M4 - Computational Dynamics

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1 Introduction

Perform a full kinematic analysis of the inverted slider-crank mechanism shown in figure 1 and determine the maximum acceleration $|\vec{r_E}|$ experienced at point E.

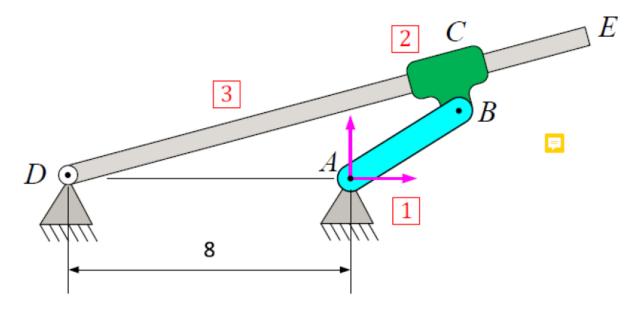
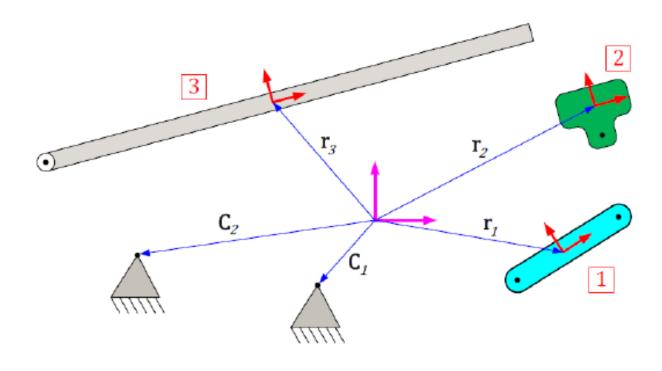


Figure 1: Slider-Crank mechanism





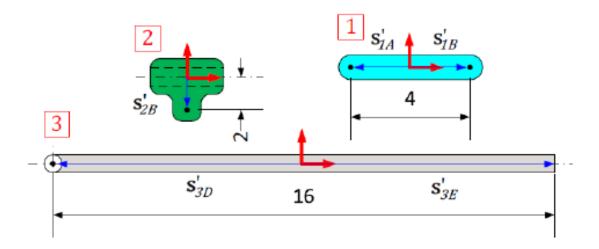


Figure 2: Expanded view of Slider-Crank mechanism

2 Exercises

- a Define joints (Constraints needed (use figure 2)
- b Setup the kinematic constraint equation Φ^K
- c Setup a driver constraint equations Φ^D so body 1 rotates at $\phi=1.5\frac{rad}{s}$
- d Do position analysis for t=0...10seconds
- e Plot graphs of results and animate
- f Determine the constraint Jacobian Φ_q
- g Setup the velocity- and acceleration equations
- h Calculate the velocity \dot{q} and acceleration \ddot{q} over time
- i Plot all results to verify their consistency (q,\dot{q},\ddot{q})
- j Determine the maximum value of the acceleration in the point E, $|\ddot{r_E}|$



3 Defining constraints

Looking at figure 1 it can be seen that 3 bodies are described in the Slider-Crank mechanism. The First arm is described by being locked into a position while rotation and controlling the slider in the end. Body 2 is a slider which is locked with the first body while rotation and thereafter translating on the third body. The third body can be seen being locked into a position while rotation based on the slider. Having 3 bodies is to have 9 generalized Cartesian coordinates but as the second body can be describes as a relative revolution-translational composite joint, 2 bodies can describe the mechanism. Following constraints are used to define the mechanism using figure 2 to reduce the number of DOF.

- 1. Absolute x-y constraint on body 3 using C_2 .
- 2. Absolute x-y constraint on body a using C_1 .
- 3. Composite revolution-translational composite joint between body 1 and 3

The number of DOF can therefore now be calculated

$$DOF = 3 \cdot NB - NH = 3 \cdot 2 - 2 - 2 - 1 = 1 \tag{3.1}$$

Having 1 DOF can now result in the mechanism can be solve by having one absolute driven constraint.

The kinematic constraint can be made by using the constraint described above and using the dimensions from figure 2.

$$\Phi^{K} = \begin{bmatrix} x_{1} - 2\cos(\theta_{1}) \\ y_{1} - 2\sin(\theta_{1}) \\ \cos(\theta_{2}) (y_{1} - y_{2} + 2\sin(\theta_{1}) - 8\sin(\theta_{2})) - \sin(\theta_{2}) (x_{1} - x_{2} + 2\cos(\theta_{1}) - 8\cos(\theta_{2})) + 2 \\ x_{2} - 8\cos(\theta_{2}) + 8 \\ y_{2} - 8\sin(\theta_{2}) \end{bmatrix}$$
(3.2)

By concatenating the kinematic constraint with the driven constraint, the constraint matrix can be defined as

$$\Phi = \begin{bmatrix}
x_1 - 2\cos(\theta_1) \\
y_1 - 2\sin(\theta_1) \\
\cos(\theta_2) (y_1 - y_2 + 2\sin(\theta_1) - 8\sin(\theta_2)) - \sin(\theta_2) (x_1 - x_2 + 2\cos(\theta_1) - 8\cos(\theta_2)) + 2 \\
x_2 - 8\cos(\theta_2) + 8 \\
y_2 - 8\sin(\theta_2) \\
\theta_1 - \frac{3t}{2}
\end{bmatrix} (3.3)$$

3.1 Deriving Jacobian

The Jacobian constraint can be found by deriving the constraint matrix by the generalised coordinates which is defined as

$$q = \begin{bmatrix} x_1 \\ y_1 \\ \theta_1 \\ x_2 \\ y_2 \\ \theta_2 \\ x_3 \\ y_3 \\ \theta_3 \end{bmatrix}$$
(3.4)



3.2 Deriving ν

Nu can be found using the chain rule on Φ to derive the velocity.

$$\nu = \Phi_q \cdot \dot{q} = -\Phi_t = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ \frac{3}{2} \end{bmatrix}$$
 (3.6)

Using equation (3.3) and taking the partial derivative, Nu can be found

3.3 Deriving γ

Gamma can be found by using the chain rule for nu.

$$\gamma = \Phi_q \cdot \ddot{q} = -(\Phi_q \cdot \dot{q})_q \cdot \dot{q} + \Phi_{qt} \cdot \dot{q} + \Phi_{tq} \cdot \dot{q} - \Phi_{tt} = -(\Phi_q \cdot \dot{q})_q \cdot \dot{q} - \Phi_{tt} =$$
(3.7)

$$\begin{bmatrix} -2\hat{\phi}\cos\left(\theta_{0}\right) \\ -2\hat{\phi}\sin\left(\theta_{0}\right) \\ -\hat{\phi}_{2}\left(\sin\left(\theta_{0}\right)\right) - \hat{\phi}_{1}\left(\hat{\theta}_{1}\left(\sin\left(\theta_{0}\right)\left(x_{1} - x_{2} + 2\cos\left(\theta_{1}\right) - \cos\left(\theta_{1}\right)\sin\left(\theta_{1}\right)\right)\right) - \hat{\phi}_{1}\left(2\cos\left(\theta_{1}\right)\sin\left(\theta_{1}\right)\right) - \hat{\phi}_{2}\left(2\cos\left(\theta_{1}\right)\sin\left(\theta_{1}\right)\right) - \hat{\phi}_{2}\left(2\cos\left(\theta_$$

The double partial derivative with respect to q and t is zero, it is removed from the equation.

4 Simulation

To simulate the position and orientation of the pendulum, values of q have to be found. As the system is nonlinear, Newton-Raphson method can be applied to approximate the values within a tolerance.

$$x_{n+1} = x_n - \frac{f(x_n)}{f'(x_n)} \tag{4.1}$$

To determine the maximum value of the acceleration at point $|\ddot{r_E}|$, the resultant acceleration have to found. By applying Pythagoras for the absolute value of the x- and y-acceleration at each point and thereafter finding the highest value, will give the resultant acceleration.

$$|\ddot{r}_{E|Result} = max(\sqrt{x_i^2 + y_i^2}) = 17.60[m/s^2]$$
 (4.2)

To determine the maximum acceleration, the angular acceleration times the radius can be used.

$$|\ddot{\ddot{r}}_{B\theta} = \dot{\omega} \cdot R = 19.00[Rad/s^2] \tag{4.3}$$



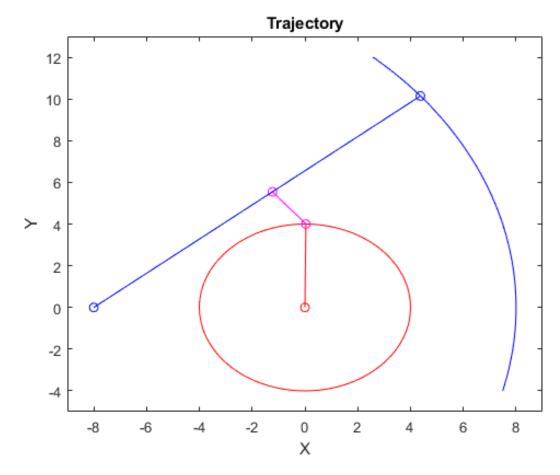


Figure 3: Trajectory



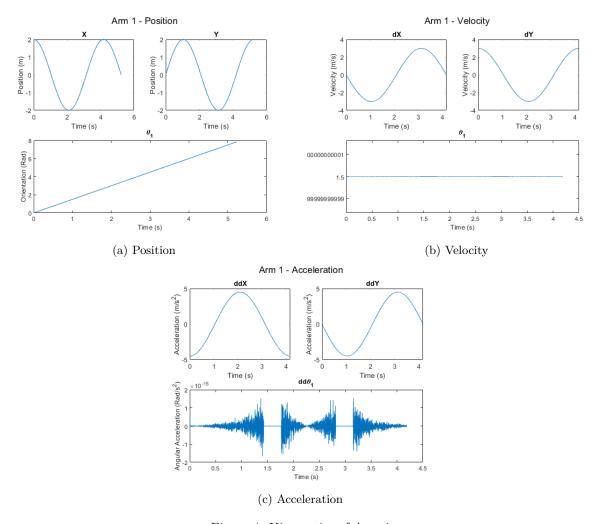


Figure 4: Kinematics of Arm 1



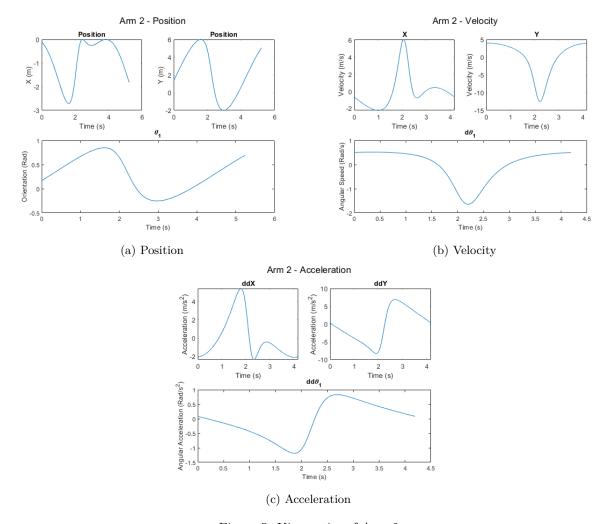


Figure 5: Kinematics of Arm 2



5 Appendix

5.1 Symbolics

```
1 sympref('AbbreviateOutput', false);
  2 syms x_1 y_1 theta_1 x_2 y_2 theta_2 x_1 x_2 omega x_1
 3 syms x_dot_1 y_dot_1 theta_dot_1 x_dot_2 y_dot_2 theta_dot_2;
 7 R = [0 -1; 1 0]
 9 	 r_1 = [x_1; y_1];
10 Al = [cos(theta_1) -sin(theta_1); sin(theta_1) cos(theta_1)];
r_2 = [x_2; y_2];
12 A2 = [cos(theta_2) -sin(theta_2); sin(theta_2) cos(theta_2)];
14
15 \quad C = -2
16 \quad Q_i = [-8; 0];
17 P_i = [8;0];
18 \text{ si-p} = [8;0];
19 vi_p = transpose([P_i(1)-Q_i(1) P_i(2)-Q_i(2)]);
20 vi = A2*vi_p
vvi = norm(Q_i - P_i);
22 \text{ si-j} = [2;0];
23
25 phi_k2 = (1/vvi)*vi_p.'*R.'*A2.'*(r_1+A1*si_j-r_2-A2*si_p)-C
26 phi_k3 = r_2 + A2*[-8; 0]-[-8; 0] % Rod x-y constraint
phi_k1 = r_1 + A1 * [-2; 0]
                                                                                                                       % Rod x-y constraint
28 phi_K = [phi_k1; phi_k2; phi_k3]
phi_D = [theta_1 - 1.5*t]
q = [x_1; y_1; theta_1; x_2; y_2; theta_2]
31 phi = [phi_K;phi_D]
32 phiq = jacobian(phi,q) % Jacobian
33 phit = -diff(phi,t)
q_d = [x_d - 1 y_d - 1 x_d -
gamma = -jacobian(phiq*q_dot,q)*q_dot-diff(phit,t)
36
37
38
39 % matlabFunction(phi,'file','Phi');
40 % matlabFunction(phiq,'file','Phi_q');
41 % matlabFunction(phit,'file','Nu');
42 % matlabFunction(gamma, 'file', 'Gamma');
```

5.2 Main

```
1 close all; clear all
* How many revolutions
4 rev = (2*pi)/1.5;
5 t - 0.0 00:
2 % Defining start values
5 t = 0:0.001:rev*n_rev; % Time-span
                           % Length of time
6 N = length(t);
s = [1; 1; pi/6; 0.5; 0.5; pi/3;]; % Guess Values
_{\rm 10}\, % Finding Position, velocity and acceleration
   [q,q_dot,q_dot] = NewtonRaphston(t,q);
12
13 pp = 15; % Percentage into the simulation
14 p = round(N*(pp/100)); % Point in simulation
15
_{16}\, % Geometry of arms
17 Arm1_x = [0.4*\cos(q(3,p))];
18 Arm1_y = [0 \ 4*sin(q(3,p))];
```



```
19 Arm2_x = [-8 \ 8 \times \cos(q(6,p))];
20 Arm2_y = [0 16*sin(q(6,p))];
22 % Plotting Trajectory
23 figure(1)
24 plot(Arm1_x, Arm1_y, 'o-');
25 hold on
26 plot(Arm2_x, Arm2_y, 'o-');
27 plot (q(1,:),q(2,:),q(4,:),q(5,:))
28 xlim([-10 10])
29 ylim([-6 12])
30 title('Trajectory')
31 xlabel('X')
32 ylabel('Y')
33 hold off
34
35 figure(2)
36 sgtitle('Arm 1 - Position')
37 subplot (2,2,1)
38 plot(t,q(1,:))
39 title('X')
40 xlabel('Time (s)')
41 ylabel('Position (m)')
42 subplot (2,2,2)
43 plot(t,q(2,:))
44 title('Y')
45 xlabel('Time (s)')
46 ylabel('Position (m)')
47 subplot(2,2,[3 4])
48 plot(t,q(3,:))
49 title('\theta_1')
50 xlabel('Time (s)')
51 ylabel('Orientation (Rad)')
52
53 figure(3)
54 sgtitle('Arm 2 - Position')
55 subplot (2,2,1)
56 plot(t,q(4,:))
57 title('X')
58 xlabel('Time (s)')
59 ylabel('Position (m)')
60 subplot (2,2,2)
61 plot(t,q(5,:))
62 title('Y')
63 xlabel('Time (s)')
64 ylabel('Position (m)')
65 subplot (2, 2, [3 4])
66 plot(t,q(6,:))
67 title('\theta_1')
68 xlabel('Time (s)')
69 ylabel('Orientation (Rad)')
71 figure (4)
72 sgtitle('Arm 1 - Velocity')
73 subplot (2,2,1)
74 plot(t,q_dot(1,:))
   title('dX')
76 xlabel('Time (s)')
77 ylabel('Velocity (m/s)')
  subplot (2,2,2)
79 plot(t,q_dot(2,:))
80 title('dY')
81 xlabel('Time (s)')
82 ylabel('Velocity (m/s)')
83 subplot(2,2,[3 4])
84 plot(t,q_dot(3,:))
85 title('\theta_1')
86 xlabel('Time (s)')
87 ylabel('Angular Speed (Rad/s)')
89 figure (5)
90 sgtitle('Arm 2 - Velocity')
91 subplot (2,2,1)
```



```
92 plot(t,q_dot(4,:))
93 title('X')
94 xlabel('Time (s)')
95 ylabel('Velocity (m/s)')
96 subplot(2,2,2)
97 plot(t,q_dot(5,:))
98 title('Y')
99 xlabel('Time (s)')
100 ylabel('Velocity (m/s)')
101 subplot (2, 2, [3 4])
102 plot(t,q_dot(6,:))
103 title('d\theta_1')
104 xlabel('Time (s)')
105 ylabel('Angular Speed (Rad/s)')
106
107 figure (6)
108 sgtitle('Arm 1 - Acceleration')
109 subplot (2,2,1)
110 plot(t,q_ddot(1,:))
111 title('ddX')
112 xlabel('Time (s)')
113 ylabel('Acceleration (m/s^2)')
114 subplot (2,2,2)
115 plot(t,q_ddot(2,:))
116 title('ddY')
117 xlabel('Time (s)')
118 ylabel('Acceleration (m/s^2)')
119 subplot (2, 2, [3 4])
120 plot(t,q_ddot(3,:))
121 title('dd\theta_1')
122 xlabel('Time (s)')
123 ylabel('Angular Acceleration (Rad/s^2)')
125 figure (7)
126 sgtitle('Arm 2 - Acceleration')
127 subplot (2,2,1)
128 plot(t,q_ddot(4,:))
129 title('ddX')
130 xlabel('Time (s)')
131 ylabel('Acceleration (m/s^2)')
132 subplot (2,2,2)
133 plot(t,q_ddot(5,:))
134 title('ddY')
135 xlabel('Time (s)')
136 ylabel('Acceleration (m/s^2)')
137 subplot(2,2,[3 4])
138 plot(t,q_ddot(6,:))
139 title('dd\theta_1')
140 xlabel('Time (s)')
141 ylabel('Angular Acceleration (Rad/s^2)')
```

5.3 Φ

```
1 function phi = Phi(t,q)
2 %Phi
       PHI = Phi(T, THETA_1, THETA_2, X_1, X_2, Y_1, Y_2)
3 %
4
        This function was generated by the Symbolic Math Toolbox version 9.0.
5
6 %
       27-Mar-2022 13:05:23
7 x_1 = q(1);
s y_1 = q(2);
9 theta_1 = q(3);
10 x_2 = q(4);
y_2 = q(5);
12 theta_2 = q(6);
13
t2 = cos(theta_1);
t3 = cos(theta_2);
17 	 t4 = sin(theta_1);
```



```
18 t5 = sin(theta_2);

19 t6 = t2.*2.0;

20 t7 = t4.*2.0;

21 t8 = t3.*8.0;

22 t9 = t5.*8.0;

23 t10 = -t8;

24 t11 = -t9;

25 phi = ...

[-t6+x_1;-t7+y_1;-t5.*(t6+t10+x_1-x_2)+t3.*(t7+t11+y_1-y_2)+2.0;t10+x_2+8.0;t11+y_2;t.*(-3.0./2.0)+therapy |
```

5.4 Φ_q

```
1 function phiq = Phi_q(q)
2 %Phi_q
       PHIQ = Phi_q(THETA_1, THETA_2, X_1, X_2, Y_1, Y_2)
3 %
        This function was generated by the Symbolic Math Toolbox version 9.0.
        27-Mar-2022 13:05:24
6 %
7 x_1 = q(1);
8 y_1 = q(2);
9 theta_1 = q(3);
10 x_2 = q(4);
y_2 = q(5);
12 theta_2 = q(6);
14
t2 = cos(theta_1);
17 	 t3 = cos(theta_2);
18 t4 = sin(theta_1);
19 t5 = \sin(theta_2);
20 	 t6 = t2.*2.0;
t7 = t4.*2.0;
22 	 t8 = t3. *8.0;
23 	 t9 = t5.*8.0;
24 	 t10 = -t8;
25 phiq = ...
       reshape([1.0,0.0,-t5,0.0,0.0,0.0,0.0,1.0,t3,0.0,0.0,t7,-t6,t3.*t6+t5.*t7,0.0,0.0,1.0,|0.0,0.0,t5,1.0
```

5.5 ν

```
1 function phit = Nu
2 %Nu
3 % PHIT = Nu
4
5 % This function was generated by the Symbolic Math Toolbox version 9.0.
6 % 27-Mar-2022 13:05:24
7
8 phit = [0.0;0.0;0.0;0.0;0.0;3.0./2.0];
```

5.6 γ



```
x_2 = q(4);
y_2 = q(5);
13 theta_2 = q(6);
15 x_dot_1 = q_dot(1);
16 y_dot_1 = q_dot(2);
17 theta_dot_1 = q_dot(3);
18 x_{dot_2} = q_{dot_4};
19 y_{dot_2} = q_{dot_5};
theta_dot_2 = q_dot(6);
22
t2 = cos(theta_1);
24 t3 = cos(theta_2);
t4 = \sin(theta_1);
26 	 t5 = sin(theta_2);
28 t7 = theta_dot_2.^2;
29 	 t8 = t2.*t5.*2.0;
30 	 t9 = t3.*t4.*2.0;
31 t10 = -t9;
32 t11 = t8+t10;
33 t12 = t11.*theta_dot_1;
34 gamma = ...
       [t2.*t6.*-2.0;t4.*t6.*-2.0;theta_dot_2.*(t12+t3.*x_dot_1-t3.*x_dot_2+t5.*y_dot_1-t5.*y_dot_1-theta_dot_
```

