PHIMECA

... solutions for robust engineering

Rare events probability estimation

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'HPC and Uncertainty Treatment – Examples with Open TURNS and Uranie'

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Outline

- Problem definition
- Brute-force estimation using Monte Carlo sampling
- Importance sampling
- Isoprobabilistic transformation
- Most-probable-failure-point(s)-based methods

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Problem definition

Given

a random vector with known probability distribution:

$$X \sim F_X$$

modelling the uncertainty attached to a component of interest.

and a performance model that characterize its state :

$$g: x \mapsto g(x)$$

with the convention:

- if $g(x) \le 0$, then the system *fails*;
- otherwise, it is safe.

Objective

Quantify the component safety level in the form of a (subjective) failure probability.

« subjective probability » = A probability that is condionned by assumptions/choices (probabilistic + performance models)

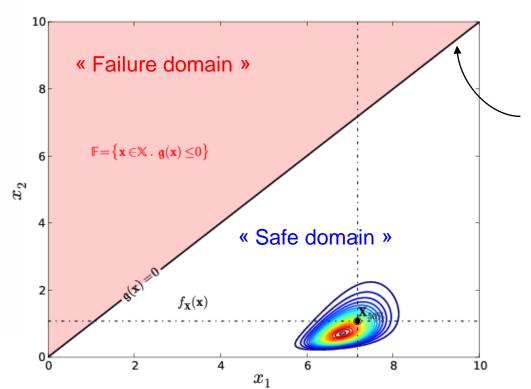


Input

• Ex : Consider a simple capacity vs demand example:

$$g(r,s) = r - s$$

with $R \sim \mathcal{LN}(\lambda_R, \zeta_R)$ and $S \sim \mathcal{LN}(\lambda_S, \zeta_S)$ and composed with a Normal copula whose shape matrix only term is $\rho_0 = 0,525$.



« Limit-state function »

$$p_f = \operatorname{Prob}[g(X) \le 0]$$

= $\operatorname{Prob}[X \in \mathbb{F}]$

Problem definition

Definitions for the failure probability

The failure probability is essentially defined as the *value of the CDF of the safety* margin $G \equiv g(X)$ at point 0.

$$p_f = F_G(0) = \int_{-\infty}^0 f_G(t) dt$$

but *G*'s distribution is rarely *known*.

It also rewrites as the sum of X's PDF over the failure domain \mathbb{F} :

$$p_f = \int_{\mathbb{F} = \{x \in \mathbb{X} : g(x) \le 0\}} f_X(x) dx$$

It eventually rewrites as the expectation of the *failure indicator function* $\mathbb{I}_{\mathbb{F}}$ over the support X of the input probability distribution:

$$p_f = \int_{\mathbb{X}} \mathbb{I}_{\mathbb{F}}(\mathbf{x}) f_{\mathbf{X}}(\mathbf{x}) d\mathbf{x} = \mathbb{E}[\mathbb{I}_{\mathbb{F}}(\mathbf{X})]$$



Problem definition

Premise

- $G \equiv g(X)$'s distribution is *rarely known* (it is in some specific cases: linear combinations of independent random variables, univariate composite distributions)
- Numerical integration techniques (e.g. quadrature rules) are not suitable for integrating indicator functions (their precision is often less than the probability's order of magnitude).

Dedicated methods

- Brute-force estimation using (intensive) Monte Carlo sampling
- Approximation methods
- Advanced, reduced variance, Monte Carlo sampling methods (not covered in this tutorial)
- Surrogate-model-based methods (not covered in this tutorial)



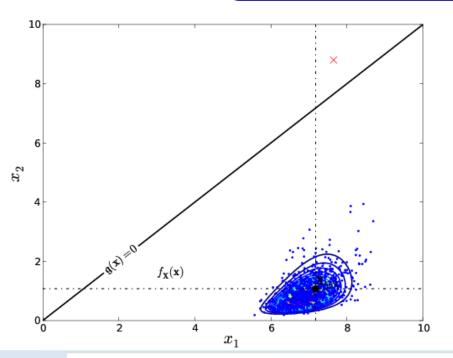
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Principle

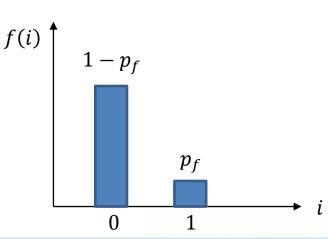
• The crude Monte Carlo estimator of the failure probability is *the empirical average* of the Bernoulli failure experiment:

$$\widehat{P}_{f,\text{MCS}} = \frac{1}{N} \sum_{i=1}^{N} \mathbb{I}_{\mathbb{F}} (X^{(i)})$$



where:

$$\mathbb{I}_{\mathbb{F}}(X) \sim \mathcal{B}\mathrm{er}\big(p_f\big)$$



Brute-force Monte Carlo estimation

Convergence

According to the *central limit theorem* (CLT), this estimator is unbiased and converges as follows:

$$\widehat{P}_{f,\text{MCS}} \underset{N \to \infty}{\sim} \mathcal{N} \left(p_f, \sqrt{\frac{p_f(1-p_f)}{N}} \right)$$

Rule of thumb: before applying the CLT, make sure that:

$$\min\{Np_f; N(1-p_f)\} \ge 10$$

The asymptotic distribution enables the calculation of $(1 - \alpha)$ -confidence intervals:

$$\hat{p}_{f,MCS} + \Phi^{-1}\left(\frac{\alpha}{2}\right)\sqrt{\frac{p_f(1-p_f)}{N}} \le p_f \le \hat{p}_{f,MCS} + \Phi^{-1}\left(1-\frac{\alpha}{2}\right)\sqrt{\frac{p_f(1-p_f)}{N}}$$

 $\underline{\mathsf{Ex}}$: For $1-\alpha=95\%$, $\Phi^{-1}\left(\frac{\alpha}{2}\right)\approx-1{,}96$ and $\Phi^{-1}\left(1-\frac{\alpha}{2}\right)\approx+1{,}96$.



Brute-force Monte Carlo estimation

Convergence

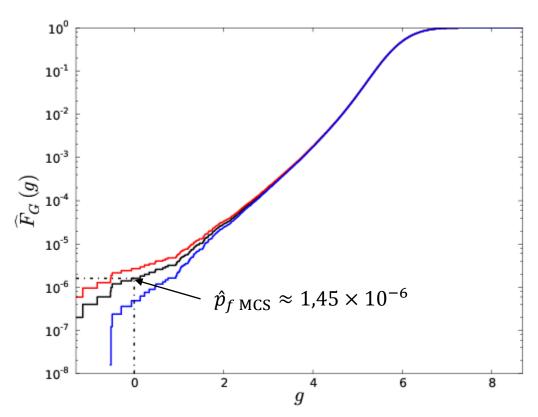
The *required sample size* drastically increases as the probability gets low:

For a given 10% target coefficient of variation

$$\delta = \sqrt{\frac{1 - p_f}{N p_f}} \approx \frac{1}{\sqrt{N p_f}}$$

$$p_f \approx 10^{-k} \Rightarrow N_{\min} \approx 10^{k+2}$$

p_f	N _{min}
10-2	10 000
10^{-3}	100 000
10^{-4}	1 000 000



Brute-force Monte Carlo estimation

Pros & cons

- + Unbiased, reference, estimator
- + Easy to implement (at least for the statistics part)
- + Rich result (it is then possible to build a good approximation of *G*'s CDF)
- + Highly distributable over highperformance computing means (*e.g.* over a cluster)

Slow convergence : requires important computing resources

When shoud it be used?

- When you don't have a choice (when no other more clever method is applicable)!
- When the performance function is fast to evaluate :
 - Simple closed-form expressions;
 - HPC resources available.



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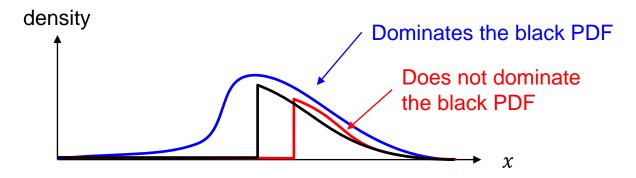
Importance sampling

Principle

Let H denote some instrumental probability distribution with PDF h satisfying the following dominance condition:

$$h(x) = 0 \Rightarrow \mathbb{I}_{\mathbb{F}}(x) f_X(x) = 0$$

that would ideally make the failure event of interest *more frequent*.



The failure probability rewrites:

$$p_f = \int_{\mathbb{X}} \mathbb{I}_{\mathbb{F}}(x) f_X(x) dx = \int_{\mathbb{X}} \frac{\mathbb{I}_{\mathbb{F}}(x) f_X(x)}{h(x)} h(x) dx$$

$$p_f = \mathbb{E}_{\mathbf{Z}} \left[\frac{\mathbb{I}_{\mathbb{F}}(\mathbf{Z}) f_{\mathbf{X}}(\mathbf{Z})}{h(\mathbf{Z})} \right]$$



Importance sampling

Use & properties

Given an N-sample:

$$\mathcal{Z} = \left\{ \boldsymbol{Z}^{(i)}, \qquad i = 1, \dots, N \right\} \sim h$$

The importance sampling estimator reads:

$$\widehat{P}_{f,h} = \frac{1}{N} \sum_{i=1}^{N} \frac{\mathbb{I}_{\mathbb{F}}(\mathbf{Z}^{(i)}) f_{X}(\mathbf{Z}^{(i)})}{h(\mathbf{Z}^{(i)})}$$

and converges according to the central limit theorem:

$$\widehat{P}_{f,h} \underset{N o \infty}{\sim} \mathcal{N}\left(p_f, \sigma_{p_f}\right)$$

The estimation variance obviously depends on h:

$$\sigma_{p_f}^2 = \frac{1}{N} \left(\mathbb{E}_{\boldsymbol{Z}} \left[\frac{\mathbb{I}_{\mathbb{F}}(\boldsymbol{Z}) f_{\boldsymbol{X}}^2(\boldsymbol{Z})}{h^2(\boldsymbol{Z})} \right] - p_f^2 \right)$$



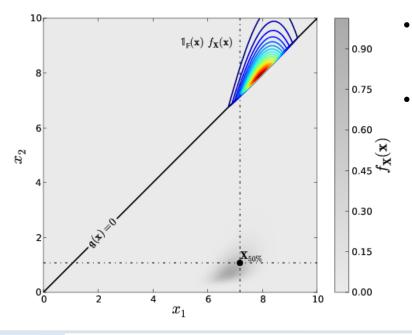
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Importance sampling

Choosing h?

- Any distribution provided the dominance condition holds.
- The best instrumental PDF yields a zero estimation variance and reads:

$$h^*(x) = \frac{\mathbb{I}_{\mathbb{F}}(x)f_X(x)}{p_f}$$



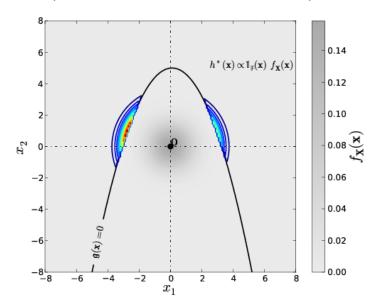
- impractical because its *normalizing*constant is the sought probability p_f !
 - confirms *intuition* :
 - it is the probability distribution of the input parameters yielding failure.
 - it barely satisfies the *dominance* condition.



Importance sampling

A fundamental concept in reliability analysis

- The objective is to explore the tail of the safety margin's probability distribution (the lower tail in our case: $p_f \equiv \text{Prob}[G \leq 0]$)...
- Using a *biased sampling technique for the input* in order to make failure much more frequent...
- And ideally, by sampling only and exhaustively failed situations (i.e. without forgetting any (significant) area of the failure domain).





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Isoprobabilistic transformation

Motivation

Spherical distributions are invariant by rotation $U \sim \mathbf{R}U$, $\forall \mathbf{R} \in \mathcal{SP}_n(\mathbb{R})$

thus enabling analytical developments (to come).

Available transformations

- Independent copula → Componentwise tranformations
- Elliptical copula → Generalized Nataf transformation
- Any other composed distribution → Rosenblatt transformation

The choice for the most-suitable transformation is automatic in OpenTURNS.

Further readings: Lebrun & Dutfoy (2009a,b,c).



Isoprobabilistic transformation

Standard space properties

- Given the *components order* in the input distribution and the Cholesky factor are fixed, the transformation is *unique* and *bijective* (it is *invertible*).
- The *probability measure is preserved*, hence the *failure probability* in the standard space equals the failure probability in the original (physical) space. ATTENTION: This does not hold for approximations though.
- The transformed performance function is defined by composition:

$$g^{\circ}(\boldsymbol{u}) = g(\boldsymbol{x}) = (g \circ T^{-1})(\boldsymbol{u}), \qquad \boldsymbol{u} \in \mathbb{R}^n$$

This, in turns, enables the definition of the *failure domain* in the standard space:

$$\mathbb{F}^{\circ} = \{ \boldsymbol{u} \in \mathbb{R}^n : g^{\circ}(\boldsymbol{u}) \le 0 \}$$



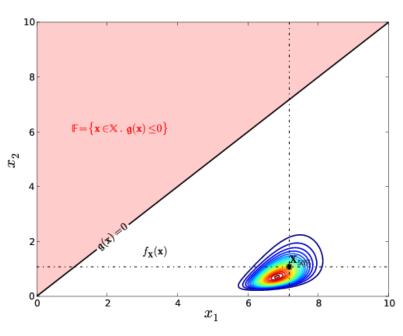
Isoprobabilistic transformation

Standard space properties

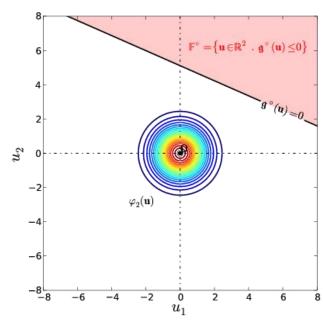
<u>Ex</u>: Consider the *capacity vs demand* example:

$$g(r,s) = r - s$$

where the variables $R \sim \mathcal{LN}(\lambda_R, \zeta_R)$ and $S \sim \mathcal{LN}(\lambda_S, \zeta_S)$ are composed with a Normal copula with shape parameter $\rho_0 = 0,525$.



Physical space



Standard space



Outline

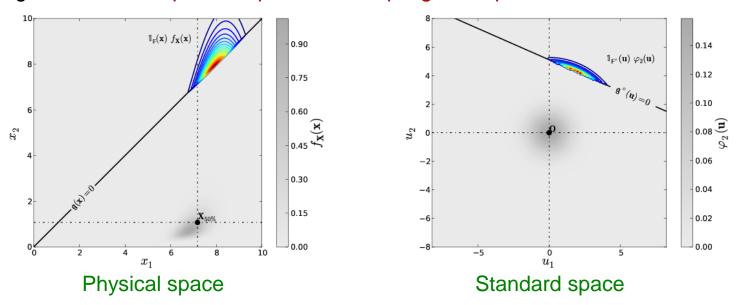
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MPFP: FORM, SORM, P*-IS & FORM- Σ

Most probable failure point(s)

Let's get back to the *optimal importance sampling concept*:



We define the most probable failure point(s) as the mode(s) of the optimal instrumental distribution:

$$u^* = \arg\max_{u \in \mathbb{R}^n} \mathbb{I}_{\mathbb{F}^{\circ}}(u) \varphi_n(u)$$

The solution for this optimization problem is *not nessarily unique*, although it is often the case in many applications (e.g. in structural mechanics).

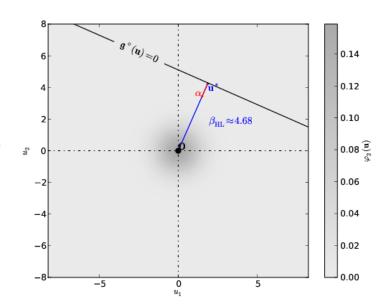
Most probable failure point(s)

Let's work on the definition:

$$u^* = \arg\max_{u \in \mathbb{R}^n} \mathbb{I}_{\mathbb{F}^{\circ}}(u) \varphi_n(u)$$

$$\boldsymbol{u}^* = \arg\max_{\boldsymbol{u} \in \mathbb{R}^n} \frac{1}{(2\pi)^{n/2}} \exp\left(-\frac{1}{2}\boldsymbol{u}^{\mathrm{T}}\boldsymbol{u}\right) : g^{\circ}(\boldsymbol{u}) \leq 0$$

$$u^* = \arg\min_{u \in \mathbb{R}^n} u^T u$$
: $g^{\circ}(u) \leq 0$



This is then equivalent to searching the *failure* point(s) in the standard space that are the closest to the origin.

Search algorithms (constrained optimization)

- The *Abdo-Rackwitz algorithm* exploits the specificities of the problem at hand:
 - The objective function is quadratic.
 - The constraint is nonlinear, but it is linearized at each step based on the information brought by the gradient.
 - The optimization steps (the moves amplitude) can either be *fixed* (small) or optimized (variable) using merit rules such as Goldstein-Armijo's.
 - The algorithm converges when the current point satisfies both:
 - $g(\mathbf{u}^*) = 0$ (the point in on the limit-state surface)
 - $\nabla_{\boldsymbol{u}} g^{\circ}(\boldsymbol{u}^{*}) / \boldsymbol{u}^{*}$ (the gradient of the constraint is colinear to that of the objective function)
- The COBYLA (Constrained Optimization BY Linear Approximations) algorithm is an interesting alternative when the partial differences of the performance function are hard to estimate (using finite differences schemes).

First-order reliability method (FORM)

- Assumption: the most probable failure point is *unique*.
- The performance function is linearized at the MPFP:

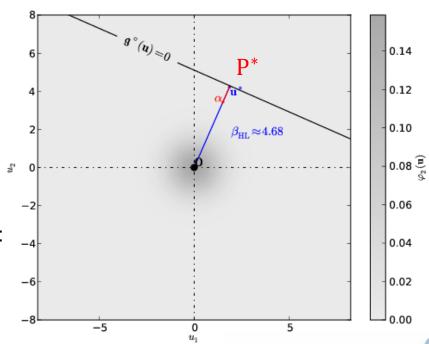
$$g_{1,\boldsymbol{u}^*}^{\circ}(\boldsymbol{u}) = g^{\circ}(\boldsymbol{u}^*) + \nabla_{\boldsymbol{u}}g^{\circ}(\boldsymbol{u}^*)^{\mathrm{T}}(\boldsymbol{u} - \boldsymbol{u}^*) = \nabla_{\boldsymbol{u}}g^{\circ}(\boldsymbol{u}^*)^{\mathrm{T}}(\boldsymbol{u} - \boldsymbol{u}^*)$$

We introduce the unit orientation vector

$$\alpha = \frac{\nabla_{\boldsymbol{u}} g^{\circ}(\boldsymbol{u}^{*})}{\|\nabla_{\boldsymbol{u}} g^{\circ}(\boldsymbol{u}^{*})\|_{2}}$$

And the *Hasofer-Lind reliability index*:

$$\beta_{\rm HL} = -\boldsymbol{\alpha}^{\rm T} \boldsymbol{u}^* = \overline{\rm OP}^*$$





First-order reliability method (FORM)

The approximate failure domain in the standard space rewrites:

$$\mathbb{F}_{1,u^*}^{\circ} = \left\{ \boldsymbol{u} \in \mathbb{R}^n : g_{1,u^*}^{\circ}(\boldsymbol{u}) \leq 0 \right\}$$

$$= \left\{ \boldsymbol{u} \in \mathbb{R}^n : \nabla_{\boldsymbol{u}} g^{\circ}(\boldsymbol{u}^*)^{\mathrm{T}}(\boldsymbol{u} - \boldsymbol{u}^*) \leq 0 \right\}$$

$$= \left\{ \boldsymbol{u} \in \mathbb{R}^n : \boldsymbol{\alpha}^{\mathrm{T}}(\boldsymbol{u} - \boldsymbol{u}^*) \leq 0 \right\}$$

$$= \left\{ \boldsymbol{u} \in \mathbb{R}^n : \boldsymbol{\alpha}^{\mathrm{T}} \boldsymbol{u} + \beta_{\mathrm{HL}} \leq 0 \right\}$$

So that we obtain the following first-order approximation of the failure probability:

$$p_{f 1, u^*} = \text{Prob}[\boldsymbol{\alpha}^{T} \boldsymbol{U} + \beta_{\text{HL}} \leq 0]$$

= $\text{Prob}[Z \leq -\beta_{\text{HL}}]$, with $Z = \boldsymbol{\alpha}^{T} \boldsymbol{U} \sim \mathcal{N}(0, 1)$

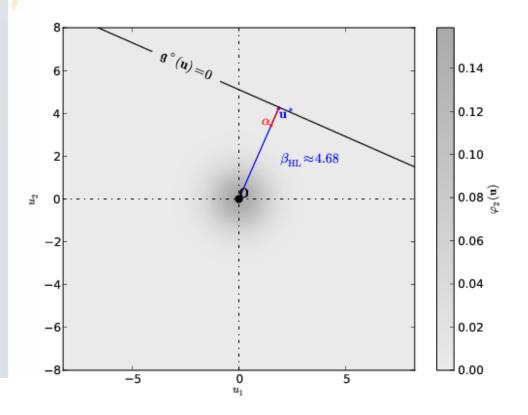
Hence:

$$p_{f 1, \boldsymbol{u}^*} = \Phi(-\beta_{\mathrm{HL}})$$



First-order reliability method (FORM)

• <u>Ex</u>: (capacity vs demand example)



 $eta_{HL} pprox 4,68$ $p_{f 1, oldsymbol{u}^*} pprox 1,44 imes 10^{-6}$

- The limit-state surface being linear in the standard space, in this particular case, FORM is the reference solution.
- Generally speaking, this is only an approximation.

e L

SORM: accounting for local curvatures

- Assuming we can compute the second-order partial derivatives of the performance *function* in the standard space.
- On peut prendre en compte l'éventuelle courbure de l'état-limite en poussant le développement de Taylor à l'ordre 2 au voisinage du P* :

$$g_{2,\boldsymbol{u}^*}^{\circ} = g^{\circ}(\boldsymbol{u}^*) + \nabla_{\boldsymbol{u}}g^{\circ}(\boldsymbol{u}^*)^{\mathrm{T}}(\boldsymbol{u} - \boldsymbol{u}^*) + \frac{1}{2}(\boldsymbol{u} - \boldsymbol{u}^*)^{\mathrm{T}}\nabla_{\boldsymbol{u}\boldsymbol{u}}g^{\circ}(\boldsymbol{u}^*)(\boldsymbol{u} - \boldsymbol{u}^*)$$

In case the standard space is spanned by Gaussian variables, Breitung has shown the following asymptotic result:

$$\left(p_{f 2, \mathbf{u}^*} \underset{\beta_{\mathrm{HL}} \to +\infty}{\to} \Phi(-\beta_{\mathrm{HL}}) \prod_{i=1}^{n} \frac{1}{\sqrt{1 + \beta_{\mathrm{HL}} \kappa_i}}\right)$$

where κ_i are the *curvatures* calculated from the Hessian matrix. This result is *valid* as soon as $1 + \beta_{HL} \kappa_i \ge 0$, i = 1, ..., n.

Lebrun & Dutfoy (2009a) generalized the approximation to *spherical distributions*.



P*-IS: MPFP(s)-centered importance sampling

- Another correction can be obtained by *importance sampling with an instrumental* PDF centered at the identified MPFP(s).
- For this, the state-of-the-art consists in using a Gaussian instrumental distribution:

$$\varphi_{n,\boldsymbol{u}^*}(\boldsymbol{u}) = \varphi_n(\boldsymbol{u} - \boldsymbol{u}^*) = \frac{1}{(2\pi)^{n/2}} \exp\left(-\frac{(\boldsymbol{u} - \boldsymbol{u}^*)^{\mathrm{T}}(\boldsymbol{u} - \boldsymbol{u}^*)}{2}\right)$$

In this case, the failure probability estimator simplifies:

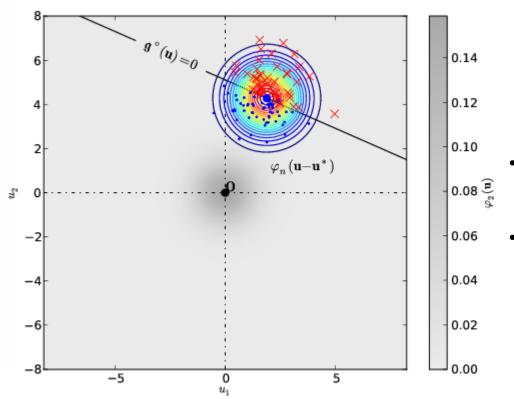
$$\widehat{P}_{f, \mathbf{u}^* \text{IS}} = \frac{\exp(-\beta_{\text{HL}}^2/2)}{N} \sum_{i=1}^{N} \mathbb{I}_{\mathbb{F}^{\circ}}(\mathbf{Z}^{(i)}) \exp(-\mathbf{Z}^{(i)} \mathbf{u}^*)$$

- It is unbiased if the dominance condition of φ_{n,u^*} over $\mathbb{I}_{\mathbb{F}^{\circ}} \times \varphi_n$ holds (unicity of the MPFP?).
- It « converges » much faster, because the sampled points fails with a probability that is close to 50% (say between 10 and 90%).



P*-IS: MPFP(s)-centered importance sampling

Ex: (capacity vs demand example)



 $p_{f,u^*IS} \approx 1,49 \times 10^{-6}$ up to a 10% coefficient of variation.

- Convergence is obtained with only 600 additional runs of g...
- Compared to 10^8 runs for crude Monte Carlo that gave:

$$\hat{p}_{f, \text{MCS}} \approx 1.45 \times 10^{-6}$$
 up to a 10% coefficient of variation.

FORM: importance factors

The unit direction vector indicates how the *reliability index evolves with respect to* the MPFP coordinates.

$$\beta_{\mathrm{HL}} = -\boldsymbol{\alpha}^{\mathrm{T}} \boldsymbol{u}^{*} = \sum_{i=1}^{n} -\alpha_{i} u_{i}^{*} \Rightarrow \alpha_{i} = -\frac{\partial \beta_{\mathrm{HL}}}{\partial u_{i}^{*}}$$

In case the distribution has a non-independent copula though, each standard variable u_i is a function of several original (physical) variable x_i , so that the α_i 's are difficult to read.



FORM: importance factors

In case the copula is Normal, Lemaire (2009) defined the following corrected *importance factors*:

$$\gamma_i = \frac{1}{\|\boldsymbol{\gamma}\|_2} \sigma_{X_i} \frac{\partial g}{\partial x_i} \bigg|_{\boldsymbol{x}=\boldsymbol{x}^*}, \qquad i = 1, ..., n$$

In the more general case, Lebrun & Dutfoy (2009c) proposed another more general, although unsigned, definition:

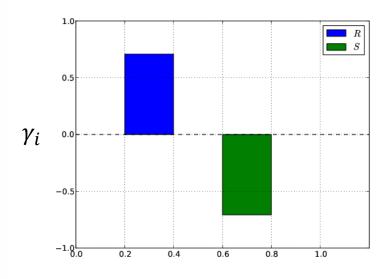
$$\gamma_i^2 = \frac{w_i^2}{\|\mathbf{w}\|_2^2}, \qquad i = 1, ..., n$$

$$\mathbf{w} = \begin{pmatrix} E^{-1}(F_{X_1}(x_1)) \\ \vdots \\ E^{-1}(F_{X_n}(x_n)) \end{pmatrix}$$



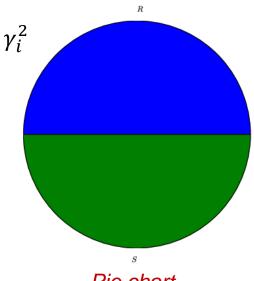
FORM: importance factors

These results are often presented in either one or both of these two charts:



Signed bar chart

 α_i or γ_i positive $\Rightarrow X_i$ is a capacity variable α_i ot γ_i negative $\Rightarrow X_i$ is a demand variable



Pie chart

The quadratic sum equals 1. Qualitative comparison of the importance of variables w.r.t. failure.



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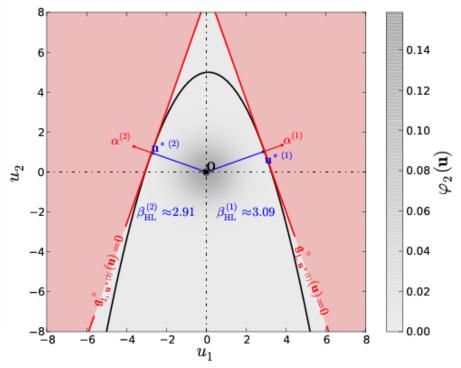
MPFP: FORM, SORM, P*-IS & FORM- Σ

FORM: Multiple design points

Ex : Consider the following limit-state function:

$$g(x_1, x_2) = b - x_2 - \kappa (u_1 - e)^2$$

where $X = U \sim \mathcal{N}(\mathbf{0}, \mathbf{I}), b = 5, \kappa = 0.5$ and e = 0.1.



- PMSoft implements an algorithm that is devoted to the search of multiple P* using:
 - a smart reset strategy;
 - exclusion balls around the already found design points.
 - See Der Kiureghian & Dakessian (1998).
- However the enumeration may lack completeness.



FORM-Σ: Serial combination of linear limit-states

- Input: for the n_{P^*} identified MPFPs:
 - reliability indices: $\boldsymbol{\beta}_{\mathrm{HL}} = \left(\beta_{\mathrm{HL}}^{(i)}, i = 1, ..., n_{P^*}\right)$
 - importance factors in the standard space: $\mathbf{A} = (\boldsymbol{\alpha}^{(i)}, i = 1, ..., n_{P^*})$
- Objective: combine these results into a single probability, the one associated to the serial system formed by the contributors.
- Solution:

$$\left[p_{f,1\Sigma} = \operatorname{Prob} \left[\boldsymbol{U} \in \bigcup_{i=1}^{n_{P^*}} \left\{ \boldsymbol{u} \in \mathbb{R}^n : \boldsymbol{\alpha}^{(i)} \, ^{\mathrm{T}} \boldsymbol{u} + \beta_{\mathrm{HL}}^{(i)} \leq 0 \right\} \right] = 1 - \Phi_{n_{P^*}}(\boldsymbol{\beta}_{\mathrm{HL}}; \boldsymbol{0}, \boldsymbol{\rho})$$

where:

$$\rho_{ij} = \boldsymbol{\alpha}^{(i) \mathrm{T}} \boldsymbol{\alpha}^{(j)}, \qquad i, j = 1, ..., n_{P^*}$$

are the « pairwise limit-states' correlation » $(-1 \le \rho \le 1)$.

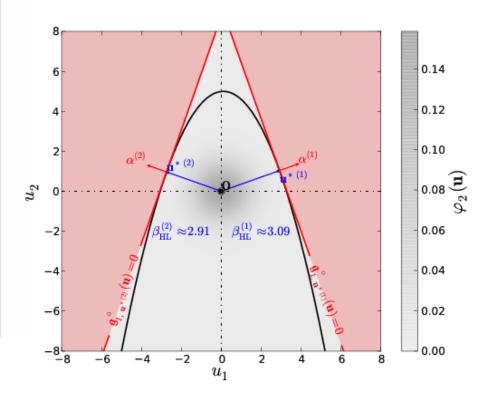


FORM-Σ : Serial combination of linear limit-states

• Ex: Consider the following limit-state function:

$$g(x_1, x_2) = b - x_2 - \kappa (u_1 - e)^2$$

where $X = U \sim \mathcal{N}(\mathbf{0}, \mathbf{I}), b = 5, \kappa = 0.5$ and e = 0.1.



The correlation between the two limitstates is:

$$\rho_{12} = \boldsymbol{\alpha}^{(1) \, \mathrm{T}} \boldsymbol{\alpha}^{(2)} \approx -0.78$$

Hence the *first-order approximation* of the serial system failure probability is:

$$p_{f_{1,\Sigma}} = 1 - \Phi_2 \left(\begin{pmatrix} 3,09 \\ 2,91 \end{pmatrix}; 0, \begin{bmatrix} 1 & -0.78 \\ -0.78 & 1 \end{bmatrix} \right)$$

 $\approx 2.82 \times 10^{-3}$

The crude Monte Carlo estimate is:

$$\hat{p}_{f,MCS} \approx 3.12 \times 10^{-3}$$

Up to a 10% coefficient of variation.



Pros & Cons

- + The most probable failure point concept is interesting because:
 - + Coordinates → singular configuration(s) of the system.
 - + Importance factors → give clues for improving reliability.
- + Affordable computational cost.

- The most probable failure point concept is dangerous:
 - non-unicity risk
 (FORM, SORM & basic P*-IS);
 - non-completeness risk (FORM- Σ).
- Missing (FORM, SORM, FORM-Σ) or subjective (P*-IS) error metric.

When should it be used?

- As a first approximation;
- Confirmed by an expert judgement about the identified failure modes.



Conclusions

 Reliability methods aim at estimating the safety level attached to a component in the form of a subjective failure probability:

$$p_f = \text{Prob}[\text{failure} \mid \text{model}]$$

- The methods reviewed in this presentation are implemented in *OpenTURNS* & *Uranie*.
- Crude Monte Carlo sampling enables exploring the model:
 - without requiring any assumption,
 - at a great computational expense though (HPC may help).
- Most-probable-failure-point(s)-based techniques enable:
 - a reduction of the computational effort (even if HPC may still help);
 - a deeper investigation of the system thanks to:
 - the most probable failure points coordinates;
 - the importance factors.



Further readings

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