ICSolar Model

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1 Steady Model

Consider the model of air and water interaction consisting of an initial inlet region (denoted by 0) and a pair of regions, an open region with pipe followed by a module, denoted by (1,2) satisfying

$$W_1: \quad \dot{m}_w C_{p,w}(T_{w,1} - T_{w,0}) - h_{wa}(T_{a,1} - T_{w,1}) = 0$$
(1)

$$A_1: \quad \dot{m}_a C_{p,a} (T_{a,1} - T_{a,0}) - h_{wa} (T_{w,1} - T_{a,1}) - h_e (T_e - T_{a,1}) - h_i (T_i - T_{a,1}) = 0$$
 (2)

$$W_2: \quad \dot{m}_w C_{p,w} (T_{w,2} - T_{w,1}) - Q_w = 0 \tag{3}$$

$$A_2: \quad \dot{m}_a C_{p,a} (T_{a,2} - T_{a,1}) - Q_a = 0 \tag{4}$$

Where i and e are interior and exterior contributions. Each pair of these forms a 'module'. In this work, we use

$$C_{p,w} = 4.218kJ/(kgK) \tag{5}$$

$$\dot{m}_w = 0.0008483kg/s \tag{6}$$

$$C_{p,a} = 1.005kJ/(kgK) \tag{7}$$

$$\dot{m}_a = 0.384kg/s \tag{8}$$

$$h_{wa} = 4.823 \times 10^{-5} kW/(Km) \tag{9}$$

$$h_i = 1.572 \times 10^{-4} kW/(Km) \tag{10}$$

$$h_e = 4.837 \times 10^{-4} kW/(Km) \tag{11}$$

(12)

With Initial and Boundary Conditions of $T_{a,0} = 20C$, $T_i = 25.0C$, $T_e = 22.5C$. At this point, we set $Q_a = 0$ as the surrounding air acts like a reservoir and its effect is currently minimal. Our inputs are $T_{w,0}$ and Q_w from experimental data. We take experimental data from the file nov25_2.csv located in the github repository.

1.1 Feb 11 data

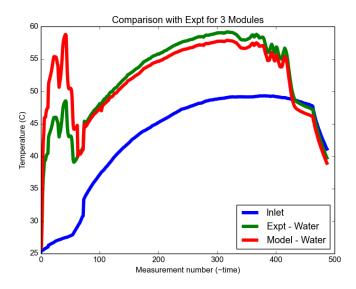


Figure 1: Comparison between experiment and model for 3 modules, water temperature in last module compared.

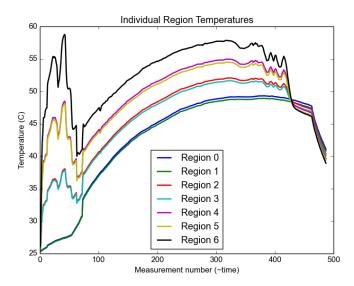


Figure 2: Model results for 3 module case, using experimental inputs. Regions 2,4,6 correspond to modules.

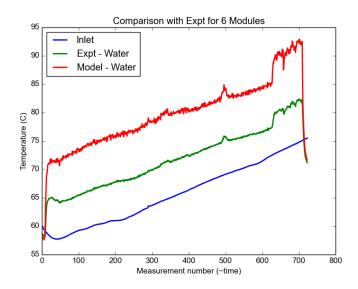


Figure 3: Comparison between experiment and model for 6 modules, water temperature in last module compared for Feb 11th data. Each module has its own Q_w from the data.

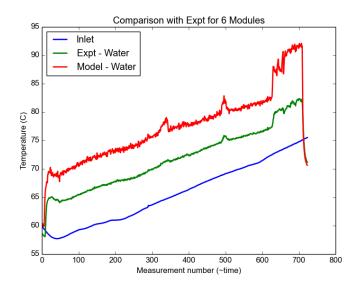


Figure 4: Same Comparison, in this case, regions 1-2, 3-4, etc are merged into one, as if the module is part of the general volume.

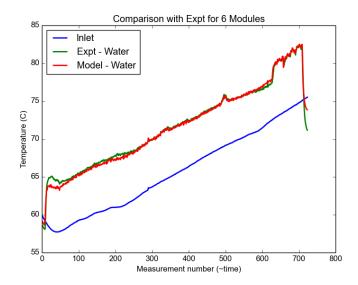


Figure 5: Same Comparison. In the model, the water flow rate is 2.4 times the number initially used. This gets closer to the experimental data.

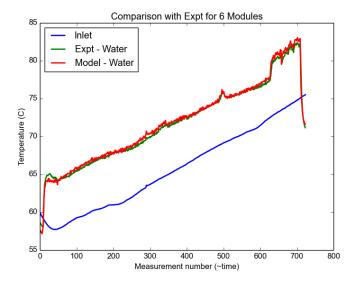


Figure 6: Same Comparison. In the model, the heat generated, Q_w in each module is 55% of the experimental number, suggesting better agreement if there is a loss of energy.

2 Unsteady Model

Consider the steady model in 4 and introduce the time derivative, $mC_p \frac{\partial T}{\partial t}$ and rearrange to get

$$W_1: m_{w,1}C_{p,w}\frac{\partial T}{\partial t} + \dot{m}_wC_{p,w}(T_{w,1} - T_{w,0}) - h_{wa}(T_{a,1} - T_{w,1}) = 0 (13)$$

$$W_2: m_{w,2}C_{p,w}\frac{\partial T}{\partial t} + \dot{m}_wC_{p,w}(T_{w,2} - T_{w,1}) - Q_w(t) = 0 (14)$$

$$A_1: \qquad m_{a,1}C_{p,a}\frac{\partial T}{\partial t} + \dot{m}_aC_{p,a}(T_{a,1} - T_{a,0}) - h_{wa}(T_{w,1} - T_{a,1}) - h_e(T_e - T_{a,1}) - h_i(T_i - T_{a,1}) \neq 15$$

$$A_2: m_{a,2}C_{p,a}\frac{\partial T}{\partial t} + \dot{m}_aC_{p,a}(T_{a,2} - T_{a,1}) - Q_a = 0 (16)$$

To handle the mass term, we need the volume. We have a length of the first tube as $L_1 = 0.15m$ and $L_{3,5,...} = 0.3m$. The cross sectional area of the tube is based on inner diameter, d = 0.003m and outer diameter of d = 0.0142m. The volume of the surrounding air we are interested in has a cross section of $0.4m \times 0.4m$. Using the density and the specific heat, we get that $m_a = 0.0576kg$, $m_w = 2.12 \times 10^{-3}kg$.

For regions with modules, we can create a small volume, $m_{a,2,4,6,...} \approx Cm_a$ and $m_{w,2,4,6,...}Cm_w$. In these results, C = 1/6.

2.1 Feb 11 data

Using the Feb 11 data, given discrete data, we can determine $Q_w(t)$ for all times by quadratic interpolation. For the initial solution, we can set every

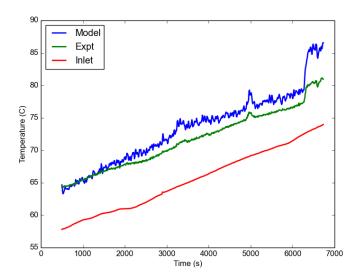


Figure 7: Same Comparison. In the model, the heat generated, Q_w in each module is 65% of the experimental number. Initially they start out in agreement, and then diverge as time goes on. Quadratic interpolation of the data (inlet temp, heat generated).