

# Chapiter 4

# Three-phase Power

# The power in three-phase regime

## *In brief*

- The instantaneous power in three phases is equal to the sum of the instantaneous powers on each phase,
- The three-phase active power is equal to the sum of the active power on each phase.
- The three-phase reactive power is equal to the sum of the reactive power on each phase.
- The total apparent power is **different** from the sum of the apparent power on each phase.

# Instantaneous Power

## Balanced Load

- In the balanced three-phase case, **there is no fluctuating power** as in the single-phase.

- Indeed, as :

$$\left\{ \begin{array}{l} v_1(t) = \sqrt{2}V \cos(\omega t + \varphi_v) \\ v_2(t) = \sqrt{2}V \cos(\omega t + \varphi_v - 2\pi/3) \text{ et} \\ v_3(t) = \sqrt{2}V \cos(\omega t + \varphi_v + 2\pi/3) \end{array} \right. \quad \left\{ \begin{array}{l} j_1(t) = \sqrt{2}J \cos(\omega t + \varphi_j) \\ j_2(t) = \sqrt{2}J \cos(\omega t + \varphi_j - 2\pi/3) \\ j_3(t) = \sqrt{2}J \cos(\omega t + \varphi_j + 2\pi/3) \end{array} \right.$$
$$p(t) = p_1(t) + p_2(t) + p_3(t) = 2VJ \left\{ \cos(\omega t + \varphi_j) \cdot \cos(\omega t + \varphi_v) \right.$$

- then:
$$\left. + \cos(\omega t + \varphi_j - 2\pi/3) \cdot \cos(\omega t + \varphi_v - 2\pi/3) \right. \\ \left. + \cos(\omega t + \varphi_j + 2\pi/3) \cdot \cos(\omega t + \varphi_v + 2\pi/3) \right\}$$

- then:

$$p(t) = VJ \left\{ 3 \cos(\varphi) + \cos(2\omega t + \varphi_i + \varphi_j) \right. \\ \left. + \cos(2\omega t + \varphi_i + \varphi_j - 4\pi/3) + \cos(2\omega t + \varphi_i + \varphi_j + 4\pi/3) \right\} = 3VJ \cos(\varphi)$$

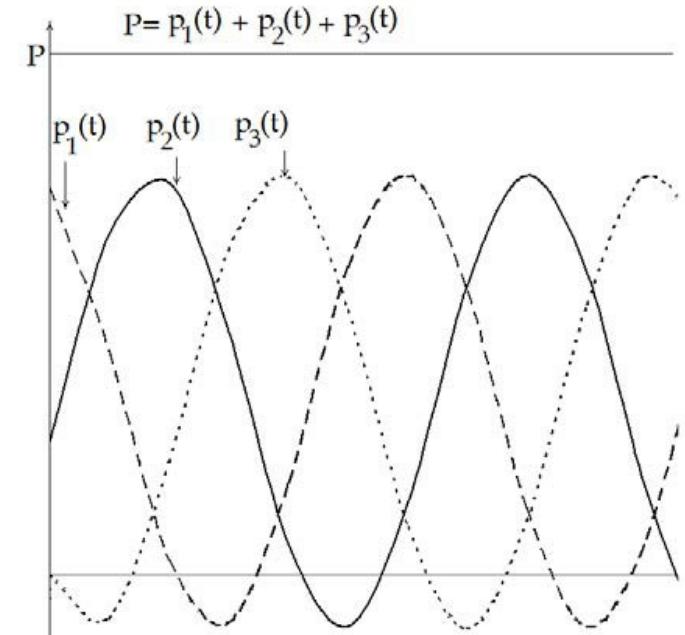
# Instantaneous Power

## Balanced Load

- Calculations of  $p(t)$  give:

$$p(t) = 3 V J \cos(\varphi)$$

- Instantaneous power is constant,
- It equals 3 times the active power in a single phase
- No fluctuating powers whatever the nature of  $Z$ .
- Disappearance of vibration phenomena in motors => engine longevity



# Active and Reactive power

## *Any load*

- The three-phase active power is equal to the sum of the active powers on each phase.

$$P = \sum_{i=0}^3 P_i = V_1 J_1 \cos(\varphi_1) + V_2 J_2 \cos(\varphi_2) + V_3 J_3 \cos(\varphi_3)$$

- The three-phase reactive power is equal to the sum of the reactive powers on each phase.

$$Q = \sum_{i=0}^3 Q_i = V_1 J_1 \sin(\varphi_1) + V_2 J_2 \sin(\varphi_2) + V_3 J_3 \sin(\varphi_3)$$

- where:

$$\varphi_1 = \varphi_v 1 - \varphi_j 1, \quad \varphi_2 = \varphi_v 2 - \varphi_j 2 \quad \text{et} \quad \varphi_3 = \varphi_v 3 - \varphi_j 3$$

- Total apparent power is different from partial apparent powers:  $S \neq \sum_{i=0}^3 S_i$

# Active and Reactive power

## Balanced Load

- We get:

$$\left\{ \begin{array}{l} V_1 = V_2 = V_3 = V \\ J_1 = J_2 = J_3 = J \\ \varphi_1 = \varphi_2 = \varphi_3 = \varphi \end{array} \right. \text{ then } \left\{ \begin{array}{l} P = P_1 + P_2 + P_3 = 3 V J \cos \varphi \\ Q = Q_1 + Q_2 + Q_3 = 3 V J \sin \varphi \end{array} \right.$$

- if the load is in a Star fashion

$$\left\{ \begin{array}{l} J = I \\ U = \sqrt{3} V \end{array} \right. \text{ then } \left\{ \begin{array}{l} P = \sqrt{3} U I \cos \varphi \\ Q = \sqrt{3} U I \sin \varphi \end{array} \right.$$

- if the load is a trdelta fashion

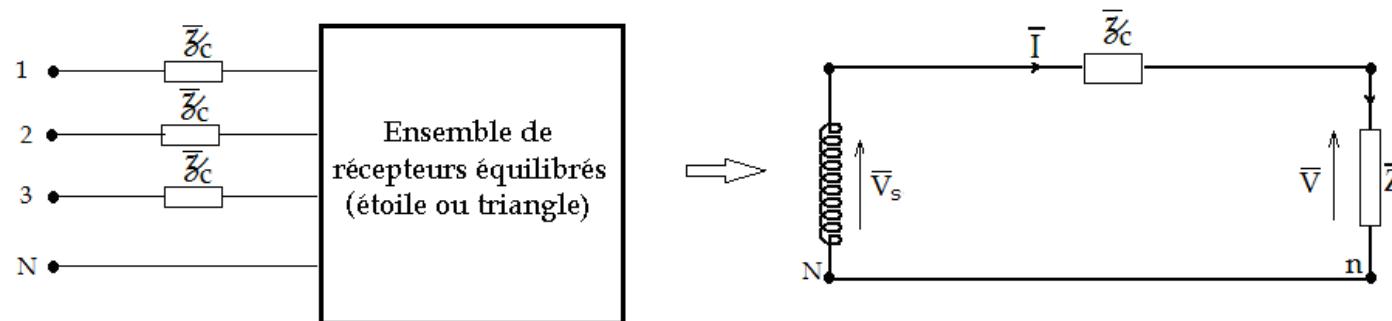
$$\left\{ \begin{array}{l} I = \sqrt{3} J \\ U = V \end{array} \right. \text{ then } \left\{ \begin{array}{l} P = \sqrt{3} U I \cos \varphi \\ Q = \sqrt{3} U I \sin \varphi \end{array} \right.$$

- We obtain the same expression using the composite values of voltage and current.

# Active and Reactive power

## *Equivalent Star (balanced case)*

- As we obtained the same expressions for the power, we will use the notion of equivalent star:
- A balanced triangle installation of current and voltage  $U$  corresponds to a star assembly consuming the same energy.
- Consequently, it will be possible to determine the voltage drops as in single-phase.
- We are then interested in a single phase:



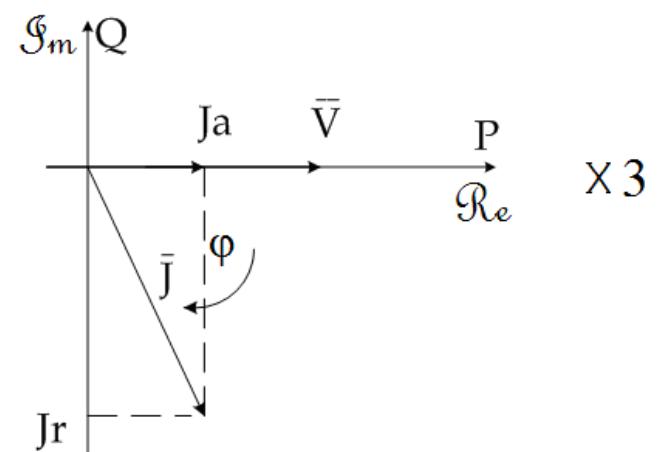
# Active and Reactive power

## *Complex notation (balanced case)*

- We return to the definition of apparent power:

$$\tilde{S} = P + j Q = 3 V J \cos \varphi + 3 j V J \sin \varphi = 3 V J e^{j\varphi} = 3 \tilde{V} \tilde{J}^*$$

- It is then possible to make a representation in the complex plane using a single phase.
- However, we must not forget that the quantities must be multiplied by 3



# Active and Reactive power

***Power Factor***  $f_p$

- Nothing changes:

$$f_p = \frac{P}{\sqrt{P^2 + Q^2}}$$

# Active and Reactive power

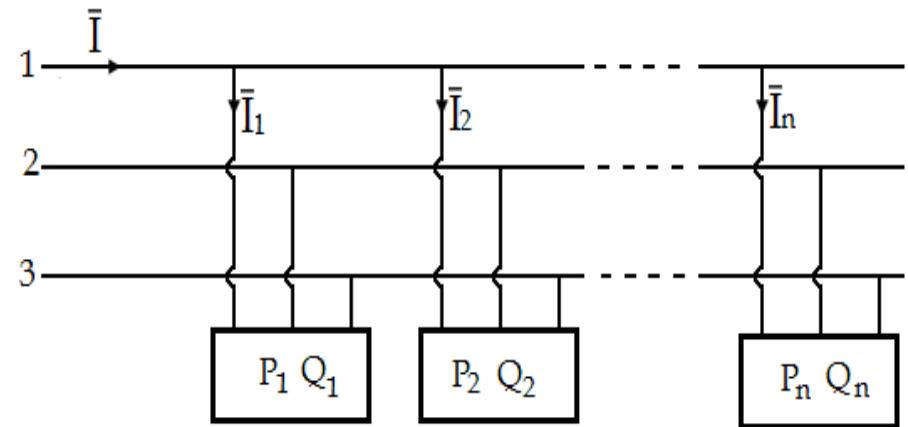
## Boucherot's Method

- Let be an installation with several balanced three-phase receivers,
- They can be either triangle or star,
- It is more practical to illustrate the currents on a single phase,

$$P_t = \sum_{i=0}^n P_i \text{ et } Q_t = \sum_{i=0}^n Q_i \text{ et } S_t = \sqrt{P_t^2 + Q_t^2}$$

- Knowing that

$$S_t = 3 VJ = \sqrt{3} U I,$$



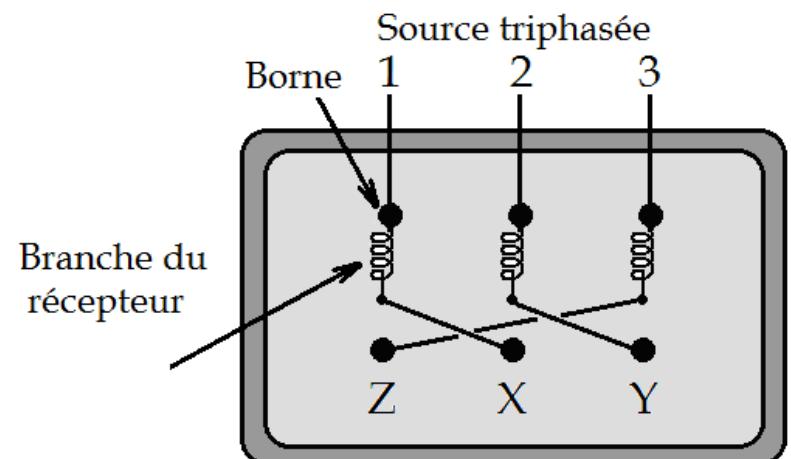
- It is possible to determine the current of the line  $I$  and the power factor  $f_p$ :

$$I = \frac{S_t}{\sqrt{3} U} \quad \text{et} \quad \cos \varphi_t = \frac{P_t}{S_t}$$

# Connection to the network

## *Three-phase receivers*

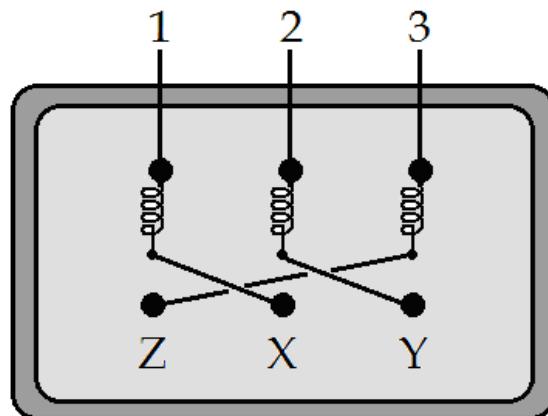
- The nameplate of certain three-phase equipment bears the indication  $U_1/U_2$  with  $U_2 = \sqrt{3} U_1$ . Example 220 V / 380 V.
- This indicates that the device can be set to operate under these two regimes. How?
- The device contains six terminals allowing the receiver to be configured as a star or triangle.
- The receiver branch is designed to work with  $U_1$  (for instance 220 V),



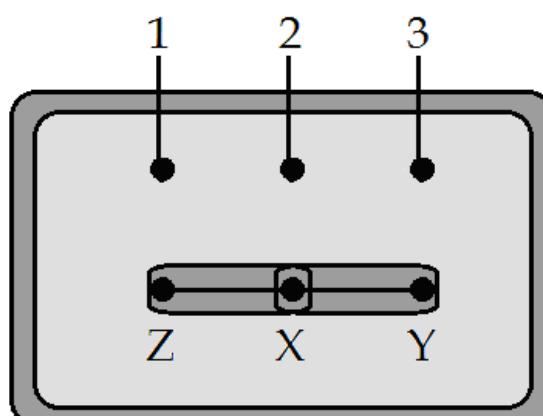
# Connection to the network

## *Three-phase receivers*

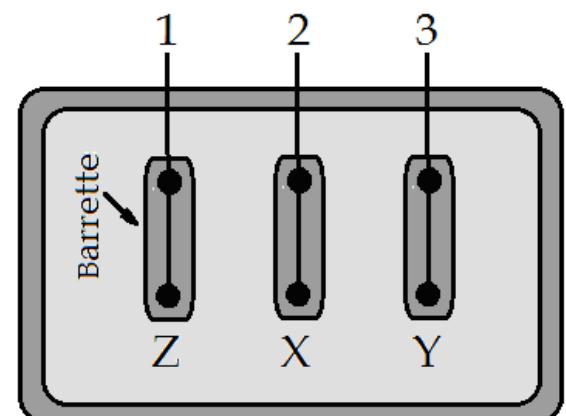
- If the compound voltage of the network  $U_{s1} = U_1$  then, the delta topology is the most suitable,
- If  $U_{s1} = \sqrt{3} U_1$ , then, the star topology is the most suitable,
- We use strips to configure the receiver.



Terminal board



« Star » Coupling



« Delta » Coupling

# Connection to the network

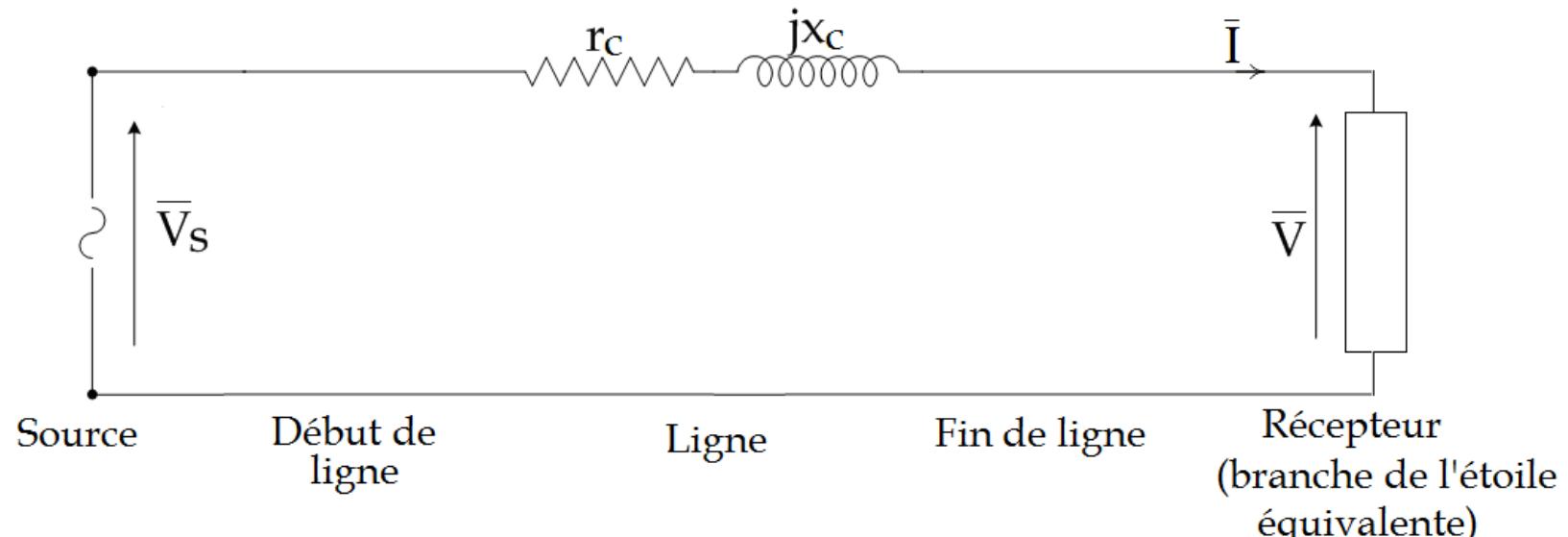
## *Single phase receivers*

- The homes are powered by 220 V / 50 Hz
- Each home is connected to one phase,
- The goal being to balance the three-phase system in order to have a neutral current of small value,
- Semi-industrial installations use compound voltages. They require a three-phase installation.
- It is necessary to respect the indications on the loads.

# Voltage Drops

## Balanced case

- As the loads are balanced, then we consider only one phase.
- The neutral line carries no current:



# Voltage Drop

## **Balanced case**

- We keep the same definition as for the single phase

$$\Delta V = |\tilde{V}_s| - |\tilde{V}|$$

- We add a definition for compound voltages:

$$\Delta U = \sqrt{3} (|V_s| - |V|)$$

- We can use the approximate **Kapp** formulae to estimate voltage drop:

$$\Delta V = r_c I \cos \varphi + x_c I \sin \varphi$$

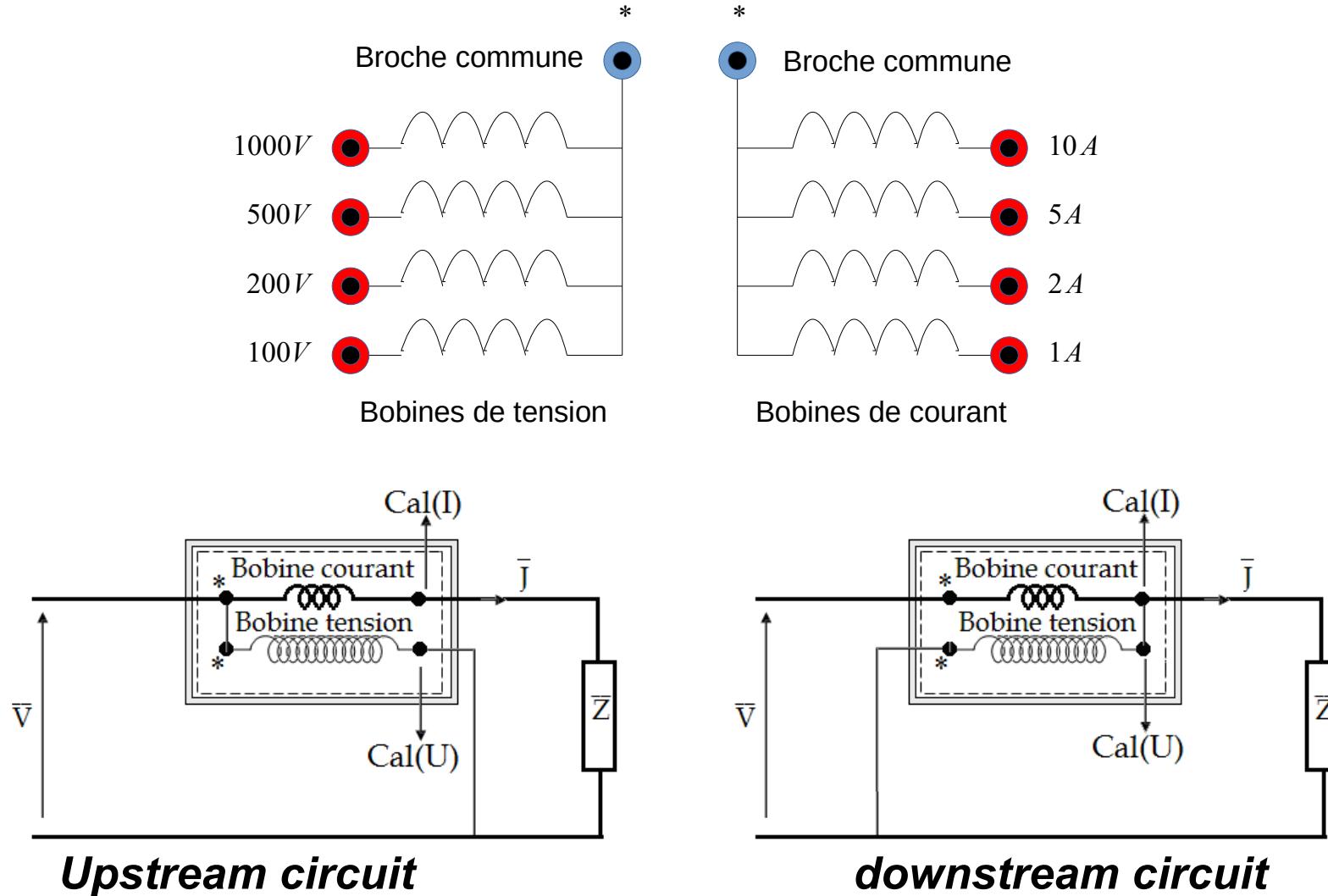
# Power measurement in 3-phase

## ***Wattmeter Principle***

- Appareil qui a une déviation proportionnelle à la puissance active (ie  $VJ \cos \varphi$ )
- Il possède donc deux types de circuits (bobines)
  - La bobine courant utilisée comme un ampèremètre (placée en série). Elle possède une faible résistance.
  - Une bobine tension utilisée comme un voltmètre (placée en parallèle). Elle possède une importante résistance interne.
- Chaque bobine correspond à un calibre de tension et de courant.
- Le symbole « \* » correspond au point commun à tous les calibres.

# Power measurement in 3-phase

## Wattmeter Principle



# Power measurement in 3-phase

## *Single Wattmeter method*

- We have in general:

$$P = V_1 J_1 \cos \varphi_1 + V_2 J_2 \cos \varphi_2 + V_3 J_3 \cos \varphi_3 = V (J_1 \cos \varphi_1 + J_2 \cos \varphi_2 + J_3 \cos \varphi_3)$$

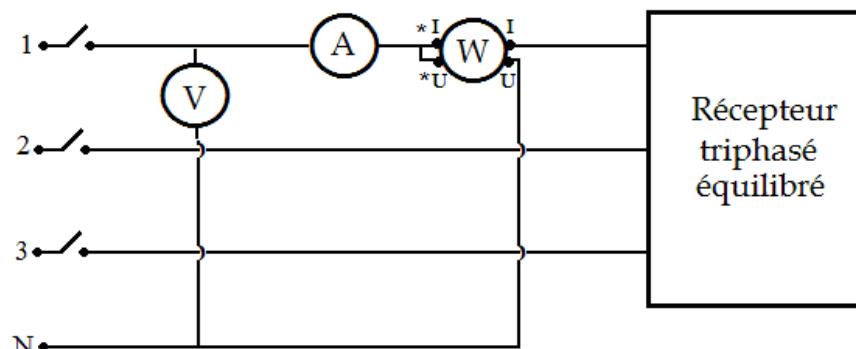
$$Q = V_1 J_1 \sin \varphi_1 + V_2 J_2 \sin \varphi_2 + V_3 J_3 \sin \varphi_3 = V (J_1 \sin \varphi_1 + J_2 \sin \varphi_2 + J_3 \sin \varphi_3)$$

- If the loads are balanced:

$$P = 3 V J \cos \varphi \quad \text{and} \quad Q = 3 V J \sin \varphi$$

- It is then sufficient to consider one phase and then multiply by 3:

$$P = 3 \times \text{lecture}$$



- It is understood that we use the equivalent star diagram when it comes to a triangle topology (i.e.  $I = J$ )

# Power measurement in 3-phase

## *Single Wattmeter method*

- Apparent power measurement:
  - Use a voltmeter and an amperemeter

$$S = \sqrt{3} V J = \sqrt{3} V I = \sqrt{3} U I$$

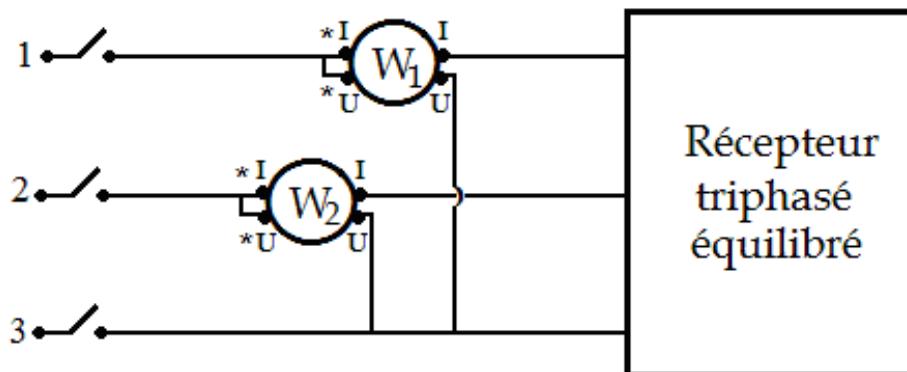
- Deduce reactive power:

$$Q = \sqrt{(\sqrt{3} U I)^2 - P^2}$$

# Power measurement in 3-phase

## *Two Wattmeters method*

- Possibility of measuring active and reactive power,
- Method adapted for a balanced three-phase circuit,
- Take the sign into account because it is algebraic values that are read.



- According to the schematic, we read in the wattmeter and knowing that  $I = J$

$$W_1 = U_{13} I_1 \cos \varphi_{u13, j1}$$

$$W_2 = U_{23} I_2 \cos \varphi_{u23, j2}$$

# Power measurement in 3-phase

## Two Wattmeters method

- We had:

$$W_1 = U_{13} I_1 \cos \varphi_{u13, j1}$$

$$W_2 = U_{23} I_2 \cos \varphi_{u23, j2}$$

- But:  $\varphi_{u13, j1} = \pi/6 - \varphi$  and  $\varphi_{u23, j2} = \pi/6 + \varphi$

- Then:

$$W_1 = U I \cos\left(\frac{\pi}{6} - \varphi\right) \quad \text{and} \quad W_2 = U I \cos\left(\frac{\pi}{6} + \varphi\right)$$

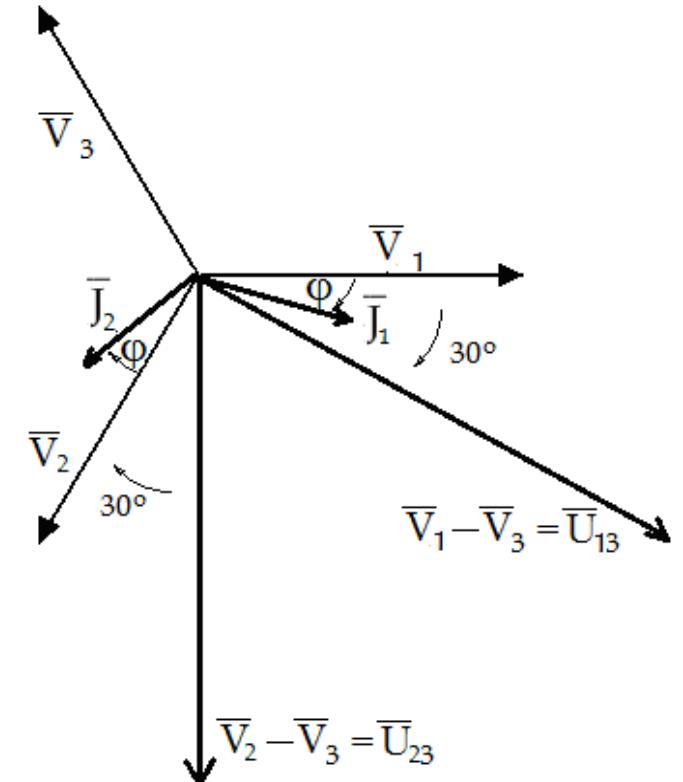
- If we calculate the sum:

$$W_1 + W_2 = 2 U I \cos\left(\pi/6\right) \cos \varphi = \sqrt{3} U I \cos \varphi = P$$

- If we calculate the difference:

$$W_1 - W_2 = 2 U I \sin\left(\pi/6\right) \sin \varphi = U I \sin \varphi = Q / \sqrt{3}$$

Then:  $P = W_1 + W_2$  and  $Q = \sqrt{3}(W_1 - W_2)$



# Power measurement in 3-phase

## ***Two Wattmeters method***

- The method remains valid for measuring active power in the case of unbalance without neutral:
- Indeed as:

$$j_1 + j_2 + j_3 = 0$$

- Then:

$$\begin{aligned} p(t) &= v_1 j_1 + v_2 j_2 + v_3 j_3 = v_1 j_1 + v_2 j_2 + v_3 (-j_1 - j_2) \\ &= j_1 (v_1 - v_3) + j_2 (v_2 - v_3) = j_1(t) u_{13}(t) - j_2(t) u_{23}(t) \end{aligned}$$

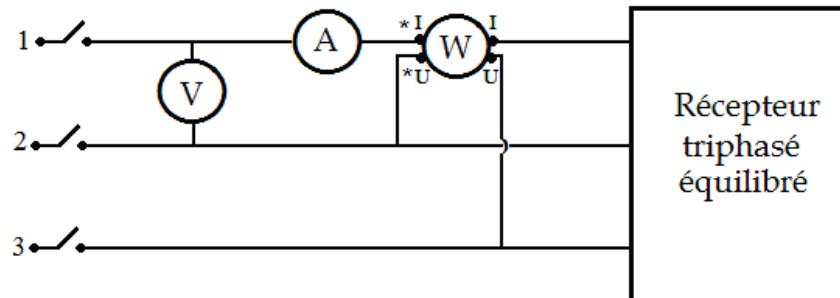
- By taken the average value in both sides:

$$P = J_1 U_{13} \cos(\varphi_{u13, j1}) + J_2 U_{23} \cos(\varphi_{u23, j2}) = W_1 + W_2$$

# Power measurement in 3-phase

## *Boucherot's Method to measure Q*

- Allows you to measure the reactive power of a balanced three-phase circuit using a wattmeter.
- The following figure illustrates the circuit to use:



- We show that:

$$W = U I \sin \varphi \quad \text{and then} \quad Q = \sqrt{3} W$$

# Power measurement in 3-phase

## Boucherot's Method to measure Q

- Indeed:

$$W = U_{23} I_1 \cos \varphi_{u23, j1}$$

- But according to Phasor diagram (Fresnel):

$$\varphi_{u23, j1} = \pi/2 - \varphi$$

- and then:

$$W = U I \sin \varphi$$

- and finally:

$$Q = \sqrt{3} W$$

- By using a voltmeter and an amperemeter, we deduce  $P$ :

$$P = \sqrt{S^2 - Q^2} \quad \text{avec} \quad S = \sqrt{3} U I$$

