# **Energy conversion I**

#### Lecture 17:

#### **Topic 5: Induction Motors (S. Chapman ch. 7)**

- Induction Motor Construction
- Basic Induction Motor Concepts
- The Equivalent Circuit of an Induction Motor.
- Power and Torque in Induction Motor.
- Induction Motor Torque-Speed Characteristics
- Starting Induction Motors
- Speed Control of Induction Motor
- Determining Circuit Model Parameters

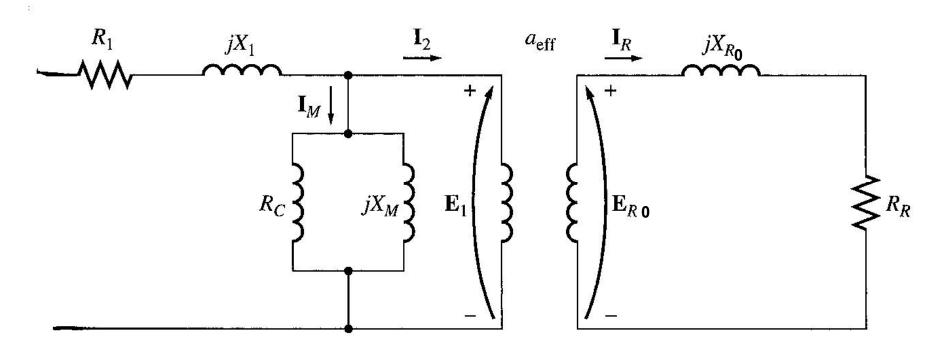
#### Transformer Model of blocked Rotor Induction motor:

- Rotating magnetic flux induces voltage in both stator and rotor windings
- Stator and rotor winding have flux leakage modeled by leakage inductances
- Stator and rotor winding have resistance modeled by winding resistances
- Iron core loss (both in stator and rotor)
- Magnetizing inductance having magnetizing current
- Magnetizing current in magnetizing inductance is the origin of air-gap flux
- Iron loss depends on the magnetic operating point and can be modeled by a resistor in parallel with magnetizing inductance

As can be seen is very similar to a transformer!!

### **Transformer Model of blocked Rotor Induction motor:**

### And therefore the per phase equivalent circuit is:



$$\frac{E_1}{E_{R0}} = \frac{N_{se}}{N_{re}} = a_{eff}$$

$$I_{R} = \frac{E_{R0}}{R_{R} + jX_{R0}}$$

X<sub>1</sub> and X<sub>R</sub> leakage reactances

#### **Effect of Rotor Rotation:**

When rotor is moving with  $n_m$  rpm:

Frequency of induced voltage :  $f_r = sf_s$ 

Amplitude of induced voltage :  $E_R = sE_{R0}$ 

Leakage reactance:  $X_R = s X_{R0}$ 

$$I_{R} = \frac{E_{R}}{R_{R} + jX_{R}} = \frac{sE_{R0}}{R_{R} + jsX_{R0}} = \frac{E_{R0}}{\frac{R_{R}}{S} + jX_{R0}}$$

$$\downarrow I_{R}$$

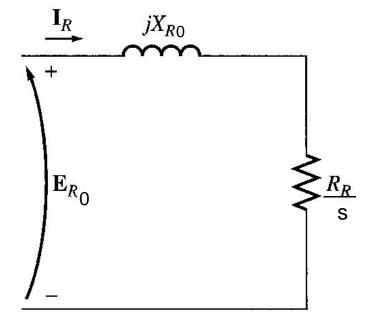
$$\downarrow J_{R}$$

$$\downarrow E_{R}$$

$$\downarrow R_{R}$$

$$\downarrow R_{R}$$

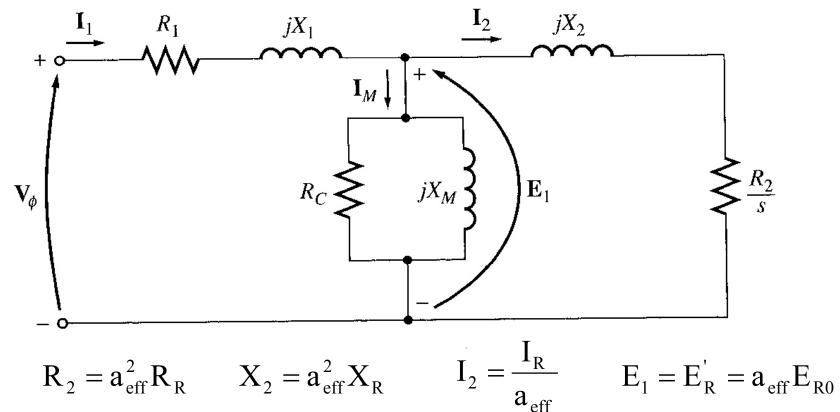
Attention: Both torque and Rotor field depend on the amplitude of I<sub>R</sub>



# The Equivalent Circuit of an Induction Motor

Rotating rotor equivalent circuit is in the secondary of an ideal transformer with a turn ration of:  $a_{eff} = N_{se} / N_{re}$ 

Rotor Equivalent circuit can be seen from the primary (stator):

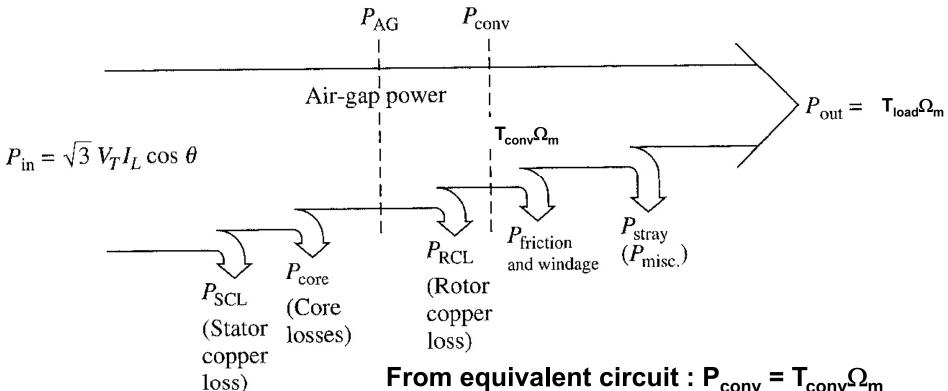


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#### **Power Flow of an Induction Motor**

Input power (Electrical) : P<sub>in</sub> =√3V<sub>T</sub>I<sub>L</sub>cosθ

Output power (Mechanical) :  $P_{out} = T_{load}\Omega_{m}$ 



From equivalent circuit :  $P_{conv} = T_{conv}\Omega_{m}$ Core Losses are usually lumped with mechanical losses

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#### **Power of an Induction Motor**

#### **Using per-phase equivalent circuit:**

$$I_1 = \frac{V_{\phi}}{Z_{eq}}$$

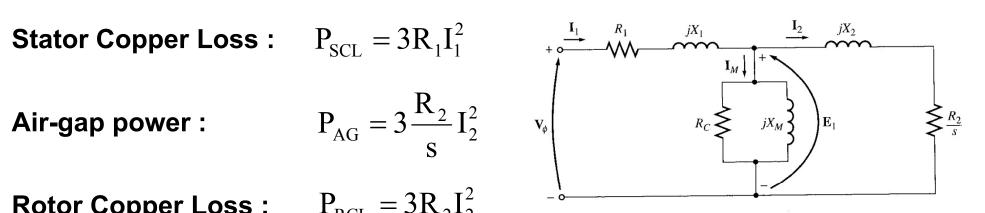
$$Z_{eq} = R_1 + jX_1 + (R_c \text{ II } jX_M \text{ II } (R_2/s + jX_2)$$

$$P_{SCL} = 3R_1I_1^2$$

$$P_{AG} = 3\frac{R_2}{s}I_2^2$$

Rotor Copper Loss:  $P_{RCI} = 3R_2I_2^2$ 

$$P_{RCL} = 3R_2I_2^2$$



Developed Mechanical Power: 
$$P_{conv} = P_{AG} - P_{RCL} = 3R_2I_2^2(\frac{1}{s}-1)$$

Other equations:

$$P_{RCL} = sP_{AG}$$

$$P_{conv} = (1 - s)P_{AG}$$

# **Torque of an Induction Motor**

Output power: 
$$P_{out} = P_{conv} - P_{F\&W} - P_{misc}$$

Output Torque : 
$$T_{load} = \frac{P_{out}}{\Omega_m}$$

Using Equivalent circuit  $P_{conv}$  and consequently  $T_{ind}$  can be calculated:

$$T_{\text{ind}} = \frac{P_{\text{conv}}}{\Omega_m}$$

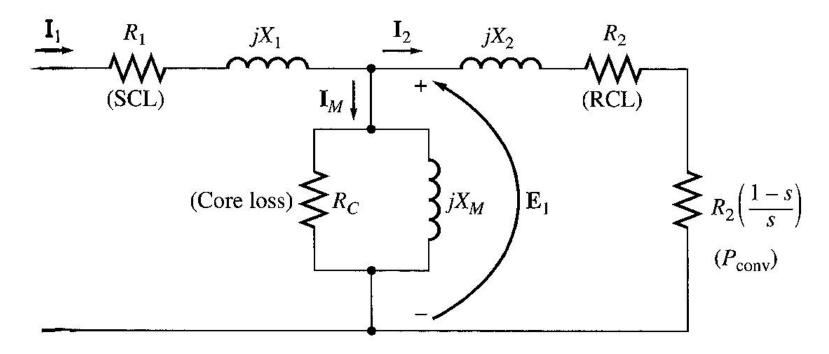
Since: 
$$P_{conv} = (1-s)P_{AG}$$
,  $\Omega_m = (1-s)\Omega_s$ 

Since: 
$$P_{\text{conv}} = (1-s)P_{\text{AG}}$$
,  $\Omega_m = (1-s)\Omega_s$   
Then:  $T_{\text{ind}} = \frac{P_{\text{conv}}}{\Omega_m} = \frac{(1-s)P_{AG}}{(1-s)\Omega_s} = \frac{P_{AG}}{\Omega_s}$   $\Omega_s = \frac{\omega_s}{\frac{p}{2}}$  Mechanical Synchronous speed

$$\Omega_s = rac{\omega_s}{p}$$
 **Mechanical** Synchronous spee

## **Rotor Modified Equivalent Circuit of an Induction Motor**

Separating rotor cupper loss and converted power we can have the following equivalent circuit:



### **Example:**

A 460V, 25hp, 60Hz, 4 pole, Y-connected induction motor has the following impedances in ohms per phase referred to the stator circuit:

$$R_1 = 0.641 \Omega$$

$$R_2 = 0.332 \Omega$$

$$X_1 = 1.106 \Omega$$

$$X_2 = 0.464 \Omega$$

$$X_m = 26.3 \Omega$$

The total rotational losses are 1100W and are assumed to be constant.

The core loss is lumped in with the rotational losses. For a rotor slip of 2.2% at the rated voltage and rated frequency, find the motor's

$$E- \tau_{ind}$$
 and  $\tau_{load}$ 

#### **Solution:**

### A-Speed

The synchronous speed: 
$$n_{sync} = \frac{120f_e}{p} = \frac{120 \times 60}{4} = 1800 \text{ rpm}$$

Therefore:  $n = (1-s)n_{sync} = (1-0.022) \times 1800 = 1760 \text{ rpm}$ 

#### **B- Stator current**

To find the stator current, input impedance should be calculated:

$$Z_{in} = R_1 + jX_1 + (jX_M II (R_2/s + jX_2))$$

$$= 0.641 + j1.106 + \frac{j26.3(\frac{0.332}{0.022} + j0.464)}{\frac{0.332}{0.022} + j(26.3 + 0.464)}$$

$$= 11.72 + j7.79 = 14.07 \angle 33.6^{\circ}$$

Therefore the current is : 
$$I_1 = \frac{V_{\phi}}{Z_{in}} = \frac{460/\sqrt{3}}{14.07\angle 33.6^{\circ}} = 18.88\angle -33.6^{\circ}$$

C- Power factor :  $PF = cos33.6^{\circ} = 0.833$  lagging

### D- P<sub>conv</sub> and P<sub>out</sub>:

$$P_{conv} = P_{AG}(1-s)$$

$$P_{AG} = P_{in} - P_{SCL} = \sqrt{3} \times 460 \times 18.88 \times \cos 33.6^{\circ} - 3 \times (18.88)^{2} \times 0.641 = 11845 \text{ W}$$

$$P_{conv} = 11845 \times (1 - 0.022) = 11585 \text{ W}$$

$$P_{\text{out}} = P_{\text{conv}} - P_{\text{rot}} = 11585 - 1100 = 10485 \text{ W} = \frac{10485}{746} = 14.1 \text{ hp}$$

### E- $\tau_{ind}$ and $\tau_{load}$ :

$$T_{ind} = \frac{P_{AG}}{\Omega_{s}} = \frac{11845}{1800 \times \frac{2\pi}{60}} = 62.8 \text{ N.m} \qquad T_{load} = \frac{P_{out}}{\Omega_{m}} = \frac{10485}{1760 \times \frac{2\pi}{60}} = 56.9 \text{ N.m}$$

#### F- Efficiency:

$$P_{AG} = \frac{Pout}{P_{in}} \times 100\% = \frac{10485}{\sqrt{3} \times 460 \times 18.88 \times \cos 33.6} = \frac{10485}{12530} \times 100\% = 83.7\%$$