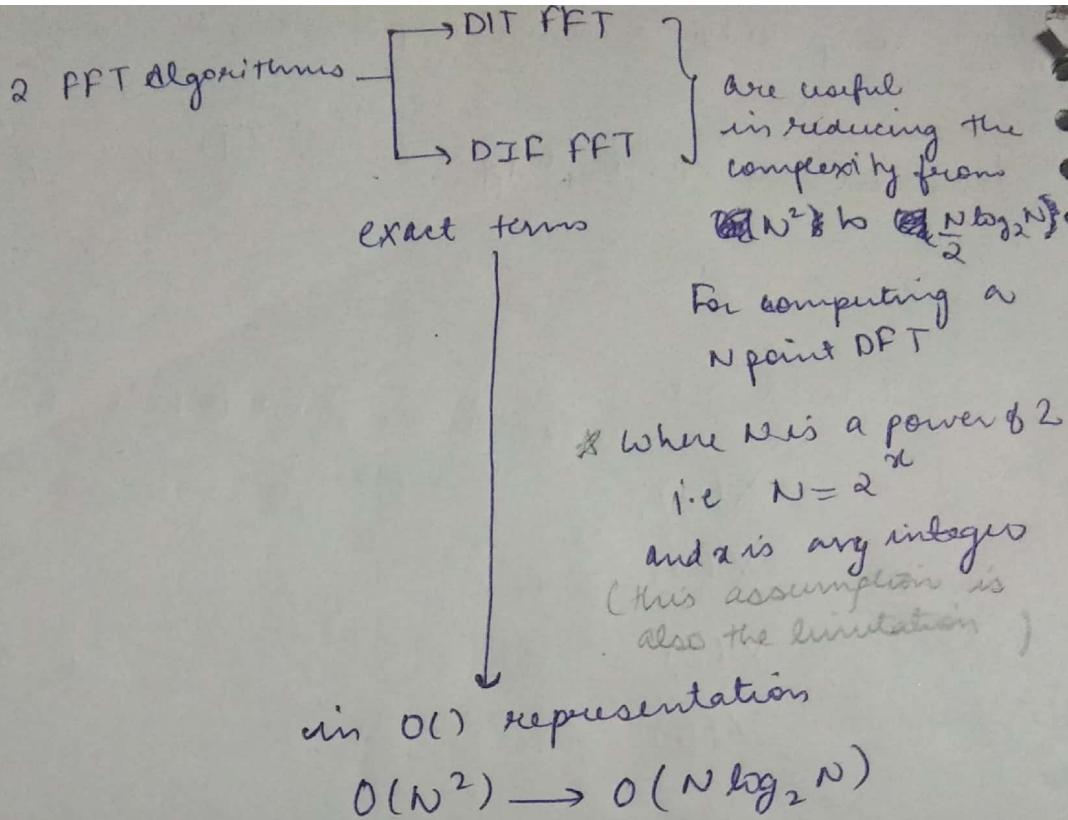


31/10/18



1 2 4 8 16 32 64 128 256 512

 32

As the numbers are increasing the spacing b/w them is also increasing, which means now there are more numbers for which we cannot find DFT using these methods.
For ex: Btw 256 and 512, there are 256 numbers for which the assumption is not satisfied.

To use this algorithm at any cost and no restriction on input size.

Solution 1
→ Modulo

$x(0), x(1)$ and $x(2)$. Apply modulo operator, we will get a length ≤ 2 . $x(2)$ will get added to $x(0)$

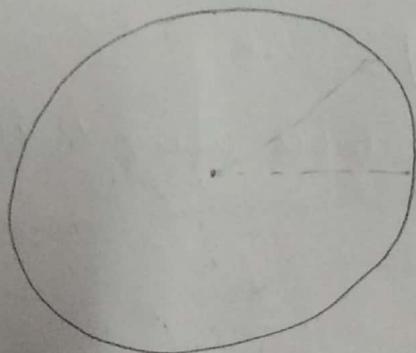
Solution 2:
Add zeros to make a 3 point DFT into a 4 point DFT.
This is a better option.

Suppose we want to have a 17 point DFT then we will compute 32 point DFT. We will have to see which is a bigger module 17^2 or $16 \log_2 32$.

Error in the worst case scenario, using this algorithm is a useful option.

We need to go the upper bound ceil $129 - 256$, so this algorithm can be used as a default.

Spectral Representation



DTFT
↓
complete
information

DFT
↳ gives information about
specific N points

$$-\pi \leq \omega \leq \pi$$

When ω is a continuous variable from $-\pi$ to π then it is a DTFT.

If we compute N point DFT then we divide the circle into N equal parts.

Spectral component of the input signal on that particular angles.

As $N \rightarrow \infty$ DFT is equal to DTFT

In a continuous signal we are looking for the number of cycles per second.

Sampling Frequency = f_s . This is for the signals of continuous type

$$f_s = \text{Number of samples/sec}$$

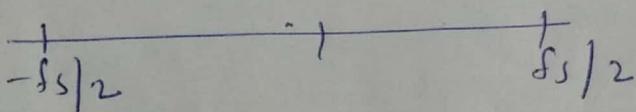
The connection point is Nyquist theorem.

This is a connection point b/w a continuous time signal to a discrete time signal.

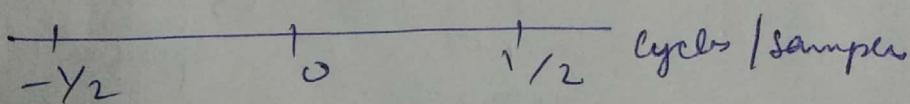
Input cannot have more than $f_s/2$.

If the input is more than $f_s/2$, then we get aliasing in the spectral domain.

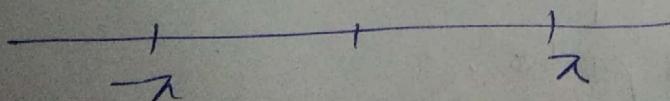
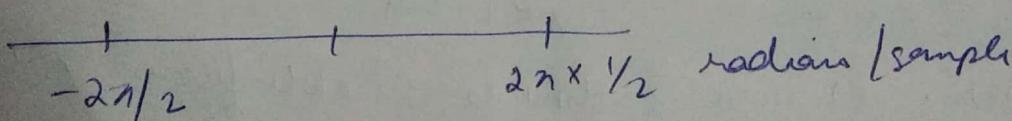
Nyquist Interval:



The highest Frequency representable using Nyquist interval is $f_s/2$



cycle = 2π radians



This is the scale we are operating on

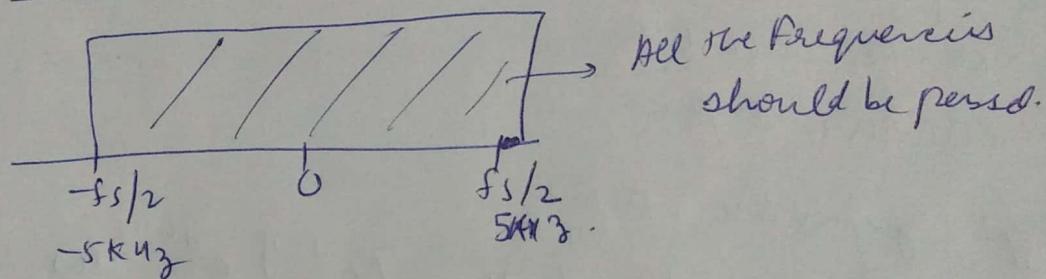
Using Nyquist Sampling Theorem can be connected to digital.

If f_s is increased in analog, representable Frequency will increase.

Digital representation is a fixed representation with respect to fixed f_s . If f_s is changed, there will be a different representation. They will map to different frequencies.

f_s - sampling Frequency

Nyquist Interval



All the Frequencies after 5KHz should be blocked

$$f_s = 10\text{KHz}$$

$$\text{If } f_s = 10\text{KHz}$$

~~Even symmetric spectrum because~~

w scale ranging from $\frac{\pi f}{f_s}$ to $\frac{\pi t}{f_s}$

Low Pass Filter - It should pass all the Frequencies.

Ideal low pass filter $\omega_c = \pi/5$ radian / samp

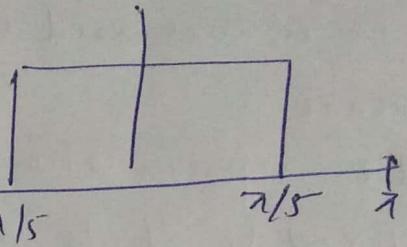
In terms of analog Frequencies $f_c = 1\text{KHz}$ with $f_s = 10\text{KHz}$

$$\omega = \frac{2\pi f}{f_s} \rightarrow \text{This is the conversion to get back to the digital Scale.}$$

$$u(e^{j\omega}) = 1 \quad -\frac{\pi}{5} \leq \omega \leq \frac{\pi}{5}$$

$$|u(e^{j\omega})| = 1 \quad -\pi/5 \leq \omega \leq \pi/5$$

$$= 0 \quad \text{otherwise}$$



$$\angle u(e^{j\omega}) = 0 \quad -\pi < \omega < \pi$$

Zero phase response

An impulse response can be implemented using

→ Non Recursive FIR

→ Recursive IIR

Applying Inverse DTF

$$h_{LPP}(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} u_{LPP}(e^{j\omega}) e^{j\omega n} d\omega$$

$$\frac{1}{2\pi} \int_{-\pi/5}^{\pi/5} 1 \cdot e^{j\omega n} d\omega = \left[\frac{e^{j\omega n}}{jn} \right]_{-\pi/5}^{\pi/5}$$

Generalizing : for any general ω_2

$$\left[\frac{e^{j\omega_2 n}}{jn} \right]_{-\omega_2}^{\omega_2}$$

$$\frac{1}{2\pi} \left[\frac{e^{j\frac{\pi}{5}n}}{jn} - \frac{e^{-j\frac{\pi}{5}n}}{jn} \right]$$

$$= \frac{1}{n} \sin\left(\frac{\pi}{5}n\right) = \frac{\sin\left(\frac{\pi}{5}n\right)}{n}$$

$$\left[\frac{e^{j\omega_c n}}{jn} \right]_{-\omega_c}^{\omega_c} = \frac{1}{2\pi} \left[\frac{e^{j\omega_c n}}{jn} - \frac{e^{-j\omega_c n}}{jn} \right]$$

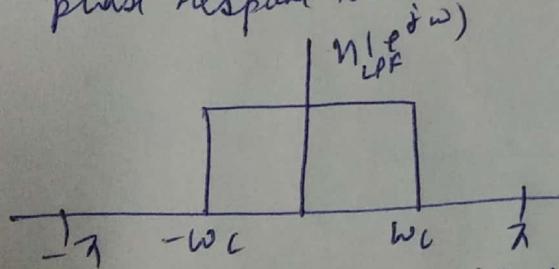
$$= \frac{\sin\omega_c n}{\pi n}$$

where ω_c is any frequency ranging from $0 \text{ to } \pi$
 $h_{LPF}(n) = \frac{\sin\omega_c n}{\pi n}$ This function is not valid for $n=0$

$$\text{Infinite Impulse Response } h_{LPF}(0) = \frac{\omega_c}{\pi} \quad n=0$$

Perfect non causal system

phase response should be zero



We are calling this as ideal Filter because there is a sharp gain.

Gain can be any value b/w 0 and 1. There is only one such point of uncertainty ω_c .

This filter has zero phase response.

If zero phase response then there is no need to wait for the output.

5/11/12

To build:

N-length FIR Systems

(LowPass Filter with cut off w_c)

It should form a causal system.

Ideal System gives us IIR and noncausal system

Now, we have to leave some information to get FIR and causal system.

There can be infinite methods to convert IIR into FIR i.e. the conversion is not unique.

We need to provide some extra information to do make it unique.

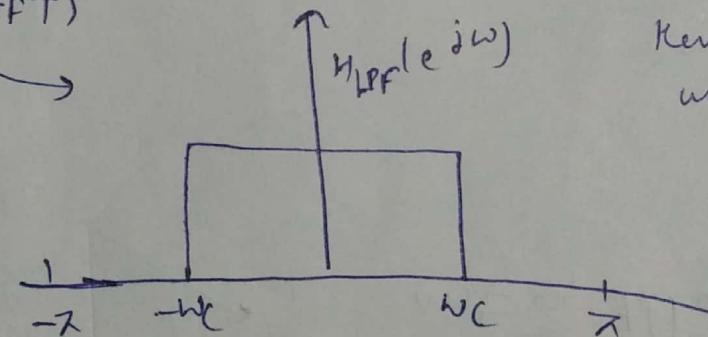
Then evaluate each method and define a cost function,

if cost function \rightarrow minimum (unique)

\rightarrow maximum (unique)

How to determine the cost function?

Ideal LPF Filter (DTFT)



since it is a continuous function
Hence we are using DTFT not DFT

After converting it into FIR, find its DTFT coefficient

and compute

$$\int_{-\pi}^{\pi} |H_{LPF}(e^{jw}) - H_{FIR}(e^{jw})|^2 \cdot dw \quad (\text{Least square error})$$

The one that gives the least solution is the best solution.

defined in transform domain

This cost function is the difference energy function

By using Parseval's Relationship, converting the previous equation into time domain

$$\sum_{n=-\infty}^{\infty} |h_{LPP}(n) - \hat{h}_{LPF}(n)|^2$$

The least value using both will be equal

If we take $-2 \leq n \leq 2$ one function is defined in this range (\hat{h}_{LPF})

$$SE = \sum_{n=-\infty}^{-3} |h_{LPP}(n) - \hat{h}_{LPF}(n)|^2 + \underbrace{\sum_{n=-2}^2 [h_{LPP}(n) - \hat{h}_{LPF}(n)]^2}_{(\hat{h}_{LPF})} + \sum_{n=3}^{\infty} |(h_{LPP}(n) - \hat{h}_{LPF}(n))|^2$$

other is going from $-\infty$ to ∞

\hat{h}_{LPF} is zero
within these ranges
Hence the cost is fixed

This sum plays
the major role

We want this sum to be
zero.

↳ Best case

This has variable cost

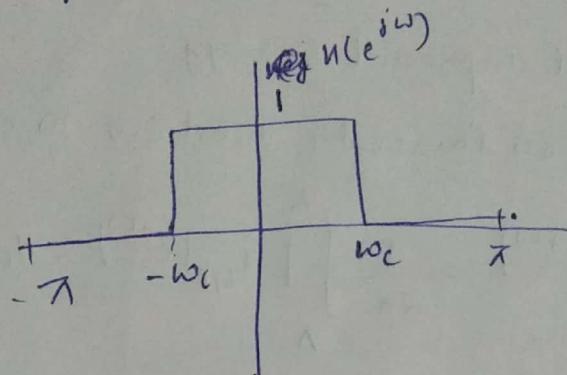
In this $-2 \leq n \leq 2$, the
value of \hat{h}_{LPF} should be
equivalent to ideal
Filter

Least Square Solution

2/11/18

$$\hat{h}_{LPP}(n) = h_{LPF}(n)$$

Ideal Frequency Response of LPF



$$H(e^{j\omega}) = \begin{cases} 1 & -\omega_c \leq \omega \leq \omega_c \\ 0 & \text{Otherwise} \end{cases}$$

IDTFT $\angle H(e^{j\omega}) = 0 \rightarrow$ zero phase response is most appreciated systems and hence is ideal

$$h_{LPP}(n) = \frac{\sin \omega_c n}{\pi n} \quad n \neq 0 \quad = h_{LPF}(-n)$$

\hookrightarrow symmetric about y-axis

(Infinite lengths) $= \frac{\omega_c}{\pi} \quad n=0$

but we require a N length FIR system

We can calculate the error in ① Time Domain

② Frequency Domain

These two representations have one thing equal which is the energy of the signal.

$$\text{Now error signal} = \hat{h}(n) - h_{LPP}(n)$$

does not represent energy.

We need to use Parseval's relation to equate the two

$$E_{LPP}(e^{j\omega}) = \frac{1}{2\pi} \int_{-\pi}^{\pi} |\hat{h}_{LPP}(e^{j\omega}) - h_{LPP}(e^{j\omega})|^2 d\omega$$

$$e_{LPP}^2(n) = \sum_{m=-\infty}^{\infty} [\hat{h}_{LPP}(m) - h_{LPP}(m)]^2 \quad \text{--- (1)}$$

Now we need to find the value of n for which e_{LPP}^2 is minimum.
we can divide eq(1) into 3 parts

$$e_{LPP}^2(n) = \underbrace{\sum_{m=-\infty}^{N/2-1} (\quad)}_{\text{I}} + \underbrace{\sum_{m=N/2}^{N/2} (\quad)}_{\text{II}} + \underbrace{\sum_{m=N/2+1}^{\infty} (\quad)}_{\text{III}}$$

but $\hat{h}_{LPP}(m)$ is defined only $-N/2 \leq m \leq N/2$
in range \rightarrow

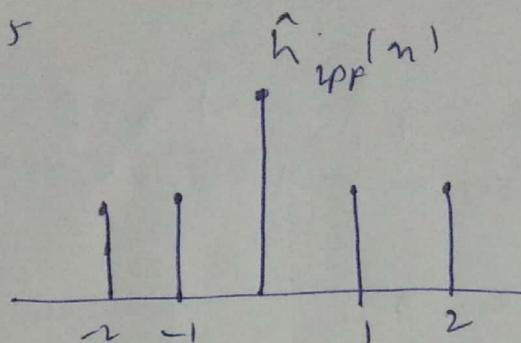
which makes 1st and 3rd term to be of fixed
cost and independent of $\hat{h}_{LPP}(m)$.

Now $e_{LPP}^2(n)$ will be minimum when 2nd term is zero
which is possible when $\hat{h}_{LPP}(m) = h_{LPP}(m)$

This solution is still not unique
as we can take any value of N
by choosing this range
as it gives us symmetry
about y-axis.

If we don't mention symmetricity about y-axis then we will not achieve zero phase response.

Example
For $N = 5$



Now, the resultant system is non-causal (Finite non causality)
but we required a causal system.

Causal System $\rightarrow \hat{h}_{LPP}(n-2)$
phase will be changed $e^{-j2\omega}$

$$\hat{h}_{LPP}(n) \xleftrightarrow{\text{DTFT}} \hat{h}_{LPP}(e^{j\omega})$$

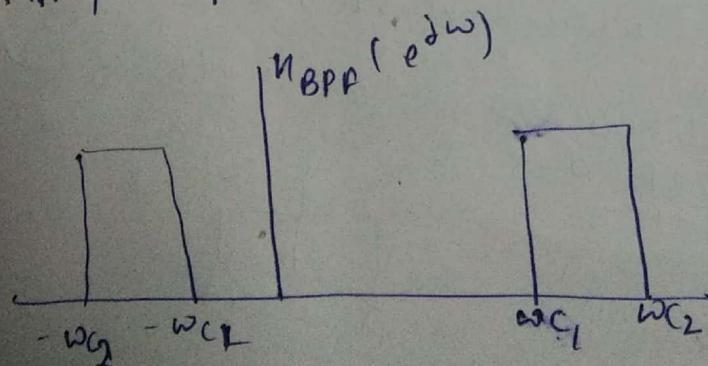
$$\hat{h}_{LPP}(n-2) \xleftrightarrow{\text{DTFT}} e^{-j2\omega} \hat{h}_{LPP}(e^{j\omega})$$

phase will be $0^\circ + 2\omega$
Initial phase

$\boxed{\text{Ist conclusion}}$
 $\boxed{\text{linear phase}}$

IInd → Our device works best in terms of
least square method
Result → Linear Phase n -length FIR lowpass filter

Derive for HPF, BPF, Band Stop Filter



This is implementable
this will preserve the envelope of the signal.

14/11/18

Format of Project Report

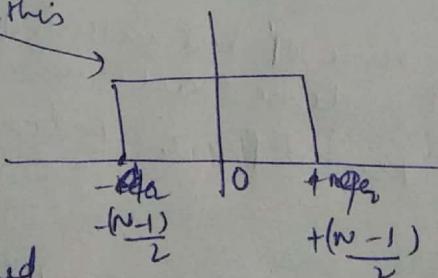
- i) First page should include Title & Group Member details
 - ii) Paper
 - iii) Individual Understanding (comprehension) of paper
 - iv) Implementation
 - Program (with sufficient comment)
 - Results
 - v) Conclusion of Results
- More weightage

① For any impulse response, if it is symmetric then it has a linear phase in frequency domain

② The final frequency response of $\hat{h}_{LPF}(n)$

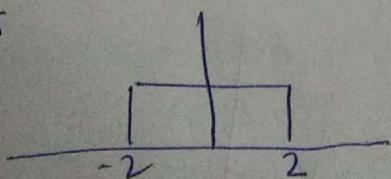
Two possible Symmetry \rightarrow even symmetry
 \rightarrow odd symmetry

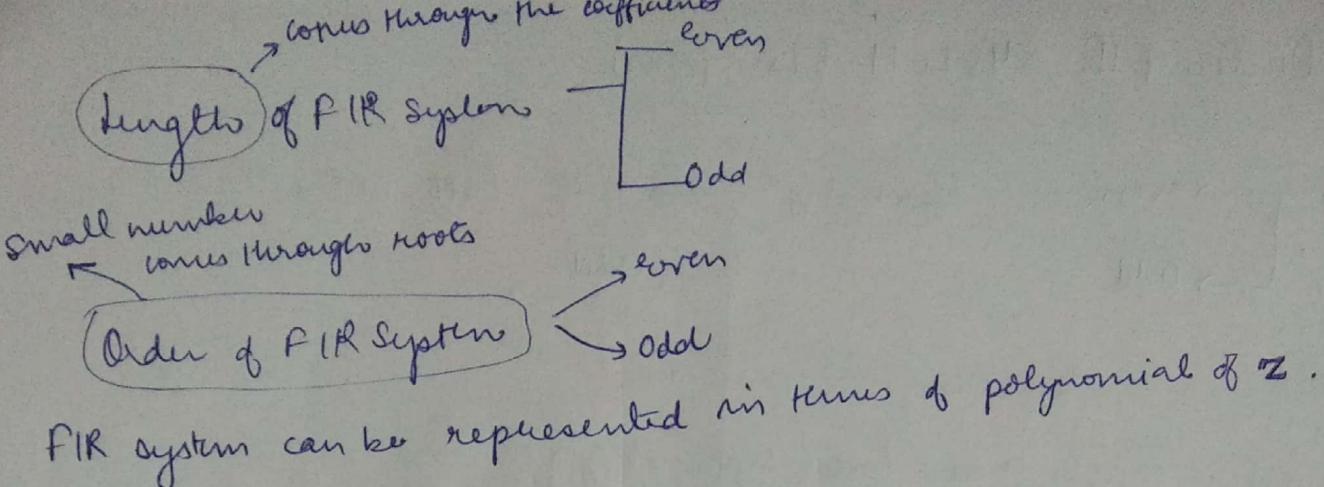
* N must be Odd For this
because when we plot from $-N/2$ to $N/2$
0 is also included which makes N odd.



where N is the length of the system

For ex For N = 5





No. of coefficients > No. of roots

For n^{th} order system

No. of coefficients $\rightarrow n+1$
 roots $\rightarrow n$

Two possible combinations

System Symmetry & Order

Good way of
representing

It has $\rightarrow 1$ dimension

of less

eg

Symmetry & Length

$$h(e^{j\omega}) \cdot e^{-j2\omega} = e^{-j2\omega} \left[h(0)e^{j2\omega} + h(1)e^{j\omega} + h(2) + h(3)e^{-j\omega} + h(4) \right]$$

$$\begin{aligned} &= e^{-j2\omega} \left[h(0)e^{j2\omega} + h(1)e^{j\omega} + h(2) + h(1)e^{-j\omega} + h(0)e^{-j2\omega} \right] \\ &= e^{-j2\omega} \left[2h(0) \left(\frac{e^{j2\omega} + e^{-j2\omega}}{2} \right) + h(1)(e^{j\omega} + e^{-j\omega}) + h(2) \right] \end{aligned}$$

$$h(e^{j\omega}) = e^{-j2\omega} \left[2h(0)\cos 2\omega + 2h(1)\cos \omega + h(2) \right]$$

magnitude part

Phase part
which has linear phase

-2ω

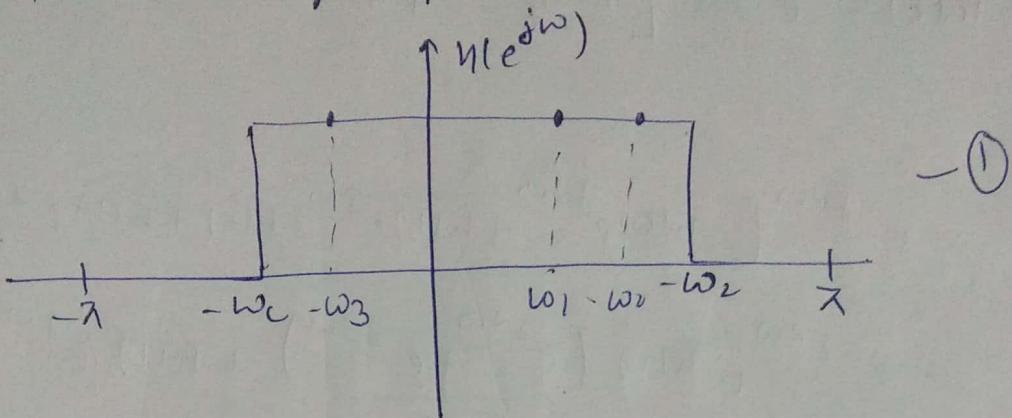
$$h(e^{j\omega}) = e^{-j\frac{N}{2}\omega} \left[h\left(\frac{N}{2}\right) + 2 \sum_{n=1}^{\frac{N}{2}-1} h\left(\frac{N}{2}-n\right) \cos n\omega \right]$$

If we know the frequency response, by using the above equation
we can find out the impulse response scale factors in
time domain ($h\left(\frac{N}{2}\right)$ etc)

$$h(e^{j\omega}) = e^{-j2\omega} \left[2h(0)\cos 2\omega + 2h(1)\cos \omega + h(2) \right]$$

We need to find $h(0), h(1), h(2)$

For a LPF, the Frequency response we have is



we have 3 unknowns ($h(0), h(1), h(2)$) , then minimum three equations are required .

But, we have more than 3 equations here.

which means more equations, less number of unknowns.
thus, there can be many solutions .

$$H(z) = h(0) + h(1)z^{-1} + h(2)z^{-2} + h(3)z^{-3} + h(4)z^{-4}$$

Order of polynomial = 4

* Degree of freedom = No. of coefficients = 2 ($h(0), h(1)$)

We are designing a N order polynomial with
 $\frac{N}{2}$ degree of freedom.

This is the limitation of this technique.

This is the cost we are paying for getting the FIR
LPF Filter linear phase .

If we remove the linear phase condition , we will get
N order polynomial with N degree of freedom
but that will increase the no. of unknowns h_0 .

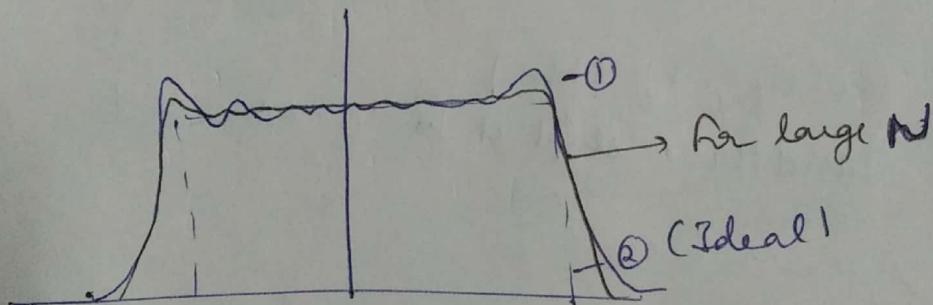
Let us assume three frequencies w_1, w_2, w_3 on Graph. Using these we will get the step coefficient which might not have minimum error.

In order to get minimum error, we should use least square method using all the three points available.

for least square

$$\frac{1}{2\pi} \int_{-\pi}^{\pi} |(1)e^{jw}) - (\hat{h}(e^{jw}))|^2 dw$$

For large N , the estimated step impulse response will have more coefficients matching with the ideal response, thus it will be more close to ideal behaviour.

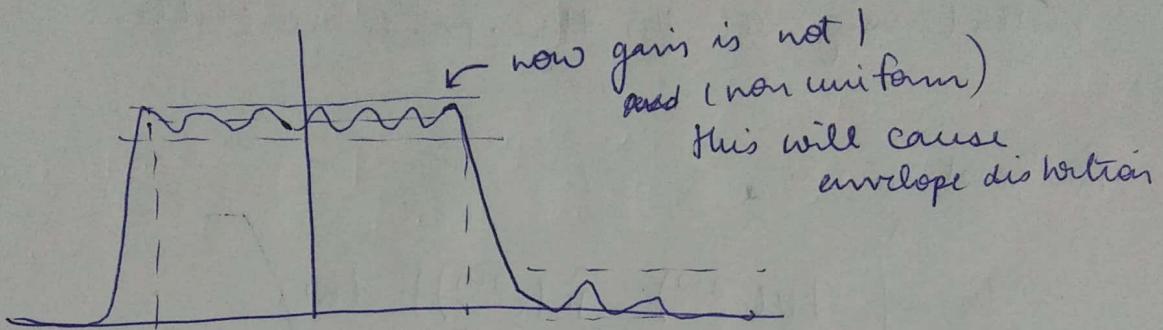


Explain/Ex

But even for $N \rightarrow \infty$, there will be some error, because of the discontinuity at two places. Error can never be zero.

Impulse Response with Odd Symmetry

- ① Differentiator (CPM Modulation / Demodulation)
- ② Hilbert Transform (SSB)



To get a Finite Response

Use a Window

$$w(n) = 1 \quad 0 \leq n \leq N-1$$

$$w(n) = 1 \quad -N/2 \leq n \leq N/2$$

multiply by $(h(n))$
and then shift it to $0 \leq n \leq N-1$

In Frequency domain, the one with least
number of oscillations gives the best
solution

19/11/18

For $N=2$

no. of coefficients = 3

$$\{h(0), h(1), h(2)\}$$

for even symmetry $h(0) = h(2)$

$$H(z) = h(0)z^0 + h(1)z^{-1} + h(2)z^{-2}$$

$$\begin{aligned} H(e^{j\omega}) &= h(0) + h(1)e^{-j\omega} + h(2)e^{-j2\omega} \\ &= h(0) + h(1)e^{-j\omega} + h(0)e^{-j2\omega} \\ &= h(0)(1 + e^{-j2\omega}) + h(1)e^{-j\omega} \end{aligned}$$

$$H(z^{-1}) = h(0) + h(1)z + h(2)z^2$$

multiply by z^{-2}

$$z^{-2}(H(z^{-1})) = h(0)z^{-2} + h(1)z^{-1} + h(2)$$

\uparrow
compare this with

$$h(2) = h(0)$$

$$H(z) = h(0) + h(1)z^{-1} + h(0)z^{-2}$$

These two
equations are
equal

$$\boxed{H(z) = z^{-N} H(z^{-1})}$$

This is called ~~Reciprocal~~ Image polynomial.

$H(z) = z^{-N} H(z^{-1})$ implies if we have a zero at some z
then we will also have ~~zero~~ zero at some z^{-1}

Ex: $u(z_1) = 0$

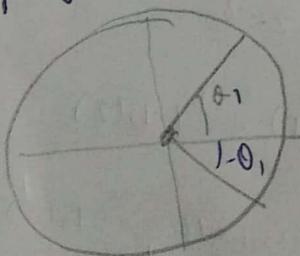
$z = z_1$ is the root of the polynomial

Ref 2. $\boxed{u\left(\frac{1}{z_1}\right) = 0}$

In order to make a linear phase system, if we take a root z_1 ,
then we should also take $\frac{1}{z_1}$ as the other root.

for a real polynomial $\begin{cases} \text{coefficients are real} \\ \text{roots are real} \end{cases}$

For a complex polynomial complex roots should
be in conjugate pair.
so that we get real coefficients



This will make the polynomial real.

For a complex zero (root), we have total 4 zeros

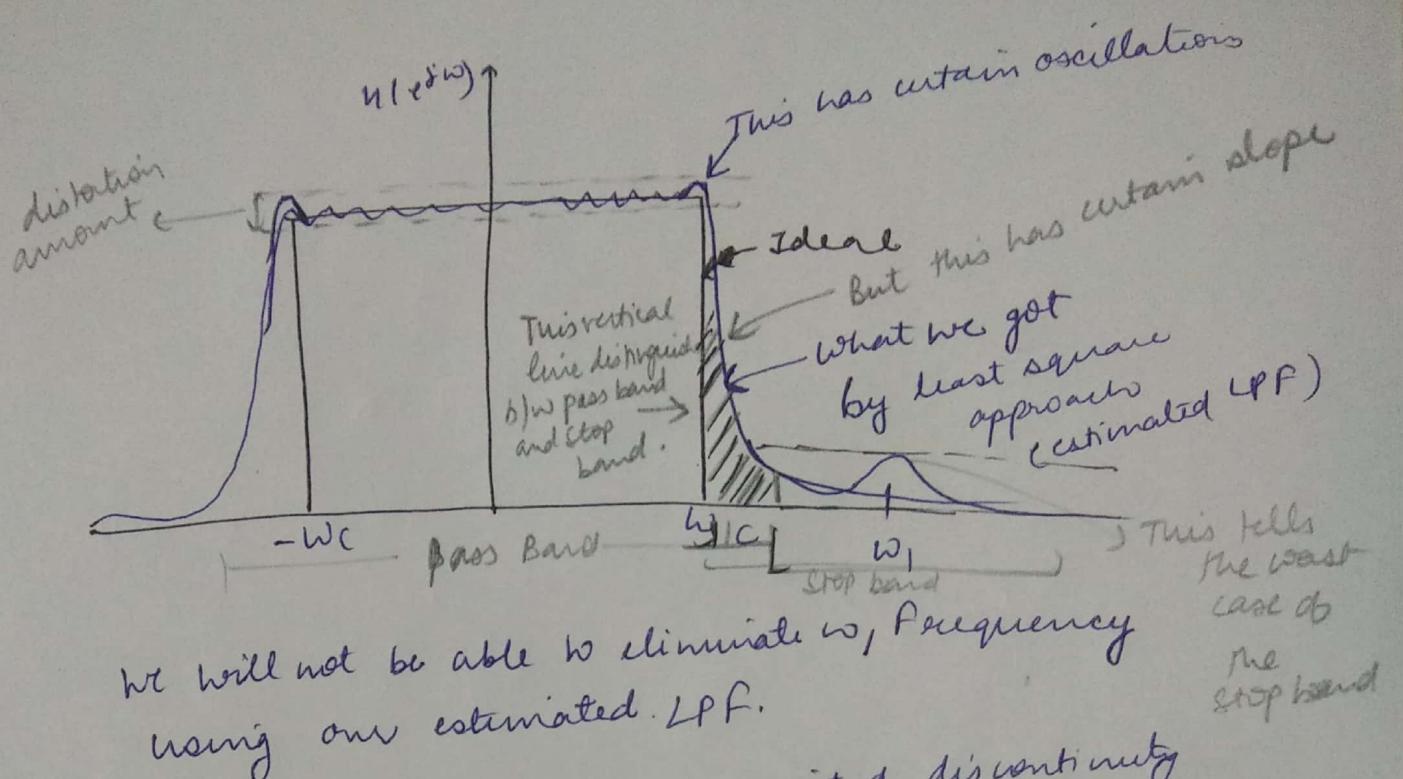
complex zeros $(\alpha + \beta i)$ conjugate $(\alpha - \beta i)$

For symmetry and linear phase $\frac{1}{\alpha + \beta i}$

For symmetry and linear phase $\frac{1}{\alpha - \beta i}$

there, 4 zeros

Ideal Lowpass Filter



Highest gain ~~keep~~ is at the point of discontinuity

Highest gain in the stop band should be reduced to zero.
→ pass band should be reduced to 1.

region marked like this

→ This region neither belongs to pass band nor stop band
and is called transition region.

