). The initial methods for representing 2-forms (blocks and 1-form splitting) have initially also been implemented here, but have since been changed to correctly display.

This time the 'result' calculated by the two form finder (described previously) has three entries, each of which needs to be split into two equal parts (again, used to be customisable by the user, to display non-uniqueness when represented using split 1-forms. That process used six components (two for each plane) calculated from the found 2-form, which were plotted as stacks. Only three of which are now needed because the new representation is identical to equal splitting, however, the six were kept in the code. This is because that allows us to still use the eq\_to\_comps function, which always works with two inputs. These are then plotted similarly to the process of doing so on  $\mathbb{R}^2$ . It is done by a function (form\_2\_components\_plot\_3), nearly identical to the one used on  $\mathbb{R}^2$ , with the

change that this one accepts all parameters in three dimensional grids and splits them correctly to corresponding planes, which is completed through slicing. This slicing is done an if-elif-else statement, one test for each axis projection. These deal with slicing grids, stack components and the slicing of the 2-form signs array. The strange thing about this slicing is that, due to the way meshgrids are defined; while the component along the z axis is in fact a slice of [:,:,height] as expected. The x and y slicing is switched. Also, singularities now not only must be excluded in the components (or in the magnitude) but also when the 2-form sign is to be taken. It may also be noted that this function, as the corresponding one on  $\mathbb{R}^2$ , also has (for the same reason) s\_max set to two.

An extra process is required to make tubes update in the viewing axis accordingly to changing the height along it. This is because when expressions are proportional to functions of the viewing axis coordinate, they would not scale, they would simply be an additional constant that would vanish in the representation because of our applied relative scaling of stacks. A global scaling needs to be applied to correctly handle this. This is done by finding the maximum value across all height points (excluding singularities), defined globally, for that two form component, dividing the local maximum (in the plane) by that global maximum and multiplying the relative scaling array by that value.

It may be worth noting that a slider has not been implemented to complete the process of changing the viewing height along the viewing axis. This was due to issues with Tkinter sliders, in getting them to go up in any, user defined intervals (without rounding, as then the exact value has to be found in the array to obtain its index for slicing).

# Singularities

It was noticed when experimenting with the Vector Field Analyser https://math.la.asu.edu/~kawski/vfa2/index.html that singularities in fields break the code. Worst of all, singularities that fall on or near grid points, break the linear scaling, making the entirety of it plot as a zero field (relatively). Not only that but singularities were not displaying when off the grid, and undefined regions were simply not plotted. We have decided to input such options into our code.

To begin with, there are some issues with the ideal scenario of finding all singularities, plotting them on and excluding them from scaling. However, this is difficult mainly due to the fact that no function has been found that will record singularities in mathematical expressions above  $\mathbb{R}^2$ . Only SymPy 'singularities has been found' which functions for single variables functions and has inconvenient outputs (for plotting).

Many attempts were made to include such in our code, with limited success. The end result includes a three way mechanism for coping with singularities. First of all, if any such points (including not a number evaluations, infinities and values above 1e15 that python at times mistakes for infinities) lie on a grid point, they are removed and plotted on. If the value was large, or infinite (according to python evaluation), it is plotted as a red circle. If it was evaluated as NaN, it is plotted as a grey square. If singularities lie off grid points, two options are given to the user. They can search through the region with a finer grid of a chosen number of points per side, or define their own singularity.

If they choose to search, the code runs through a grid of finer points (as specified) looking for on grid large values (above 1000), or infinities and plotting them as described above (but smaller). The mechanism for doing to is made for efficient by not saving all points to evaluate at, however, it can still be very slow for very fine grids, therefore the user is warned of slow processing if the value they input is above 200 per axis.

If they choose to define their own singularities. They can do so by defining an equation in y, an equation in x or by supplying point coordinates. This will plot the given equation on the graph. These plots will stack if more than one is given. Many expressions can also be input simultaneously by separating them with a semi-colon (';'). If the expression in y is input in terms of y only (or conversely the x expression is in terms of x only), it is assumed to be and error and is plotted as if the opposing variables was given. For example, inputting  $x = \sqrt{4-x^2}$ , instead of solving the equation for x , a line of  $x = \sqrt{4-y^2}$  is plotted.

The point option accepts points in the format:  $x_1,y_1;x_2,y_2$ . Here,  $(x_1,y_1)$  is the first point

to be checked and  $(x_2,y_2)$  is the second. The code does not accept brackets surrounding the point coordinates.

When an expression or a point singularity is input, the code will check for singular points along it. If it does not find any (not even a single point), it will warn the user that the code could not find any singularity at their asked positioning. Perhaps it is worthy of note that, despite such warning being showed, as asked, the lines/points checked will be plotted regardless. It is also important to note that the code will not display this, even if most points evaluate not to be singular. This has been implemented because evaluations are not very exact and can at times be faulty.