

Automation

Laboratory Exercise 1

CONTINUOUS-TIME LINEAR TIME-INVARIANT (LTI) SYSTEMS – DESCRIPTION, ANALYSIS AND CONTROL DESIGN

Assume a single-input single-output (SISO) LTI system given by the differential equation:

$$a_2 \cdot y''(t) + a_1 \cdot y'(t) + a_0 \cdot y(t) = b_0 \cdot u(t)$$

where $u(t)$ and $y(t)$ is the input and output, respectively.

Replace the general constants a_2 , a_1 , a_0 , b_0 with the values according to your individual assignment and perform the following tasks:

1. Write the transfer function. Determine the zeros, poles, order and relative order. Then decide if the system is stable/unstable; underdamped/overdamped/critically damped; and minimum phase/non-minimum phase.
2. Calculate the step response and the impulse response functions (analytically, i.e. “manually”) and plot the graphs of both calculated functions. Then plot the step and impulse responses by using the MATLAB commands and compare the obtained results.
3. Express the sinusoidal transfer function (frequency response function) and plot the Nyquist diagram (Nyquist plot) on the basis of the analytical calculations (via “table of values”). Then plot the Nyquist diagram by using the MATLAB command and compare the obtained results. Moreover, plot also the Bode diagrams (Bode plots) – just in MATLAB is enough.
4. Choose 2 arbitrary controller design methods (including the application of a stability criterion) and design 2 continuous-time controllers that ensures the stable feedback control system and reference tracking. Perform a simulation for each controller in the MATLAB+SIMULINK environment. (Consider a step-wise reference signal with step change from 1 to 2 in the half of simulation time).

(SISO).

$$a_2 \cdot y''(t) + a_1 \cdot y'(t) + a_0 \cdot y(t) = b_0 \cdot u(t)$$

Where:

$$a_0 = 3$$

$$a_1 = 5$$

$$a_2 = 2$$

$$b_0 = 4$$

$$y(0) = 0$$

$$y'(0) = 0$$

1. Transfer Function:

$$\mathcal{L}[2y''(t) + 5y'(t) + 3y(t)] = \mathcal{L}[4u(t)]$$

$$- 2 * \mathcal{L}[y''] + 5 * \mathcal{L}[y'] + 3 * \mathcal{L}[y] = 4 * \mathcal{L}[u]$$

$$- 2 * \left[S^2 \mathcal{L}(y) - y(0) - y'(0) \right] + 5 * [S \mathcal{L}(y) - y(0)] + 3 * [\mathcal{L}(y)] = 4 * [\mathcal{L}(u)]$$

$$- 2 S^2 * Y(s) + 5 S * Y(s) + 3 * Y(s) = 4 * \mu(s)$$

$$- (2 S^2 + 5 S + 3) * Y(s) = 4 * \mu(s)$$

$$- G(s) = \frac{Y(s)}{\mu(s)} = \frac{4}{2S^2 + 5S + 3}$$

Poles:

$$2S^2 + 5S + 3 = (2S + 3) * (S + 1)$$

$$S \neq -\frac{3}{2} \quad \& \quad S \neq -1$$

Zeros: constant.

Transfer Function order is: 2

Relative order is: 2

All Poles are negative in the left-hand side of the S-plane \rightarrow System is stable.

All Poles are real numbers and different \rightarrow System is overdamped.

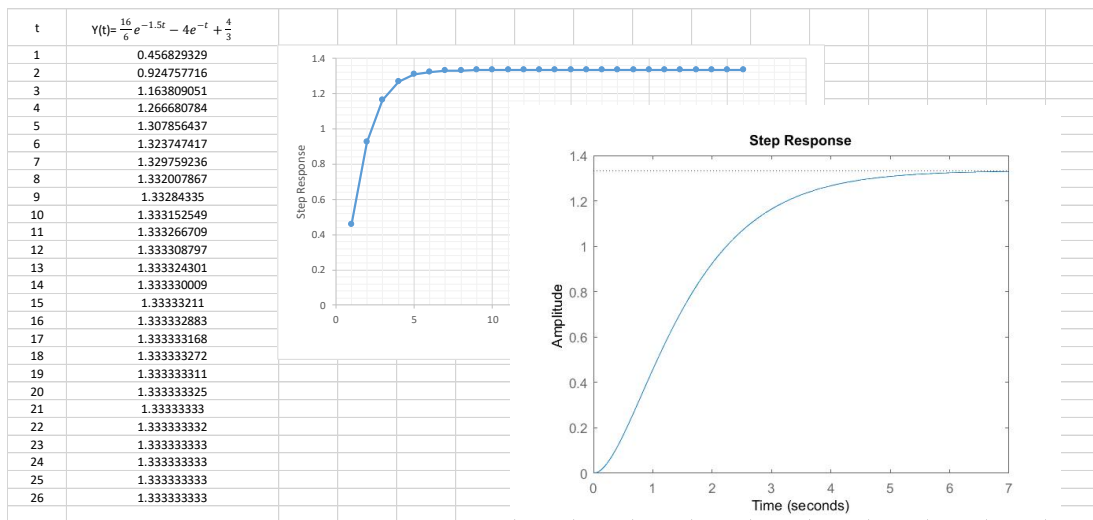
No Zeros in the right-hand side of the S-plane \rightarrow System is minimum Phase.

2. Step Response:

$$\mathcal{L}^{-1}\left[\frac{G(s)}{s}\right] = \mathcal{L}^{-1}\left[\frac{4}{s * (2s + 3) * (s + 1)}\right] = \mathcal{L}^{-1}\left[\frac{A}{s} + \frac{B}{(2s + 3)} + \frac{C}{(s + 1)}\right]$$

$$\mathcal{L}^{-1}\left[\frac{4}{s} + \frac{\frac{16}{3}}{(2s + 3)} + \frac{-4}{(s + 1)}\right] = \frac{16}{6}e^{-1.5t} - 4e^{-t} + \frac{4}{3}$$

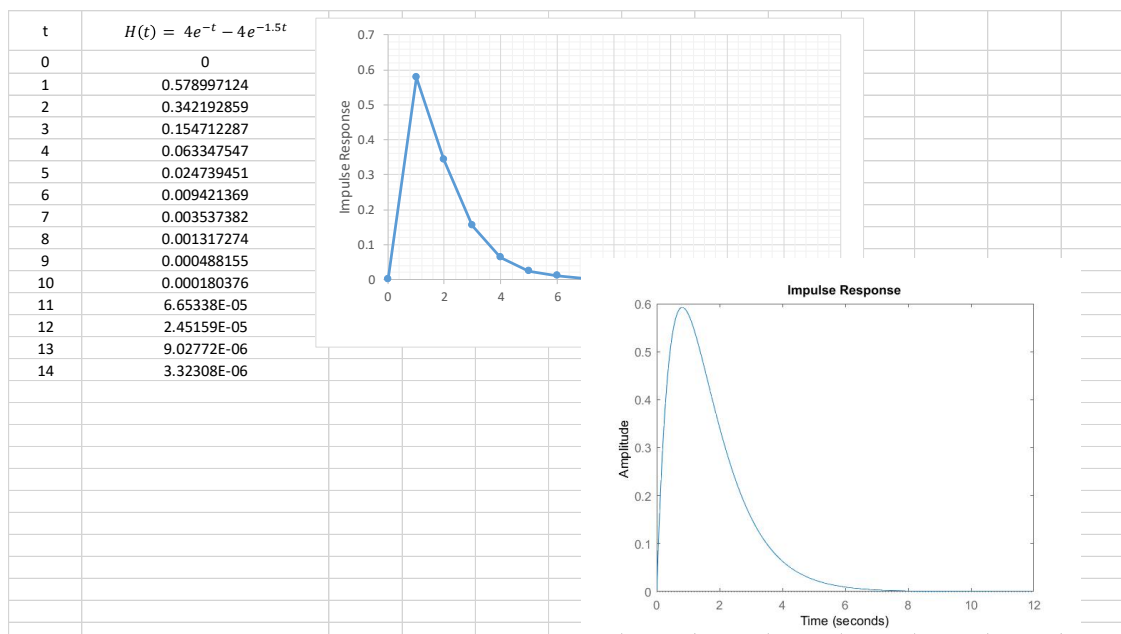
$$\therefore Y(t) = \frac{16}{6}e^{-1.5t} - 4e^{-t} + \frac{4}{3}$$



Impulse Response:

$$\mathcal{L}^{-1}[G(s)] = \mathcal{L}^{-1}\left[\frac{4}{2s^2 + 5s + 3}\right] = \mathcal{L}^{-1}\left[\frac{A}{(2s + 3)} + \frac{B}{(s + 1)}\right] = \mathcal{L}^{-1}\left[\frac{-8}{(2s + 3)} + \frac{4}{(s + 1)}\right]$$

$$H(t) = 4e^{-t} - 4e^{-1.5t}$$



3. Frequency Response:

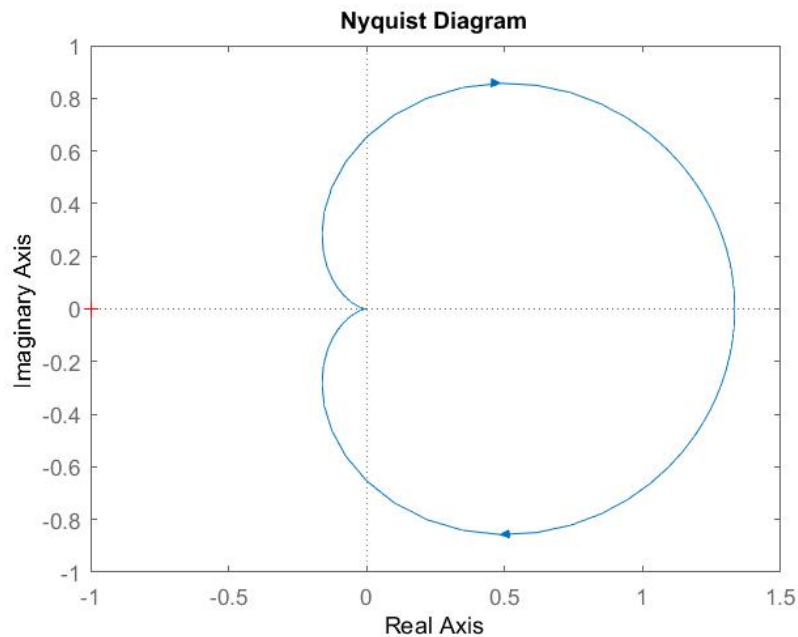
$$H(i\omega) = \frac{4}{2 * (i\omega)^2 + 5 * (i\omega) + 3}$$

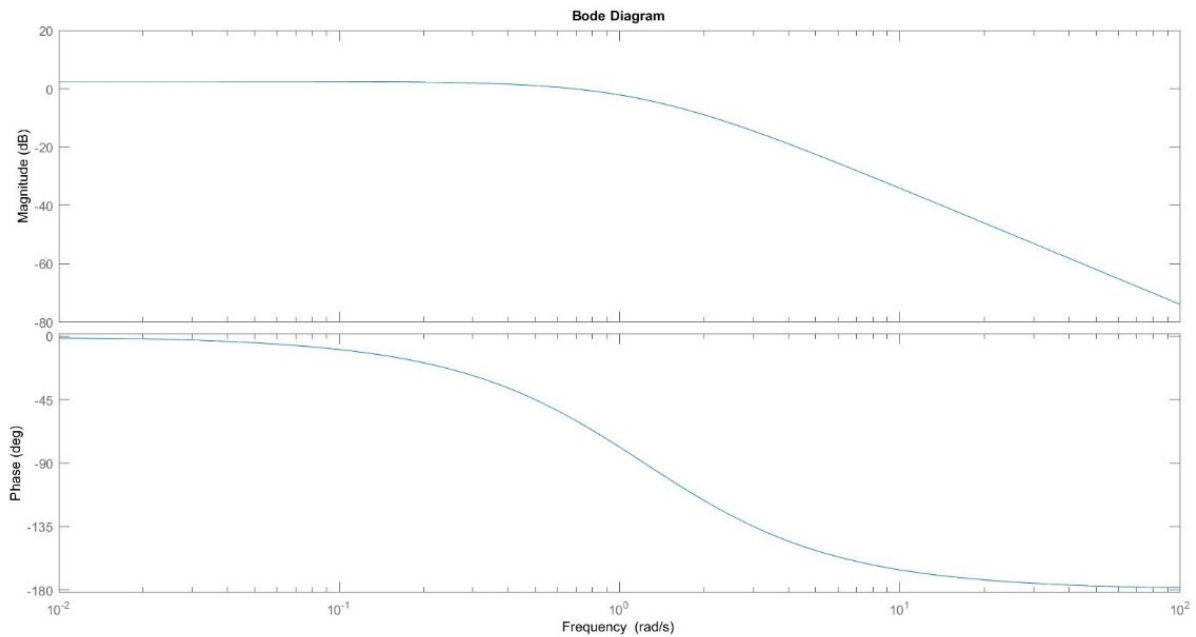
$$H(i\omega) = \frac{4}{2 * (i\omega)^2 + 5 * (i\omega) + 3} = \frac{4}{-2\omega^2 + 5 * (i\omega) + 3} * \frac{-2\omega^2 - 5 (i\omega) + 3}{-2\omega^2 - 5 (i\omega) + 3}$$

$$H(i\omega) = \frac{-8\omega^2 - 20(i\omega) + 12}{4\omega^4 + 13\omega^2 + 9} = \left[\frac{-8\omega^2 + 12}{4\omega^4 + 13\omega^2 + 9} \right] - \left[\frac{20(\omega)}{4\omega^4 + 13\omega^2 + 9} \right] i$$

$$\text{Amplitude} = |H(i\omega)| = \sqrt{\left[\frac{-8\omega^2 + 12}{4\omega^4 + 13\omega^2 + 9} \right]^2 + \left[\frac{20(\omega)}{4\omega^4 + 13\omega^2 + 9} \right]^2}$$

$$\text{Phase}(\phi) = \arctan \frac{\text{Imaginary}}{\text{Real}} = \arctan \left[\frac{\left[\frac{20(\omega)}{4\omega^4 + 13\omega^2 + 9} \right]}{\left[\frac{-8\omega^2 + 12}{4\omega^4 + 13\omega^2 + 9} \right]} \right]$$





4. PI- Controller setting on the basis of the step response (Overdamped):

Stability criterion (feedback closed loop)

PI controller: TF $[C(s)]$ $C(s) = \frac{q_1s + q_0}{s}$

$$1 + C(s) * G(s) = 0$$

$$[G(s)poles * C(s)poles] + [G(s)Zeros * C(s)Zeros] = 0$$

$$s * (2s^2 + 5s + 3) + 4 * (q_1s + q_0) = 2s^3 + 5s^2 + (3 + 4q_1)s + 4q_0 = 0$$

To guarantee feedback closed loop system stability it's necessary for the following term to not change Signs. (Routh-Hurwitz Criterion)

$$\frac{(15 + 20q_1) - (8q_0)}{5} > 0$$

$$q_1 > \frac{8q_0 - 15}{20}$$

$$4q_0 > 0$$

$$q_0 > 0$$

Take (integrator gain) $q_0 = 0.5$

Then, (Proportion gain) $q_1 > 0.55$

s^3	2	$(3+4q_1)$
s^2	5	$4q_0$
s^1	$\frac{(15 + 20q_1) - (8q_0)}{5}$	0
s^0	$4q_0$	0

Form Step Response

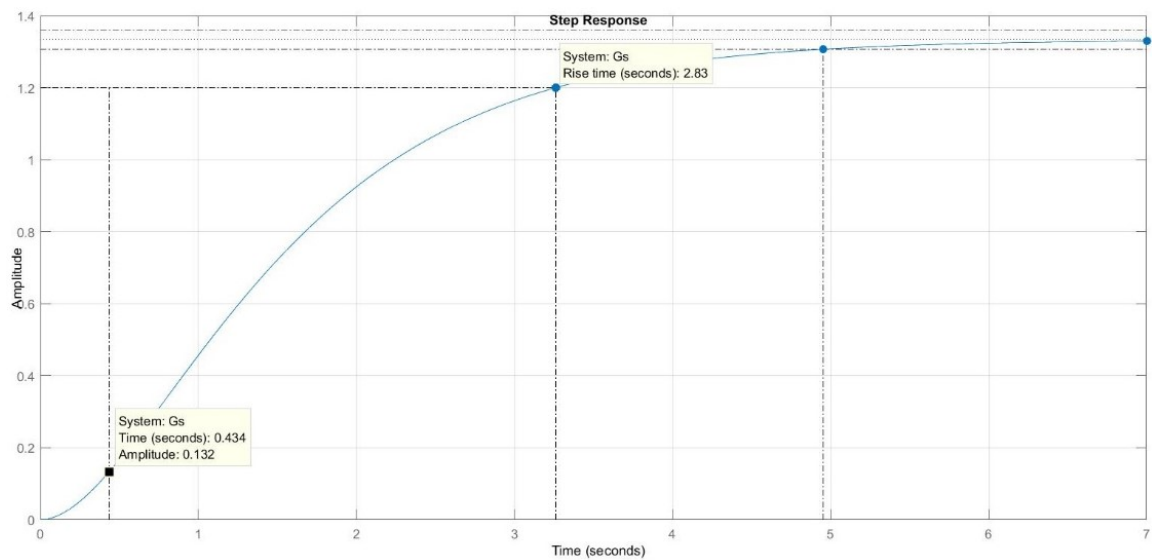
$T_u = 0.434$ seconds

$T_n = 2.396$ seconds

$$\gamma = \frac{T_n}{T_u} = \frac{2.396}{0.434} = 5.52$$

$$Kr = 0.9 * \gamma * \frac{1}{K} = 0.9 * 5.52 * \frac{3}{4} = 3.72$$

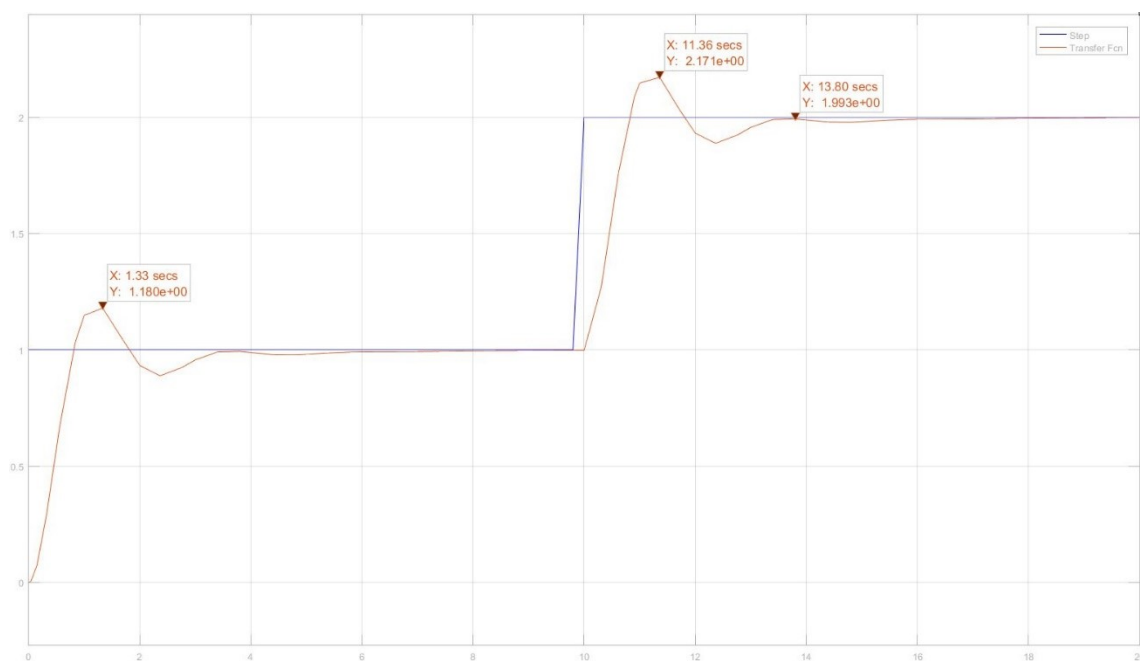
$$T_I = 3.5 * T_u = 3.5 * 0.434 = 1.51$$



Results:

System is stable.

Overshoot= 17%



5. PI-Controller (Cohen-Coon Method):

T1@ 0.283 K= 0.86 second

T2@ 0.631 K= 1.77 second

$$T = \frac{3}{2}(t_2 - t_1) = 1.36$$

$$\theta = t_2 - T = .41$$

$$r = \frac{\theta}{T} = 0.3$$

$$Kr = \frac{1}{K*r} \left(0.9 + \frac{r}{12} \right) = 2.31$$

$$TI = \frac{30+3r}{9+20r} * \theta = 0.84$$

Results:

Stable system

Overshoot = 0.4%

