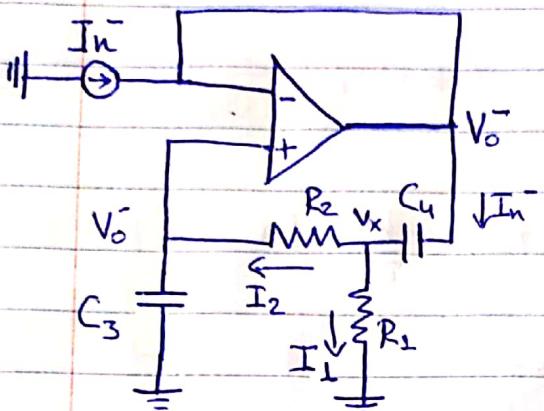


Άσκηση 1

Θα χρησιμοποιούσουμε επαρδανία για τις 3 πηγές θρύψου.



• Έστω μήδος I_n^-

$$V_o^- = V^- = V^+$$

$$I_n^- = I_1 + I_2$$

$$I_1 = \frac{V_x}{R_L}$$

$$I_2 = \frac{V_x - V_o^-}{R_2} = V_o S C_3 \Rightarrow$$

$$\Rightarrow V_x = R_2 \cdot V_o S C_3 + V_o^- = V_o^- (1 + S R_2 C_3)$$

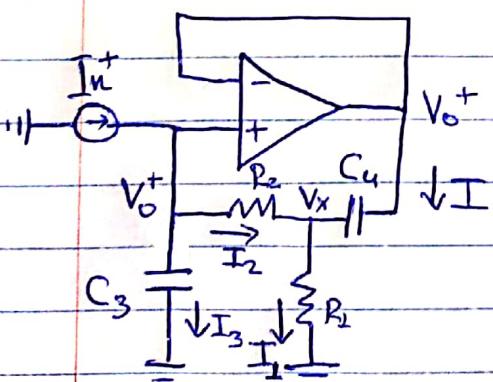
$$\text{Όποτε } I_n^- = \frac{V_o^- (1 + S R_2 C_3)}{R_L} + V_o S C_3 = V_o^- \left(\frac{1 + S R_2 C_3 + S C_3}{R_L} \right)$$

$$I_n^- = (V_o^- - V_x) S C_4 = V_o^- (S R_2 C_3 \cdot S C_4)$$

Αν οι τα παρανήνω σχούλες:

$$V_o^- (S R_2 C_3) \cdot S C_4 = V_o^- \left(\frac{1 + S R_2 C_3 + S R_L C_3}{R_L} \right) \Rightarrow$$

$$\Rightarrow V_o^- = 0 \quad , \quad H_L(j\omega) = 0$$



• Έστω μήδος I_n^+

$$I_n^+ = I_2 + I_3$$

$$I_2 = I_1 - I \Rightarrow \frac{V_o - V_x}{R_2} = \frac{V_x}{R_L} - I$$

$$\text{όπου } I = (V_o - V_x) S C_4 \text{ απα}$$

$$\frac{V_o - V_x}{R_2} = \frac{V_x}{R_L} - (V_o - V_x) S C_4 \Rightarrow$$

$$\frac{V_o}{R_2} + S C_4 V_o = \frac{V_x}{R_L} + S C_4 V_x + \frac{V_x}{R_2} \Rightarrow$$

$$\Rightarrow V_o = \frac{\frac{1}{R_1} + SC_4 + \frac{L}{R_2}}{\frac{1}{R_2} + SC_4} V_x \Rightarrow V_x = \frac{\frac{1}{R_2} + SC_4}{\frac{1}{R_2} + \frac{L}{R_1} + SC_4} V_o$$

$$I_n^+ = I_2 + I_3 = I_2 + V_o SC_3 = \frac{V_o - V_x}{R_2} + V_o SC_3 \Rightarrow$$

$$I_n^+ = V_o \left[\frac{1}{R_2} + SC_3 - \frac{\frac{1}{R_2} + SC_4}{\frac{1}{R_1} + \frac{L}{R_2} + SC_4} \right] \Rightarrow$$

$$\Rightarrow I_n^+ = V_o \left[\frac{1}{R_2} \left[\frac{\frac{1}{R_1}}{\frac{1}{R_1} + \frac{1}{R_2} + SC_4} \right] + SC_3 \right]$$

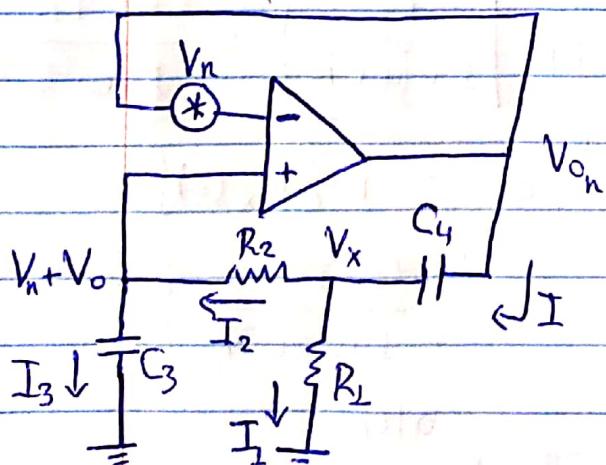
$$H_2(j\omega) = \frac{1}{\frac{1}{R_2} \left[\frac{\frac{1}{R_1}}{\frac{1}{R_1} + \frac{1}{R_2} + j\omega C_4} \right] + j\omega C_3} \Rightarrow$$

$$\Rightarrow H_2(j\omega) = \frac{R_1 + R_2 + j\omega R_1 R_2 C_4}{1 - R_1 R_2 C_3 C_4 \omega^2 + j\omega C_3 (R_1 + R_2)}$$

$$|H_2(j\omega)|^2 = \frac{(R_1 + R_2)^2 + (R_1 R_2 C_4 \omega)^2}{(1 - R_1 R_2 C_3 C_4 \omega^2)^2 + (C_3 (R_1 + R_2))^2 \omega^2}$$

$$\text{KOU} \quad \overline{I_n^+} = |H_2(j\omega)|^2 \overline{I_{n_0}^2}$$

• Eστω μόνο V_n



$$V^- = V^+ = V_{o_n} + V_n$$

$$I_3 = I_2 = (V_n + V_o) SC_3$$

$$I_1 = \frac{V_x}{R_1}$$

$$I = (V_o - V_x) SC_4 = I_2 + I_1$$

$$I_2 = \frac{V_x - (V_n + V_{o_n})}{R_2}$$

$$\text{Αρχ} \quad (V_n + V_{o_n}) SC_3 = \frac{V_x - (V_n + V_{o_n})}{R_2} \Rightarrow V_x = (V_n + V_{o_n}) [SC_3 R_2 + 1]$$

$$(V_{on} - V_x) SC_4 = \frac{V_x - (V_n + V_{on})}{R_2} + \frac{V_x}{R_L} \Rightarrow$$

$$\Rightarrow [V_{on} - (V_n + V_{on})(SC_3 R_2 + 1)] SC_4 = (V_n + V_{on}) SC_3 + \frac{(V_n + V_{on})}{R_L} (1 + SC_3 R_2)$$

$$\Rightarrow V_{on} \left(SC_4 - S^2 C_3 R_2 C_4 - SC_4 - SC_3 - \frac{1}{R_L} - \frac{SC_3 R_2}{R_L} \right) = V_n \left(SC_3 + \frac{1 + SC_3 R_2}{R_L} + \frac{S^2 C_3 R_2 C_4}{R_L} + SC_4 \right)$$

$$\Rightarrow \frac{V_{on}}{V_n} = - \frac{S^2 C_3 R_2 C_4 + S \left(C_3 + C_4 + \frac{C_3 R_2}{R_L} \right) + \frac{1}{R_L}}{S^2 C_3 R_2 C_4 + S \left(C_3 + \frac{C_3 R_2}{R_L} \right) + \frac{1}{R_L}}$$

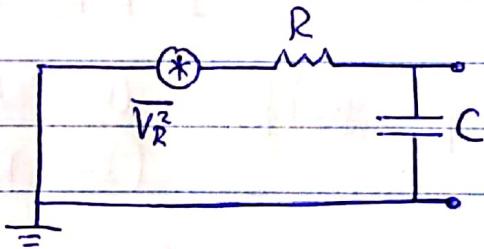
απα $|H_3(j\omega)|^2 = \frac{\left(\frac{1}{R_L} - \omega^2 R_2 C_3 C_4\right)^2 + \left(\omega \left(C_3 + C_4 + \frac{C_3 R_2}{R_L}\right)\right)^2}{\left(\frac{1}{R_L} - \omega^2 R_2 C_4 C_3\right)^2 + \left(\omega \left(C_3 + \frac{C_3 R_2}{R_L}\right)\right)^2}$

και $PSD = |H_3(j\omega)|^2 V_{n_0}^2$

Συνοδική στην εξόδο: $PSD_{o_1} = |H_2(j\omega)|^2 \overline{I_{n_0}^2} + |H_3(j\omega)|^2 \overline{V_{n_0}^2}$

Άσκηση 5

$$H = \frac{\frac{1}{SC}}{R + \frac{1}{SC}} = \frac{L}{1 + SCR}$$



$$H(j\omega) = \frac{L}{L + j\omega C R}$$

$$PSD = S_x = |H(j\omega)|^2 V_n^2 = 4kTR \left| \frac{L}{1 + j\omega CR} \right|^2 = \frac{4kTR}{1 + \omega^2 C^2 R^2}$$

$$S_x(f) = \int_{-\infty}^{+\infty} R_x(t) e^{-2\pi i t f} dt = F\{R_x(t)\}$$

Απα $R_x(t) = F^{-1}\{S_x(f)\} = F^{-1}\left\{ \frac{4kTR}{1 + \omega^2 C^2 R^2} \right\}$

Fourier: $\frac{2\alpha}{\alpha^2 + (2\pi f)^2} \leftrightarrow e^{-\alpha|t|}$

$$\frac{4kTR}{1+\omega^2 C^2 R^2} = \frac{\frac{4kTR}{C^2 R^2}}{\frac{1}{C^2 R^2} + (2\pi f)^2} = \frac{\alpha = \frac{1}{RC}}{\alpha^2 + (2\pi f)^2} =$$

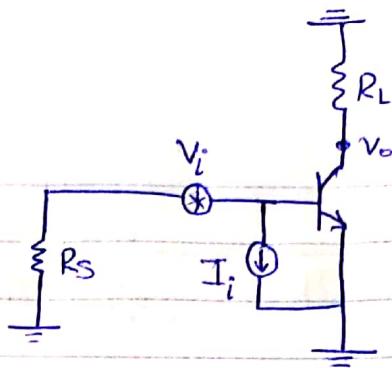
$$= 2kTR \frac{2\alpha}{\alpha^2 + (2\pi f)^2}$$

$\alpha = \sqrt{\frac{1}{RC}}$

$$R_x(t) = 2kT R e^{-\frac{|t|}{RC}}$$

Aorknon 4

$$g_m = \frac{I_c}{V_T} = 40 \frac{mA}{V}$$

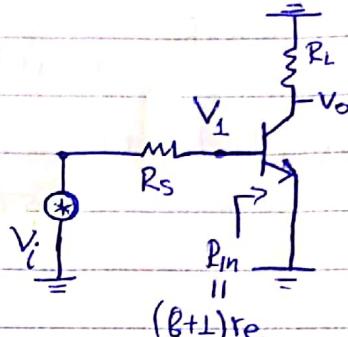


Enaddndia

• Εστω μέρος V_i

$$\frac{V_o}{V_L} = -g_m \cdot R_L \quad (\text{C})$$

$$\frac{V_L}{V_i} = \frac{R_{in}}{R_{in} + R_s} = \frac{(B+1) r_e}{(B+1) r_e + R_s}$$

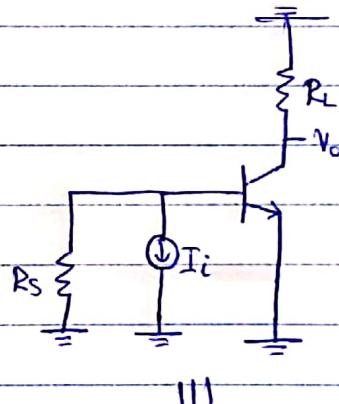


$$\frac{V_o}{V_i} = \frac{V_o}{V_L} \cdot \frac{V_L}{V_i} = -400 \cdot 0,565 \frac{V}{V} = -226 \frac{V}{V}$$

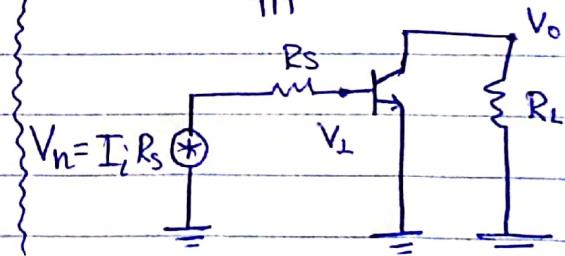
• Εστω μέρος I_i

Apa έχουμε Σανά:

$$\frac{V_o}{V_n} = \frac{V_o}{V_L} \cdot \frac{V_L}{V_i} = -226 \frac{V}{V}$$



$$\Rightarrow \frac{V_o}{I_i} = -226 \cdot R_s = -226 \frac{V}{mA}$$



Apa στην είσοδο έχουμε PSD:

$$\overline{V_o^2} = \left| \frac{V_o}{V_i} \right|^2 \cdot \overline{V_i^2} + \left| \frac{V_o}{I_i} \right|^2 \cdot \overline{I_i^2}$$

$$= 226^2 \cdot 4kT \left(\frac{1}{2g_m} \right) + (226 \cdot 10^3)^2 \cdot 2q (I_B)$$

$$= (1,06 \cdot 10^{-14} + 3,26 \cdot 10^{-13}) \frac{V^2}{Hz} = 3,37 \cdot 10^{-13} \frac{V^2}{Hz}$$

H συνάρτηση μεταφορέα's ονws unodxiosnke και npix είναι:

$$\frac{V_o}{i_s} = -226 \frac{V}{mA}$$

Άρα στην είσοδο έχουμε:

$$PSD_i = \frac{\overline{V_o^2}}{(226 \cdot 10^3)^2} = \frac{3,37 \cdot 10^{-13}}{5,1 \cdot 10^{10}} \frac{A^2}{Hz} = 6,61 \cdot 10^{-24} \frac{A^2}{Hz}$$

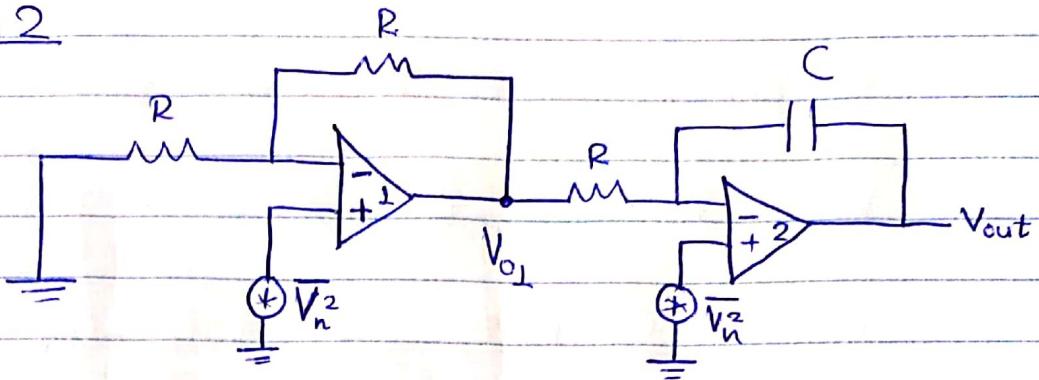
Για cutoff στα 2MHz έχουμε:

$$MDS_i = \sqrt{6,61 \cdot 10^{-24} \cdot 2 \cdot 10^6} A = 3,63 \cdot 10^{-9} A$$

H προσθοίμων στo LTSPICE για την συγκεκριμένη σύσκονθη
repariθεται στo τέλος της εργασίας αναφορά's.

Aσκηνον 2

A)



$$V_{o1} = \left(1 + \frac{R}{R}\right) V_n$$

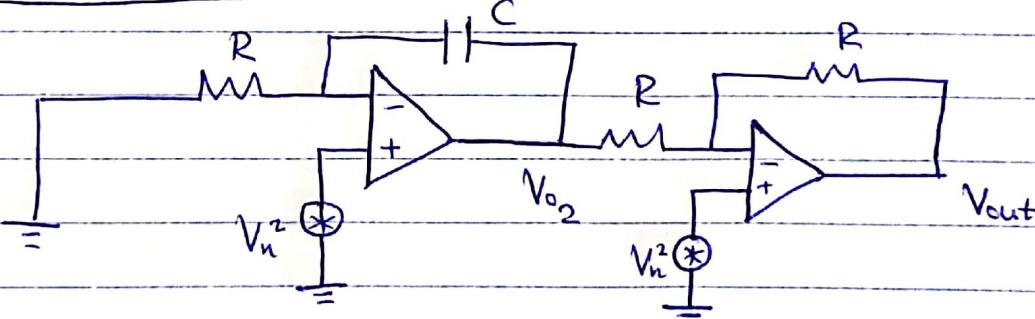
$$\overline{V_{o1}^2} = 4 \overline{V_n^2}$$

Γ)

$$\frac{V_{out}}{V_{o1}} = -\frac{\frac{1}{SC}}{R} \quad \overline{V_{out1}^2} = \left| -\frac{\frac{1}{SC}}{R} \right|^2 4 \overline{V_n^2} = \frac{4 \overline{V_n^2}}{\omega^2 C^2 R^2}$$

$$\frac{V_{out}}{V_n} = \left(1 + \frac{1/SC}{R}\right) \quad \overline{V_{out2}^2} = \left| \left(1 + \frac{1/SC}{R}\right) \right|^2 \overline{V_n^2} = \\ = \left(1 + \frac{1}{\omega^2 C^2 R^2}\right) \overline{V_n^2}$$

$$\overline{V_{out}^2} = \left(\frac{5}{(\omega C R)^2} + 1 \right) \overline{V_n^2}$$



B)

$$\frac{V_{o2}}{V_n} = \left(1 + \frac{1/CS}{R}\right) \Rightarrow \overline{V_{o2}^2} = \left(1 + \frac{1}{\omega^2 C^2 R^2}\right) \overline{V_n^2}$$

Δ)

$$\frac{V_{out}}{V_{o2}} = -\frac{R}{R} = -1$$

$$\frac{V_{out}}{V_n} = \left(1 + \frac{R}{R}\right) = 2$$

Σύνολική PSD : $\overline{V_{out2}^2} = \overline{V_{o2}^2} \cdot 1 + \overline{V_n^2} \cdot 4 = \left(5 + \frac{1}{(\omega C R)^2}\right) \overline{V_n^2}$

Ε) Στις χαμηλές συχνότητες προτιμώ το δεύτερο κύκλωμα, διότι για μικρά ως ο θόρυβος καθορίζεται κατά κύριο λόγο από τον παραγόντα με το $(wCR)^2$ στον παρανομαστή. Επομένως επιλέγουμε το κύκλωμα με το χαμηλότερο συντελεστή σε αυτού τον όρο. Αντίθετα, στις υψηλές συχνότητες όπου ο θόρυβος εξαρτάται κυρίως από τον σταθερό όρο, επιλέγουμε το πρώτο κύκλωμα.

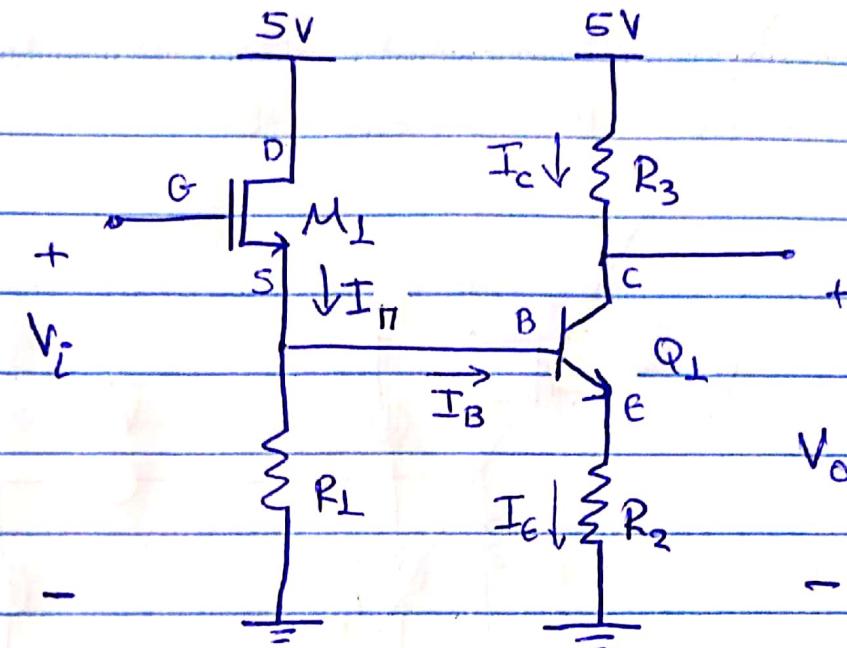
Άσκηση 3

DC Ανάδυση

$$V_{BE} = V_T \ln \left(\frac{I_C}{I_S} \right)$$

$$= 25 \text{ mV} \cdot \ln \frac{10^{-3}}{10^{-16}}$$

$$\Rightarrow V_{BE} = 0,748 \text{ V}$$



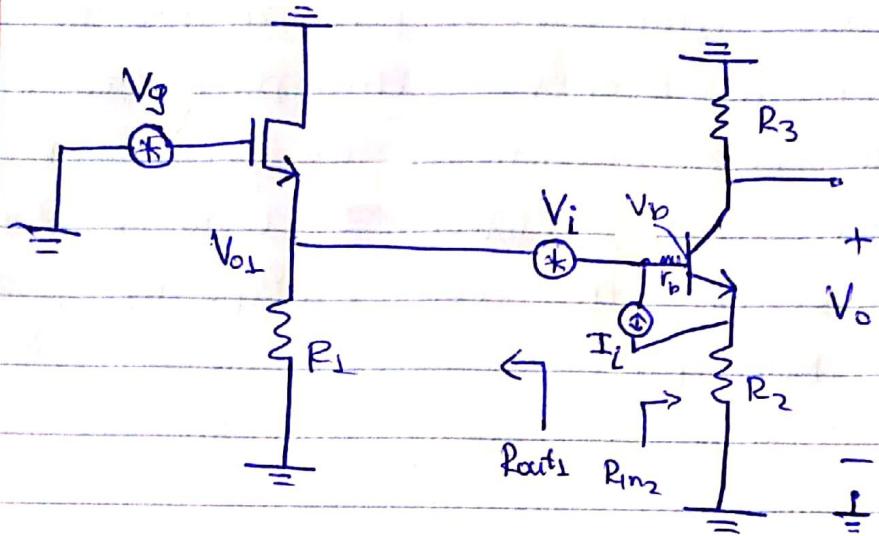
NTK

$$V_{BE} + I_C \cdot R_2 = (I_\pi - I_B) R_L$$

$$I_\pi = \frac{V_{BE} + I_C \cdot R_2}{R_L} + I_B = \frac{V_{BE} + \frac{I_C}{\alpha} R_2}{R_L} + \frac{I_C}{\beta} \Rightarrow$$

$$\Rightarrow I_\pi = 284 \text{ mA}$$

$$g_m = \sqrt{2 I_\pi \cdot \mu_n C_{ox} \cdot \frac{W}{L}} = 5,83 \frac{\text{mA}}{\text{V}}$$



Ersatzanordnung

• Vg

$$R_{in_2} = R_2(B+1) + r_b + r_n = R_2(B+1) + r_b + \frac{B}{g_m_{BJT}} = 12,7 \text{ k}\Omega$$

$$\frac{V_{0L}}{Vg} = \frac{R_{in_2}/R_1}{R_{in_2}/R_1 + \frac{1}{g_m}} = 0,65 \frac{\text{V}}{\text{V}}$$

$$\frac{V_b}{V_{0L}} = \frac{r_n + R_2(B+1)}{r_b + r_n + R_2(B+1)}$$

$$\frac{V_o}{V_b} = \frac{-R_3 g_m_{BJT} \cdot r_e}{R_2 + r_e}$$

alpha

$$\frac{V_o}{Vg} = \frac{V_o}{V_b} \cdot \frac{V_b}{V_{0L}} \cdot \frac{V_{0L}}{V_g} = \frac{-R_3 g_m_{BJT} \cdot r_e}{R_2 + r_e} \cdot \frac{r_n + R_2(B+1)}{r_b + r_n + R_2(B+1)}$$

• $\frac{R_{in_2}/R_1}{R_{in_2}/R_1 + \frac{1}{g_m}} = -10,2 \frac{\text{V}}{\text{V}}$

• V_i

$$\frac{V_o}{V_i} = \frac{V_o}{V_b} \cdot \frac{V_b}{V_{o1}} = \frac{V_o}{V_b} \cdot \frac{r_n + R_2(B+1)}{r_b + r_n + R_2(B+1) + R_{out1}} = -16$$

j510

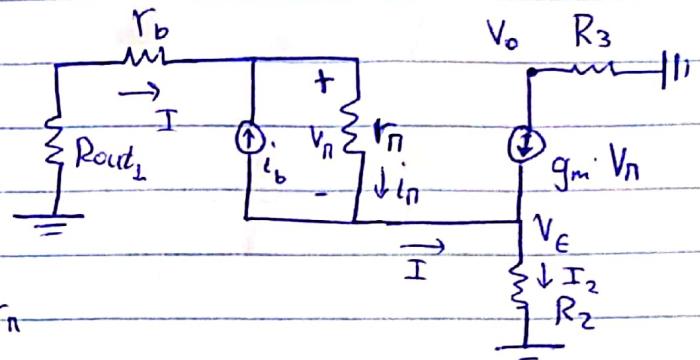
• I_i

$$R_{out1} = \frac{1}{g_m} \parallel R_1 = 108,89 \Omega$$

$$V_o = -g_m \cdot V_n \cdot R_3 \Rightarrow V_n = \frac{-V_o}{g_m R_3}$$

$$I = i_n - i_b \quad i_n = V_n / r_n$$

$$I_2 = g_m \cdot V_n + i_n - i_b$$



$$V_n + V_E = -I \cdot (r_b + R_{out1}) \Rightarrow V_n + I_2 \cdot R_2 = -I (r_b + R_{out1})$$

$$\Rightarrow V_n + (g_m V_n + i_n - i_b) R_2 = -(i_n - i_b) (r_b + R_{out1})$$

$$\Rightarrow V_n + (g_m V_n + \frac{V_n}{r_n} - i_b) R_2 = -(\frac{V_n}{r_n} - i_b) (r_b + R_{out1})$$

$$\Rightarrow V_n \left(1 + g_m + \frac{1}{r_n} \right) R_2 - i_b \cdot R_2 = V_n \left(-\frac{1}{r_n} \cdot r_b + R_{out1} \right) + i_b (r_b + R_{out1})$$

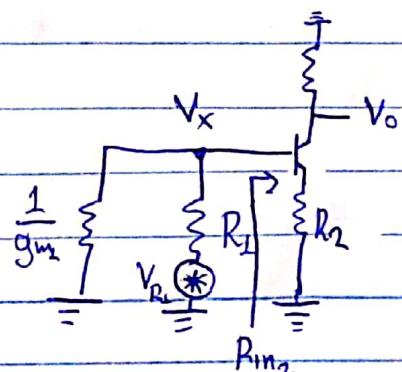
$$\Rightarrow -\frac{V_o}{g_m R_3} \left[\left(1 + g_m + \frac{1}{r_n} \right) R_2 + \frac{r_b + R_{out1}}{r_n} \right] = i_b (R_2 + r_b + R_{out1})$$

$$\frac{V_o}{i_b} = \frac{g_m R_3 (R_2 + r_b + R_{out1})}{R_2 + g_m R_2 + \frac{R_2}{r_n} + \frac{r_b + R_{out1}}{r_n}} = -4,82 \frac{V}{mA}$$

• Θερμικός θύρας R_1

$$V_x = \frac{\frac{1}{g_m} \parallel R_{in2}}{\frac{1}{g_m} \parallel R_{in2} + R_1} V_{R_1}$$

$$\frac{V_o}{V_x} = \frac{V_o}{V_b} \cdot \frac{V_b}{V_{o1}} = -16$$

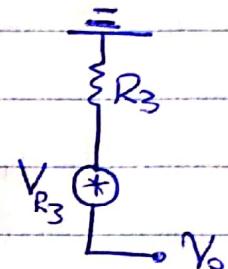


$$\frac{V_o}{V_{R_1}} = \frac{V_o}{V_x} \cdot \frac{V_x}{V_{R_1}} = -16 \cdot 0,357 = -5,72 \frac{V}{V}$$

- Θερμικός θόρυβος R_3

Θεωρούμε ότι ανά την έξοδο βρέθηκε $r_o = \infty$ για το BJT

Apa $\frac{V_o}{V_{R_3}} = 1$



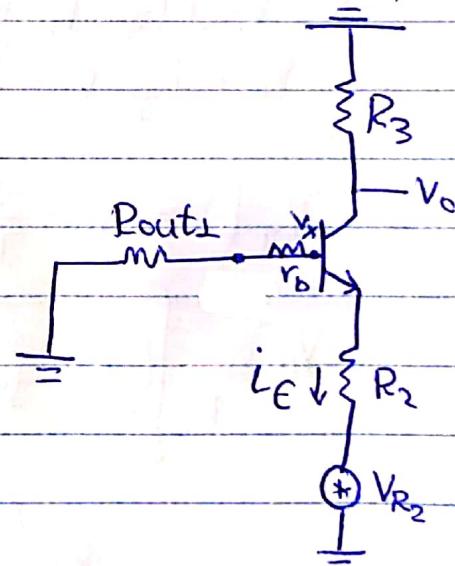
- Θερμικός θόρυβος R_2

$$i_E = -\frac{V_{R_2}}{R_2 + r_e + \frac{R_{out1} + r_b}{\beta + 1}}$$

$$V_o = +\alpha \left(\frac{V_{R_2}}{R_2 + r_e + \frac{R_{out1} + r_b}{\beta + 1}} \right) R_3$$

$$\Rightarrow \frac{V_o}{V_{R_2}} = \frac{\alpha R_3}{R_2 + r_e + \frac{R_{out1} + r_b}{\beta + 1}}$$

$$\Rightarrow \frac{V_o}{V_{R_2}} = 15,89 \frac{V}{V}$$



Έχουμε τις συναρτήσεις μεταφοράς για όλες τις πηγές θορύβου, δρισκώ τη συνολική PSD στην έξοδο

$$\begin{aligned}
 V_o^2 &= \left| \frac{V_o}{V_g} \right|^2 \bar{V_g}^2 + \left| \frac{V_o}{V_i} \right|^2 \bar{V_i}^2 + \left| \frac{V_o}{i_b} \right|^2 \bar{I_i}^2 + \left| \frac{V_o}{V_{R_1}} \right|^2 \cdot \bar{V_{R_1}}^2 + \bar{V_{R_3}}^2 + \left| \frac{V_o}{V_{R_2}} \right|^2 \bar{V_{R_2}}^2 \\
 &= 10,2^2 \cdot 4kT \frac{2}{3} \frac{1}{g_m} + 16^2 \cdot 4kT \left(r_b + \frac{1}{2g_{m_{BJT}}} \right) \\
 &\quad + (4,82 \cdot 10^3)^2 2q I_B + 5,72^2 4kT \cdot R_1 \\
 &\quad + 4kT R_3 + 15,89^2 4kT \cdot R_2 \\
 &= (1,97 \cdot 10^{-16} + 4,78 \cdot 10^{-16} \\
 &\quad + 7,43 \cdot 10^{-17} + 1,63 \cdot 10^{-16} \\
 &\quad + 3,32 \cdot 10^{-17} + 4,191 \cdot 10^{-16}) \frac{V^2}{Hz} = 1,36 \cdot 10^{-15} \frac{V^2}{Hz}
 \end{aligned}$$

Apa $PSD_{in} = \frac{PSD_{out}}{\frac{V_o}{V_g}} = \frac{PSD_{out}}{10,2^2} = 1,31 \cdot 10^{-17} \frac{V^2}{Hz}$