

Design Proposal: Unbalanced MZI for Group Index Extraction

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Abstract—The goal of this report is to simulate, design and experimentally characterize Mach-Zehnder interferometers (MZIs) to extract the group index of a silicon strip waveguide. The devices will be characterized after fabrication and the measured values will be compared to simulations made using Lumerical MODE and Lumerical INTERCONNECT. Furthermore, fabrication uncertainties will be investigated by characterizing multiple MZIs of the same configuration.

I. INTRODUCTION

Silicon photonics is a key enabling technology for high-bandwidth optical interconnects in data centers and high-performance computing [1]. It promises the integration of multiple function into a single package making use of the advanced fabrication technologies developed for microelectronics promising high-complexity at low cost [2]. The Mach-Zehnder interferometer (MZI) specifically is an important building block for optical switches and modulators in silicon photonics [3], [4]. They operate based on converting a phase shift between two optical paths into an intensity change at the output. They can further be utilized to extract waveguide parameters such as the group index n_g and the waveguide dimensions [5]. In this work, multiple unbalanced MZI with different path length differences ΔL between 30 μm and 200 μm will be designed and characterized to extract the group index of a quasi-TE mode in a silicon strip waveguide with 220 nm height and 500 nm width on silicon oxide. To check the fabrication reproducibility of the proposed photonic circuits, one interferometer design with $\Delta L = 90 \mu\text{m}$ will be fabricated three times. The group index will be calculated using the free spectral range (FSR) of the interferometer and be compared to simulations.

First, the theoretical background of the MZI will be discussed. Then, the waveguide will be simulated using Lumerical MODE to create a compact waveguide model. After that, the MZI will be constructed and simulated using Lumerical INTERCONNECT. Then, the proposed layout and fabrication will be discussed. After fabrication, the circuit will be experimentally characterized and the results will be compared to the simulations.

II. THEORY

In this section, the transfer function of an unbalanced MZI will be discussed following calculations from [2]. From that, the free spectral range (FSR) of the MZI will be calculated and the formula used for extracting the group index will be discussed.

The unbalanced MZI consists of an input that is split into two branches including two waveguides of different lengths and then recombined. In this work, y-branches are used to split and later recombine the signal.

At the first y-branch, the input intensity $I_i \sim |E_i|^2$ is split equally to the upper and lower branch of the interferometer with E_i describing the electric field. Therefore, both branches have the field $E_i/\sqrt{2}$ after the first y-branch.

The propagation of the light through the waveguides is described by the propagation constant $\beta = \frac{2\pi n_{eff,j}(\lambda)}{\lambda} + i\frac{\alpha_j}{2}$ with wavelength λ , refractive index n_j and loss α_j of the respective waveguide with length L_j . Neglecting losses ($\alpha \approx 0$), the electric field at the end of each waveguide $E_{o,j}$ is

$$E_{o,j} = \frac{E_i}{\sqrt{2}} e^{-i\beta_j L_j}, j = 1, 2. \quad (1)$$

The two outputs are then combined at the second y-branch so that the output at the end of the MZI can be described as

$$E_o = \frac{E_{o,1} + E_{o,2}}{\sqrt{2}} = \frac{E_i}{2} (e^{-i\beta_1 L_1} + e^{-i\beta_2 L_2}), \quad (2)$$

or in terms of the intensity

$$\frac{I_o}{I_i} = \frac{1}{4} \cdot |e^{-i\beta_1 L_1} + e^{-i\beta_2 L_2}|^2 = \frac{1}{2} (1 + \cos(\beta_1 L_1 - \beta_2 L_2)). \quad (3)$$

Due to the wavelength-dependence of the propagation constant, the output of the MZI is therefore a wavelength-dependent sinusoidally varying function. The period of this function is the FSR of the interferometer. Using the same waveguide material and dimensions ($\beta_1 = \beta_2$) in an unbalanced MZI ($L_1 \neq L_2$) with path length difference $\Delta L = L_2 - L_1$, equation (3) reduces to

$$\frac{I_o}{I_i} = \frac{1}{2} (1 + \cos(\beta(\lambda) \cdot \Delta L)). \quad (4)$$

The $FSR = \Delta\lambda = \lambda_{m+1} - \lambda_m$ can then be calculated knowing that the phase shift between two adjacent peaks is $\beta_m \Delta L - \beta_{m+1} \Delta L = 2\pi$. Assuming β varies linearly in λ , one can find $\frac{d\beta}{d\lambda} = -\frac{2\pi}{\lambda^2} (n - \frac{dn}{d\lambda} \lambda)$ [6]. The FSR can therefore be calculated using

$$FSR = \frac{\lambda^2}{\Delta L (n - \lambda \frac{dn}{d\lambda})} = \frac{\lambda^2}{\Delta L n_g}. \quad (5)$$

Finally, the group index n_g can be calculated for known path differences ΔL after measuring the FSR of the proposed MZIs according to

$$n_g = n - \lambda \frac{dn}{d\lambda} = \frac{\lambda^2}{FSR \cdot \Delta L}. \quad (6)$$

In the experiment, the group index will be calculated by measuring the spectrum of the MZI, identifying adjacent maxima and computing the FSR. The latter can be averaged over multiple fringes to reduce the error and then inserted into equation (6).

III. MODELING AND SIMULATION

Lumerical MODE [7] is used to extract the wavelength dependent effective index and group index of the silicon waveguide and develop a compact model for the waveguide. The data will then be exported to Lumerical INTERCONNECT [8] for the simulation of the optical circuit.

A. Waveguide simulations using Lumerical MODE

The waveguide-width was set to 500 nm and the height was set to 220 nm to follow common fabrication standards. The simulated mode profile of the first-order quasi-TE-mode is shown in figure 1.

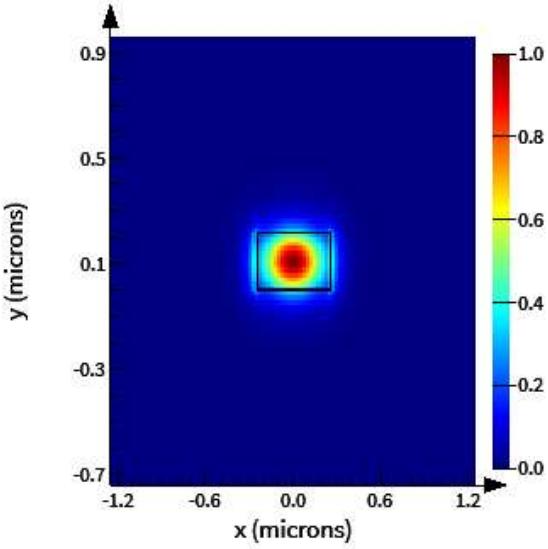


Fig. 1. Simulated waveguide mode profile of the first-order quasi-TE mode of the 500 nm x 220 nm silicon waveguide.

Then, a wavelength sweep between 1500 nm und 1600 nm according for material and waveguide dispersion was performed. The resulting effective index and group index are shown in figure 2 and figure 3.

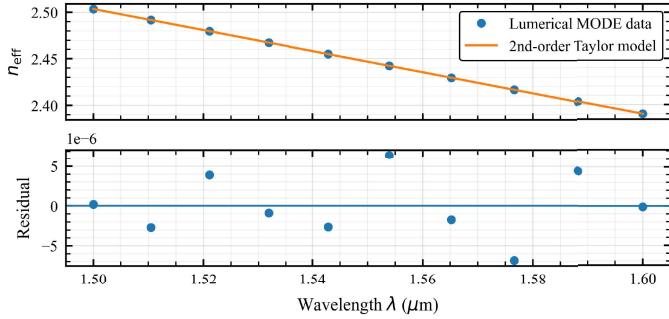


Fig. 2. Effective index n_{eff} calculated in Lumerical MODE and fit following equation (7) vs. wavelength for the first-order quasi-TE mode (1500–1600 nm).

Afterwards, the compact model for the waveguide was derived according to [2]

$$n_{\text{eff}}(\lambda) = n_1 + n_2(\lambda - \lambda_0) + n_3(\lambda - \lambda_0)^2. \quad (7)$$

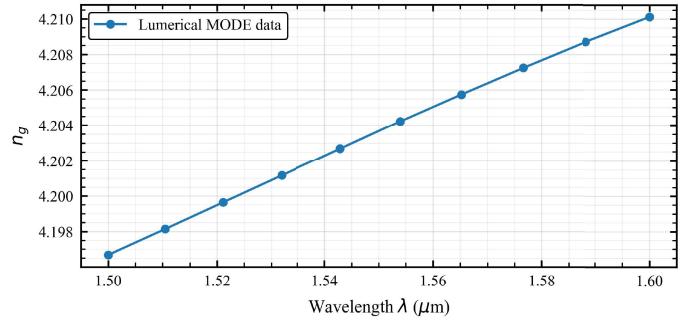


Fig. 3. Group index n_g vs. wavelength for the first-order quasi-TE mode (1500–1600 nm).

Fitting the data directly in with python and inserting them into equation (7) for $\lambda_0 = 1550$ nm and for the first quasi-TE-mode leads to

$$n_1 = 2.4468225 \pm 0.0000022, \quad (8)$$

$$n_2 = (-1.13340 \pm 0.00004) \mu\text{m}^{-1}, \quad (9)$$

$$n_3 = (-0.0450 \pm 0.0016) \mu\text{m}^{-2}, \quad (10)$$

$$\lambda_0 = 1.55 \mu\text{m}. \quad (11)$$

Uncertainties reported here reflect the statistical uncertainty of the polynomial regression (fit covariance only). They do not include fabrication tolerances or simulation/model uncertainty. For readability, the coefficients are rounded leading to

$$n_{\text{eff}}(\lambda) = 2.447 - 1.133 \mu\text{m}^{-1}(\lambda - \lambda_0) - 0.045 \mu\text{m}^{-2}(\lambda - \lambda_0)^2, \quad (12)$$

with λ and λ_0 in μm .

B. MZI simulation using Lumerical INTERCONNECT

The MZI was constructed in Lumerical INTERCONNECT as shown in figure 4. The MZI consists of two y-branches (ebeam_y_1550) whose S-parameters were taken from SiEPIC EBEAM INTERCONNECT Library and two waveguides which were imported from Lumerical MODE. The length of waveguide one was set to 100 μm whereas the length of waveguide two was varied between 130 μm and 300 μm to analyze the FSR for ΔL between 30 μm and 200 μm as shown in table I and in figure 5. The fit-only uncertainty of the calculated FSR is sub-pm, which is below the wavelength resolution of the characterization laser (10 pm) and therefore not included here. Furthermore, two grating couplers (GC_TE_1550_8degOxide_BB) from the SiEPIC EBEAM INTERCONNECT Library were added. An optical network analyzer (ONA) was included to simulate the expected FSR and transmission spectra of the device shown in figures 6 and 7.

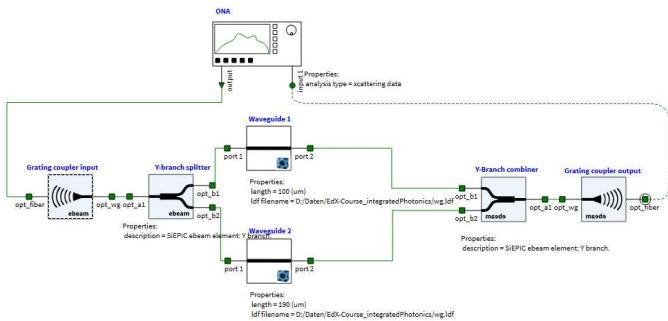


Fig. 4. Exemplary MZI-model implemented in Lumerical INTERCONNECT including the two grating couplers and the optical network analyzer (ONA) used to evaluate the circuit.

TABLE I

EXPECTED FSR AT 1550 NM FOR DIFFERENT ΔL . THE FSR WAS CALCULATED USING EQUATIONS (5) AND (12).

ΔL (μm)	FSR (nm)
30	19.05
60	9.52
90	6.35
120	4.76
150	3.81
200	2.86

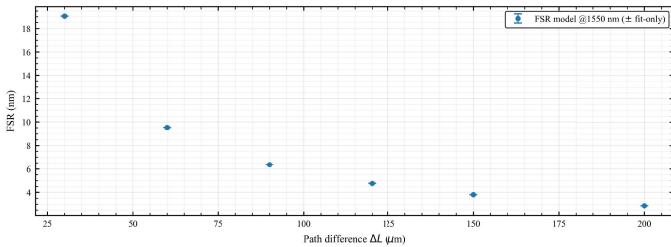


Fig. 5. Calculated FSR vs. wavelength using equation (5) and the path length differences depicted in table I for the first-order quasi-TE mode. The corresponding uncertainties were obtained by Gaussian error propagation using the fit covariance matrix only. For the final comparison with measured data, uncertainties will be estimated using the four-corner method.

Figure 6 shows two exemplary MZI transmission spectra of the quasi-TE mode for 90 μm and 200 μm path difference. As expected, the FSR decreases for larger path length differences.

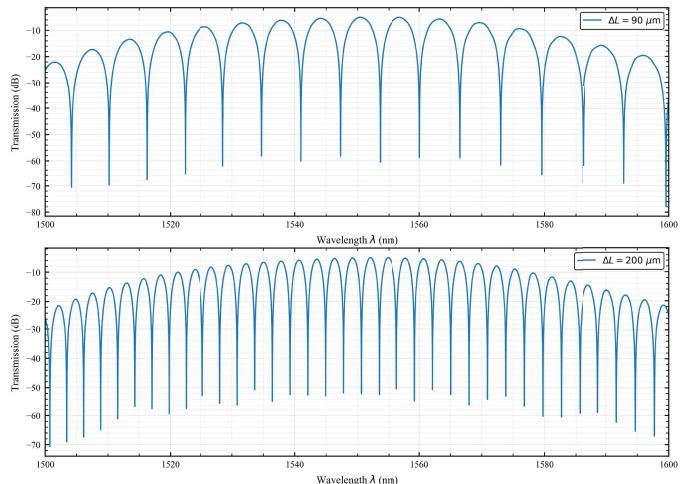


Fig. 6. Exemplary transmission spectra of the proposed MZI with (top) 90 μm and (bottom) 200 μm path difference.

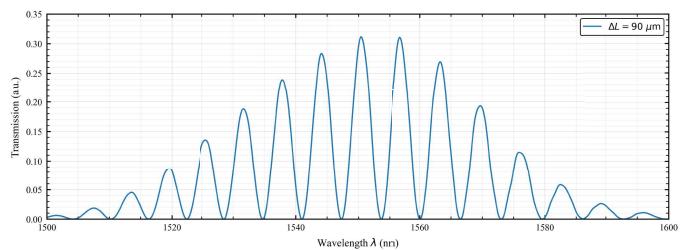


Fig. 7. Exemplary MZI transmission of the quasi-TE mode for $\Delta L=90$ μm in arbitrary units.

IV. LAYOUT

The devices proposed in Table I were designed in KLayout using the SiEPIC version 0.5.31 and EBeam - v0.4.53. An overview of the layout is shown in figure 8 and described in table II. Three devices were added compared to table I: CAL1 consists of only one y-branch and three grating couplers. It is used to evaluate the splitting ratio of the y-branch. DE consists of two grating couplers connected by a waveguide to characterize the grating couplers for calibration. MZI0 is a MZI with no path length difference, again for calibration.

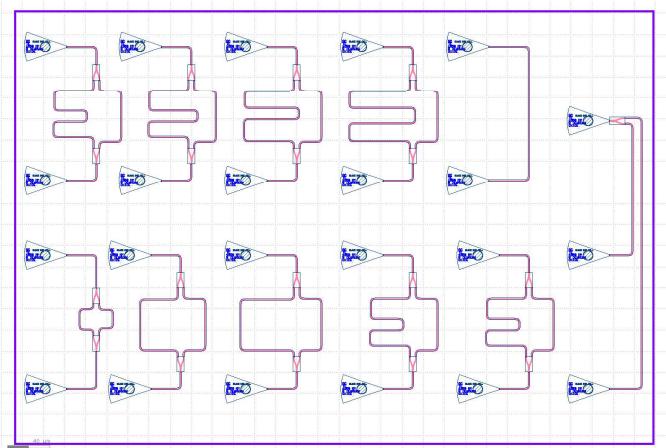


Fig. 8. Proposed layout on the allocated space of 410 μm x 610 μm.

TABLE II
DEVICE NAME VS. PATH LENGTH DIFFERENCE ΔL

Device Name	ΔL (μm)
CAL1	N/A, used for calibration
DE	N/A, used for calibration
MZI0	0
MZI1	30
MZI2	60
MZI3	90
MZI4	90
MZI5	90
MZI6	120
MZI7	150
MZI8	200

V. FABRICATION

To be completed later.

VI. EXPERIMENTAL DATA

To be completed later.

VII. ANALYSIS

To be completed later.

VIII. CONCLUSION

To be completed later.

IX. ACKNOWLEDGEMENTS

To be added.

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