#### Mooring Forces Calculator (Port or Starboard on Quay)

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#### What does this Excel Sheet do?

This Excel sheet helps you calculate the environmental forces on a vessel when it is moored by Port or Starboard Side aligned with the Quay (as shown in figure on right)

It further calculates the Line Tensions on the Mooring Lines, and reports the Factor of Safety for each mooring line

#### How to use this Excel Sheet

The user is asked for some inputs for the Vessel, Cargo and Environment and Mooring Line Configuration. The Input cells are highlighted in blue.

The user has to provide all the inputs highlighted in blue. Please do not make any changes to the output sheets

For some inputs, Tables and charts are required to be referred. These Tables and charts are provided alongwith for the user to enter these inputs.

Once all inputs are provided, the Environmental forces are calculated, and from these forces, the Mooring Line Tensions are calculated

The user should conduct separate checks for normal and heavy weather conditions. Factors of safety are 9.0 for normal, and 3.0 for heavy weather condition

The mooring pattern should be investigated for both ballast and fully loaded cases for each weather condition

#### Coordinate System and Axes (See figure on right)

The origin of coordinate system is at fwd end of the vessel longitudinally, Centreline transversely and at Mean Sea Level vertically

X-axis is positive towards aft, Y-axis is positive towards the quay, Z-axis is positive vertically upwards

#### Assumptions/Limitations

Mooring line arrangement should be symmetrical about the midship of the vessel

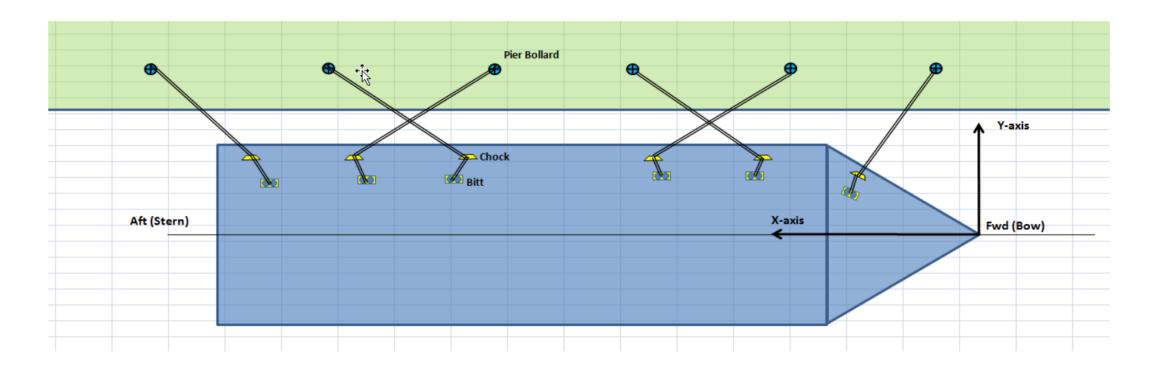
Wind and current forces are assumed to be steady state in nature. Wave force is assumed to be negligible

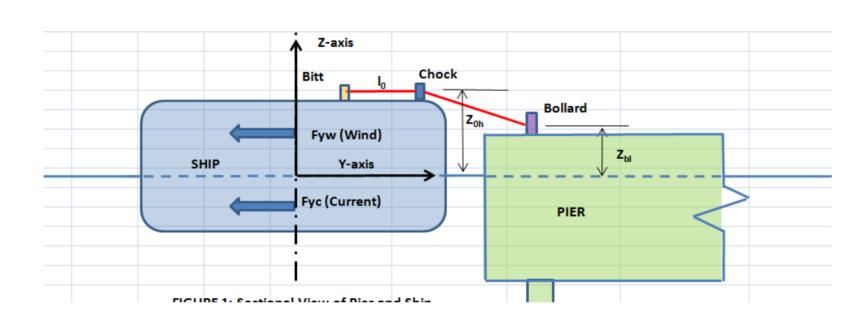
The line spring coefficients are constant, i.e., the Cyoung's modulus of mooring lines does not vary much with line tension forces

#### References

1. DDS-582-1 Calculations for Mooring Systems, Department of the Navy, Naval Sea Systems Command, Washington DC, 20362-5101

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### MOORING FORCES CALCULATION - VESSEL INPUTS

General Particulars						
Particular		Value	Default Value	Units		
Acceleration due to Gravity	g	9.81	9.81	m/s <sup>2</sup>		
Density of air	$ ho_{air}$	1.23	1.23	kg/m³		
Density of Water	$ ho_{water}$	1025	1025	kg/m³		
	Vessel Partio	culars				
Particular		Value		Units		
Vessel Name		Ship 1				
Principal Particulars						
Length Waterline (LWL)	LWL	116.74		m		
Breadth	В	12.53		m		
Mean Draft (Working)	Т	4.27		m		
Ship XCG (Longitudinal CG) - from Bow	Xcg	57.91	58.37	m		
Displacement	Δ	3403.75		MT		
Wetted Surface Area <sup>1</sup>	S	1631.37	1631.37	m <sup>2</sup>		

Wind Areas				
End projected wind area <sup>2</sup>	A <sub>e</sub>	0		m <sup>2</sup>
Side projected wind Area	A <sub>s</sub>	845.44		m <sup>2</sup>
Vessel Type (1 - for Normal shape, 2 - for Hull				
Dominated shape)		1	1	

¹The default Wetted Surface Area, S, is approximated by formula S = 2.588 \* √(Displacement \* LWL). User can input a different figure if available

<sup>&</sup>lt;sup>2</sup>The End Projected wind Area should be input as zero if the environment is only in transverse direction

## MOORING FORCES CALCULATION INPUTS- ENVIRONMENT

Wind and Current Parameters							
Particular Value Default Value Units							
Design Wind Speed	$V_{\rm w}$	25.72	20	m/s			
Wind Angle (See Fig 1) - from 0 to 180 deg	$\theta_{\rm w}$	90		degrees			
Current Speed	V <sub>c</sub>	1.5432	0.5	m/s			
Current Angle (See Fig 2) - from 0 to 180 deg	$\theta_{\rm c}$	0		degrees			
Water Depth	WD	13.72		m			

## Wind at angle $\theta_w$

# Aft (Stern) Fwd (Bow) 0 Degree 180 Degree $\theta_{\rm W}$ (deg) $\theta_{\rm Should}$ be entered as the angle made by wind with the bow of the vessel. $\theta$ should be between 0 and 180 degrees (same for Port or Stbd wind)

Fig 1: Wind Angle

# Current at angle $\theta_{C}$

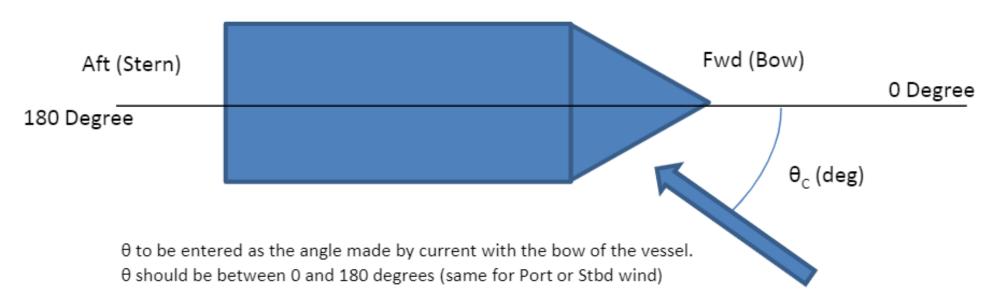
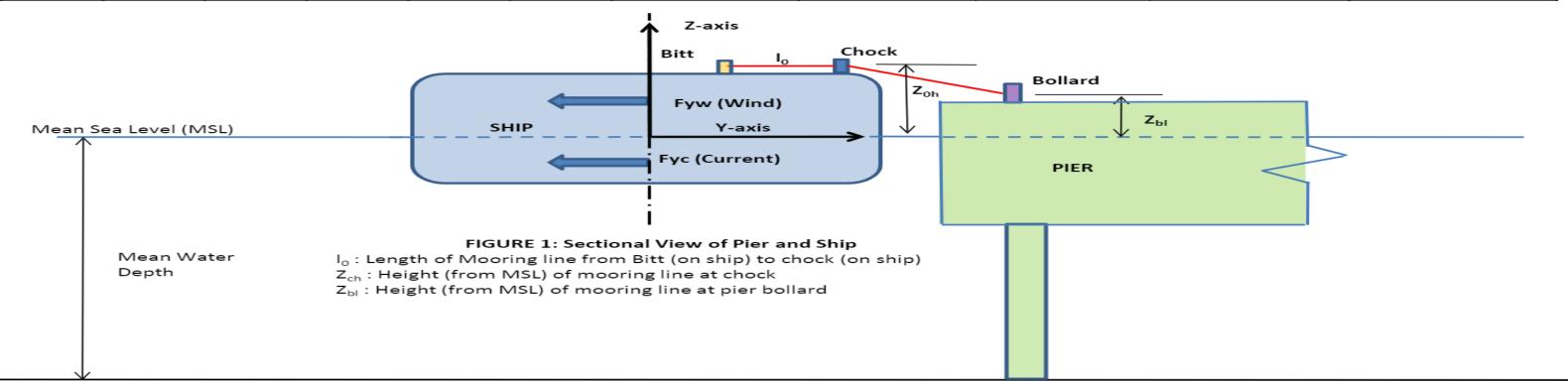


Fig 1: Current Angle

#### MOORING FORCES CALCULATION INPUTS- MOORING LINES

Please input the mooring line properties in this worksheet. The maximum number of mooring lines possible is 16. The mooring pattern should be symmetrical about the vessel's midship

Line No.		ordinates o ee Figs 1 &			oordinates a ee Figs 1 &	at pier (m) 2)	Line Length from Bitt to Chock (m) (See Fig 2)	Young's modulus of rope (GPa)	No. of rope parts	Cross Sectional Area of <u>one</u> rope (mm²)	Minimum breaking Strength of <u>one</u> rope (MT)
	X <sub>ch</sub>	Y <sub>ch</sub>	Z <sub>ch</sub>	X <sub>bl</sub>	Y <sub>bl</sub>	Z <sub>bl</sub>	Ι <sub>ο</sub>	E	n	а	MBS <sub>rope</sub>
1	0	0	6.4	-7.32	8.23	2.74	3.66	1.378	3	1291	33.3
2	4.88	1.52	5.79	0	8.23	2.74	2.44	1.378	3	1291	33.3
з	11.58	2.74	5.49	21.95	8.23	2.74	2.44	1.378	3	1291	33.3
4	21.34	4.88	4.72	7.32	8.23	2.74	2.44	1.378	3	1291	33.3
5	96.93	6.1	2.9	102.41	8.23	2.74	3.05	1.378	3	1291	33.3
6	106.68	5.33	3.05	95.1	8.23	2.74	2.44	1.378	3	1291	33.3
7	110.95	4.88	3.2	117.04	8.23	2.74	2.44	1.378	3	1291	33.3
8	118.87	3.05	3.2	124.36	8.23	2.74	3.35	1.378	3	1291	33.3
9	80.47	6.1	2.9	87.78	8.23	2.74	2.44	1.378	3	1291	33.3
10											
11											
12											
13											
14											
15											
16											



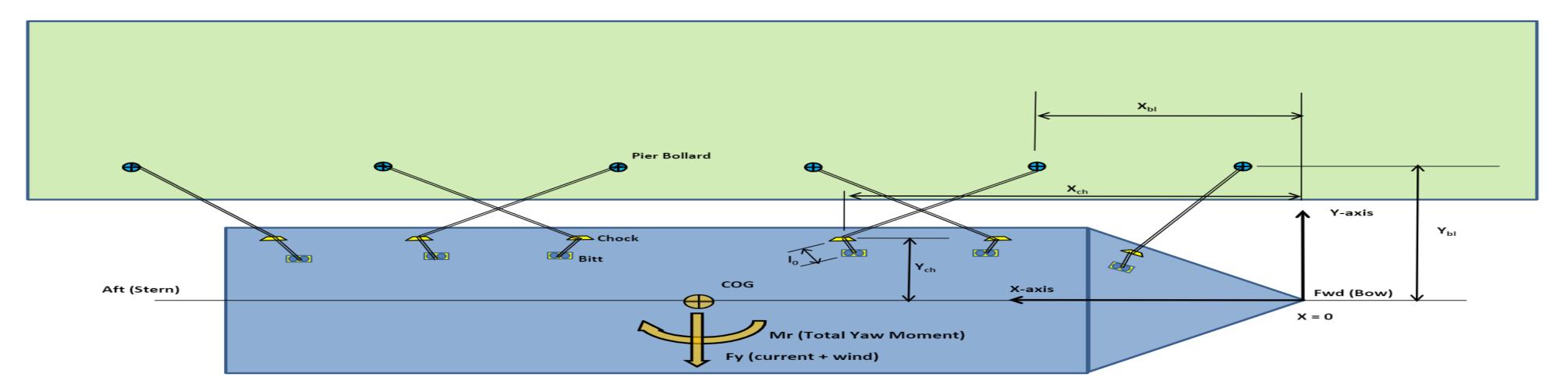


Fig 2: Plan View of a Typical Mooring Pattern

(for reference only, not reflective of actual mooring pattern entered by user)

 $X_{\text{ch}}$ : Longitudinal distance of mooring line chock from vessel's bow  $Y_{\text{ch}}$ : Transverse distance of mooring line chock from vessel'' Centerline

#### Wind Forces and Yaw Moment Calculation\*

\* References:

1. DDS 582-1 Calculations for Mooring Systems, DDS-582-1-d(1)

 $F_{YW} = 1/2 * C_{YW} \rho_{air} * V_W^2 * A_s$  (Wind Force in Transverse direction)

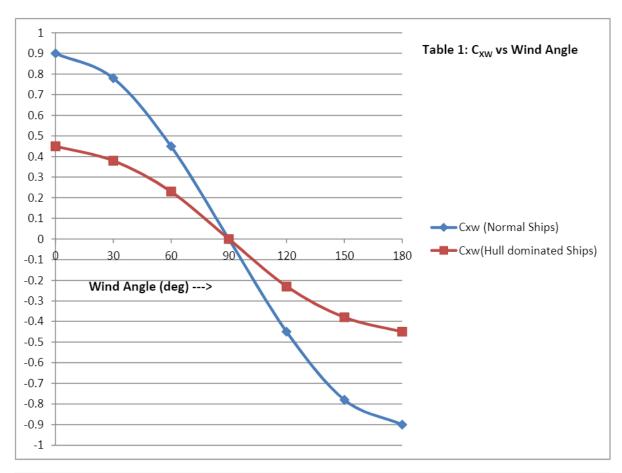
 $F_{XYW} = 1/2 * C_{XYW} \rho_{air} * V_W^2 * A_S * LWL$  (Wind Yaw Moment)

 $\rho_{air}$  = Density of Air,  $V_w$  = Wind Speed,  $A_E$  = End projected Wind Ares,  $A_S$  = Side Projected Wind Area

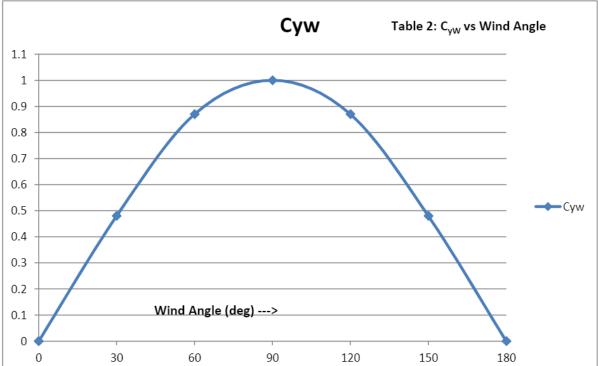
 $C_{xw}$  = Longitudinal Wind Force Coefficient (See Table 1),  $C_{yw}$  = Lateral Wind Force Coefficient (See Table 2),  $C_{xyw}$  = Wind Yaw Moment Coefficient (See Table 3)

Basic Parameters						
Particulars	Notation	Value	Units			
	HULL	•				
Length of Waterline	LWL	116.74				
End projected wind area	A <sub>e</sub>	0	m <sup>2</sup>			
Side projected Wind Area	A <sub>s</sub>	845.44	m <sup>2</sup>			
Design Wind Speed	V <sub>w</sub>	25.72	m/s			
Density of air	$ ho_{air}$	1.23	kg/m <sup>3</sup>			
Wind Angle	$\theta_{\rm w}$	90	degrees			
Ship Type (1 - Normal, 2 - Hull dominated)		1				
	Wind Force Coefficients					
Longitudinal Wind Force Coefficient	C <sub>XW</sub>	0	See Table 1			
Lateral Wind Force Coefficient	C <sub>YW</sub>	1	See Table 2			
Wind Yaw Moment Coefficient	C <sub>XYW</sub>	-0.037	See Table 3			

WINDLOAD					
Longitudinal Wind Force	$F_{XW} = 1/2 * C_{xw} * \rho_{air} * V_w^2 * A_E$	0.00	MT		
Lateral Wind Force	$F_{YW} = 1/2 * C_{yw} * \rho_{air} * V_w^2 * A_S$	35.06	MT		
Total Factored Windage Area of Hull in Lateral Direction	$M_W = 1/2 * C_{xyw} * \rho_{air} * V_w^2 * A_S * LWL$	-151.44	MT-m		



C <sub>xw</sub>						
Angle (deg)	Cnormal	Chull				
0	0.9	0.45				
30	0.78	0.38				
60	0.45	0.23				
90	0	0				
120	-0.45	-0.23				
150	-0.78	-0.38				
180	-0.9	-0.45				



C <sub>YW</sub>					
Angle (deg)	C <sub>YW</sub>				
0	0				
30	0.48				
60	0.87				
90	1				
120	0.87				
150	0.48				
180	0				

			Cxyw	Table 3: C <sub>xyW</sub> vs Wind Angle
0.04			Wind Angle (de	g)>
0	30	60	90 120	150
				<b>—</b>
-0.06				
-0.16				

C <sub>2</sub>	ΥW
Angle (deg)	C <sub>XYW</sub>
0	0
10	0.023
30	0.054
45	0.063
60	0.054
90	-0.037
120	-0.14
135	-0.155
150	-0.14
180	0

#### Current Forces and Yaw Moment Calculation\*

\* References:

1. DDS 582-1 Calculations for Mooring Systems, DDS-582-1-d(2)

Current Forces and Moments are given by:

#### $F_{YC} = 1/2 * C_{YC} \rho_{water} * V_c^2 * LWL * T$ (Current Force in Transverse direction)

 $F_{XYC} = 1/2 * C_{XYC} \rho_{air} * V_c^2 * LWL^2 * T$  (Current Yaw Moment)

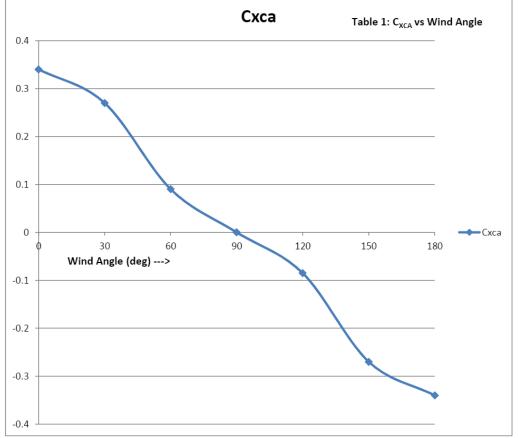
 $\rho_{\text{water}}$  = Density of Water,  $V_{\text{C}}$  = Current Speed,  $C_{\text{XCA}}$  = Longitudinal Current Skin Friction Coefficient (Table 1),  $C_{\text{XCB}}$  = Longitudinal Current Drag Coefficient  $C_{\text{YC}}$  = Lateral Current Force Coefficient (See Table 2),  $C_{\text{XYC}}$  = Current Yaw Moment Coefficient (See Table 3), S = Wetted Surface Area of Hull

Note 1:  $C_{XCB}$  is given by formula  $C_{XCB} = C_{YC} * \cos^2 \theta_C$ 

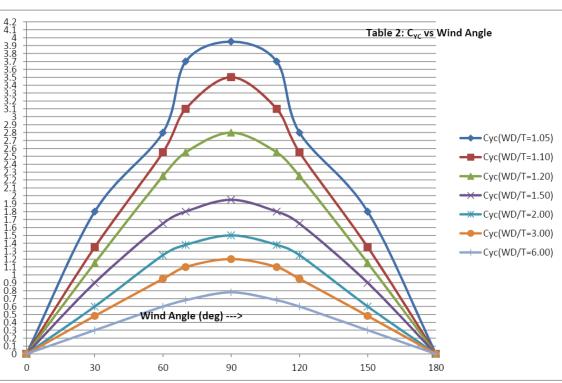
Basic Parameters								
Particulars	Notation	Notation Value						
HULL								
Length of Waterline	LWL	116.74	h m					
Breadth	В	12.53	m m					
Draft	Т	4.27	m m					
Water Depth	WD	13.72	m m					
Wetted Surface Area	S	1631.37	m <sup>2</sup>					
Design Current Speed	V <sub>C</sub>	1.5432	. m/s					
Density of water	$ ho_{ m water}$	1025	kg/m³					
Current Angle	θ <sub>C</sub>	(	degrees					
Ratio of Water Depth to Draft WD/T	WD/T	3.22						
	Current Force Coeffic	cients						
Longitudinal Current Skin Friction Coefficient	C <sub>XCA</sub>	0.3400	See Table 1					
Lateral Current Force Coefficient	C <sub>YC</sub>	0.0000	See Table 2					
Longitudinal Current Drag Coefficient	C <sub>XCB</sub>	0.0000	$C_{YC} * cos^2 \theta_C$					
Current Yaw Moment Coefficient	C <sub>XYC</sub>	0.0000	See Table 3					

WINDLOAD						
Longitudinal Current Force	$F_{XC} = 1/2 * \rho_{water} * V_c^2 * B* (C_{XCA} * S/LWL + C_{XCB} * T)$	<b>7.41</b> MT				
Lateral Current Force	$F_{YC} = 1/2 * C_{YC} * \rho_{water} * V_c^2 * LWL*T$	<b>0.00</b> MT				
Current Yaw Moment	$F_{xyc} = 1/2 * C_{xyc} * \rho_{water} * V_c^2 * LWL^2 * T$	<b>0.00</b> MT-m				

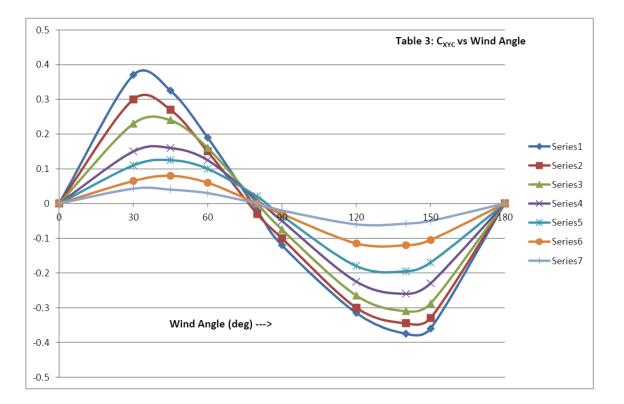
# MOORING FORCES CALCULATOR (PORT/STBD ON QUAY) www.thenavalarch.com



C <sub>2</sub>	(CA
Angle (deg)	C <sub>xca</sub>
0	0.34
30	0.27
60	0.09
90	0
120	-0.085
150	-0.27
180	-0.34
•	



С <sub>УС</sub>													
Angle (deg)	WD/T = 1.05	WD/T = 1.10	WD/T = 1.20	WD/T = 1.50	WD/T = 2.00	WD/T = 3.00	WD/T = 6.00						
0	0	0	0	0	0	0	0						
30	1.8	1.35	1.15	0.9	0.6	0.48	0.3						
60	2.8	2.55	2.25	1.65	1.25	0.95	0.6						
70	3.7	3.1	2.55	1.8	1.38	1.1	0.68						
90	3.95	3.5	2.8	1.95	1.5	1.2	0.78						
110	3.7	3.1	2.55	1.8	1.38	1.1	0.68						
120	2.8	2.55	2.25	1.65	1.25	0.95	0.6						
150	1.8	1.35	1.15	0.9	0.6	0.48	0.3						
180	0	0	0	0	0	0	0						



C <sub>XYC</sub>														
Angle (deg)	WD/T = 1.05	WD/T = 1.10	WD/T = 1.20	WD/T = 1.50	WD/T = 2.00	WD/T = 3.00	WD/T = 6.00							
0	0	0	0	0	0	0	0							
30	0.37	0.3	0.23	0.15	0.11	0.065	0.043							
45	0.325	0.27	0.24	0.16	0.125	0.08	0.04							
60	0.19	0.15	0.16	0.125	0.1	0.06	0.03							
80	-0.02	-0.03	0	0.01	0.02	0	0							
90	-0.12	-0.1	-0.075	-0.05	-0.035	-0.03	-0.02							
120	-0.315	-0.3	-0.265	-0.225	-0.18	-0.115	-0.06							
140	-0.375	-0.345	-0.31	-0.26	-0.195	-0.12	-0.058							
150	-0.36	-0.33	-0.288	-0.23	-0.17	-0.105	-0.05							
180	0	0	0	0	0	0	0							

# **Final Total Forces and Moment**

\* References:

1. DDS 582-1 Calculations for Mooring Systems, DDS-582-1-d(3)

FINAL FORCES AND MOMENTS									
Longitudinal Wind + Current Force	$F_X = F_{XC} + F_{XW}$	7.41	MT						
Lateral Wind + Current Force	$F_{Y} = F_{YC} + F_{YW}$	35.06	MT						
Total Yaw Moment	$M_r = M_C + M_W - 0.48 * LWL * F_X$	-566.40	MT-m						

#### MOORING FORCES CALCULATION - MOORING LINE FORCES

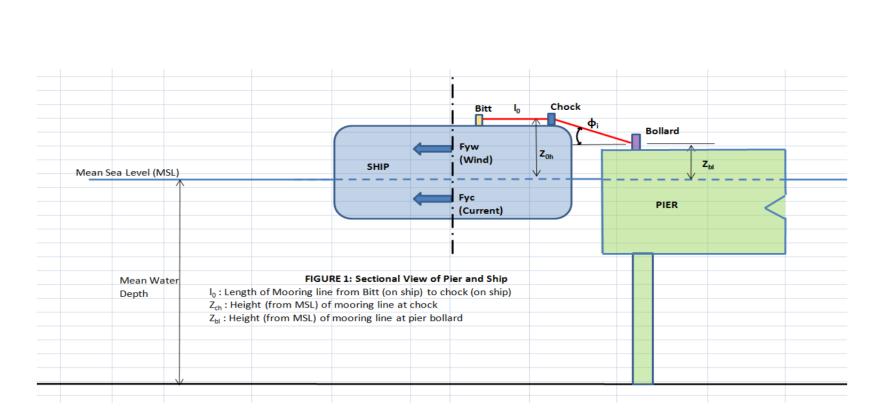
\* References:

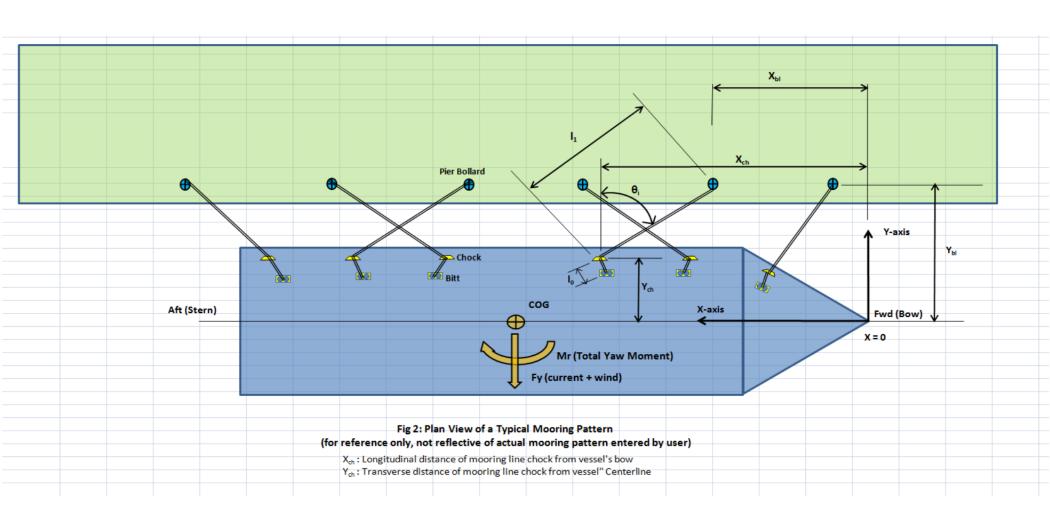
1. DDS 582-1 Calculations for Mooring Systems, DDS-582-1-e

\*Note: Factor of Safety should be more than 9 for Normal environment, and more than 3 for extreme environment

F <sub>Y</sub> (kN)	343.95	a (kN/m)	1910.042	δ <sub>y</sub> (m) =	0.266				
$M_r$ (kN-m)	-5556.40	b (kN)	117866.463	$\delta_y = (F_y * c - (M_r + F_r))$	$_{y}$ * $X_{cg}$ )*b)/(ac-b <sup>2</sup> )				
$X_{cg}(m)$	57.91	c (kN-m)	12175733.665	γ (radian)	-0.001399758				
				$\gamma = (F_v * b - (M_r + F_v * X_{cs}) * a)/(b^2 - ac)$					

Line No	1	ordinates o e Fig 1 & Fi	,	Bollard Co See	ordinates a e Fig 1 & Fi	,	$I_{1} = \sqrt{\{(X_{ch} - X_{bl})^{2} + (Y_{ch} - Y_{bl})^{2}\}}$ See Fig 2	$\Delta Z_i = Z_{ch} - Z_{bl}$ See Fig 1	Cross Sectional Area of one rope (mm²)	No. of rope parts	Cross Sectional Area of mooring line (mm²)	Minimum breaking Strength of one rope (MT)	Minimum breaking Strength of Mooring Line (MT)	Young's modulus of rope (GPa)	$\cos \theta_i = (Y_{bl} - Y_{ch})/I_1$ See Fig 2	$\phi_i = \tan^{-1}(\Delta Z_i/I_1)$ See Fig 1	$\cos {f \varphi}_i$	Line Length from Bitt to Chock (m) See Fig 2	$L_i = I_0 + I_1/\cos \phi_i$ (m)	$k_i = a_i * E_i/L_i$ $(kN/m)$	$k_{yi} = k_i *$ $cos\theta_i * cos\phi_i$ $(kN/m)$	k <sub>yi</sub> * X <sub>ch</sub> (kN)	k <sub>yi</sub> * X <sub>ch</sub> <sup>2</sup> (kN-m)	$F_{yi} = k_{yi} * (\delta_y + X_{ch} * \gamma)$ (MT)	$T_i = F_{yi}/(\cos\theta_i * \cos\phi_i)$ (MT)	FS <sub>i</sub> (Factor of Safety) = MBS/T <sub>i</sub>
	X <sub>ch</sub>	Y <sub>ch</sub>	Z <sub>ch</sub>	X <sub>bl</sub>	$Y_{bl}$	Z <sub>bl</sub>	l <sub>1</sub>	$\Delta Z_{i}$	а	n	a <sub>i</sub> = n x a	MBS <sub>rope</sub>	MBS = MBS <sub>rope</sub> x n	E <sub>i</sub>	cos θ <sub>i</sub>	фі	cos φ <sub>i</sub>	Io	L <sub>i</sub>	k <sub>i</sub>	k <sub>yi</sub>	k <sub>yi</sub> * X <sub>ch</sub>	k <sub>yi</sub> * X <sub>ch</sub> <sup>2</sup>	F <sub>yi</sub>	T <sub>i</sub>	FS <sub>i</sub>
1	0	0	6.4	-7.32	8.23	2.74	11.01	3.66	1291	3	3873	33.3	99.9	1.378	0.748	18.388	0.94894	3.66	15.262	349.682	248.042	0.000	0.000	6.737	9.498	10.518
2	4.88	1.52	5.79	0	8.23	2.74	8.3	3.05	1291	3	3873	33.3	99.9	1.378	0.808	20.177	0.93863	2.44	11.283	473.027	358.943	1751.642	8548.012	9.499	12.519	7.980
3	11.58	2.74	5.49	21.95	8.23	2.74	11.73	2.75	1291	3	3873	33.3	99.9	1.378	0.468	13.194	0.97360	2.44	14.488	368.372	167.858	1943.798	22509.185	4.282	9.397	10.631
4	21.34	4.88	4.72	7.32	8.23	2.74	14.41	1.98	1291	3	3873	33.3	99.9	1.378	0.232	7.824	0.99069	2.44	16.985	314.211	72.367	1544.311	32955.599	1.745	7.578	13.183
5	96.93	6.1	2.9	102.41	8.23	2.74	5.88	0.16	1291	3	3873	33.3	99.9	1.378	0.362	1.559	0.99963	3.05	8.932	597.502	216.362	20971.968	2032812.860	2.884	7.965	12.542
6	106.68	5.33	3.05	95.1	8.23	2.74	11.94	0.31	1291	3	3873	33.3	99.9	1.378	0.243	1.487	0.99966	2.44	14.384	371.036	90.087	9610.515	1025249.783	1.076	4.430	22.551
7	110.95	4.88	3.2	117.04	8.23	2.74	6.95	0.46	1291	3	3873	33.3	99.9	1.378	0.482	3.787	0.99782	2.44	9.405	567.451	272.922	30280.742	3359648.291	3.092	6.429	15.538
8	118.87	3.05	3.2	124.36	8.23	2.74	7.55	0.46	1291	3	3873	33.3	99.9	1.378	0.686	3.487	0.99815	3.35	10.914	489.004	334.881	39807.348	4731899.415	3.416	4.988	20.028
9	80.47	6.1	2.9	87.78	8.23	2.74	7.61	0.16	1291	3	3873	33.3	99.9	1.378	0.280	1.204	0.99978	2.44	10.052	530.955	148.579	11956.139	962110.519	2.330	8.325	12.000
10																										
11																										
12																										
13																										
14																										
15																										
16																										
	·																				a = 1178.54	b = 66102.98	c = 6481723.73			





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