

SOLUTIONS TO ASSIGNMENT 5

Q6. Solution: $T = T(x, t)$

$$dT = \frac{\partial T}{\partial x} dx + \frac{\partial T}{\partial t} dt$$

$$\left. \frac{dT}{dt} \right|_{\text{particle}} = \frac{\partial T}{\partial x} \left. \frac{dx}{dt} \right|_{\text{particle}} + \frac{\partial T}{\partial t}$$

or

$$\frac{DT}{dt} = \left. \frac{dT}{dt} \right|_{\text{particle}} = u \frac{\partial T}{\partial x} + \frac{\partial T}{\partial t}$$

For the given data, $u = U = \text{constant}$

$$\frac{\partial T}{\partial x} = \frac{\partial}{\partial x} \left[T_0 - \alpha e^{-x/L} \sin\left(\frac{2\pi t}{\tau}\right) \right] = \frac{\alpha}{L} e^{-x/L} \sin\left(\frac{2\pi t}{\tau}\right)$$

$$\frac{\partial T}{\partial t} = \frac{\partial}{\partial t} \left[T_0 - \alpha e^{-x/L} \sin\left(\frac{2\pi t}{\tau}\right) \right] = -\frac{2\pi}{\tau} \alpha e^{-x/L} \cos\left(\frac{2\pi t}{\tau}\right)$$

Substituting,

$$\frac{DT}{dt} = \left[\frac{U}{L} \sin\left(\frac{2\pi t}{\tau}\right) - \frac{2\pi}{\tau} \cos\left(\frac{2\pi t}{\tau}\right) \right] \alpha e^{-x/L} \text{ deg/s}$$

Q7. Solution:

Basic equations :

$$0 = \frac{\partial}{\partial t} \int \rho dV + \int \rho \vec{v} \cdot d\vec{A}$$

$$-\nabla p + \rho \vec{g} = \rho \frac{D\vec{v}}{Dt} \quad \vec{F} = -\int p d\vec{A}$$

(a) For the deformable CV shown

$$0 = \frac{\partial}{\partial t} \int_0^y \rho w x dy + \rho w x y = \rho w x \frac{dy}{dt} + \rho w x y$$

But $dy/dt = -v$ and hence $u = \frac{vx}{y}$

If $y = b_0$ at $t = 0$, then $y = b = b_0 - vt$ at any time t

$$\therefore u = \frac{vx}{b}$$

(b) $a_x = \frac{Du}{Dt} = u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \frac{\partial u}{\partial t}$

Assumptions: (i) $u = u(y)$, $w = 0$

$$a_x = \frac{vx}{b} \left(\frac{v}{b} \right) + \frac{\partial u}{\partial b} \frac{db}{dt} = \frac{v^2 x}{b^2} + \left(-\frac{vx}{b^2} \right) (-v) = \frac{2v^2 x}{b^2} \leftarrow a_x$$

(c) From Euler's equation in the x direction with $g_x = 0$

$$\frac{\partial p}{\partial x} = -\rho a_x = -\frac{2\rho v^2 x}{b^2}$$

(d) $p - p_{atn} = \int_{-x}^x \frac{\partial p}{\partial x} dx = \int_{-x}^x -\frac{2\rho v^2}{b^2} x dx = -\frac{\rho v^2 x^2}{b^2} \Big|_{-x}^x = \frac{\rho v^2 L^2}{b^2} \left[1 - \left(\frac{x}{L} \right)^2 \right]$

(e) $F_y = \int (p - p_{atn}) dA = 2 \int_0^L \frac{\rho v^2 L^2}{b^2} \left[1 - \left(\frac{x}{L} \right)^2 \right] w dx$
 $= 2 \int_0^L \frac{\rho v^2 L^3}{b^2} \left[1 - \left(\frac{x}{L} \right)^2 \right] w d\left(\frac{x}{L} \right) = \frac{2\rho v^2 L^3 w}{b^2} \left[\left(\frac{x}{L} \right) - \frac{1}{3} \left(\frac{x}{L} \right)^3 \right]_0^1$

$$F_y = \frac{4\rho v^2 L^3 w}{3b^2} \leftarrow (\text{upward, since } F_y > 0) \quad F_y$$

Q8. Solution:

Basic equation: $\frac{\partial p}{\partial n} = \rho \frac{V^2}{R}$

Assumptions: (1) steady flow (2) frictionless flow
(3) neglected body forces
(4) constant speed along each streamline

At the inlet section, $v = v(y)$

$$\therefore \frac{\partial p}{\partial n} = - \frac{\partial p}{\partial y} = \rho \frac{V^2}{R} = \rho V^2 \frac{\partial y}{R \partial y}$$

$$\therefore dp = - \frac{\rho V^2}{R \partial y} 2y dy$$

$$p_{42} - p_0 = \int_0^{42} dp = - \frac{2\rho V^2}{R \partial y} \int_0^{42} y dy = - \frac{2\rho V^2}{R \partial y} \left[\frac{y^2}{2} \right]_0^{42}$$

$$p_{42} - p_0 = - \frac{\rho V^2}{R \partial y} \frac{1}{2} = - \frac{\rho V^2}{4R}$$

$$p_{42} - p_0 = -1.225 \frac{\text{kg}}{\text{m}^3} \times \left(20 \frac{\text{m}}{\text{s}}\right)^2 \times 0.5 \text{m} \times \frac{1}{4} \times \frac{1}{0.6\text{m}} \times \frac{\text{N}\cdot\text{s}^2}{\text{kg}\cdot\text{m}}$$

$$p_{42} - p_0 = -30.6 \text{ N/m}^2 \quad \leftarrow p_{42} - p_0$$

Q9.

For 2-D incompressible flow $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$, so $\frac{\partial u}{\partial x} = - \frac{\partial v}{\partial y}$

$$u = \int \frac{\partial u}{\partial x} dx + f(y) = \int - \frac{\partial v}{\partial y} dx + f(y) = \int -2xy dx + f(y) = -2xy + f(y)$$

Choose the simplest solution, $f(y) = 0$, so $u = -2xy$. Hence

$$\vec{V} = -2xy\hat{i} + y^2\hat{j} = y[-2x\hat{i} + y\hat{j}]$$

$$\vec{a}_p = u \frac{\partial \vec{V}}{\partial x} + v \frac{\partial \vec{V}}{\partial y} = -2xy[-2y\hat{j}] + y^2[-2x\hat{i} + 2y\hat{j}]$$

$$\vec{a}_p = 2x^2y^2\hat{i} + 2xy^3\hat{j} = 2xy^2[x\hat{i} + y\hat{j}]$$

At the point (2,1)

$$\vec{a}_p = 2 \times \frac{1}{1.5} \times (1)^2 \text{ m/s}^2 [2\hat{i} + 1\hat{j}] = 4\hat{i} + 2\hat{j} \text{ m/s}^2 \quad \leftarrow \vec{a}_{(2,1)}$$

$$\vec{V} = \frac{1}{1.5} [-2(2)(1)\hat{i} + (1)^2\hat{j}] = -4\hat{i} + \hat{j} \text{ m/s}$$

The unit vector tangent to the streamline is

$$\hat{e}_t = \frac{\vec{V}}{|\vec{V}|} = \frac{-4\hat{i} + \hat{j}}{[(4)^2 + (1)^2]^{1/2}} = -0.970\hat{i} + 0.243\hat{j}$$

The unit vector normal to the streamline is

$$\hat{e}_n = \hat{k} \times \hat{e}_t = \hat{k} \times (-0.970\hat{i} + 0.243\hat{j}) = -0.243\hat{i} - 0.970\hat{j}$$

The normal component of acceleration is

$$a_n = -\frac{V^2}{R} = \vec{a} \cdot \hat{e}_n = (4\hat{i} + 2\hat{j}) \cdot (-0.243\hat{i} - 0.970\hat{j})$$

$$-\frac{V^2}{R} = -2.91 \text{ m/s}^2$$

$$R = \frac{V^2}{2.91} = \frac{17 \text{ m}^2/\text{s}^2}{2.91 \text{ m/s}^2} = 5.84 \text{ m} \quad \leftarrow R_{(2,1)}$$

Q10.

Solution: Apply Bernoulli and then y-momentum equation

Basic eq.: $\frac{p}{\rho} + \frac{V^2}{2} + gz = \frac{p}{\rho} + \frac{V^2}{2} + gz$

- Assumptions:
- (1) steady flow
 - (2) incompressible flow
 - (3) frictionless flow
 - (4) flow along a streamline
 - (5) $p_1 = p_2 = p_{atm}$

Then

$$V_2 = [V_1^2 + 2g(z_1 - z_2)]^{1/2}$$

$$V_2 = [(6.3)^2 \frac{m^2}{s^2} + 2 \times 9.81 \frac{m}{s^2} (-1.55m)]^{1/2}$$

$$V_2 = 3.05 \text{ m/s}$$

By definition, $p_{02} = p_2 + \frac{1}{2} \rho V_2^2 = p_{atm} + \frac{1}{2} \rho V_2^2$, so

$$p_{02 \text{ gage}} = \frac{1}{2} \times 999 \frac{kg}{m^3} \times (3.05)^2 \frac{m^2}{s^2} \times \frac{N \cdot s^2}{kg \cdot m} = 4.65 \text{ kPa (g)} \rightarrow p_{02}$$

Apply y-momentum equation to CV surrounding plate

Basic eq.: $F_{sy} + F_{by} = \frac{\partial}{\partial t} \int_{CV} \rho V_y dV + \int_{CV} \rho V_y \vec{V} \cdot d\vec{A}$

- Assumptions:
- (6) neglect mass in CV
 - (7) V_2 enters CV uniformly
 - (8) $V_3 = V_4 = 0$

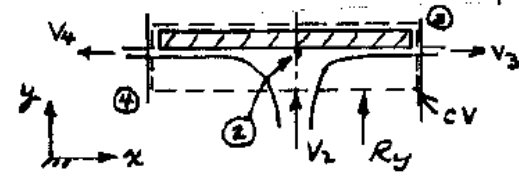
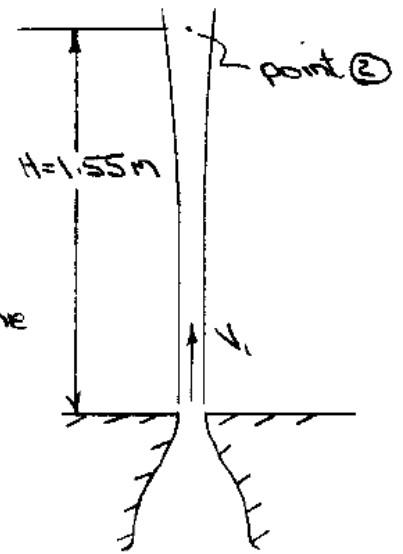
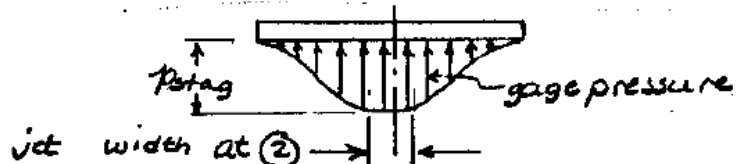
Then

$$R_y = V_2 \{-p_2 A\} + V_3 \{m_3\} + V_4 \{m_4\} = -p_2 A V_2 \quad \text{and}$$

$$K_y = -R_y = p_2 A V_2 = 999 \frac{kg}{m^3} \times 6.3 \frac{m}{s} \times 600 \text{ mm}^2 \times 3.05 \frac{m}{s} \times \frac{m^2}{10^6 \text{ mm}^2} \times \frac{N \cdot s^2}{kg \cdot m}$$

$$K_y = 11.5 \text{ N (force up)}$$

The pressure distribution on the plate is as shown.



Q11.

Solution:

Basic equation: $\frac{p_1}{\rho} + \frac{V_1^2}{2} + g z_1 = \frac{p_2}{\rho} + \frac{V_2^2}{2} + g z_2$



Assumptions: (1) steady flow (4) flow along a streamline
(2) incompressible flow (5) $z_1 = z_2$
(3) no friction

From the Bernoulli equation $p_1 = \frac{1}{2} \rho (V_2^2 - V_1^2)$

From continuity for uniform flow, $V_1 A_1 = V_2 A_2$

$$\therefore V_2 = V_1 \frac{A_1}{A_2} = 4 \frac{\pi (0.05)^2}{\pi (0.01)^2} = 7 \frac{m}{s}$$

and

$$p_1 = \frac{1}{2} \rho (V_2^2 - V_1^2) = \frac{1}{2} \times 999 \frac{kg}{m^3} [(7)^2 - (4)^2] \frac{m^2}{s^2} \times \frac{N \cdot s^2}{kg \cdot m} = 164 \text{ kPa (gage)}$$

To determine the force required to hold the plug, apply the x-component of the momentum equation to the CV shown.

$$F_{s_x} + \sum F_x = \frac{\partial}{\partial t} \int_{CV} u \rho dV + \int_{CS} u \rho \vec{V} \cdot d\vec{A}$$

$$p_1 A_1 - F = u_1 \{-\dot{m}\} + u_2 \{\dot{m}\} = \dot{m}(u_2 - u_1) = \rho V_1 A_1 (V_2 - V_1)$$

$$F = p_1 A_1 - \rho V_1 A_1 (V_2 - V_1)$$

$$= 164 \times 10^3 \frac{N}{m^2} \times \frac{\pi (0.05)^2}{4} - 999 \frac{kg}{m^3} \times 7 \frac{m}{s} \times \frac{\pi (0.05)^2}{4} (7 - 4) \frac{m}{s} \times \frac{N \cdot s^2}{kg \cdot m}$$

$$F = 322 \text{ N} - 170 \text{ N} = 152 \text{ N (in direction shown)}$$