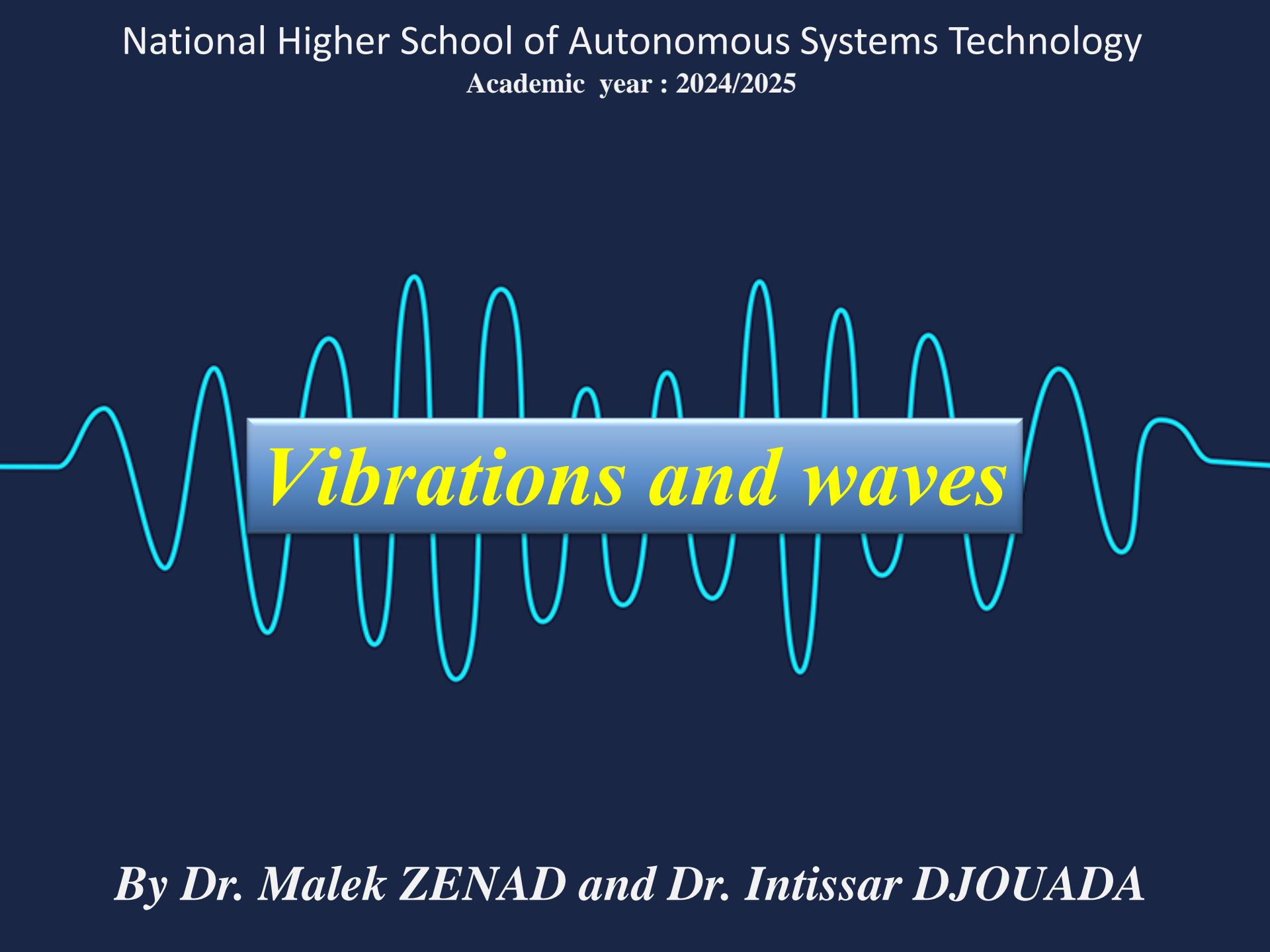


National Higher School of Autonomous Systems Technology

Academic year : 2024/2025



# *Vibrations and waves*

*By Dr. Malek ZENAD and Dr. Intissar DJOUADA*

# Chapter 2 : Free vibration of undamped single degree of freedom systems

$$\frac{d}{dt} \left( \frac{\partial(L)}{\partial \dot{q}} \right) - \frac{\partial(L)}{\partial q} = 0$$

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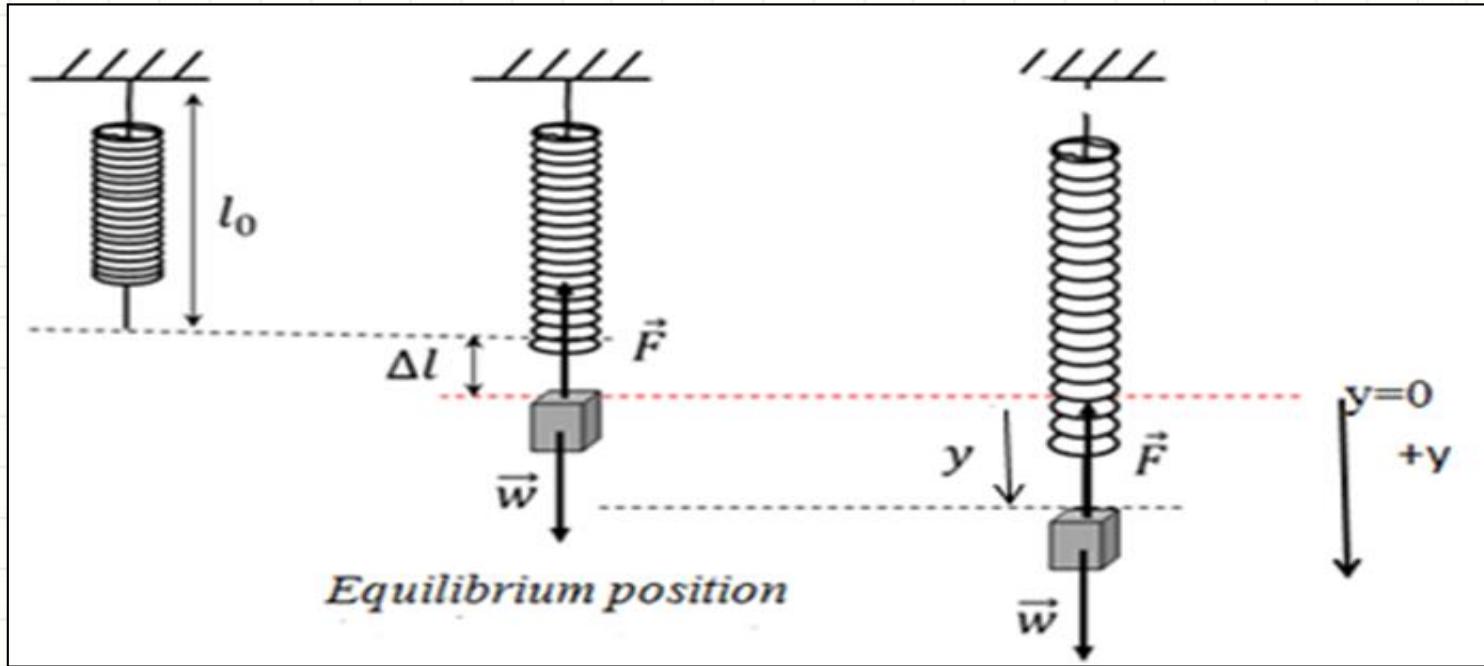
**3- Simple Pendulum**

**4- LC circuit**

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

Consider the single-degree-of-freedom (SDOF) system shown in the figure below. The spring is initially in the unstretched position. It is assumed that the spring obeys Hooke's law.



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass- spring

- **Hooke's law** describes the relationship between the force exerted by a spring and its extension or compression. The law is expressed as:

$$F = -k \cdot x \quad \text{or} \quad F = -ky \quad \text{Where:}$$

- F is the force exerted by the spring (N),
  - k is the spring constant or stiffness (N/m),
  - x is the extension or compression of the spring from its equilibrium position (m).
- The negative sign indicates that the force exerted by the spring is always in the opposite direction of the extension or compression. This force is known as the **restoring force** because it works to return the spring to its equilibrium position.

## Chapter 2 : Free vibration of undamped single degree of freedom systems

## **1- Vertical mass-spring**

### a) Using Newton's Second Law

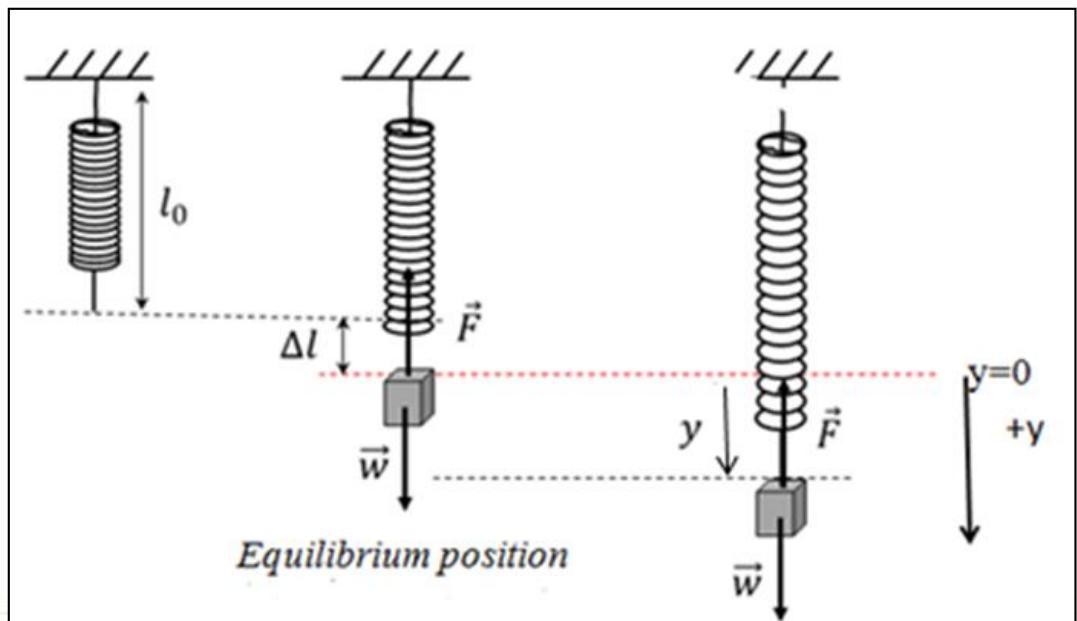
When the mass  $m$  (**weight  $W$** ) is applied, the spring will deflect to a static equilibrium position

$l_0$ : The spring's natural length

- At equilibrium:  $y=0$

$$\sum \vec{F} = \vec{0} \quad \Rightarrow \quad \vec{W} + \vec{T} = \vec{0}$$

$$\Rightarrow \Delta l = \frac{mg}{k}$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

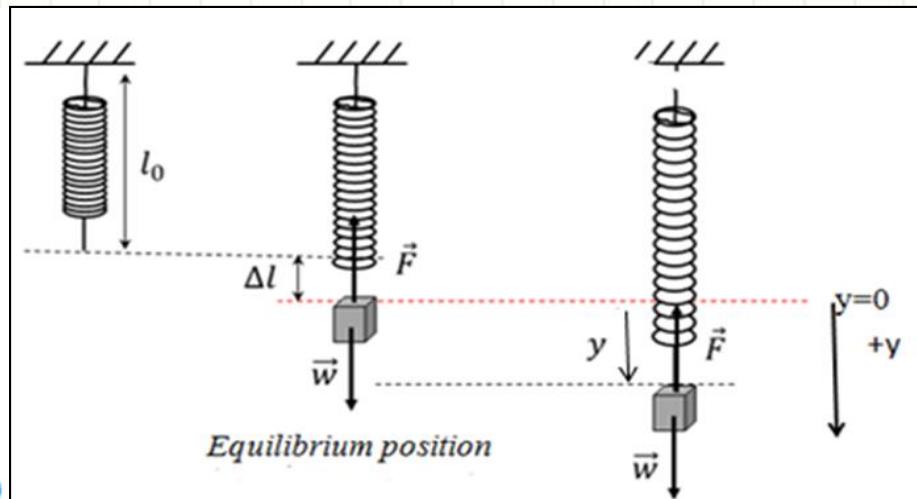
- When the system is in motion:

$$\sum \vec{F} = m\vec{a} \Rightarrow \vec{W} + \vec{T} = m\vec{a}$$

Oy:  $mg - k(y + \Delta l) = ma$

$$mg - k\Delta l - ky = ma \dots \dots \dots (2)$$

According to equation (1)  $mg - k\Delta l = 0$



$$(2) \quad ma + ky = 0 \Rightarrow m\ddot{y} + ky = 0 \Rightarrow \ddot{y} + \frac{k}{m}y = 0$$

$$\Rightarrow \ddot{y} + \omega_n^2 y = 0 \quad \text{Where} \quad \omega_n = \sqrt{\frac{k}{m}}$$

$\omega_n$  is called natural frequency

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

#### b) Using Lagrange's equation

The **Lagrangian**  $L = T - U$

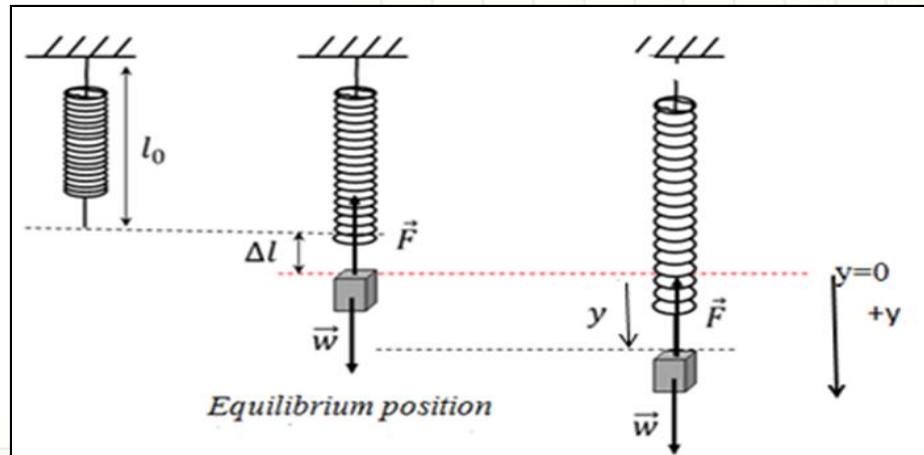
$$\vec{r}_m \begin{pmatrix} 0 \\ y \end{pmatrix} \Rightarrow d\vec{r}_m \begin{pmatrix} 0 \\ dy \end{pmatrix} \Rightarrow \vec{v} \begin{pmatrix} 0 \\ \dot{y} \end{pmatrix}; \vec{w} \begin{pmatrix} 0 \\ mg \end{pmatrix}$$

➤ Kinetic energy

$$T = T_m \Rightarrow T = \frac{1}{2} m \dot{y}^2$$

➤ Potential energy

$$U = U_m + U_k$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

$$U = - \int_0^y \vec{W} \cdot d\vec{r}_m = - \int_0^y mg dy = -mgy$$

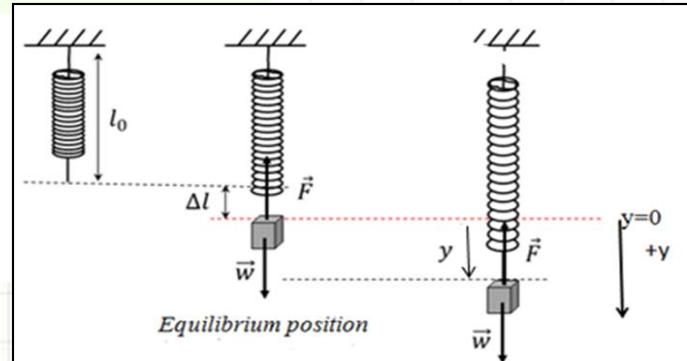
$$U_K = \frac{1}{2} k(y + \Delta l)^2$$

$$U = \frac{1}{2} k(y + \Delta l)^2 - mgy \dots\dots\dots(3)$$

At equilibrium  $\left. \frac{\partial U(y)}{\partial y} \right|_{y_{eq}=0} = 0 \quad k(y + \Delta l) - mg \Big|_{y=0} = 0$

$$\Rightarrow \Delta l = \frac{mg}{k} \dots\dots\dots(4)$$

By substituting equation (4) into (3)



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

By substituting equation (4) into (3)

$$U = \frac{1}{2}k(y + \Delta l)^2 - mgy \quad \Rightarrow \quad U = \frac{1}{2}ky^2 + \frac{1}{2} \cdot 2ky \cdot \Delta l + \frac{1}{2}k\Delta l^2 - mgy$$

$$U = \frac{1}{2}ky^2 + ky \frac{mg}{k} - mgy + cte \quad \Rightarrow \quad U = \frac{1}{2}ky^2 + \cancel{mgy} - \cancel{mgy} + cte , \quad cte = \frac{1}{2}k\Delta l^2$$

$$\Rightarrow U = \frac{1}{2}ky^2 + cte$$

$$L = T - U \quad \Rightarrow \quad L = \frac{1}{2}m\dot{y}^2 - \frac{1}{2}ky^2 + cte$$

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = 0 \quad \text{Lagrange's equation in the case of a conservative system}$$

$$\frac{\partial L}{\partial \dot{q}} = m\dot{y} \quad \Rightarrow \quad \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) = \frac{d}{dt} (m\dot{y}) = m\ddot{y}$$

$$\frac{\partial L}{\partial q} = -ky$$

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}} \right) - \frac{\partial L}{\partial q} = 0 \quad \Rightarrow \quad m\ddot{y} + ky = 0 \quad \Rightarrow \quad \ddot{y} + \frac{k}{m}y = 0$$

$$\Rightarrow \ddot{y} + \omega_n^2 y = 0 \quad \text{Where} \quad \omega_n = \sqrt{\frac{k}{m}}$$

$\omega_n$  is called natural frequency

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

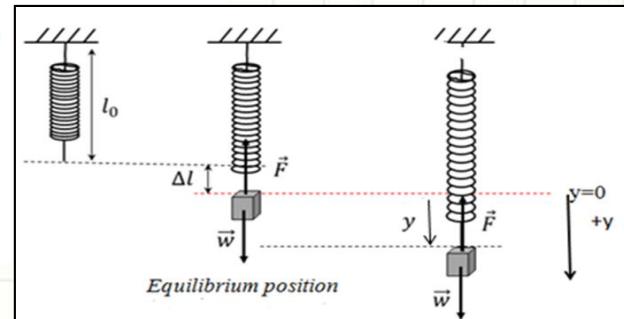
- $\ddot{y} + \frac{k}{m}y = 0$
- This equation is a second order linear homogeneous ordinary differential equation with constant coefficients.

The general solution of this differential equation takes a form of

$$y(t) = y_0 \cos(wt + \varphi) \quad \text{or} \quad y(t) = y_0 \sin(wt + \varphi')$$

We can find the values of  $y_0$  and  $\varphi$  using initial conditions

- The solution is based on the initial conditions



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 1- Vertical mass-spring

- The motion of an object can be described in terms of its
  - Displacement  $y(t) = y_0 \cos(w_n t + \varphi)$
  - Velocity  $v(t) = \frac{dy}{dt} = \dot{y}$   $\Rightarrow \dot{y}(t) = -w_n y_0 \sin(w_n t + \varphi)$
  - Acceleration  $a(t) = \frac{dv}{dt} = \frac{d^2y}{dt^2} = \ddot{y}$   $\Rightarrow \ddot{y}(t) = -w_n^2 y_0 \cos(w_n t + \varphi)$

$$\ddot{y}(t) = -w_n^2 y(t) \Rightarrow \text{Simple Harmonic motion}$$

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 2- Horizontal mass- spring

#### 2- Horizontal mass spring

Consider a mass attached to a massless spring on a frictionless surface, as shown below.

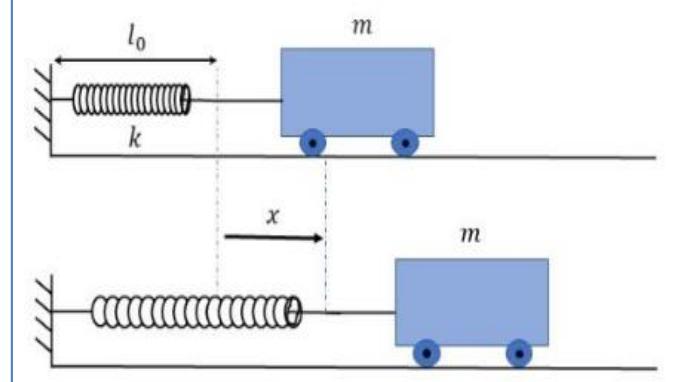
- Using Lagrange's equation:

$$T = \frac{1}{2} m \dot{x}^2 , \quad U = \frac{1}{2} k x^2$$

- Lagrangian of the system:

$$L = T - U \Rightarrow L = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} k x^2$$

$$\Rightarrow \frac{d}{dt} \left( \frac{\partial(L)}{\partial \dot{q}} \right) - \frac{\partial(L)}{\partial q} = 0 \Rightarrow \ddot{x} + \frac{k}{m} x = 0 \Rightarrow \ddot{x} + w_n^2 x = 0$$



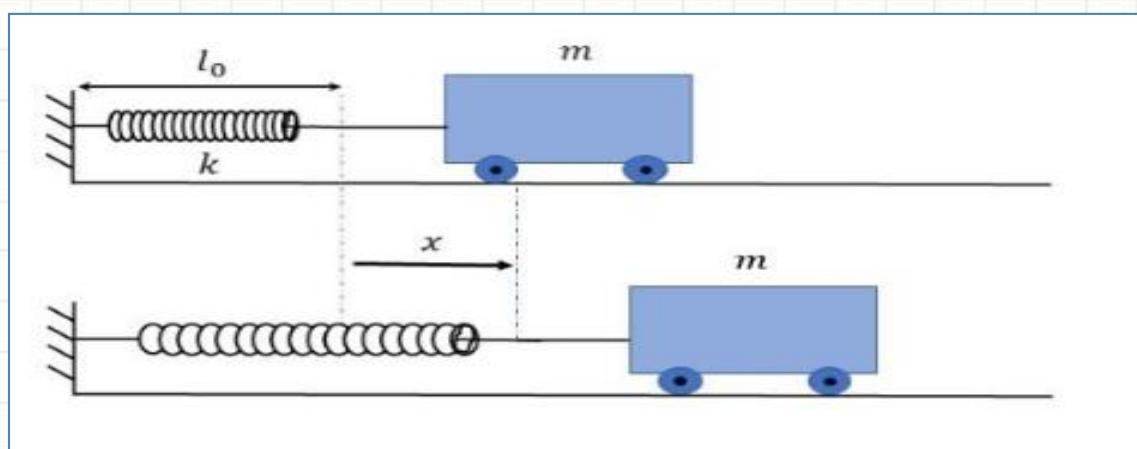
## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 2- Horizontal mass- spring

- This equation is a second order linear homogeneous ordinary differential equation with constant coefficients.

Where  $\omega_n = \sqrt{\frac{k}{m}}$  The natural frequency of the system.

- It is important to note that this frequency is independent of the initial conditions



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 3- Simple Pendulum

➤ Position vector

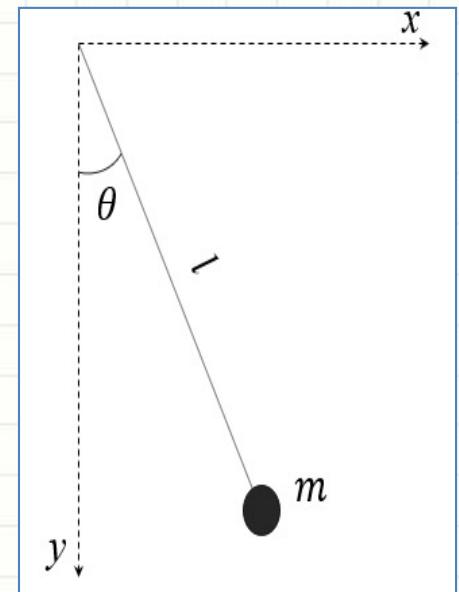
$$\vec{r}_m \begin{pmatrix} l \sin\theta \\ l \cos\theta \end{pmatrix} \Rightarrow \vec{dr}_m \begin{pmatrix} l \cos\theta \ d\theta \\ -l \sin\theta \ d\theta \end{pmatrix} \Rightarrow \vec{v}_m \begin{pmatrix} l \cos\theta \dot{\theta} \\ -l \sin\theta \dot{\theta} \end{pmatrix}$$

➤ Weight

$$\vec{w} \begin{pmatrix} 0 \\ mg \end{pmatrix}$$

➤ Potential energy

$$U = - \int_0^\theta \vec{w} \cdot \vec{dr}_m = - \int_0^\theta mg \cdot (-l \sin\theta \ d\theta) = +lmg \int_0^\theta \sin\theta \ d\theta$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 3- Simple Pendulum

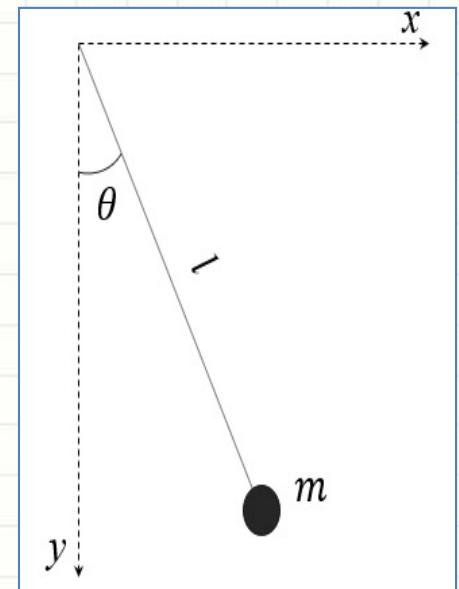
✓ For small oscillations  $\Rightarrow \theta \ll 1 \Rightarrow \cos\theta = 1 - \frac{\theta^2}{2}$

$$\Rightarrow U = lmg \frac{\theta^2}{2}$$

$$T = \frac{1}{2}mv^2 \Rightarrow T = \frac{1}{2}m l^2\dot{\theta}^2$$

➤ The Lagrangian of the system |

$$L = T - U \Rightarrow L = \frac{1}{2}m l^2\dot{\theta}^2 - lmg \frac{\theta^2}{2}$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

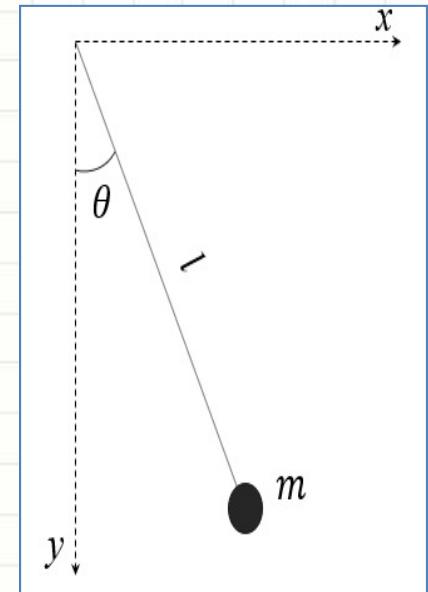
### 3- Simple Pendulum

Lagrange equation  $\frac{d}{dt} \left( \frac{\partial(L)}{\partial \dot{q}} \right) - \frac{\partial(L)}{\partial q} = 0 \quad \Rightarrow \quad \frac{d}{dt} \left( \frac{\partial(L)}{\partial \dot{\theta}} \right) - \frac{\partial(L)}{\partial \theta} = 0$

➤  $\frac{\partial L}{\partial \dot{\theta}} = m l^2 \dot{\theta}$

➤  $\frac{d}{dt} \left( \frac{\partial(L)}{\partial \dot{\theta}} \right) = \frac{d}{dt} (m l^2 \dot{\theta}) = m l^2 \ddot{\theta}$

➤  $\frac{\partial(L)}{\partial q} = lmg\theta$



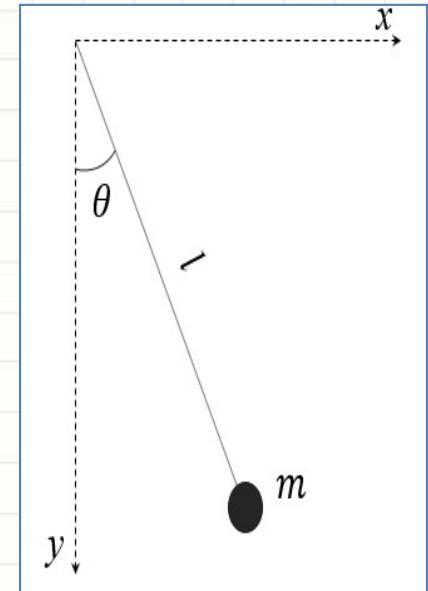
## Chapter 2 : Free vibration of undamped single degree of freedom systems

### 3- Simple Pendulum

$$\frac{d}{dt} \left( \frac{\partial(L)}{\partial \dot{q}} \right) - \frac{\partial(L)}{\partial q} = 0 \quad \Rightarrow \quad m l^2 \ddot{\theta} + lmg\theta = 0$$

$$\ddot{\theta} + \frac{g}{l} \theta = 0 \quad \Rightarrow \quad \ddot{\theta} + \omega_n^2 \theta = 0$$

Where  $\omega_n = \sqrt{\frac{g}{l}}$  is the natural frequency of the system



### 3- Simple Pendulum

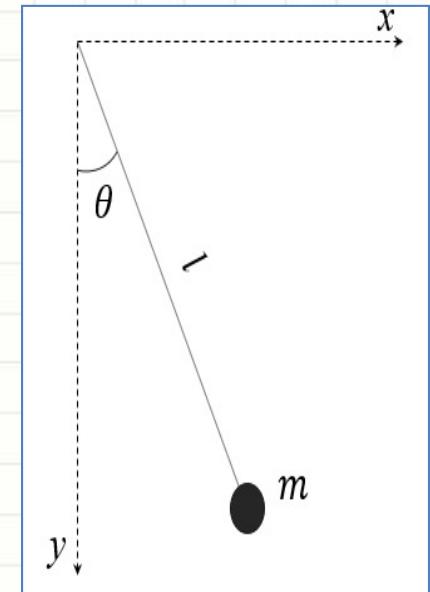
➤  $\ddot{\theta} + \omega_0^2 \theta = 0$

The general solution of this differential equation takes a form of

$$\theta(t) = \theta_0 \cos(wt + \varphi) \quad \text{or} \quad \theta(t) = \theta_0 \sin(wt + \varphi')$$

We can find the values of  $\theta_0$  and  $\varphi$  using initial conditions

- The solution is based on the initial conditions



### 4- LC circuit

#### 4- LC circuit

Considérant un circuit LC

By applying Kirchhoff's loop rule:

$$V_c + V_L = 0 \quad \Rightarrow \quad \frac{q}{c} + L \frac{di}{dt} = 0 \quad \Rightarrow \quad \frac{q}{c} + L \frac{d^2q}{dt^2} = 0$$

$$\ddot{q} + \frac{q}{LC} = 0 \quad \Rightarrow \quad \ddot{q} + \omega_n^2 q = 0 \quad \Rightarrow \quad \omega_n = \sqrt{\frac{1}{LC}}$$

$\omega_n$ : The natural frequency of the circuit

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### Electro-mechanical analogy for free oscillation



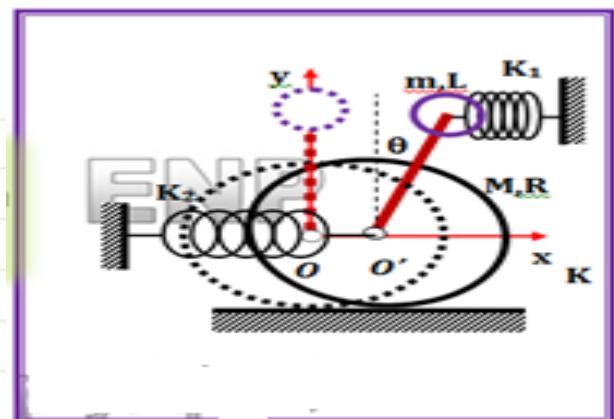
Mechanical system	Electrical system
$m\ddot{x} + kx = 0$	$L\ddot{q} + \frac{q}{c} = 0$
Elongation $x$	Charge $q$
Velocity $\dot{x}$	Current $i$
Mass $m$	Inductance $L$
Spring $k$	Inverse of capacitance $\frac{1}{c}$
Kinetic energy $\frac{1}{2}m\dot{x}^2$	Energy of the inductor $\frac{1}{2}Lq^2$
Potential energy $\frac{1}{2}kx^2$	Energy of the capacitor $\frac{1}{2c}q^2$

## Chapter 2 : Free vibration of undamped single degree of freedom systems

### Application exercise

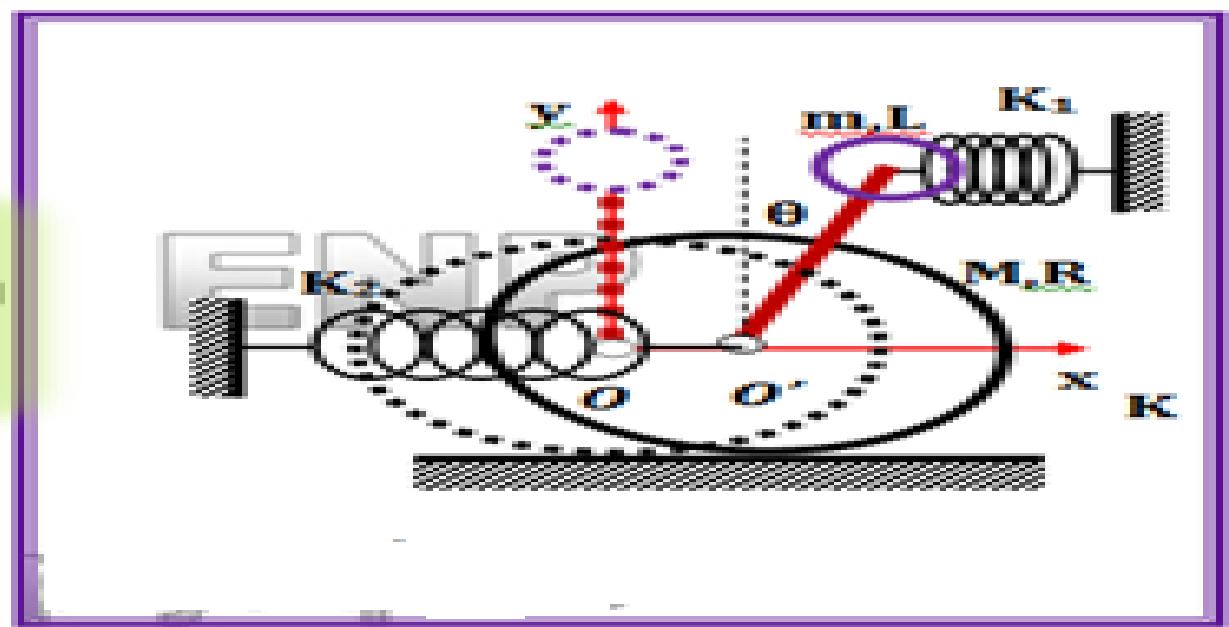
In the system shown in the figure, the cylinder ( $M, R$ ) can **roll freely** on a horizontal support. Along a radius, a rod of negligible mass and length  $L = 2R$  is welded, at the end of which a point mass  $m$  is attached. The cylinder is connected at its center of mass to a fixed wall by a spring with stiffness  $K_2$ , and the point mass is connected to another fixed wall using a spring with stiffness  $K_1$ . **At equilibrium, both springs are neither stretched nor compressed**, and the system's position is represented by dashed lines. For small oscillations, determine:

- The potential energy of the system and the condition for oscillation, if it exists
- The kinetic energy of the system
- The natural angular frequency of the oscillations



## Application exercise

$$\vec{r}_m \begin{cases} R\theta + L \sin \theta \\ L \cos \theta \\ 0 \end{cases} \xrightarrow{\text{d}\theta} \vec{dr}_m \begin{cases} (R + L \cos \theta) d\theta \\ -L \sin \theta d\theta \\ 0 \end{cases} \xrightarrow{\text{d}t} \vec{v}_m \begin{cases} (R + L \cos \theta)\dot{\theta} \\ -L \sin \theta \dot{\theta} \\ 0 \end{cases}$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

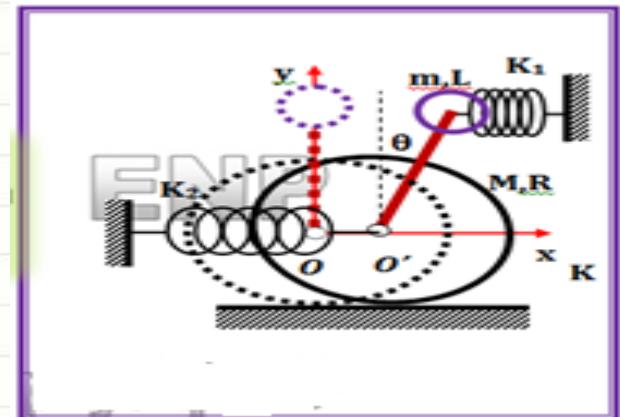
### *Application exercise*

$$\mathbf{U} = \mathbf{U}_m + \mathbf{U}_{K_1} + \mathbf{U}_{K_2}$$

$$\overrightarrow{w_m} \begin{pmatrix} 0 \\ -mg \end{pmatrix}$$

$$U = - \int_0^\theta \overrightarrow{w_m} \cdot \overrightarrow{dr_m} = - \int_0^\theta -mg \cdot (-L \sin\theta \ d\theta)$$

$$= \int_0^\theta mgL(-\sin\theta) d\theta = mgL[\cos\theta]_0^\theta = mgL(\cos\theta - 1)$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

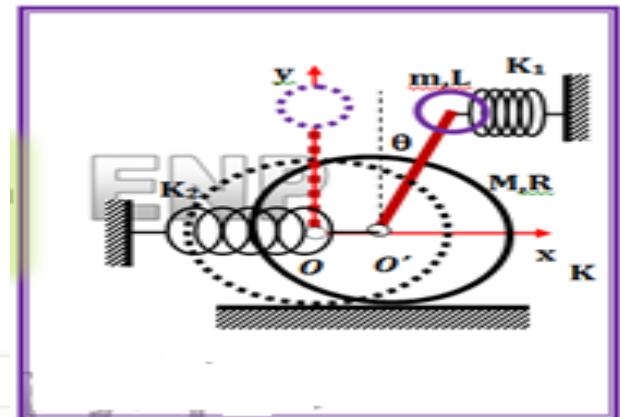
### Application exercise

$$\cos \theta \cong 1 - \frac{\theta^2}{2} \quad \rightarrow \quad U_m = -mgL \frac{\theta^2}{2}$$

$$U_{K_1} = \frac{1}{2} K_1 (R\theta + L\theta)^2$$

$$U_{K_1} = \frac{1}{2} K_1 (R+L)^2 \theta^2$$

$$U_{K_2} = \frac{1}{2} K_2 R^2 \theta^2$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

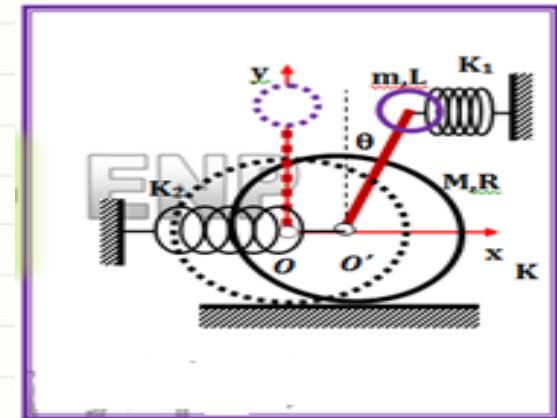
### Application exercise

$$U = -mgL \frac{\theta^2}{2} + \frac{1}{2} (K_1(R+L)^2 + K_2R^2)\theta^2$$

➤ Condition of oscillation

$$\left. \frac{\partial^2 U}{\partial \theta^2} \right|_{\theta=0} > 0 \quad \Rightarrow$$

$$K_1(R+L)^2 + K_2R^2 > mgL$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### Application exercise

$$\mathbf{T} = \mathbf{T_m} + \mathbf{T_M}$$

$$\mathbf{T} = \frac{1}{2} m V_m^2 + \frac{1}{2} M V_M^2 + \frac{1}{2} I_{M/\Delta} \dot{\Theta}^2$$

$$V_m^2 = ((R + L \cos \theta) \dot{\theta})^2 + (-L \sin \theta \dot{\theta})^2$$

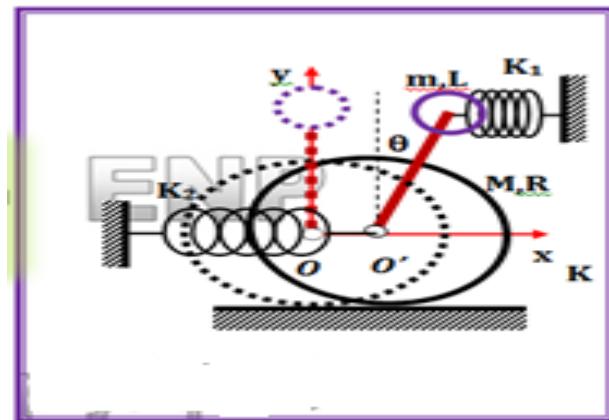
$$V_m^2 = (R \dot{\theta})^2 + (2RL \cos \theta) (\dot{\theta})^2 + (L \cos \theta \dot{\theta})^2 + (L \sin \theta \dot{\theta})^2$$

$$\cos \theta \approx 1$$



$$V_m^2 = (R^2 + 2RL + L^2) \dot{\theta}^2$$

$$\vec{V}_m \begin{cases} (R + L \cos \theta) \dot{\theta} \\ -L \sin \theta \dot{\theta} \\ 0 \end{cases}$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

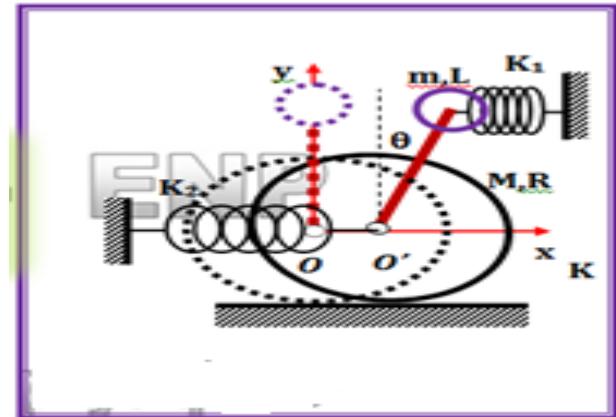
### Application exercise

$$V_m^2 = (R + L)^2 \dot{\theta}^2$$

$$T = \frac{1}{2} m V_m^2 + \frac{1}{2} M V_M^2 + \frac{1}{2} I_{M/\Delta} \dot{\theta}^2$$



$$T = \frac{1}{2} m(R + L)^2 \dot{\theta}^2 + \frac{1}{2} M(R\dot{\theta})^2 + \frac{1}{2} \left( \frac{1}{2} M R^2 \right) \dot{\theta}^2$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

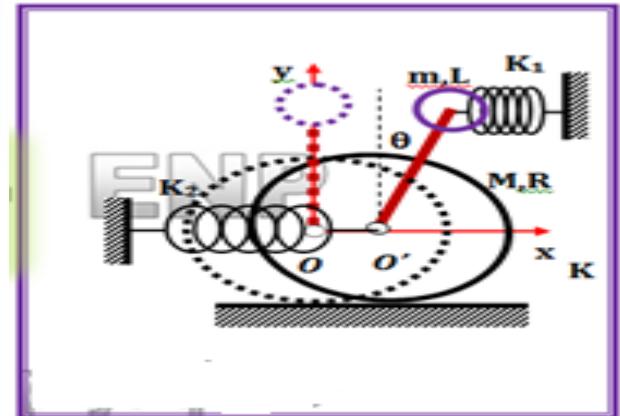
### Application exercise

$$T = \frac{1}{2} (m(R + L)^2 + \frac{3}{2} MR^2) \dot{\theta}^2$$

$$L = T - U$$



$$L = \frac{1}{2} \left( m(R + L)^2 + \frac{3}{2} MR^2 \right) \dot{\theta}^2 - \frac{1}{2} (K_1(R+L)^2 + K_2R^2 - mgL)\theta^2$$



## Chapter 2 : Free vibration of undamped single degree of freedom systems

### Application exercise

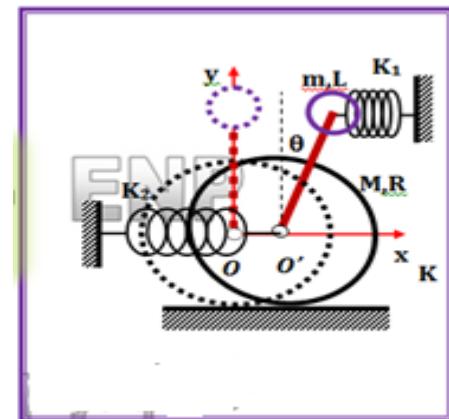
$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\theta}} \right) - \frac{\partial L}{\partial \theta} = 0$$



$$\left( m(R+L)^2 + \frac{3}{2}MR^2 \right) \ddot{\theta} + (K_1(R+L)^2 + K_2R^2 - mgL) \theta = 0$$



$$\ddot{\theta} + \frac{K_1(R+L)^2 + K_2R^2 - mgL}{m(R+L)^2 + \frac{3}{2}MR^2} \theta = 0$$



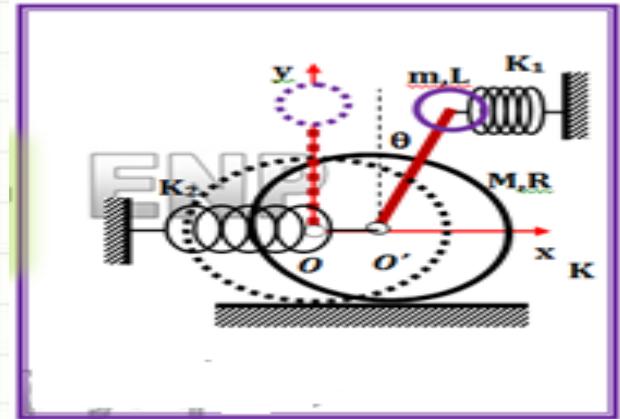
## Chapter 2 : Free vibration of undamped single degree of freedom systems

### Application exercise

$$\omega = \sqrt{\frac{K_1(R + L)^2 + K_2R^2 - mgL}{m(R + L)^2 + \frac{3}{2}MR^2}}$$

➤ Condition of oscillation

$$K_1(R + L)^2 + K_2R^2 > mgL$$



### Application exercise

➤ Condition of oscillation

$$\left. \frac{\partial^2 U}{\partial \theta} \right|_{\theta=0} > 0 \rightarrow$$

$$K_1(R + L)^2 + K_2 R^2 > mgL$$

