

Universitat Politècnica de Catalunya  
Facultat de Matemàtiques i Estadística

Master in Advanced Mathematics and Mathematical Engineering  
Master's thesis

**Planng and Control of a  
Multiple-Quadcopter System  
Cooperatively Carrying a Slung  
Payload in Dynamical  
Environments**

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# Abstract

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# Chapter 1

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## Introduction

### 1-1 Theme Relevance and Justification

#### 1-1-1 Omni-wheeled robots

#### 1-1-2 Model Predictive Control

### 1-2 Research Objective

The objective of the research included in this thesis is to:

*Design a control algorithm for systems with an omni-wheeled robot and demonstrate it in simulated and real scenarios.*

### 1-3 Thesis Context

This thesis is a result of the collaboration between Facultat de Matemàtiques i Estadística (FME) and Institut de Robòtica i Informàtica Industrial (IRI). During the summer of 2018 I contacted Lluís Ros looking for a suitable project for my Master's Thesis and he proposed me this one.

## 1-4 Notation

Throughout this thesis the following notation will be used:

	Symbol	Definition
Scalars:	$x$	
Vectors:	$\mathbf{x}$	
Elements of vector:	$\mathbf{x}(i)$	$i$ -th element of vector $\mathbf{x}$
Position vectors:	$\mathbf{p}_x$	
Coordinates of position vector:	$x_x, y_x, z_x$	x,y,z coordinates of position $\mathbf{p}_x$
Matrices:	$\mathbf{X}$	
Sets:	$\mathcal{X}$	
Time derivatives:	$\dot{x}$	$\frac{\partial x}{\partial t}$
Desired values:	$\bar{x}$	desired value of $x$
Predicted values:	$\hat{x}$	predicted value of $x$

**Table 1-1:** Thesis Notation

All vectors are column vectors and all positions are expressed in the East-North-Up (ENU) inertial frame unless otherwise stated.

# Problem Formulation

### 2-1 Omni-wheeled robot

The robot can be represented as a rigid body in a planar space. The location of the robot's Center Of Mass (COM) is defined as  $\mathbf{p}_0 \in \mathbb{R}^2$  and the yaw of the robot is represented as  $\psi \in \mathbb{R}$ .

Assuming the robot has  $n \in \mathbb{Z}_{>0}$  wheels, we can define their

### 2-2 Dynamic Model

### 2-2-1 Motor Dynamics Identification

The motors in our robot are controlled by velocity inputs. We will represent the inputs of the  $i$ -th motor as  $u_i \in [-1, 1]$ . The motors are also equipped with encoders from which we can deduce the angle of each wheel, denoted as  $\theta_i \in \mathbb{R}$ .

We can try to identify the model using process model identification. A tool that, given some identification data and a transfer function with unknown parameters, estimates the value of the parameters. We will assume that the relationship between input velocity and the real velocity follow a linear transfer function:

$$\frac{\dot{\theta}_i(s)}{u_i(s)} = \frac{K_i}{1 + \tau_i s} \rightarrow \frac{\theta_i(s)}{u_i(s)} = \frac{K_i}{s(1 + \tau_i s)} \quad 2-1$$

Which corresponds to the following set of ODEs:

$$\dot{\theta}_i + \tau \ddot{\theta}_i = u K \quad 2-2$$

To obtain the identification data we can make the arduino generate a square wave and record the data from the encoder. This will give us data discretized with different time-intervals as the time-interval will depend on the loop size. To get data with equal time-intervals we can set a higher sampling frequency and interpolate the values between each sample.

When identifying the model we saw that the values of  $K$  were different for varying amplitudes as we can see in figure 2-1.

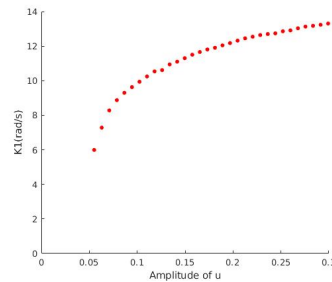


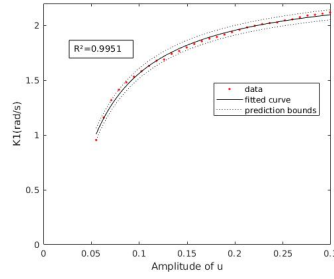
Figure 2-1: Relationship between  $K_1$  and the amplitude of  $u$

As the relationship looks like it has a vertical and a horizontal asymptote, we will try to model it with a rational function of the form:

$$K_i = \frac{a_i u_i + b_i}{u_i + c_i} \quad 2-3$$

Do experiments for higher values of amplitude (when lab is empty)

see if  $\tau$  depends on  $u$



**Figure 2-2:** Predicted relationship between  $K_1$  and the amplitude of  $u$

### 2-2-2 Aerodynamic Drag

We will use the same model for aerodynamic drag model as in [6]. The drag on the payload, denoted as  $\mathbf{F}_{Dl} \in \mathbb{R}^3$ , is modeled using a quadratic drag model, while the drag on each quadrotor, denoted as  $\mathbf{F}_{Di} \in \mathbb{R}^3$ , is modeled using a linear drag model.

$$\mathbf{F}_{Dl} = -k_{Dl} \|\dot{\mathbf{p}}_l\|^2 \frac{\dot{\mathbf{p}}_l}{\|\dot{\mathbf{p}}_l\|} = -k_{Dl} \|\dot{\mathbf{p}}_l\| \dot{\mathbf{p}}_l \quad 2-4$$

$$\mathbf{F}_{Di} = -k_{Di} \|\dot{\mathbf{p}}_i\| \frac{\dot{\mathbf{p}}_i}{\|\dot{\mathbf{p}}_i\|} = -k_{Di} \dot{\mathbf{p}}_i \quad \forall i \in \{1 \dots n\} \quad 2-5$$

Where  $k_{Dl} \in \mathbb{R}$  and  $k_{Di} \in \mathbb{R}$  are the drag constants identified in [6].

### Drag Inclusion in Equations of Motion (EOMs)

To use include drag in our problem we need to include the drag force calculated in equations 2-4 and 2-5 in the EOMs declared in equations ?? and ??.

The drag force on the drones  $\mathbf{F}_{Di}$  can be added to the input force  $\mathbf{F}_{ui}$  (we will denote this sum as  $\mathbf{F}_{uDl}$ ). The drag force on the payload can be included by subtracting  $\frac{\mathbf{F}_{Dl}}{m_l}$  from all appearances of  $\ddot{\mathbf{p}}_l$  in the EOMs, in the same way that  $g\mathbf{e}_3$  is subtracted. The resulting EOMs from these changes are:

$$\dot{\mathbf{q}}_i = \mathbf{w}_i \times \mathbf{q}_i \quad \forall i \in \{1 \dots n\} \quad 2-6$$

$$\mathbf{M}_q(\ddot{\mathbf{p}}_l - g\mathbf{e}_3 - \frac{\mathbf{F}_{Dl}}{m_l}) = \sum_{i=1}^n (-m_i l_i \|\mathbf{w}_i\|^2 \mathbf{q}_i + \mathbf{F}_{uDl}^{\parallel}) \quad 2-7$$

$$\mathbf{w}_i = \frac{1}{l_i} \mathbf{q}_i \times (\ddot{\mathbf{p}}_l - g\mathbf{e}_3 - \frac{\mathbf{F}_{Dl}}{m_l}) - \frac{1}{m_i l_i} (\mathbf{q}_i \times \mathbf{F}_{uDl}^{\perp}) \quad \forall i \in \{1 \dots n\} \quad 2-8$$

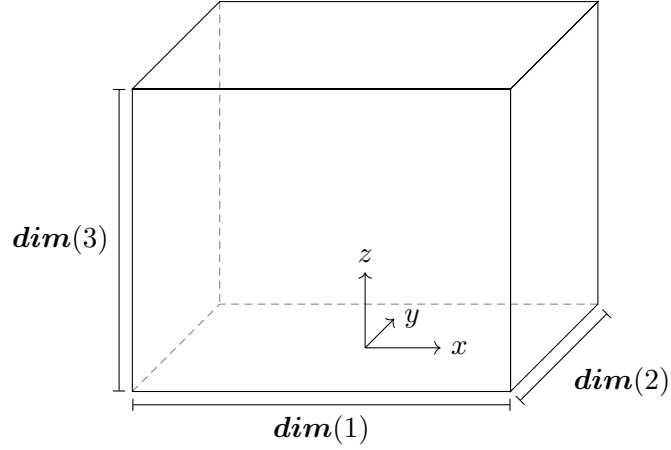


Figure 2-3: Environment Schematic

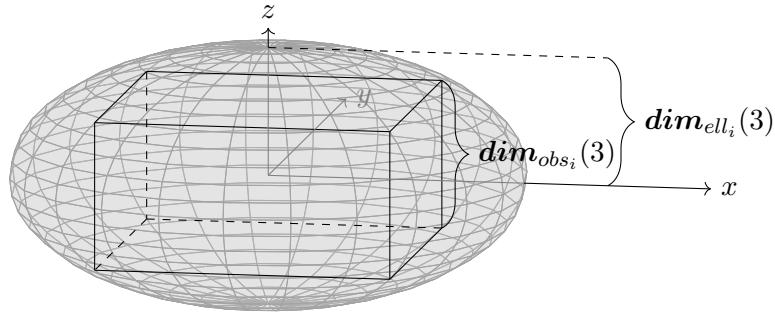


Figure 2-4: Obstacle dimensions

### 2-2-3 Environment Definition

The environment is defined as a 3 dimensional box with the origin in the floor's center. We denote the box's dimensions as  $\mathbf{dim} \in \mathbb{R}_{>0}^3$ . A schematic of the environment can be seen in figure 2-3.

### 2-2-4 Obstacle Modeling

Obstacles are modeled as three dimensional boxes and their behavior is modeled as linear movement using a Kalman Filter. This is required so that the planner takes into account future movement of the obstacles. The number of obstacles is denoted by  $n_{obs} \in \mathbb{Z}_{\geq 0}$ , their center position by  $\mathbf{p}_{obs_i} \in \mathbb{R}^3$  and their dimension by  $\mathbf{dim}_{obs_i} \in \mathbb{R}_{>0}^3$ .

Often we will use the smallest ellipsoid that contains the box. The equations to find the radial dimensions of the ellipsoid (denoted as  $\mathbf{dim}_{ell_i} \in \mathbb{R}^3$ ) are:

$$\mathbf{dim}_{ell_i} = \frac{\sqrt{3}}{2} \mathbf{dim}_{obs_i} \quad \forall i \in \{1 \dots n_{obs}\} \quad 2-9$$

A schematic of an obstacle and its dimensions can be seen in figure 2-4. For further explanation refer to his thesis[6].

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# Glossary

## List of Acronyms

<b>FME</b>	Facultat de Matemàtiques i Estadística
<b>IRI</b>	Institut de Robòtica i Informàtica Industrial
<b>MPC</b>	Model Predictive Control
<b>COM</b>	Center Of Mass
<b>ENU</b>	East-North-Up
<b>EOMs</b>	Equations of Motion

## List of Symbols

### Greek Symbols

$\phi_i \in \mathbb{R}$	Pitch of the $i$ -th quadrotor
$\theta_i \in \mathbb{R}$	Roll of the $i$ -th quadrotor
$\varphi_i \in \mathbb{R}$	Second payload angle of the $i$ -th quadrotor
$\vartheta_i \in \mathbb{R}$	First payload angle of the $i$ -th quadrotor

### Latin Symbols

$\Delta t \in \mathbb{R}_+$	Time between stages in the Model Predictive Control (MPC) formulation
$e_3 \in \mathbb{R}^3$	Down vector, $[0, 0, -1]^T$
$\mathbf{F}_{Di} \in \mathbb{R}^3$	Aerodynamic drag on the $i$ -th drone
$\mathbf{F}_{Dl} \in \mathbb{R}^3$	Aerodynamic drag on the payload
$\mathbf{F}_{uDi}$	Addition of $\mathbf{F}_{ui}$ and $\mathbf{F}_{Di}$
$\mathbf{F}_{ui} \in \mathbb{R}^3$	Input force of the $i$ -th quadrotor
$\mathbf{F}_{ui}^{\parallel} \in \mathbb{R}^3$	Orthogonal projection of $\mathbf{F}_{ui}$ along $\mathbf{q}_i$
$\mathbf{F}_{ui}^{\perp} \in \mathbb{R}^3$	Orthogonal projection of $\mathbf{F}_{ui}$ to the plane normal to $\mathbf{q}_i$
$\mathbf{M}_q \in \mathcal{S}_+^3$	Mass Matrix
$\mathbf{p}_i \in \mathbb{R}^3$	Position of the $i$ -th quadrotor
$\mathbf{p}_l \in \mathbb{R}^3$	Payload's location
$\mathbf{q}_i \in \mathbb{S}^2$	Direction of the $i$ -th link
$\mathbf{T}_i \in \mathbb{R}^3$	Tension exerted on the $i$ -th drone
$\mathbf{w}_i \in \mathbb{R}^3$	Rotation of the $i$ -th link's direction
$\mathbf{z} \in \mathbb{R}^{3n+2+n_{var}}$	Asd
$\mathbf{dim} \in \mathbb{R}_{>0}^3$	Environment dimensions
$\mathbf{dim}_{ell_i} \in \mathbb{R}^3$	Ellipsoid dimensions of the $i$ -th obstacle
$\mathbf{dim}_{obs_i} \in \mathbb{R}_{>0}^3$	Dimension of the $i$ -th obstacle
$\mathbf{p}_{obs_i} \in \mathbb{R}^3$	Position of the $i$ -th obstacle
$\mathbf{ss}_i \in \mathbb{R}^6$	System states for the $i$ -th quadrotor
$\mathbf{ss}_{\dot{z}i} \in \mathbb{R}^2$	System states of $h_{\dot{z}}$ for the $i$ -th quadrotor
$\mathbf{ss}_{\phi i} \in \mathbb{R}^2$	System states of $h_{\phi}$ for the $i$ -th quadrotor
$\mathbf{ss}_{\theta i} \in \mathbb{R}^2$	System states of $h_{\theta}$ for the $i$ -th quadrotor
$C_x$	Cost of objective x
$h_{\dot{z}}$	Identified system for $\dot{z}$
$h_{\phi}$	Identified system for $\phi$
$h_{\theta}$	Identified system for $\theta$
$k \in \mathbb{R}_+$	Maximum iteration factor for external planner
$k_{Di} \in \mathbb{R}$	Drag constant of the $i$ -th quadrotor
$k_{Dl} \in \mathbb{R}$	Drag constant of the payload
$l_i \in \mathbb{R}_{>0}$	Length of the $i$ -th link

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$m_i \in \mathbb{R}_{>0}$	Mass of the $i$ -th quadrotor
$m_l \in \mathbb{R}_{>0}$	Payload's mass
$N \in \mathbb{Z}_+$	Number of stages in the MPC formulation
$n \in \mathbb{Z}_{>0}$	Number of quadrotors
$n_{maxit} \in \mathbb{Z}_+$	Maximum number of iterations of the MPC solver
$n_{obs} \in \mathbb{Z}_{\geq 0}$	Number of obstacles
$n_{var} \in \mathbb{Z}_{>0}$	Number of variables in the state vector
$slack \in \mathbb{R}_{\geq 0}$	First slack variable
$slack_{env} \in \mathbb{R}$	Second slack variable
$t_{horizon} \in \mathbb{R}_+$	Planning time horizon
$t_{it}$	Time per iteration
$t_{MPC} \in \mathbb{R}_+$	MPC solve time
$t_{step} \in \mathbb{R}_+$	Control loop time
$W_x$	Weight of objective x

### Other

$S^2 \subset \mathbb{R}^3$	Set of unit vectors in $\mathbb{R}^3$
$slacks \in \mathbb{R}^2$	Slack variables
$u_i \in \mathbb{R}^3$	Inputs of the $i$ -th quadrotor
$u_t \in \mathbb{R}^{3n}$	Inputs of all quadrotors
$x \in \mathbb{R}^{n_{var}}$	State vector