

Figure D [PLESHOW)

E: and effector (x,y) end effector position

(9.,92) : foint angles of 01,02 from absolut ref. respectively

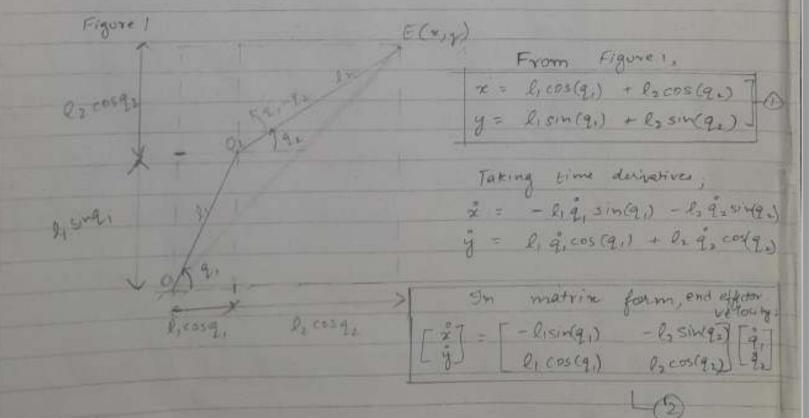
Assume: 0, Origin (0,0)

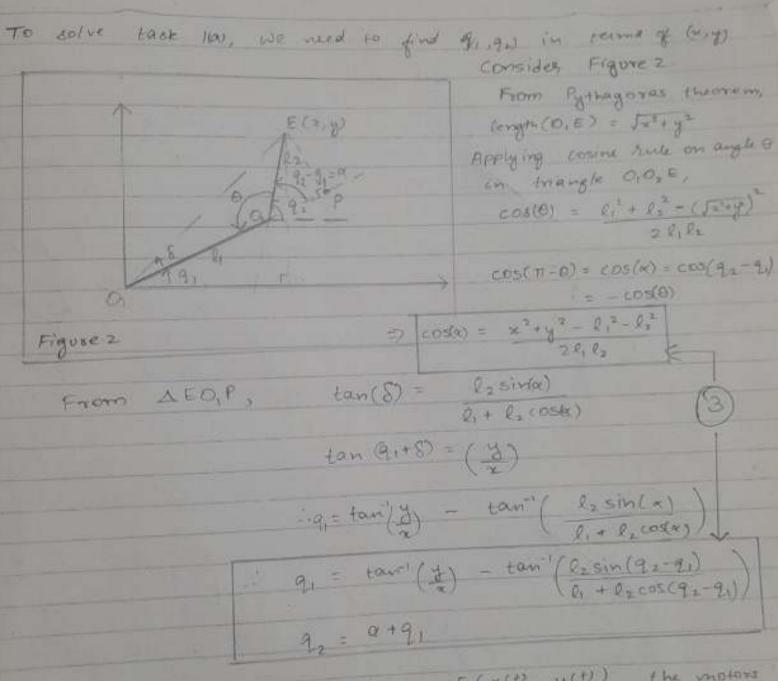
Irestal, Assume motors mo, 2 mo, connected

O(0,0) (8) 9, Irestal at joints 0,202 respectively Presume ma & max can have ability to control torques T, of Te applied at 0, 202 or the positions of angles 9,892

Task 1 (0) Tracking (x,y) using (2,140) (b) Tracking (z, y) using (t, Te) 10 noutralizing the dynamics (or 9,192)

Task Iai : solution





To track a given trajectory E(vct), yct)), the motors at 0, and 02 to be controlled in position control mode to achieve 9, 29, angular position at each time step.

Task TZ: Applying constant forcete against a wall Constant force Fo is applied through force control (torque control) made of the motors M1 at B1 & M2

at 02 respectively. assuming a hosizontal plane here to T2 Solution: (We are F.B.D of entire general overview of relevant manipulator Ny= Fy7 forces on the FBD 13) EX Na : Fre -> Also, we break to into Fx & fy F.B. D & link DID: Try liesse, Figure 5 Conserving moments about F-B-D & link 0, 2 02 in figures 4, 5,6, = Mon = 0 => Fylacosq - Falasing SMOZ=0 > Fylocosq - Fylosing = T Figure 6 To solve T2, we use 3) to position the end effector at the wall

and @ to apply necessary forus(torques)

Task 73: Make the end effector act as a spring centred at P(xo, yo) using a control scheme

Solution to task Ta:

2R manipulator as torques(TICH) step) Model the dynamics of the don

esp? cancel the torque dynamics

Peps: Insert the spring dynamics of Francy = - K(y-yo)

at the end effector.

Step1: We use Logrange's equations to derive dynamics TaskTIB)) Lagrangian L = K - V

(Kinetic (potential energy) energy)

> d (dL) - dL = Q' _ 5 dt (di) - dl = Q' _ 5 Generalized forces derived
> using principle of virtual us using principle of virtual work

 $K = \frac{1}{2} \operatorname{Io}_1 \omega_{0_1}^2 +$ 1 7 0 c4 Wcq + 1 m2 vc2 => k= 1 (1 mil, 2) 2, + 1 (12) mil 2) 22 + 1 mil 2 pure votation about O Potation of C.G. translation of OzE

 $6\frac{270}{4} = (2i\hat{q}_1)^2 + (2i\hat{q}_1)^2 + 22i\hat{q}_1 + 22i\hat{q}_2 \cos(q_1 - q_1)$ V= mgli sin(q) + mg (2, sin(q)) + 22 sin(q2))

page = 1 m. e. 2. 1 - (mg 2. sirey) + vmg 2(sirey, + mg 2 mg) Applying Lagrangian from equ (5) $i = \tau_1 = m_1 l_1^2 q_1 + m_2 l_1^2 q_1 + m_2 l_1 l_2 q_2 \cos(q_2 - q_1)$ $- m_2 - l_1 l_2 q_1^2 \sin(q_2 - q_1) + m_2 l_1 \cos(q_2) + m_2 g_1 \cos(q_2)$ $- 2 \cos(q_2 - q_1) + m_2 g_1 \cos(q_2) + m_2 g_1 \cos(q_2)$ $Q_2 = T_2 = m_2 l_2^2 \dot{q}_1 + m_2 l_3 l_2 \dot{q}_1 \cos(q_2 - q_3) + m_2 l_3 l_2 \dot{q}_1 \sin(q_3)$ $+ m_2 q_2 \cos(q_3)$ The Gorgne dynamics in @ solve tack 16 Z: Saving T. L. T. from @ as Traymamics & T. and aim to obtain E(x,y) through (3) dynamics based solution.

Step 3: Calculation of spring dynamics.

Fapring = -k_x(x-x0) = -k_x(xdisplacement) = others.

Fapring y = -k_y(y-y0) = -k_y(ydisplacement) = others.

Using x = dx, y = dy in (1),

Fylicosq1 - Fxlising1 = T1

=> ky dylpos(q1) - kx dxl1sing1) = Tispring

ky dylpos(q2) - kx dxl2sin(q2) = T2spring

L(7)

To achieve spring - like behaviour from end effector, we need to account for the torque of the 2R manipulator dynamics calculated in (6)

Thotal proton Tispring + Tidynamics

Thotalmotors = To spring + Todynamica