

Modelling hydrogels at both ends of the temperature spectrum

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with Grae Worster (University of Cambridge) and Tom Montenegro-Johnson (University of Warwick)

ETH Zurich Department of Materials, 27th May 2025

LEVERHULME
TRUST



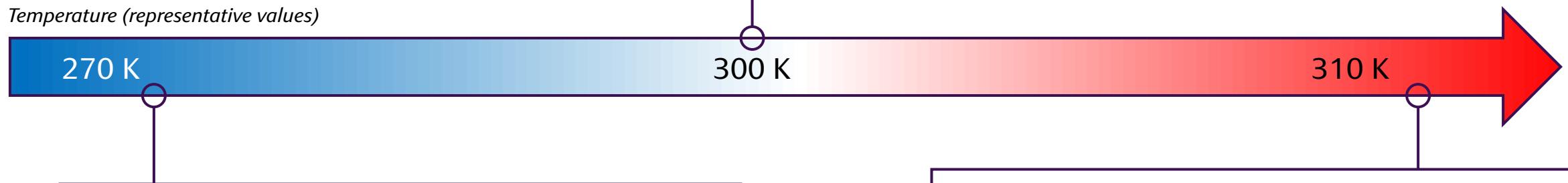
Overview

1. Thinking about gels like a mathematician

Osmosis · elastic stresses · equilibrium swelling · transport of water · shape change in swelling/drying · behaviour at interfaces · characterising a gel

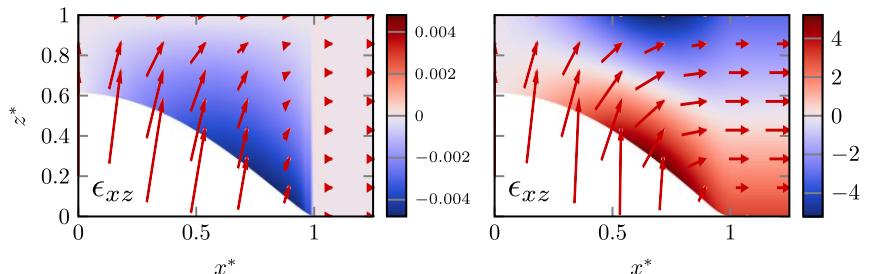


Temperature (representative values)



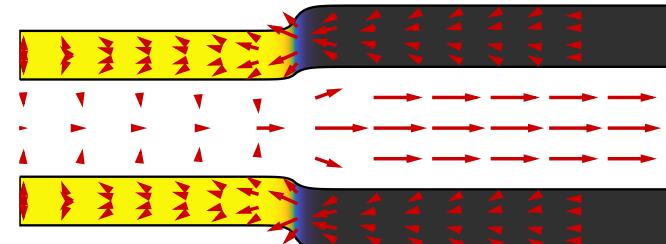
2. Freezing hydrogels at low(-ish) temperatures

Formation of pure ice · cryosuction · applying our model to GelFrO · a 2D model · stress buildup



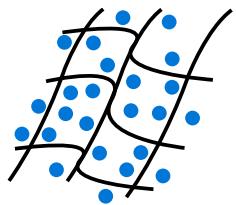
3. Building with thermo-responsive gels

Heating effects on swelling · heat transfer in gels · building pumps with collapsing tubes



What, another gel model?

Usual approach: an energy density function with contributions from everything that could affect behaviour.



$$\mathcal{W} = \frac{k_B T}{2\Omega_p} [\text{tr} (\mathbf{F}_d \mathbf{F}_d^\top) - 3 + 2 \log \phi] + \frac{k_B T}{\Omega_f} \left[\frac{1-\phi}{\phi} \log(1-\phi) + \chi(\phi, T)(1-\phi) \right]$$

Gaussian-chain elasticitypolymer volume fraction
Mixing of polymer and water

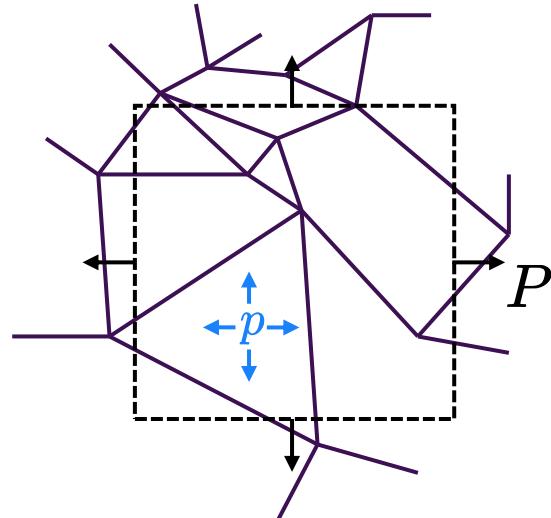


- Messy and very specific for certain gels – lots of parameters
- Not ‘macroscopic’ enough in nature – elasticity ignores water
- Measured relative to a dry state: is this ever physically realisable?
- Transient states are harder to describe than equilibria

What, another gel model?

A geophysicist's approach: separate contributions from stress into a 'pore pressure' and an 'effective stress'

$$\boldsymbol{\sigma} = -p\mathbf{I} + \boldsymbol{\sigma}_{\text{eff}}$$



Bulk pressure (or thermodynamic pressure) the isotropic stress exerted by a sample of gel; our familiar concept of pressure



Pervadic pressure (or Darcy pressure, "pore" pressure) is the pressure as would be measured by a transducer separated by a partially-permeable membrane from the gel.

$$P = p + \Pi$$

osmotic effects?
isotropic elasticity?
generalised osmotic pressure

In soil science: p is the pore pressure, P is the overburden pressure

In colloids: p is [related to] the chemical potential, Π is the osmotic pressure

$$\mathbf{u} = -\frac{k}{\mu_l} \nabla p$$

permeability
relative fluid flux
(dynamic) viscosity of fluid



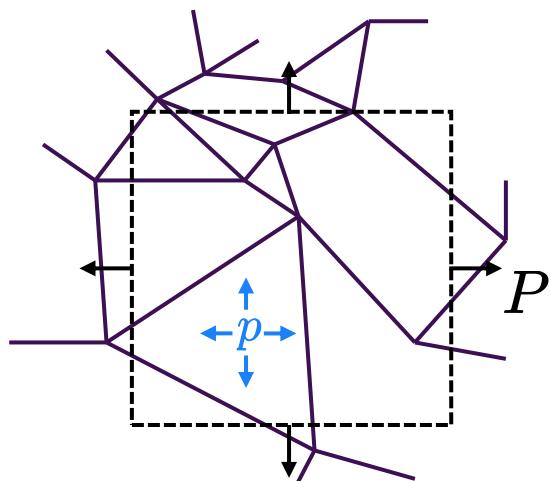
What, another gel model?

$$\boldsymbol{\sigma} = -p\mathbf{I} + \boldsymbol{\sigma}_{\text{eff}}$$
$$P = p + \Pi$$

Linear (Biot) poroelasticity specifies a linear-elastic constitutive relation linking strains to effective stresses.

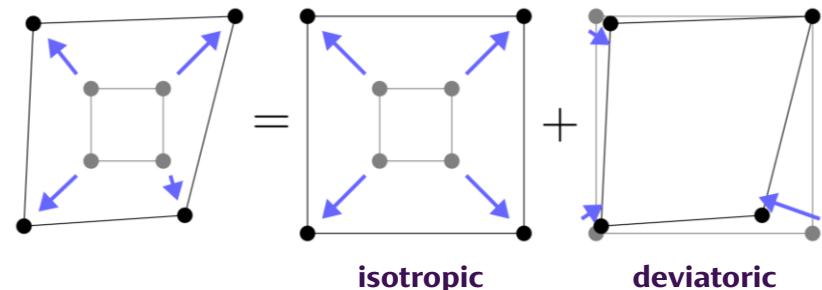


Hydrogels swell a lot, with potentially large strains: linear is no good!



One way around this: use **finite strain (nonlinear) elastic models** for effective stress.

e.g. Hencky model $\boldsymbol{\sigma}_{\text{eff}} = \frac{\Lambda\phi}{2} \text{tr}(\ln(\mathbf{F}\mathbf{F}^T))\mathbf{I} + \frac{M-\Lambda}{2} \ln(\mathbf{F}\mathbf{F}^T)$



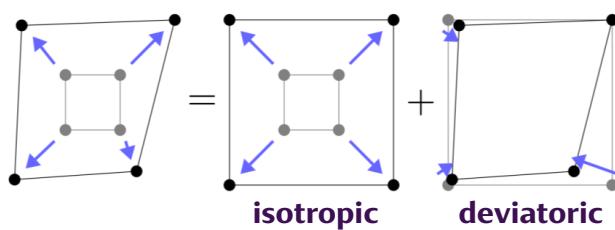
isotropic

deviatoric

Linear-elastic-nonlinear-swelling (LENS)

$$\boldsymbol{\sigma} = -p\mathbf{I} + \boldsymbol{\sigma}_{\text{eff}}$$

$$P = p + \Pi$$



Key idea: assume linearity only in the **deviatoric strain** from some **fully-swollen reference state** $\phi \equiv \phi_0$

Therefore, the deviatoric part of $\boldsymbol{\sigma}_{\text{eff}}$ must depend linearly on the deviatoric part of the Cauchy strain (the isotropic part could be huge)

$$\mathbf{e} = \frac{1}{2} [(\nabla \xi) + (\nabla \xi)^T] = \left[1 - \left(\frac{\phi}{\phi_0} \right)^{1/3} \right] \mathbf{I} + \boldsymbol{\epsilon}$$

isotropic strain
 depends only on degree to
 which gel is swollen

deviatoric strain
 assumed small

$$\boldsymbol{\sigma}_{\text{eff}} = -\Pi(\phi)\mathbf{I} + 2\mu_s(\phi)\boldsymbol{\epsilon}$$

isotropic part must be (-) osmotic pressure
 since the isotropic part of the total stress tensor is (-) the bulk pressure

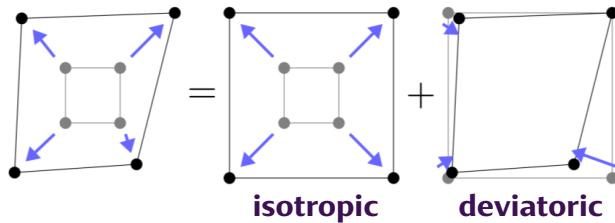
shear modulus depends on swelling!
 dry gels will probably be stiffer

depends on swelling alone
 isotropic strains lead to isotropic stresses –
 see the isotropic part of strain tensor
 physically intuitive result

Linear-elastic-nonlinear-swelling (LENS)

$$\boldsymbol{\sigma} = -p\mathbf{I} + \boldsymbol{\sigma}_{\text{eff}}$$

$$P = p + \Pi$$



$$\mathbf{e} = \frac{1}{2}[(\nabla \xi) + (\nabla \xi)^T] = \left[1 - \left(\frac{\phi}{\phi_0}\right)^{1/3}\right]\mathbf{I} + \boldsymbol{\epsilon}$$

$$\boldsymbol{\sigma}_{\text{eff}} = -\Pi(\phi)\mathbf{I} + 2\mu_s(\phi)\boldsymbol{\epsilon}$$

$$\mathbf{u} = (1 - \phi)(\mathbf{u}_w - \mathbf{u}_p)$$

$$\mathbf{q} = (1 - \phi)\mathbf{u}_w + \phi\mathbf{u}_p$$

- Have an expression for stress in the gel, so conservation of momentum links pressure gradients to deviatoric strains,

$$\nabla \cdot \boldsymbol{\sigma} = 0 \quad \text{so} \quad \underbrace{\nabla p}_{\substack{\text{pervadic pressure gradients} \\ \text{oppose osmotic ones}}} = -\nabla \Pi(\phi) + 2\nabla \cdot [\mu_s(\phi)\boldsymbol{\epsilon}]$$

- Since gradients in pervadic pressure drive flows, this allows us to describe gel reconfiguration (when coupled with conservation of polymer and water)

$$\frac{\partial \phi}{\partial t} + \mathbf{q} \cdot \nabla \phi = \nabla \cdot (\phi \mathbf{u}) \quad \text{alongside} \quad \mathbf{u} = -\frac{k(\phi)}{\mu_l} \nabla p$$

↑ depends on swelling
↑ phase-averaged (gel and water) flux

$$\boxed{\frac{\partial \phi}{\partial t} + \mathbf{q} \cdot \nabla \phi = \nabla \cdot \left\{ \frac{k(\phi)}{\mu_l} \left[\phi \frac{\partial \Pi}{\partial \phi} + \frac{4\mu_s(\phi)}{3} \left(\frac{\phi}{\phi_0} \right)^{1/3} \right] \nabla \phi \right\}}$$

Characterising a gel

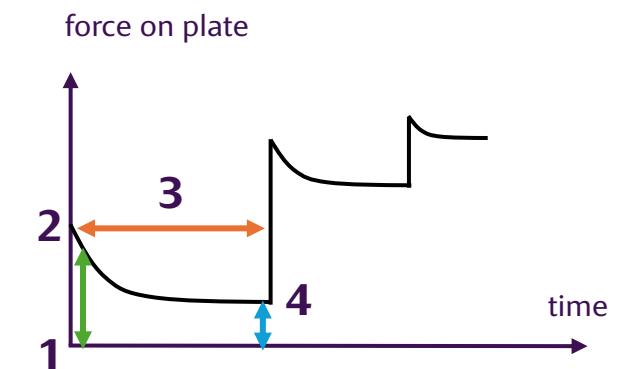
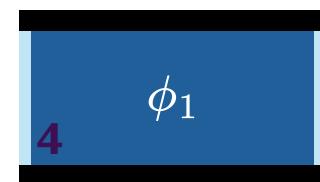
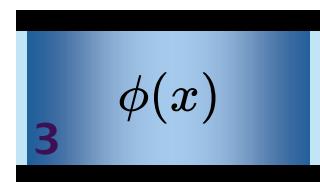
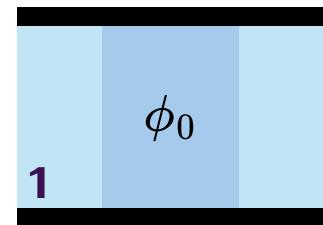
$$\frac{\partial \phi}{\partial t} + \mathbf{q} \cdot \nabla \phi = \nabla \cdot \left\{ \frac{k(\phi)}{\mu_l} \left[\phi \frac{\partial \Pi}{\partial \phi} + \frac{4\mu_s(\phi)}{3} \left(\frac{\phi}{\phi_0} \right)^{1/3} \right] \nabla \phi \right\}$$

$$\boldsymbol{\sigma} = -[p + \Pi(\phi)]\mathbf{I} + 2\mu_s(\phi)\boldsymbol{\epsilon} \quad \mathbf{u} = \frac{k(\phi)}{\mu_l} \left[\frac{\partial \Pi}{\partial \phi} + \frac{4\mu_s(\phi)}{3\phi} \left(\frac{\phi}{\phi_0} \right)^{1/3} \right] \nabla \phi$$

Shear modulus characterises the stiffness of a hydrogel and describes the initial elastic response before water diffuses through the structure

Osmotic pressure characterises the affinity for water ('desire' to swell or deswell)

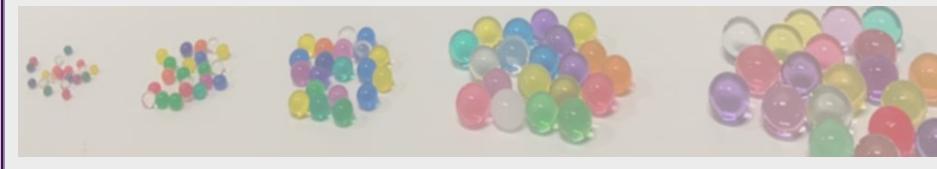
Permeability describes the resistance to viscous flow through the pore scaffold



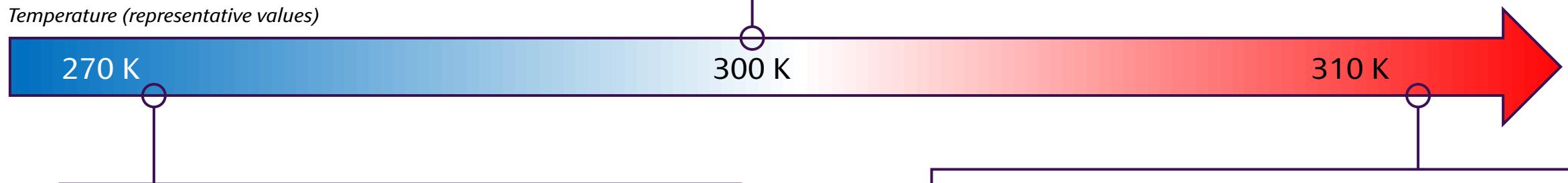
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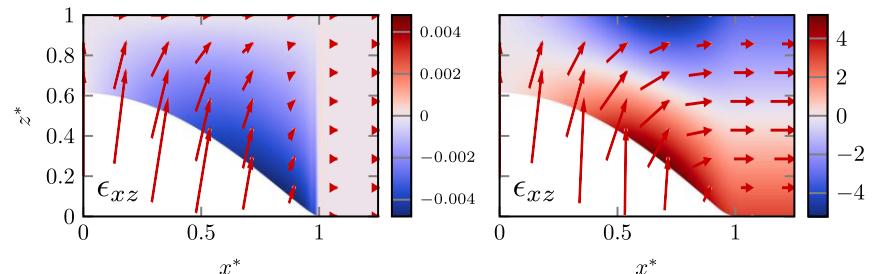


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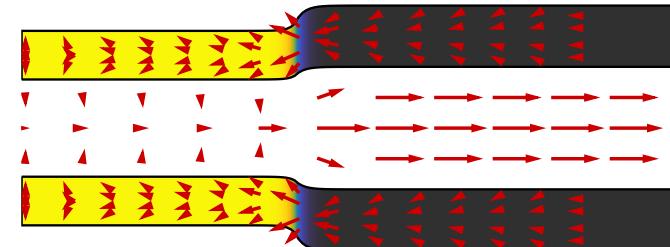
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How do gels freeze

What brings me here
analogous materials



Insight: Potholes

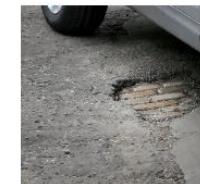
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What's new
What's hot

Insight: Roads and paths set to work named

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How to fix potholes
How to fix potholes

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Fake legs used as a pointer for pothole



The false legs make it look like someone is taking a deep dive into the large water-filled pothole

SOPHIE MONTAGUE/BBC
Helen Burchell
BBC News, Cambridgeshire

26 February 2025

A man fed up with the state of a road near his village has poked fun at a large pothole, by putting a pair of fake legs in the huge puddle it has created.

It is one of several that have formed on Wolverhampton Road in the Cambridgeshire

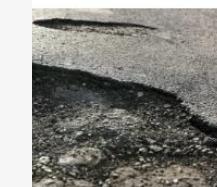
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May



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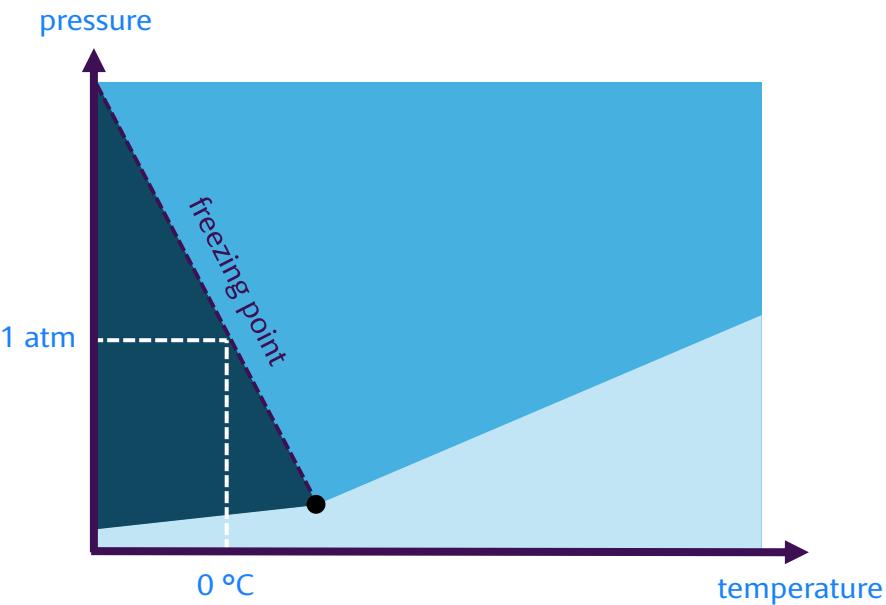
try until ice no longer

o-scale effects.

rmal expansion of ice
s, displaces the

about fluid flows?

Why don't gels freeze?



Pressure is raised inside the pore spaces owing to capillarity, so the *ice-entry temperature* is modified by the Gibbs-Thompson relation



(neither actually derived this...)

$$T_{IE} = T_m \left[1 - \frac{\gamma \kappa}{\rho_{ice} L} \right]$$

equilibrium freezing temperature (~ 273 K)

surface tension and average pore curvature
specific latent heat of fusion

This depresses the freezing point of water inside the pores. At a boundary, water will still want to freeze into ice.

At the boundary, the temperature is given by the Clausius-Clapeyron relation:

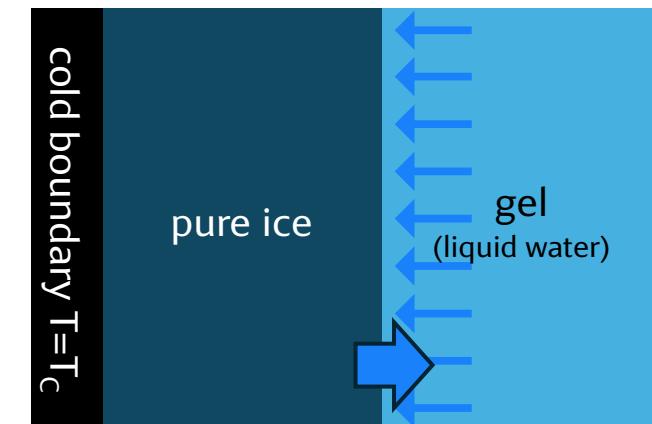


$$\beta_{water} \frac{T_L - T_m}{T_m} = \frac{p_{gel} - p_{atm}}{\rho_{ice} n \cdot \sigma \cdot n}$$

equals (-) bulk pressure

$$= -\Pi(\phi) \rho_{water}$$

assume no overburden stress $n \cdot \sigma \cdot n = -p_{atm}$



Putting ice in our gel model

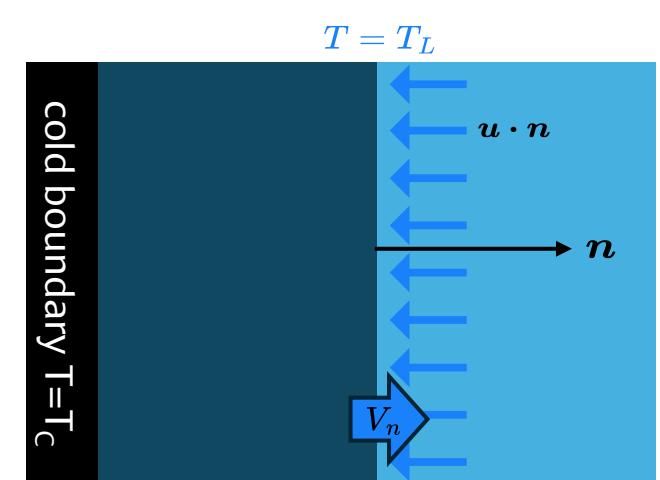
$$T_L = T_m \left[1 - \frac{\Pi(\phi)}{\rho_{\text{water}} \mathcal{L}} \right]$$

As a boundary condition on polymer fraction this sets the value of the osmotic pressure, and hence the amount of deswelling, given a liquidus temperature on the interface

As a boundary condition on temperature this sets a lower freezing point at the interface when the gel is drier

This alone doesn't quite close the model:

- Mass is conserved $\rho_{\text{ice}} V_n = -\rho_{\text{water}} \mathbf{u} \cdot \mathbf{n}$
- Stefan condition (energy is conserved) $\rho_{\text{ice}} \mathcal{L} V_n = -[\mathcal{K}(\mathbf{n} \cdot \nabla T)]_{\text{ice}}^{\text{gel}}$



Gel-freezing osmometry

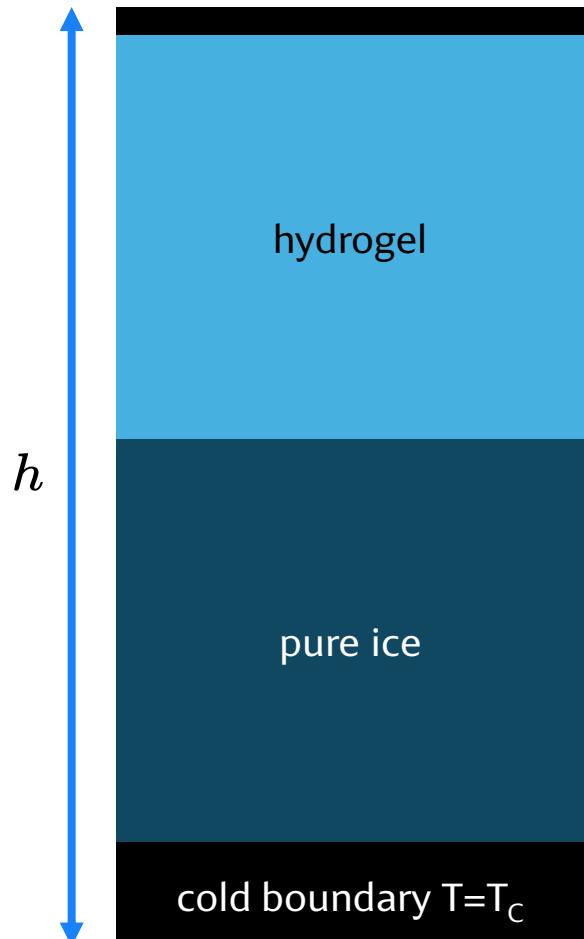
$$T_L = T_m \left[1 - \frac{\Pi(\phi)}{\rho_{\text{water}} \mathcal{L}} \right] \quad \rho_{\text{ice}} \mathcal{L} V_n = -[\mathcal{K}(\mathbf{n} \cdot \nabla T)]_{\text{ice}}^{\text{gel}} \quad \rho_{\text{ice}} V_n = -\rho_{\text{water}} \mathbf{u} \cdot \mathbf{n}$$

Consider the 1D problem with an insulated lid and a cold boundary, initially with no ice and a fully-swollen gel

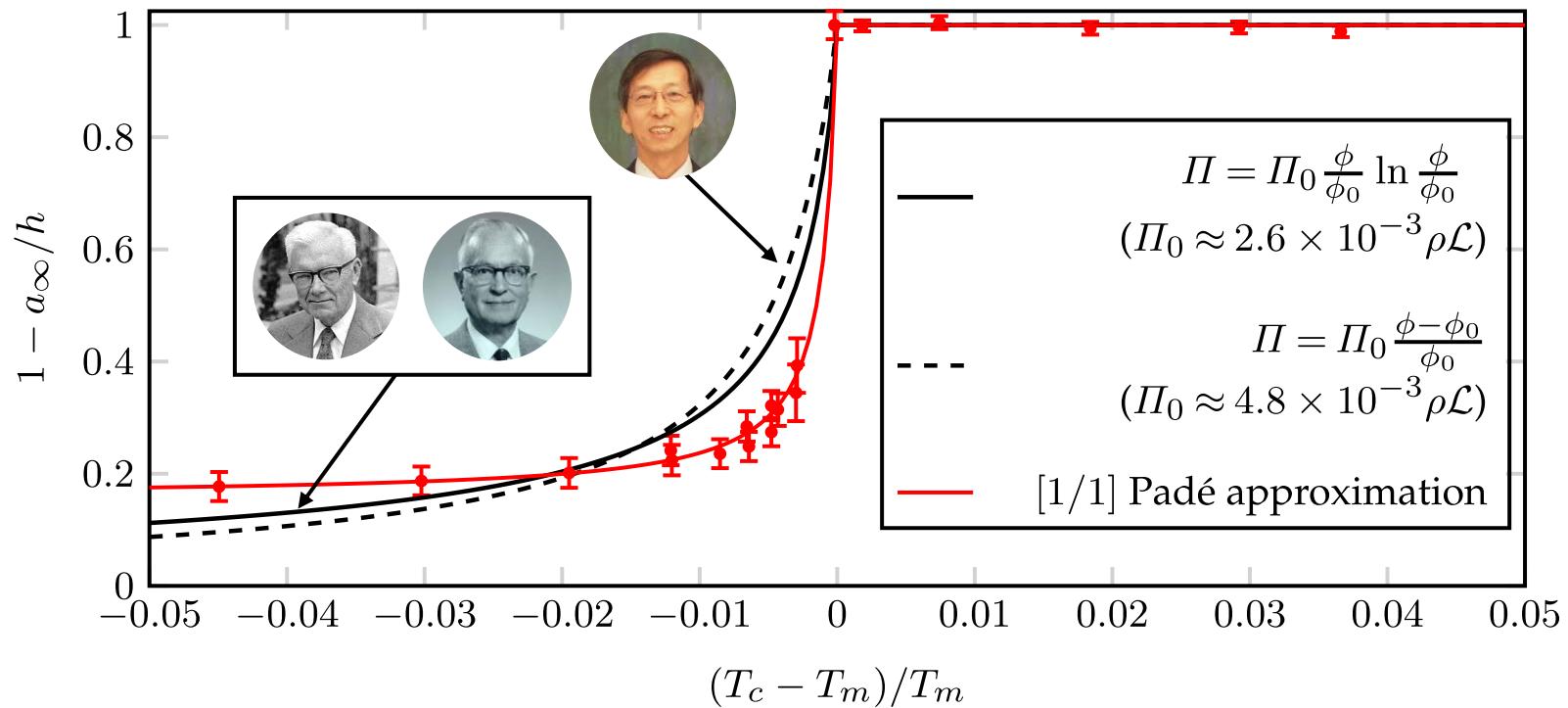
Eventually a steady state is reached. No heat fluxes, no more growth of ice, thus no fluid fluxes

- **No heat fluxes:** $T \equiv T_C = T_L$
- **No fluid fluxes:** $\phi \equiv \phi_C$ with $\phi_C(h - a_\infty) = \phi_0 h$

$$\Pi \left(\frac{\phi_0 h}{h - a_\infty} \right) = \rho_{\text{water}} \mathcal{L} (T_m - T_C)$$



Gel-freezing osmometry

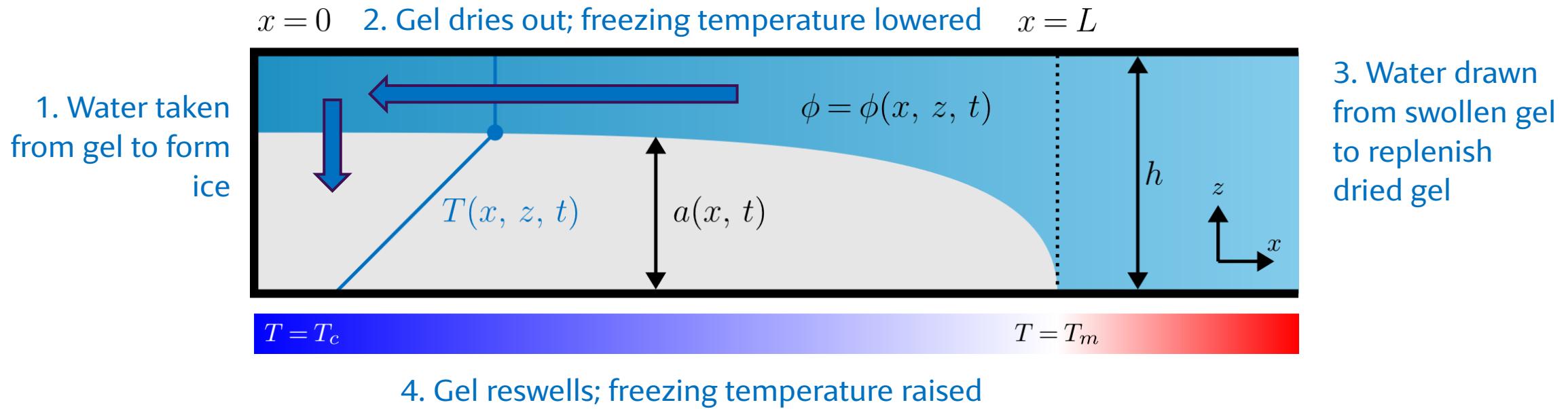


$$\Pi \left(\frac{\phi_0 h}{h - a_\infty} \right) = \rho_{\text{water}} \mathcal{L} (T_m - T_C)$$
$$\Pi(\phi) = \frac{10^{-3} \rho \mathcal{L}}{\phi_0} \frac{\phi - \phi_0}{1 - \phi/(6.6\phi_0)}$$

$= \rho$

Modelling the (transient) freezing process

So far, we have **only considered the final steady state** in freezing experiments; LENS brings us no real advantages here. To see its real use, we consider a more complicated physical setup.



- Ice grows vertically from the base but **to differing extents**
- Water drawn vertically downwards from the gel **and also horizontally** to replenish partially-dried gel

Building a mathematical model

Temperature field

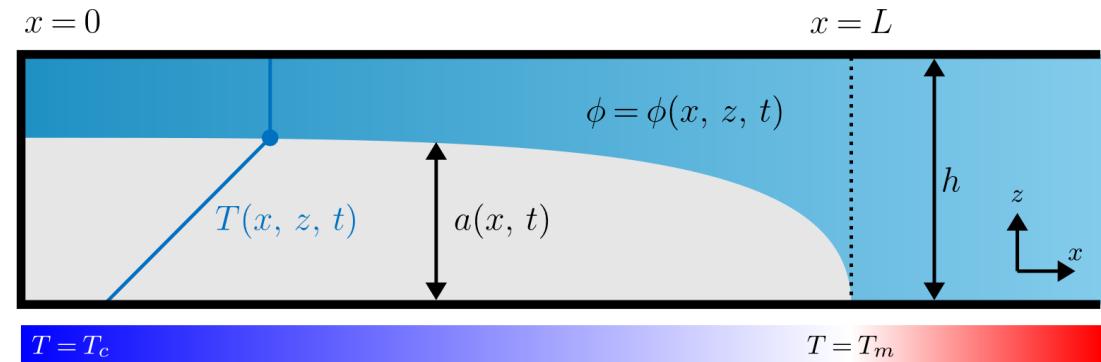
$$\frac{\partial T}{\partial t} = \kappa_{\text{ice}} \nabla^2 T \quad \text{and} \quad \frac{\partial T}{\partial t} = \kappa_{\text{gel}} \nabla^2 T$$

Gel composition

$$\frac{\partial \phi}{\partial t} + \mathbf{q} \cdot \nabla \phi + \nabla \cdot \left[\frac{\phi k(\phi)}{\mu_l} \nabla p \right] = 0 \quad \text{with} \quad \nabla p + \nabla \Pi = 2 \nabla \cdot [\mu_s(\phi) \boldsymbol{\epsilon}]$$

Ice growth

$$\rho \mathcal{L} \frac{da}{dt} = - \left[\mathcal{K} \left(\frac{\partial T}{\partial z} - \frac{\partial a}{\partial x} \frac{\partial T}{\partial x} \right) \right]_{\text{ice}}^{\text{gel}} \quad T|_{z=a(x,t)} = T_m \left[1 - \frac{\Pi(\phi)}{\rho \mathcal{L}} \right]$$



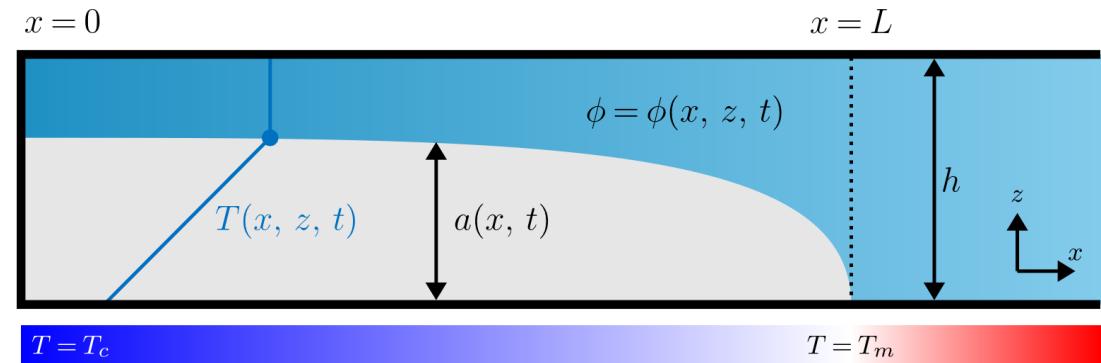
$$T = T_m - \frac{1}{2}(T_m - T_C) \left(1 + \cos \frac{\pi x}{L}\right) \quad T = T_m \quad (x \geq L)$$

- Assume the channel is slender so $\varepsilon = h/L \ll 1$
 - Take the limit of a **large Lewis number**; heat diffuses much faster than water through polymer

Building a mathematical model

Temperature field

- Linear in the ice
- Constant (equal to liquidus) in the gel
- Set by degree of deswelling



$$T = T_m - \frac{1}{2}(T_m - T_C) \left(1 + \cos \frac{\pi x}{L}\right) \quad T = T_m \quad (x \geq L)$$

Gel composition

Neumann boundary conditions on walls. Polymer fraction set by liquidus temperature on ice-gel boundary.

$$\frac{\partial \phi}{\partial t} + \left(\frac{\phi}{\phi_0}\right)^{-1/2} \frac{\partial \xi}{\partial t} \frac{\partial \phi}{\partial x} + \left(\frac{\phi}{\phi_0}\right)^{-1/2} \frac{\partial \eta}{\partial t} \frac{\partial \phi}{\partial z} = \frac{k(\phi)}{\mu_l} \frac{\partial}{\partial \phi} \left[\Pi(\phi) + 2\mu_s(\phi) \left(\frac{\phi}{\phi_0}\right)^{1/2} \right] \frac{\partial^2 \phi}{\partial z^2}$$

$\xi = (\xi, \eta)$

Ice growth

$$\frac{d}{dt}(a^2) = \frac{\kappa}{\rho \mathcal{L}} \left[(T_m - T_C) \left(1 + \cos \frac{\pi x}{L}\right) - \frac{2\Pi(\phi)}{\rho \mathcal{L}} \right]$$

undercooling

thermal conductivity

osmotic depression

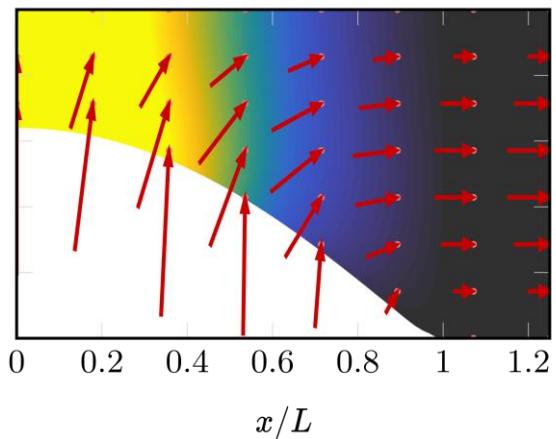
energy stored by making new ice

Where does the gel go?

No-slip boundary conditions

$$\xi = -\frac{1}{2\mu_s} \frac{\partial P}{\partial x} (h - z)(z - a)$$

$$\eta = 2 \int_z^h \left[(\phi/\phi_0)^{1/2} - 1 \right] dz' + \frac{(h-z)^2}{12\mu_s} \left[\frac{\partial^2 P}{\partial x^2} (h+2z-3a) - 3 \frac{\partial P}{\partial x} \frac{\partial a}{\partial x} \right]$$

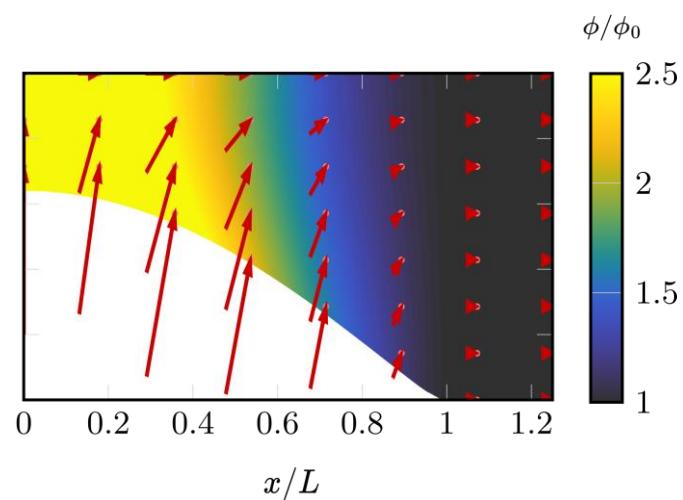


- Parabolic horizontal displacement profile
- Requires stiff gel *and* little drying or else deviatoric strains are large

Free-slip boundary conditions

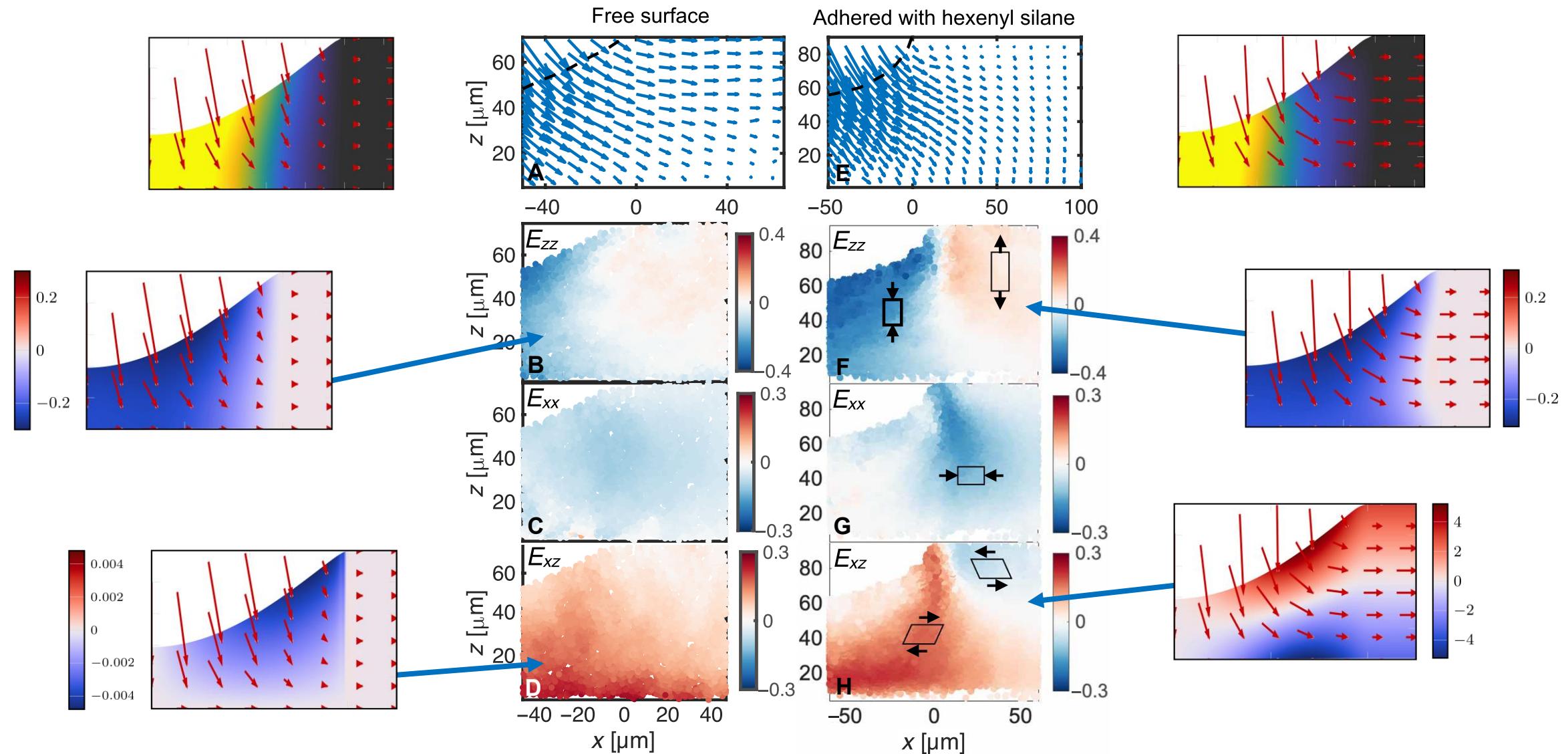
$$\xi = \int_0^x \left\{ \frac{a}{h-a} - \frac{2}{h-a} \int_a^h \left[(\phi/\phi_0)^{1/2} - 1 \right] dz' \right\} dx'$$

$$\eta = 2 \int_z^h \left[(\phi/\phi_0)^{1/2} - 1 \right] dz' + \frac{h-z}{h-a} \left\{ a - 2 \int_a^h \left[(\phi/\phi_0)^{1/2} - 1 \right] dz' \right\}$$

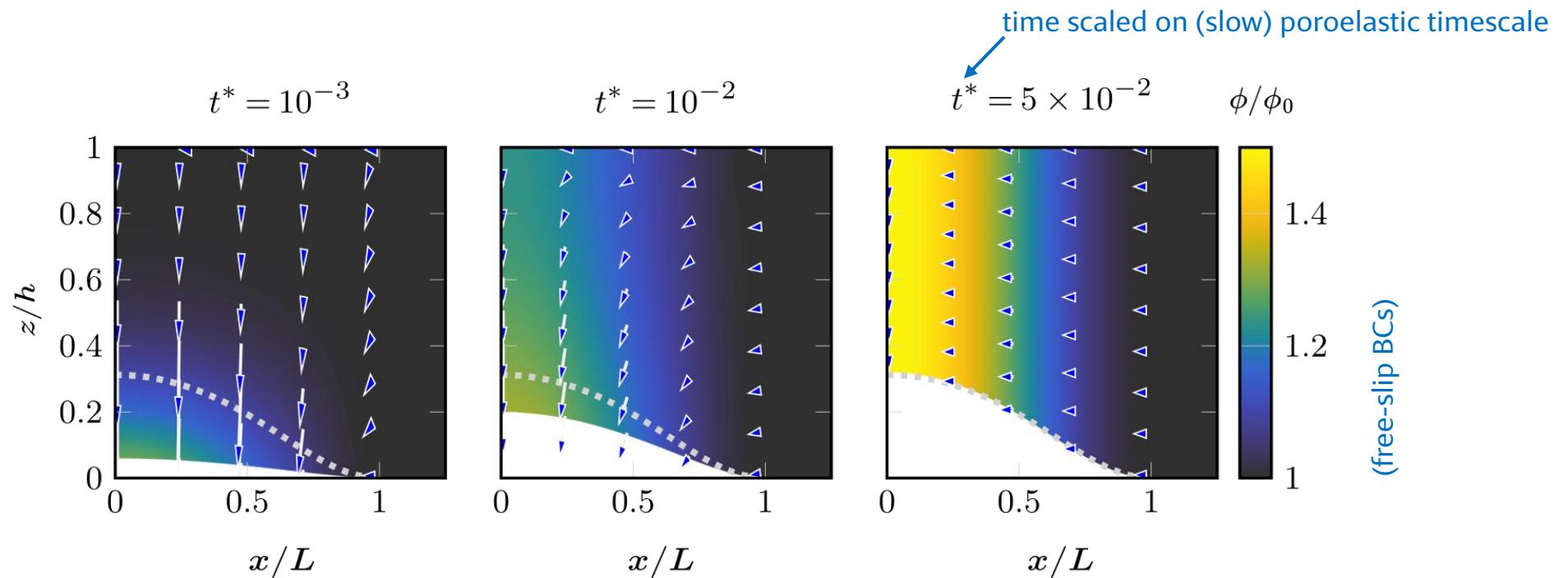


- ‘Stretched-plug’ horizontal displacement
- Requires little drying or else deviatoric strains are large, but gel can be stiff

Stress buildup in hydrogels



Where does the water go?



- Initially, the gel remains swollen and all water flows are vertically downwards: $a \approx \sqrt{\frac{\kappa}{\rho C}(T_m - T_C)} \left(1 + \cos \frac{\pi x}{L}\right) t$
- Eventually, osmotic effects begin to play a role and water is drawn from more swollen regions into drier parts of the gel
- Finally, a steady state is reached where there is no further growth of ice

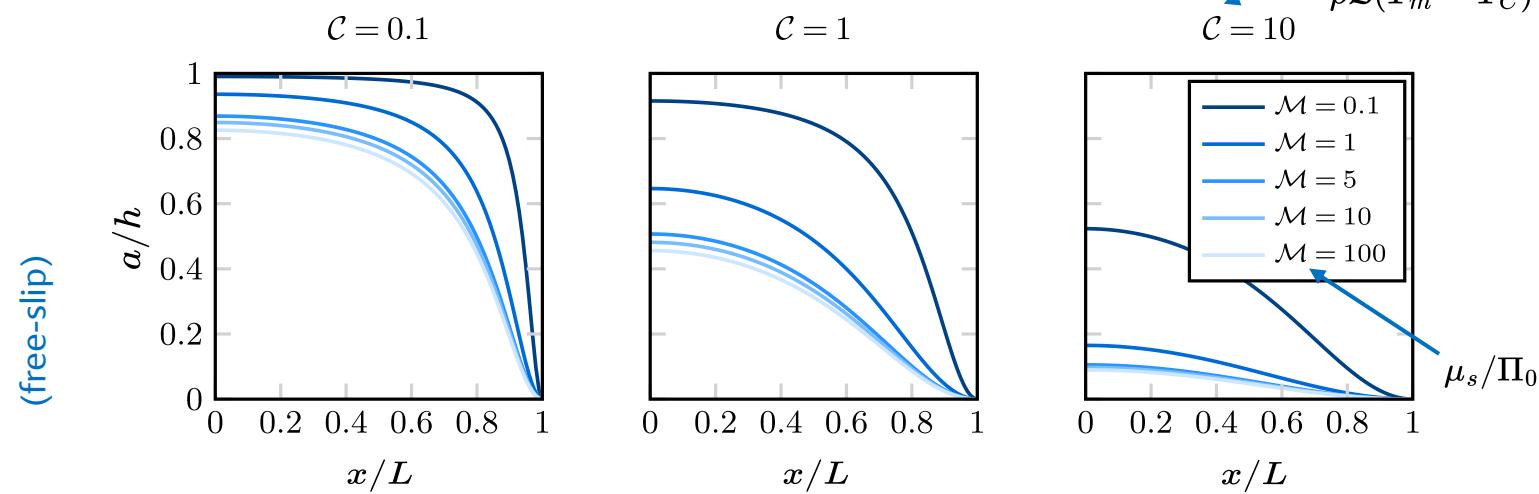
When does it all stop?

- As in the unidirectional case, freezing stops when there are no heat fluxes from the ice

$$\rho\mathcal{L}\frac{da}{dt} = - \left[\kappa \left(\frac{\partial T}{\partial z} - \frac{\partial a}{\partial x} \frac{\partial T}{\partial x} \right) \right]_{\text{ice}}^{\text{gel}} \quad \begin{array}{l} \text{gel sits on liquidus} \\ \text{slenderness approximation} \end{array}$$

- This gives $\phi = \phi_\infty(x)$ with $\Pi(\phi_\infty) = \frac{\rho\mathcal{L}}{2} \left(1 - \frac{T_C}{T_m}\right) \left(1 + \cos \frac{\pi x}{L}\right)$
- Need deviatoric stresses to balance these osmotic pressures *exactly* or else there is flow

Linear osmotic pressure $\Pi = \Pi_0(\phi - \phi_0)/\phi_0$



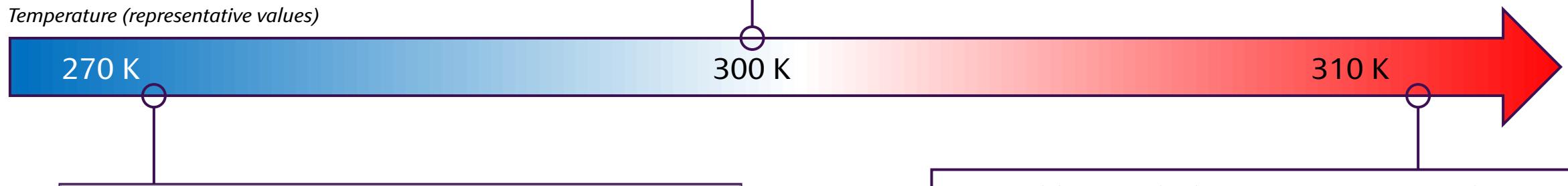
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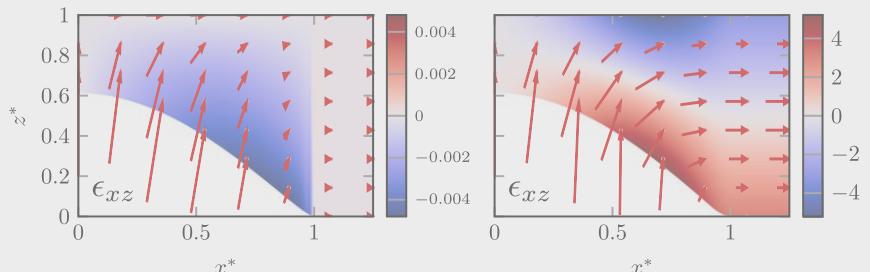


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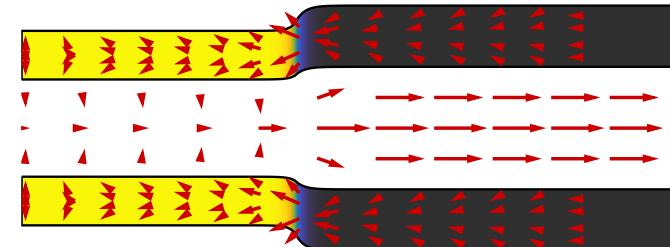
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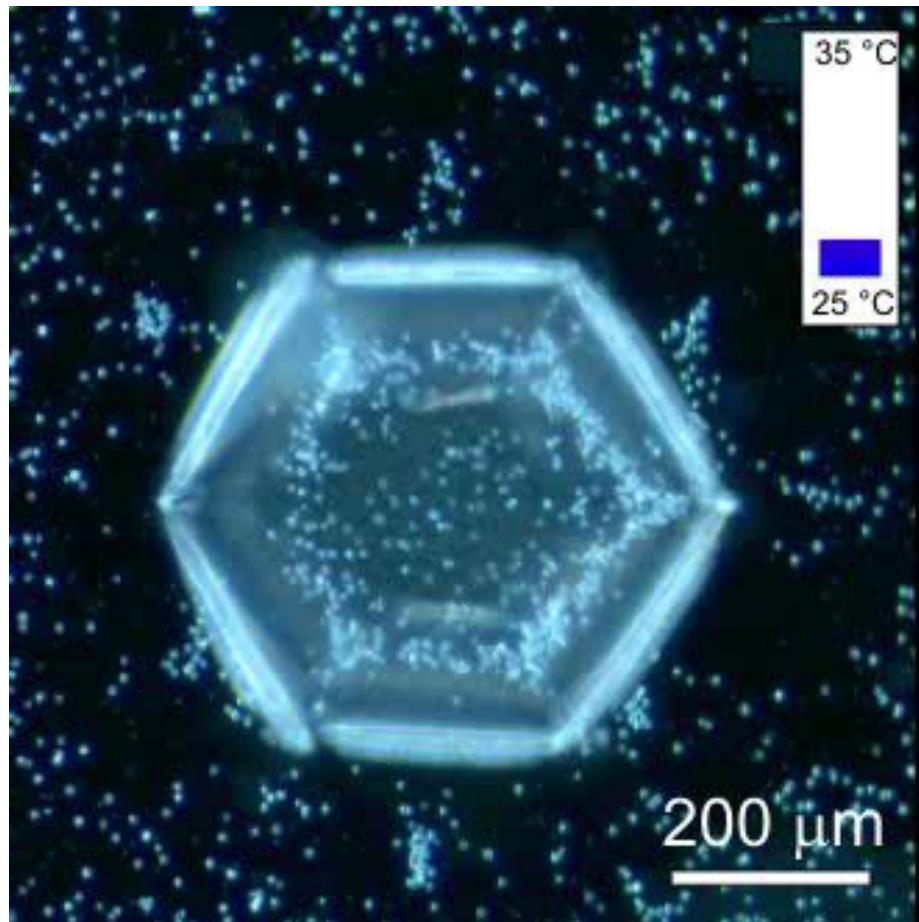
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Thermo-responsive hydrogels

Some gels, like many based on poly(N-isopropylacrylamide) (pNIPAM) undergo a transition at a critical temperature called the **Lower Critical Solution Temperature (LCST)**



Qualitatively, it appears that there is a new equilibrium (dry) polymer state above the LCST, with transition between the two states slow, mediated by diffusion of water

$$\phi_0 = \begin{cases} \phi_{00} & T \leq T_C \\ \phi_{0\infty} & T > T_C \end{cases}$$

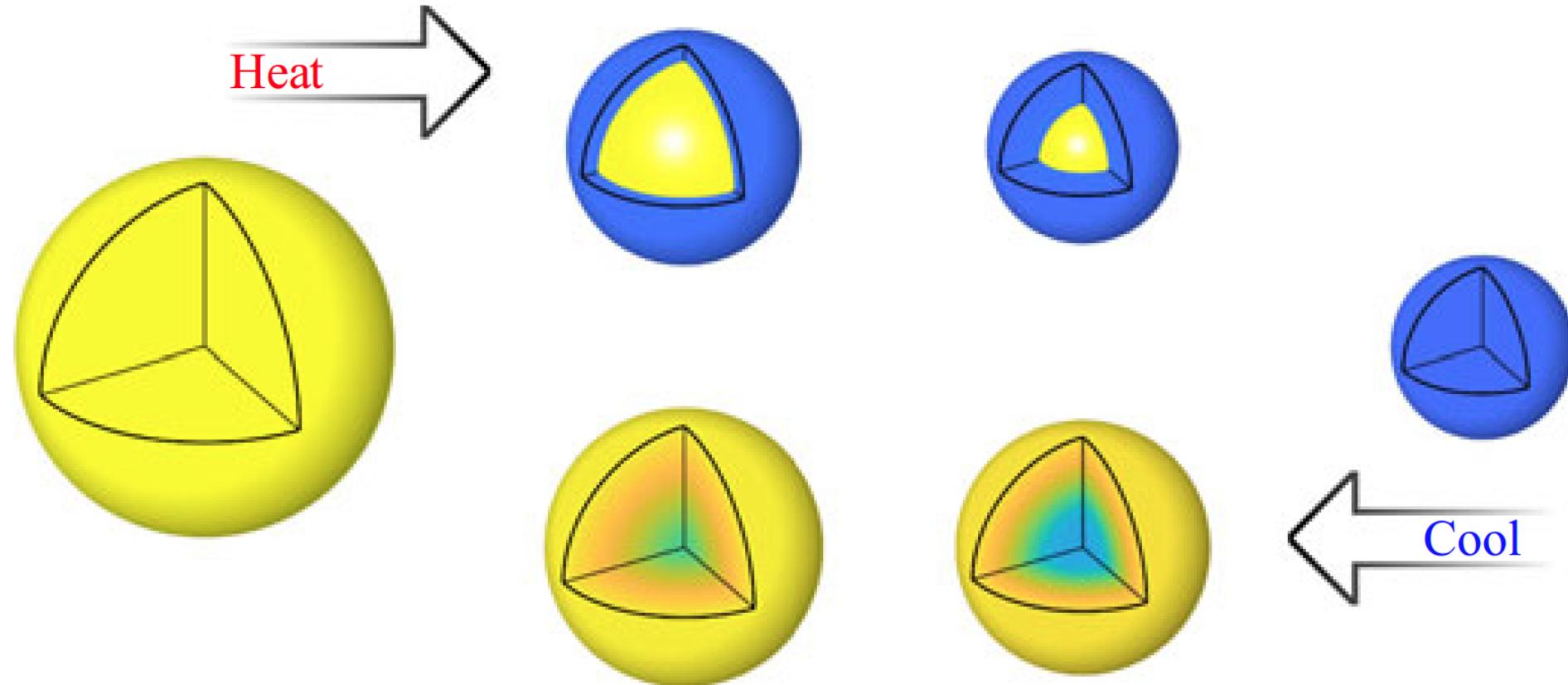
$$\mathcal{W} = \frac{k_B T}{2\Omega_p} [\text{tr}(\mathbf{F}_d \mathbf{F}_d^T) - 3 + 2 \log \phi] + \frac{k_B T}{\Omega_f} \left[\frac{1-\phi}{\phi} \log(1-\phi) + \chi(\phi, T)(1-\phi) \right]$$

Solving the implicit relation $\frac{\partial \mathcal{W}}{\partial \phi} \Big|_{\phi=\phi_0} = 0$ gives the equilibrium polymer fraction as a function of temperature if we know the interaction parameter's value



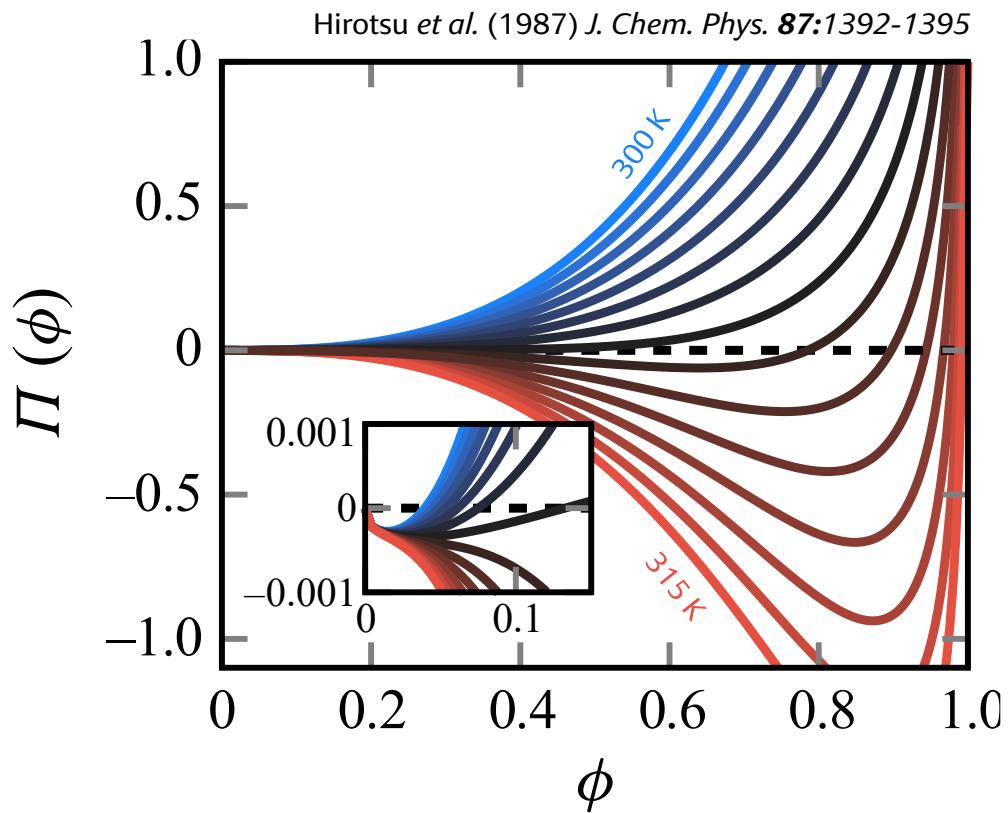
Thermo-responsive hydrogels

Take a simple functional form $\chi(\phi, T) = A_0 + A_1 T + (B_0 + B_1 T)\phi + \mathcal{O}(T^2, \phi^2)$



...we're skipping out some significant and important behaviour here, however.

Thermo-responsive hydrogels



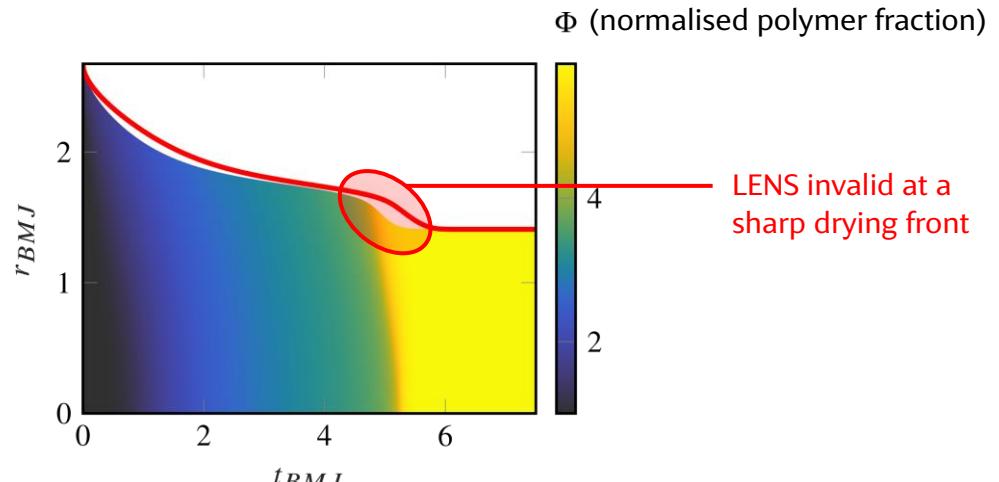
motivating our choice $\phi_0 = \begin{cases} \phi_{00} & T \leq T_C \\ \phi_{0\infty} & T > T_C \end{cases}$

If the same parameter set is used to generate a generalised osmotic pressure (in the LENS formalism), we see the same rapid switch in equilibrium values as the temperature increases

Phenomenologically, it suffices to take

$$\Pi(\phi) = \Pi_0 \frac{\phi - \phi_0(T)}{\phi_0(T)}$$

Big question: Does this work?



Heat transfer in thermo-responsive gels

How about cases where heat is evolving in a gel, close to the LCST? How is heat transferred and how can deswelling or reswelling feed back into this?

Internal energy can change via:

- ### **1. External supply of heat easy to neglect in most cases**

- ## 2. Heat generation due to viscous flows

As gels swell or deswell and water is driven through the scaffold, frictional effects can generate heat. **Positive feedback**

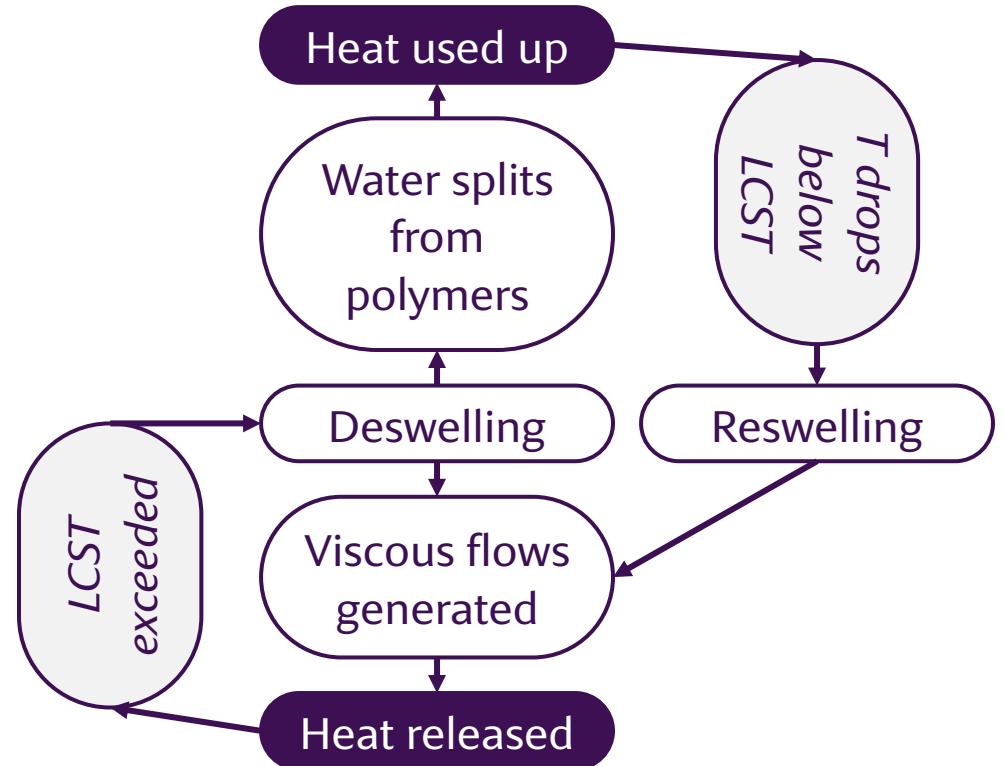
- ### 3. Heat transfer by advection

Both in the solid and liquid phases

- ## 4. Heat transfer by diffusion

- ## 5. Energy used in swelling or drying

Breaking water molecules away from polymer chains uses energy, and vice versa. **Negative feedback**



Heat transfer in thermo-responsive gels

1. External supply of heat
2. Heat generation due to viscous flows
3. Heat transfer by advection
4. Heat transfer by diffusion
5. Energy used in swelling or drying

Full derivation in JJW & Montenegro-Johnson (2025)

$$\frac{\partial T}{\partial t} + \mathbf{q} \cdot \nabla T = \frac{R}{\rho c} + \kappa \nabla^2 T + \frac{k(\phi)}{\rho c \mu_l} |\nabla p|^2 + \frac{1}{\phi} \left(\frac{\Pi(\phi)}{\rho c} + T \right) \frac{d\phi}{dt}$$

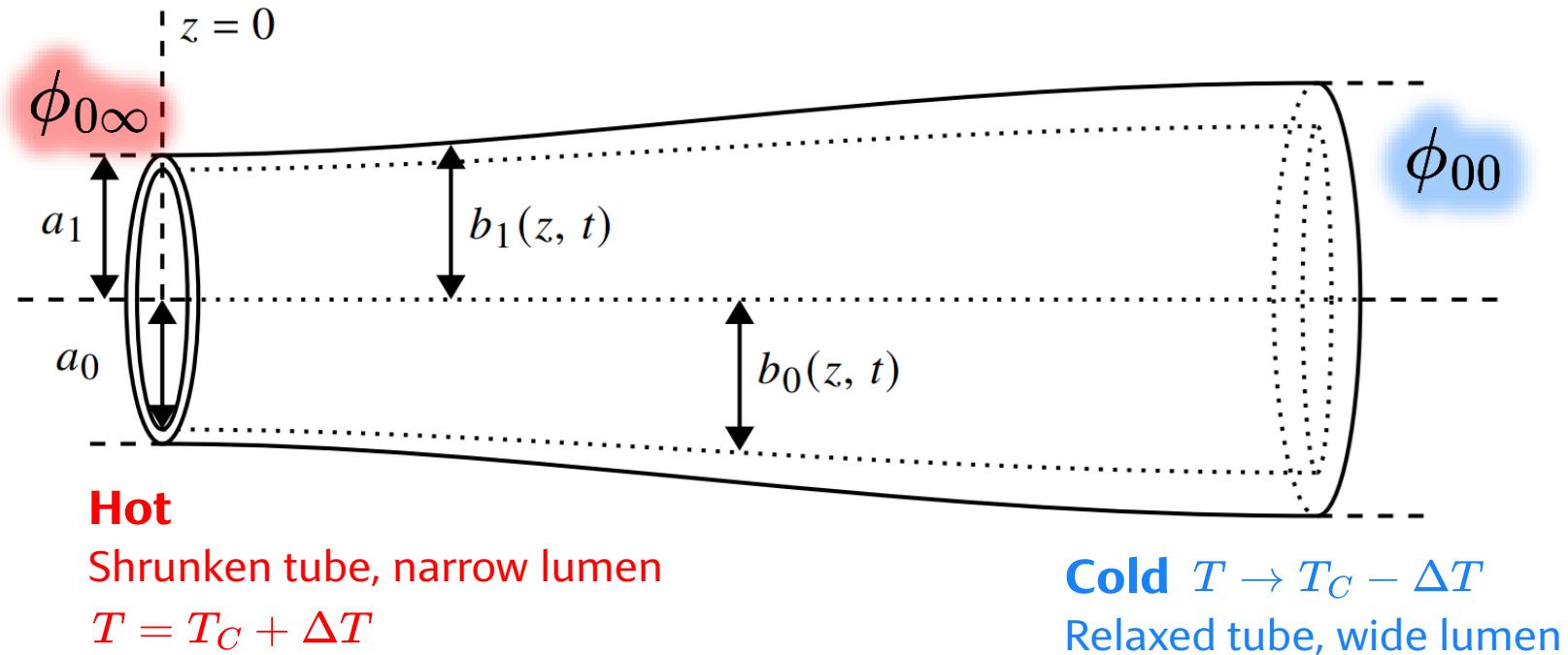
Annotations:

- External heating: R (red arrow)
- Thermal diffusivity: κ (red arrow)
- Permeability: $k(\phi)$ (orange box)
- Density: ρ (red arrow)
- Specific heat capacity: c (red arrow)
- Fluid viscosity: μ_l (red arrow)

Usually, however, reconfiguration is ‘slow’ on the timescale of heat transfer by diffusion (Lewis number – thermal diffusivity over compositional diffusivity – is large), and so we can approximate

$$\frac{\partial T}{\partial t} \approx \kappa \nabla^2 T$$

Tubes of responsive gel



1. How does a heat pulse travel (symmetrically) outwards in time?
2. What happens to the shape of the tube as the pulse passes?
3. Where does the water go? How much is driven out radially, squeezed through the lumen, or transported along the gel?

Heat transfer problem

- is easy (if we ‘spherical cow’ the problem a little...)

The thermal diffusivity of pNIPAM gels is close to that of water, so we can treat the heat transfer problem as occurring in a single infinite domain with only variation in the z direction

$$\kappa_{\text{gel}} \approx 1.8 \times 10^{-7} \text{ m}^2\text{s}^{-1}$$

Tél et al. (2014) *Int. J. Therm. Sci.* 85:47-53

$$\kappa_{\text{water}} \approx 1.43 \times 10^{-7} \text{ m}^2\text{s}$$

at 1 atm and 298 K

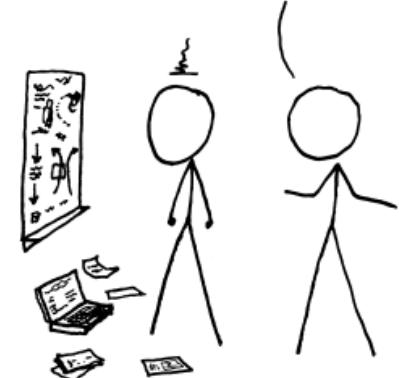
$$T - T_C = \Delta T \left[2 \operatorname{erfc} \left(\frac{z}{2\sqrt{\kappa t}} \right) - 1 \right]$$

so there is a ‘front’ at $Z_C = 2 \operatorname{erfc}^{-1} \left(\frac{1}{2} \right) \sqrt{\kappa t}$ behind which the gel is deswollen

YOU'RE TRYING TO PREDICT THE BEHAVIOR OF <COMPLICATED SYSTEM>? JUST MODEL IT AS A <SIMPLE OBJECT>, AND THEN ADD SOME SECONDARY TERMS TO ACCOUNT FOR <COMPLICATIONS I JUST THOUGHT OF>.

EASY, RIGHT?

SO, WHY DOES <YOUR FIELD> NEED A WHOLE JOURNAL, ANYWAY?



LIBERAL-ARTS MAJORS MAY BE ANNOYING SOMETIMES, BUT THERE'S NOTH'NG MORE OBNOXIOUS THAN A PHYSICIST FIRST ENCOUNTERING A NEW SUBJECT.

Deformation of the tube

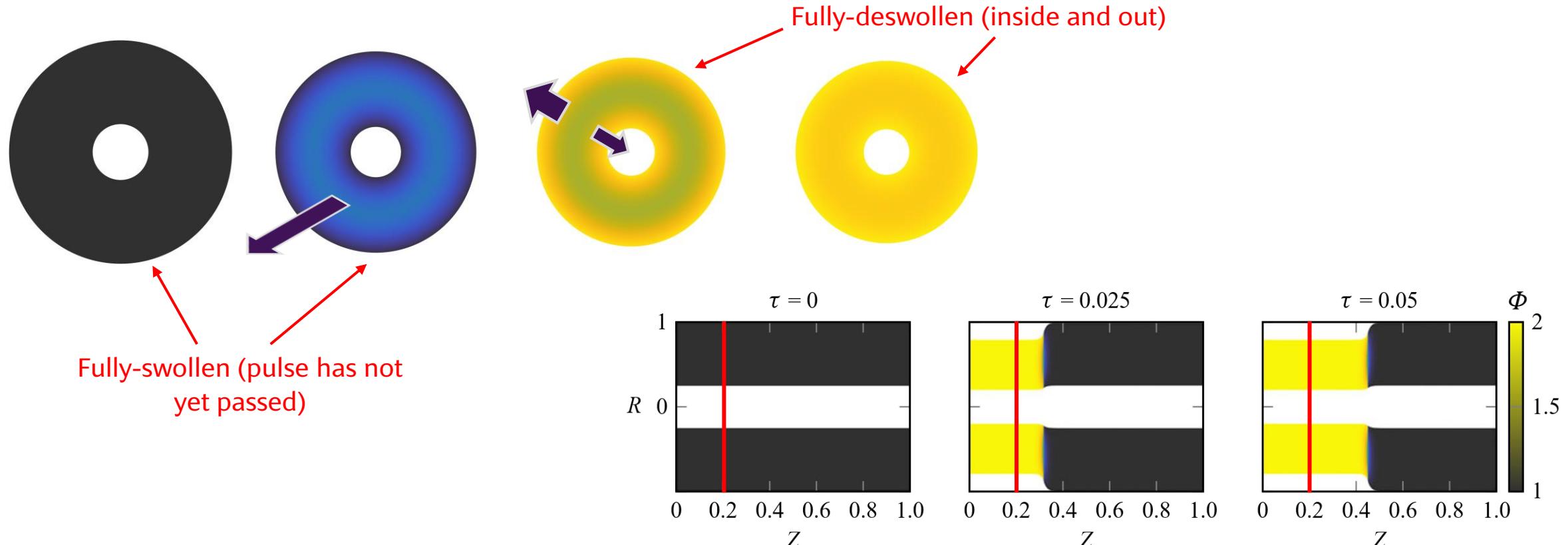
2. Shape change: is a bit harder

$$\frac{\partial \phi}{\partial t} + \mathbf{q} \cdot \nabla \phi = \frac{1}{r} \frac{\partial}{\partial r} \left[r D(\phi, T) \frac{\partial \phi}{\partial r} \right] + \frac{\partial}{\partial z} \left[D(\phi, T) \frac{\partial \phi}{\partial z} \right] \quad \text{with}$$
$$D(\phi, T) = \frac{k}{\mu_l} \left[\frac{\Pi_0(T)\phi}{\phi_0(T)} + \frac{4\mu_s}{3} \left(\frac{\phi}{\phi_{00}} \right)^{1/3} \right].$$

$\phi = \phi_0(T)$ on boundaries

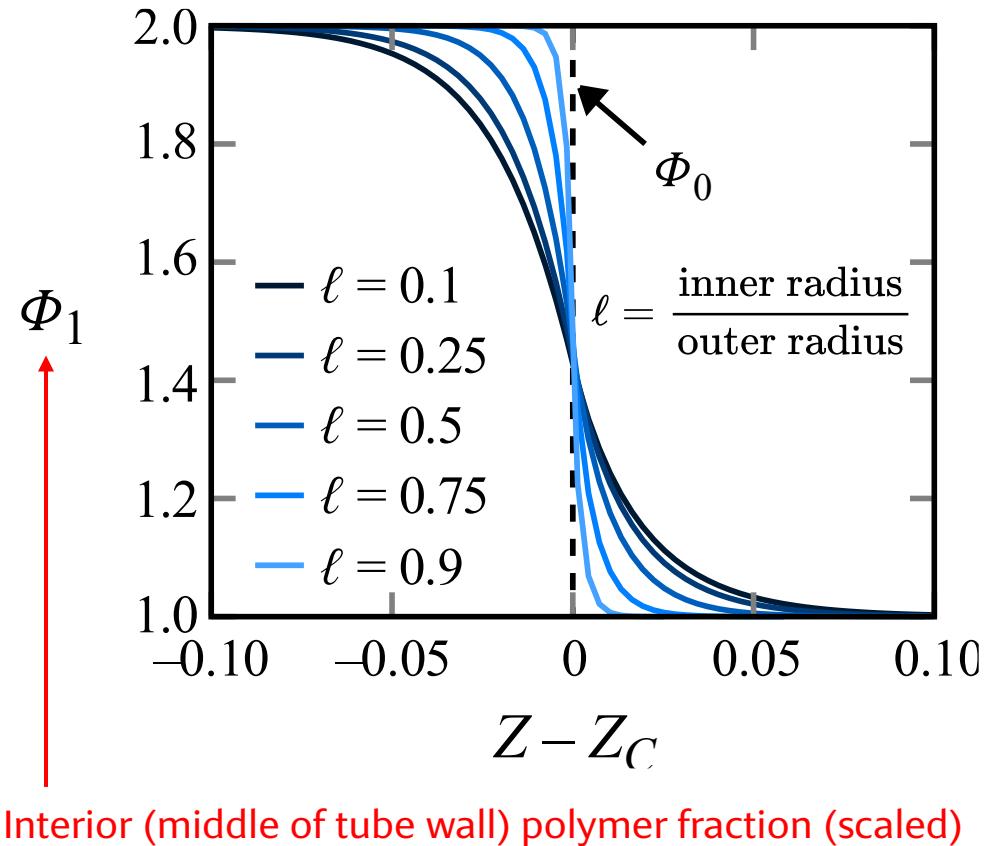
slenderness assumption:
aspect ratio small
 $\phi = \phi_1(z, t) + \varepsilon^2 \phi_2(r; z, t)$
then separate variables

To attack this problem, we assume that the tube is long and thin. Balance stresses on its interface with water to find that the gel deswells to its equilibrium value on these surfaces



Deformation of the tube

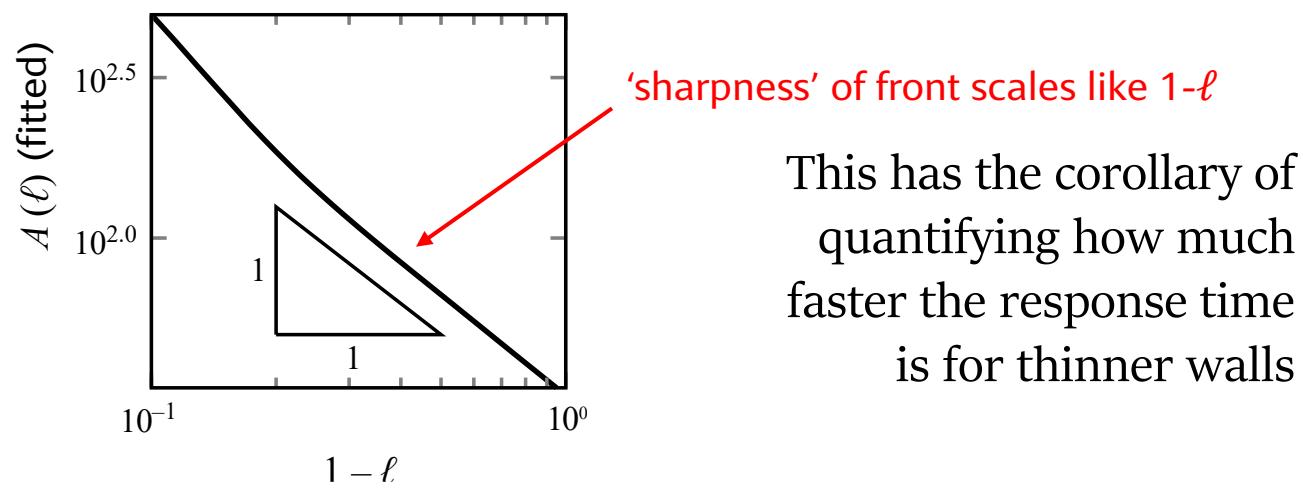
The inside and the outside instantaneously deswell, but the interior takes some time – it's slower for a thicker tube. This leads to ‘smoother’ profiles for thick tubes.



The ‘smoothed step’ profile suggests that we can nicely approximate the tube with a hyperbolic tangent,

$$\Phi_1 \approx \Phi_\infty - \frac{\Phi_\infty - 1}{2} \{1 + \tanh [A(\ell)(Z - Z_C)]\}$$

Dry polymer fraction (scaled)

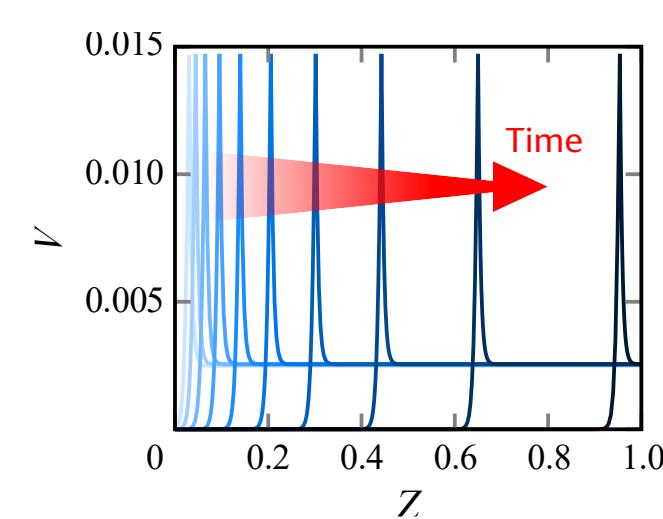
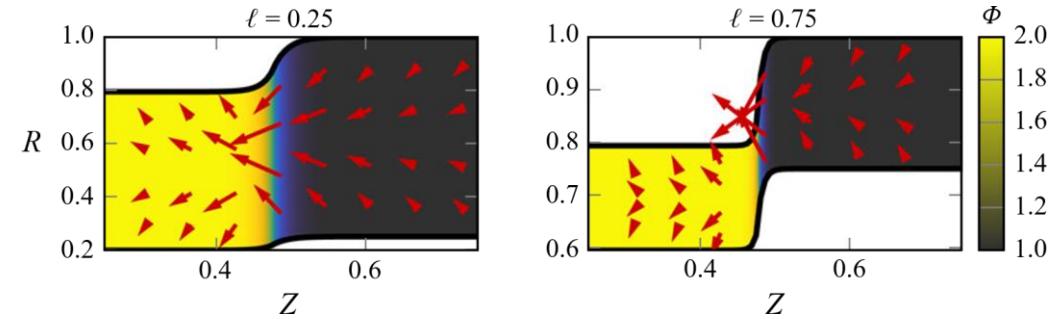
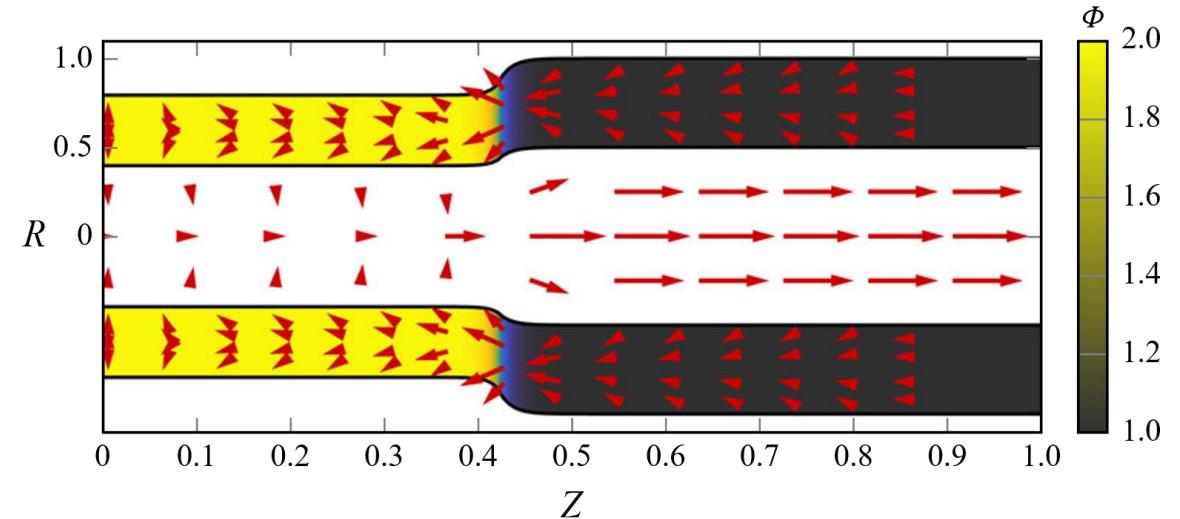


The fluid pulse

3. Fluid flows

Flows arise in three places:

- Radial fluxes from the tube walls into the surroundings as they deswell – $u_r \propto \partial\phi/\partial r$
- Axial fluxes through the gel from more swollen to less swollen regions (probably small) – $u_z \propto \partial\phi/\partial z$
- Axial fluxes arising from conservation of fluid: the tube collapses and squeezes water along its length

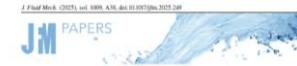


1. Introduction

Hydrogels comprise an elastic, hydrophilic, polymer scaffold saturated with adsorbed water molecules that are held in place by hydrogen bonding between the water molecules and the cross-linked polymer chains. When such gels are brought below the freezing point of water, a complicated phase transition occurs, during which ice crystals and liquid lenses [1] – so ‘mosaic’ lenses [2] – are observed. Common to these phenomena is the fact that water cannot remain in its liquid state at temperatures below 0 °C, since the ice-water transition is very low, since the ice-water temperature

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Poromechanical modelling of responsive hydrogel pumps

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Thermoresponsive hydrogels are smart materials that rapidly switch between hydrophilic (wet) and hydrophobic (dry/mosaic) states when heated past a threshold temperature, resulting in order-of-magnitude changes in gel volume. Modelling the dynamics of this switch is notoriously difficult and typically requires solving coupled poromechanical models involving extensive simulation. In this paper, we present and validate an intuitive, macroscopic description of responsive gel dynamics and use it to explore the potential of thermoresponsive hydrogels as actuators and pumps for microfluidic devices. We finish with a discussion on how such tubular structures may be used to speed up the response times of larger hydrogel smart actuators and unlock new possibilities for dynamic shape change.

Key words: polymeric, porous media

1. Introduction

Hydrogels are soft porous materials comprising a cross-linked, hydrophilic, polymer scaffold that is adsorbed onto hydrophobic polymer chains that form the porous scaffold (De 2009; Bertrand et al. 2016). Though simple in structure, their elastic and soft nature, coupled with the ability to change volume to an extreme degree by swelling or shrinking, has led to their use in a wide range of applications in medicine and agriculture (Zofkova-Meler et al. 2010; Guilleme et al. 2013). In traditional hydrogels, this volume change is triggered by the addition of water to the polymer scaffold as the polymer scaffold for water changes as a result of external stimuli such as heat, light or chemical concentration (Niemants et al. 2021), allowing for controllable swelling-shrinking cycles. Such ‘smart’ materials with tunable shape-changing behaviour have

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UK Hydrogels seminars



Cryosuction and freezing hydrogels

JJW & M. Grae Worster (2025)

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