

Hand-in 2

a) Known:

$$l = 0.16 \text{ m}$$

$$\alpha'_1 = 48^\circ$$

$$\alpha'_2 = 16^\circ$$

$$i = 0^\circ$$

$$a = 0.4 \text{ l}$$

compressor cascade

design point

Solution:

$$\varepsilon = \alpha_1 - \alpha_2, \quad \alpha_1 = \alpha'_1 + i, \quad \alpha_2 = \alpha'_2 + \delta$$

$$(i = 0) \Rightarrow \varepsilon = \alpha'_1 - \alpha'_2 - \delta$$

$$\delta = m \theta \sqrt{\frac{s}{l}}, \quad \theta = \alpha'_1 - \alpha'_2$$

$$m = 0.23 \left(\frac{2a}{l} \right)^2 + \frac{\alpha_2}{500} = 0.23 \left(\frac{2a}{l} \right)^2 + \frac{\alpha'_2 + \delta}{500}$$

$$\Rightarrow \delta = \frac{0.23 \left(\frac{2a}{l} \right)^2 + \frac{\alpha'_2}{500}}{1 - \frac{1}{500} \theta \sqrt{\frac{s}{l}}} \theta \sqrt{\frac{s}{l}} = \delta \left(\frac{s}{l} \right)$$

$$\Rightarrow \varepsilon = \alpha'_1 - \alpha'_2 - \delta \left(\frac{s}{l} \right) \quad \checkmark$$

$$\zeta = \frac{\Delta p_0}{\frac{1}{2} \rho c_m^2 l}, \quad D = s \Delta p_0 \cos(\alpha_m), \quad D = \theta_2 s c_2^2$$

$$\Rightarrow \zeta = \frac{2 \theta_2}{s \cos(\alpha_m) l} \frac{c_2^2}{c_m^2} = \left\{ \begin{array}{l} c_m = c_x / \cos(\alpha_m) \\ c_2 = c_x / \cos(\alpha_2) \end{array} \right\} =$$

$$= \frac{2 \left(\frac{\theta_2}{l} \right)}{\frac{s}{l} \cos(\alpha_m)} \frac{\cos(\alpha_m)}{\cos^2(\alpha_2)} = \left\{ \alpha_m = \tan^{-1} \left(\frac{\tan(\alpha_1) + \tan(\alpha_2)}{2} \right) \right\} =$$

$$= \frac{2 \frac{\theta_2}{l}}{\frac{s}{l} \cos(\alpha_2) \sqrt{\frac{1}{4} (\tan(\alpha_1) + \tan(\alpha_2))^2 + 1}} \quad \checkmark$$

where:

$$\frac{\theta_2}{l} = \frac{0.004}{1 - 1.17 \cdot \ln \left(\frac{f_{max,s}}{c_2} \right)}$$

$$f_{max,s} = \frac{c_2 \cos(\alpha_2)}{c_1 \cos(\alpha_1)} = \frac{0.4 \cos(16^\circ)}{0.4 \cos(48^\circ)} = 1.17$$

Hand-in 2 cont.

$$\frac{C_{\max, s}}{C_2} \approx \frac{\cos(\alpha_2)}{\cos(\alpha_1)} \left(1.12 + 0.61 \frac{s}{l} \cos^2(\alpha_1) (\tan(\alpha_1) - \tan(\alpha_2)) \right)$$

As for the physical reasons for the relations, flow deflection decreases with an increasing pitch-chord ratio, as there are less geometric features per unit length to turn the flow. The pressure loss initially decreases with a decreasing pitch-chord ratio since there's less surface area where losses due to boundary layers emerge, but then increases again. The increase is due to the large wake formations, subsequent from a large deviation angle.

b) The assumptions made to find the pressure loss, Liebleins empirically established relationships, assume in themselves an incompressible flow case. This entails that a higher maximum speed would decrease the accuracy of the assumption. Now, assuming a largely constant outflow speed C_2 , the fractions:

$$\left(\frac{C_{\max, s}}{C_2} \right)_{s/l=1} \approx 1.817, \quad \left(\frac{C_{\max, s}}{C_2} \right)_{s/l=2} \approx 1.996$$

tell us that $C_{\max, s}$ is higher for the second case and therefore the pressure loss prediction is less accurate.