

Q2. 2D fully developed steady flow,  $V_z = 0$ :  $V_z, V_y (y, z)$

C.E.  $\frac{\partial V_z}{\partial x} + \frac{\partial V_y}{\partial y} = 0 \Rightarrow V_z = \text{const.}$   $x=0, V_z=0 \Rightarrow V_z=0$

N.S.  $x$ :  $\frac{\partial p}{\partial x} = 0 \Rightarrow p = p(y)$ . At  $x=h, p = p_{\text{atm}} + y \Rightarrow p = p_{\text{atm}} + y(x, y)$   
 $\frac{\partial p}{\partial y} = 0$  N.S.  $y$  dir.  $\Rightarrow \mu \frac{\partial^2 V_y}{\partial z^2} = \rho g \Rightarrow V_y = \frac{\rho g}{2\mu} z^2 + C_1 z + C_2$

B.C.  $z=0, V_y=V_0 \Rightarrow C_2=V_0$ ;  $x=h, \frac{\partial V_y}{\partial z} = 0 \Rightarrow C_1 = -\rho g h / \mu$

$\Rightarrow V_y = V_0 - \frac{\rho g x}{\mu} (h - \frac{z}{2})$ ;  $\frac{Q}{w} = \int V_y dz = V_0 h - \rho g h^3 / 3\mu$

Q3. 2 flow regimes:  $0 < y < \frac{h}{2}$ : A  $\Rightarrow$  steady state, 2D, fully developed  $V_z^A, V_y^A = f(y)$   
 $\frac{h}{2} < y < h$ : B  $\Rightarrow V_z^B, V_y^B = f(y)$

Given  $\frac{\partial p}{\partial x} = 0, g f_x = 0$

C.E.  $\Rightarrow V_z^A = \text{const.}$  } B.C. at  $y=0 \Rightarrow V_y^A = 0$   
 $V_z^B = \text{const.}$  }  $y=h \Rightarrow V_y^B = 0$   
 N.S. in  $x$  direction  $\Rightarrow \frac{d^2 V_z^A}{dy^2} = 0 \Rightarrow V_z^A = C_1 y + C_2$  B.C.  $y=0, V_z^A = 0$   
 $\frac{d^2 V_z^B}{dy^2} = 0 \Rightarrow V_z^B = C_3 y + C_4$   $y = h/2, V_z^A = V_z^B, \mu_A \frac{dV_z^A}{dy} = \mu_B \frac{dV_z^B}{dy}$   
 $y=h, V_z^B = 0$

$\Rightarrow C_2 = 0$   
 $V_0 = C_1 h + C_4$   
 $C_1 \frac{h}{2} = C_3 \frac{h}{2} + C_4$   
 $\mu_A C_1 = \mu_B C_3$  }  $\Rightarrow V_z^A = \frac{\mu_B}{\mu_A + \mu_B} \frac{2 V_0 y}{h}$   
 $V_z^B = \frac{\mu_A}{\mu_A + \mu_B} \frac{2 V_0 (y-h)}{h} + V_0$

(Notice: velocity continuous at interface but slopes are not)



Q4. Fully developed  $\Rightarrow \frac{\partial V}{\partial z} = 0$  Assume  $V_0 = 0$  (laminar flow). Axisymmetry  $\Rightarrow \frac{\partial(\cdot)}{\partial \theta} = 0$

Steady  $\Rightarrow \frac{\partial(\cdot)}{\partial t} = 0$ ;  $\vec{V} = V_r \hat{e}_r + V_z \hat{e}_z$

C.E.  $\Rightarrow \frac{\partial(rV_r)}{\partial r} = 0 \Rightarrow rV_r = \text{const.} \Rightarrow V_r = 0$  (B.C. at  $r=R$ )

N.S.  $r$ :  $\frac{\partial p}{\partial r} = 0$ ;  $\theta: 0 = 0$ ;  $z$ :  $-\frac{\partial p}{\partial z} = -\rho g + \frac{\mu}{r} \frac{\partial}{\partial r} (r \frac{\partial V_z}{\partial r}) = 0$   
 $\frac{\partial p}{\partial r} = 0, \frac{\partial p}{\partial \theta} = 0 \Rightarrow p = f(z)$  at  $r=R-h, p = p_{\text{atm}} + z$   $\Rightarrow f(z) = p_{\text{atm}} + z \Rightarrow \frac{\partial p}{\partial z} = 0$

$\Rightarrow \frac{\mu}{r} \frac{d}{dr} (r \frac{dV_z}{dr}) = \rho g \Rightarrow V_z = \frac{\rho g}{4\mu} r^2 + C_1 \ln r + C_2$  at  $r=R, V_z = 0$   
 $r=R-h, \tau_{rz} = \mu \frac{dV_z}{dr} = 0$   
 $\Rightarrow C_1 = -\frac{\rho g (R-h)^2}{2\mu}$ ;  $C_2 = -\frac{\rho g R^2}{4\mu} + \frac{\rho g (R-h)^2 \ln R}{2\mu} \Rightarrow V_z = \frac{\rho g}{2\mu} \left\{ (R-h)^2 \ln \frac{R}{r} - \frac{(R^2 - r^2)}{2} \right\}$

Q5. radial flow  $\Rightarrow V_r \neq 0, V_\theta = V_z = 0$   $\frac{\partial(\cdot)}{\partial t} = 0, \frac{\partial(\cdot)}{\partial \theta} = 0, \frac{\partial V}{\partial z} = 0$

C.E.  $\Rightarrow \frac{\partial(rV_r)}{\partial r} = 0 \Rightarrow rV_r = \text{const.}$  at  $r=R_1, V_r = V_1 \Rightarrow V_r = \frac{R_1 V_1}{r}$

N.S.  $\frac{\partial p}{\partial \theta} = 0, \frac{\partial p}{\partial z} = -\rho g, \frac{\partial p}{\partial r} = -S V_r \frac{dV_r}{dr}$ ;  $P = p + \rho g z \Rightarrow \frac{\partial P}{\partial z} = \frac{\partial p}{\partial z} + \rho g = 0$   
 $P = P(r)$   $\frac{\partial P}{\partial r} = \frac{dP}{dr} \Rightarrow \frac{dP}{dr} = -S \left( \frac{R_1 V_1}{r} \right) \left( -\frac{R_1 V_1}{r^2} \right) = \frac{S V_1^2 R_1^2}{r^3} \Rightarrow P = -\frac{S V_1^2 R_1^2}{2 r^2} + C$   
 $P_1 = -\frac{S V_1^2 R_1^2}{2} + C \Rightarrow C = P_1 + \frac{S V_1^2 R_1^2}{2} \Rightarrow P = P_1 + \frac{S V_1^2}{2} \left( 1 - \frac{R_1^2}{r^2} \right)$

(Note by defining  $P$  we get rid of functionality of  $z$  in pressure)

Q6. Flow same as in Q2 of Tutorial sheet with  $\frac{\partial p}{\partial z} = 0 \Rightarrow V_z = C_1 \ln r + C_2$

B.C. at  $r=R_1, V_z = V_0$   $\Rightarrow V_z = V_0 \frac{\ln r/R_2}{\ln R_1/R_2}$ ;  $P_{\text{aver}} = \frac{(\text{shear force on wire}) \times V_0}{\tau_{\text{at } R_1} \times 2\pi R_1 L \times V_0}$   
 at  $r=R_2, V_z = 0$

$\Rightarrow P_{\text{aver}} = \frac{\mu V_0^2}{2\pi R_1 L \ln R_1/R_2}$

$\tau_{r3} = \mu \frac{dV_z}{dr} \bigg|_{R_1} = \frac{\mu V_0}{\ln R_1/R_2}$