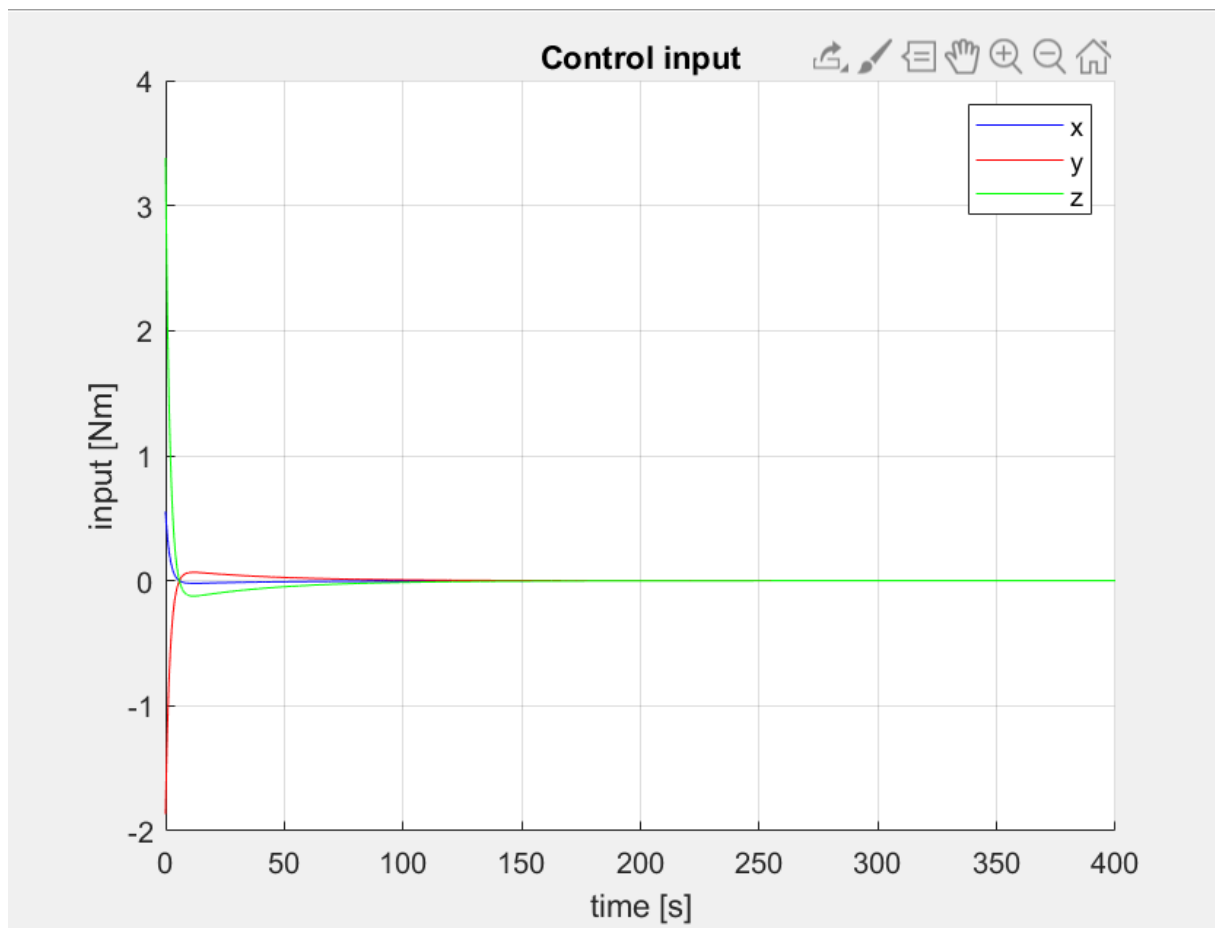
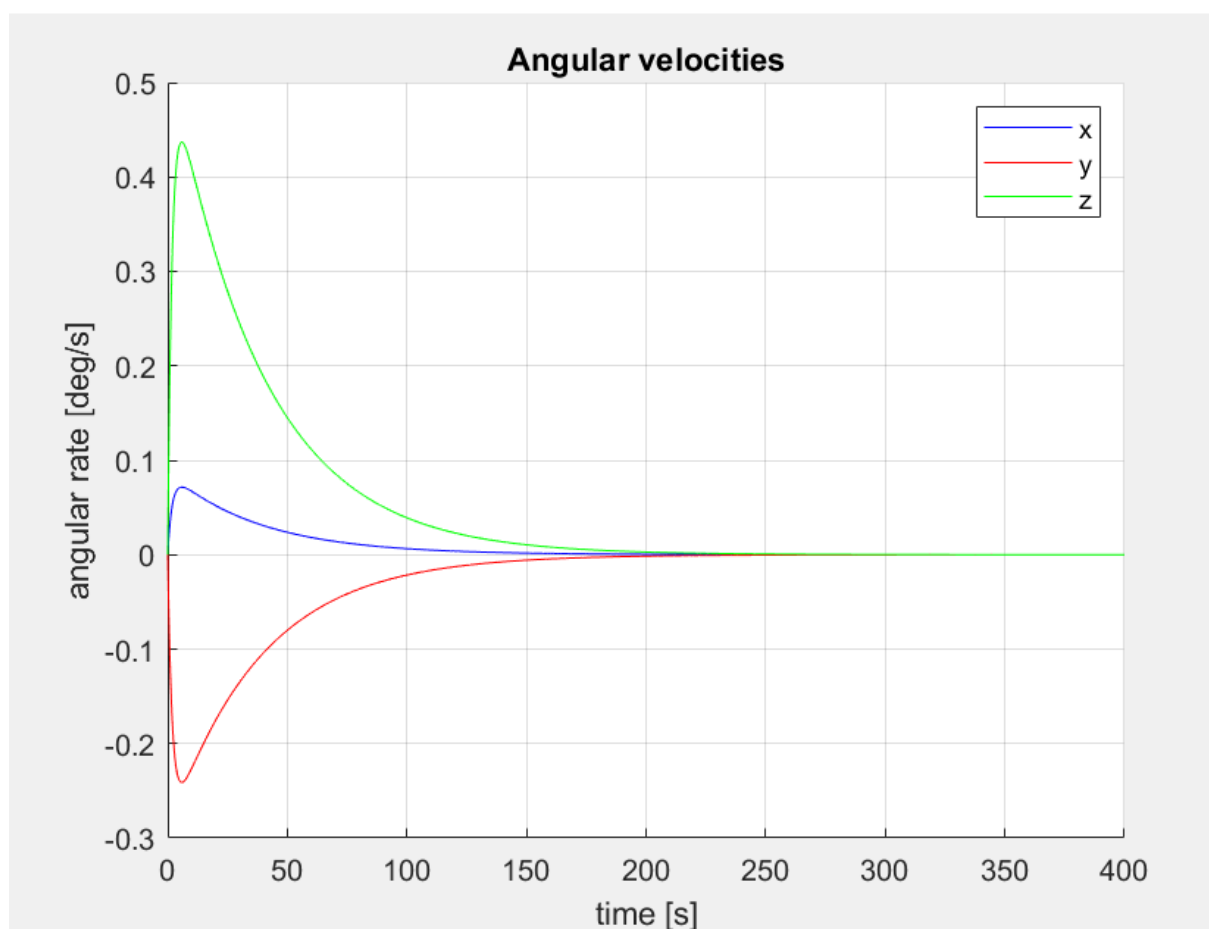
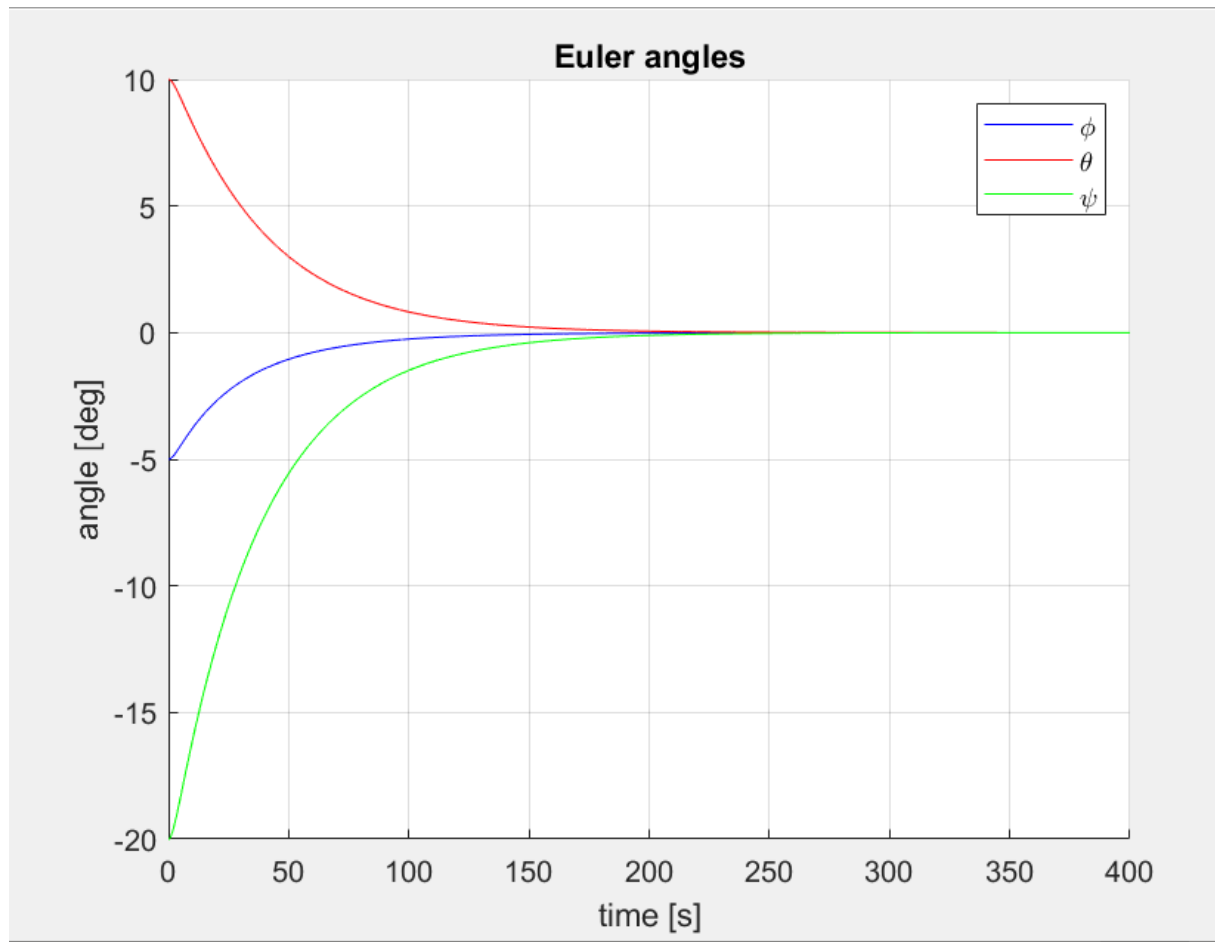


Task 1.3:







Code:

```

22  %% USER INPUTS
23  addpath(genpath("C:\Users\jacob\Documents\Student\Fartøy\MSS"));
24  h = 0.1; % sample time (s)
25  N = 4000; % number of samples. Should be adjusted
26
27  % model parameters
28  m = 180;
29  r = 2;
30  I = m*r^2*eye(3); % inertia matrix
31  I_inv = inv(I);
32
33  % constants
34  deg2rad = pi/180;
35  rad2deg = 180/pi;
36
37  phi = -5*deg2rad; % initial Euler angles
38  theta = 10*deg2rad;
39  psi = -20*deg2rad;
40
41  q = euler2q(phi,theta,psi); % transform initial Euler angles to q
42
43  w = [0 0 0]'; % initial angular rates

```

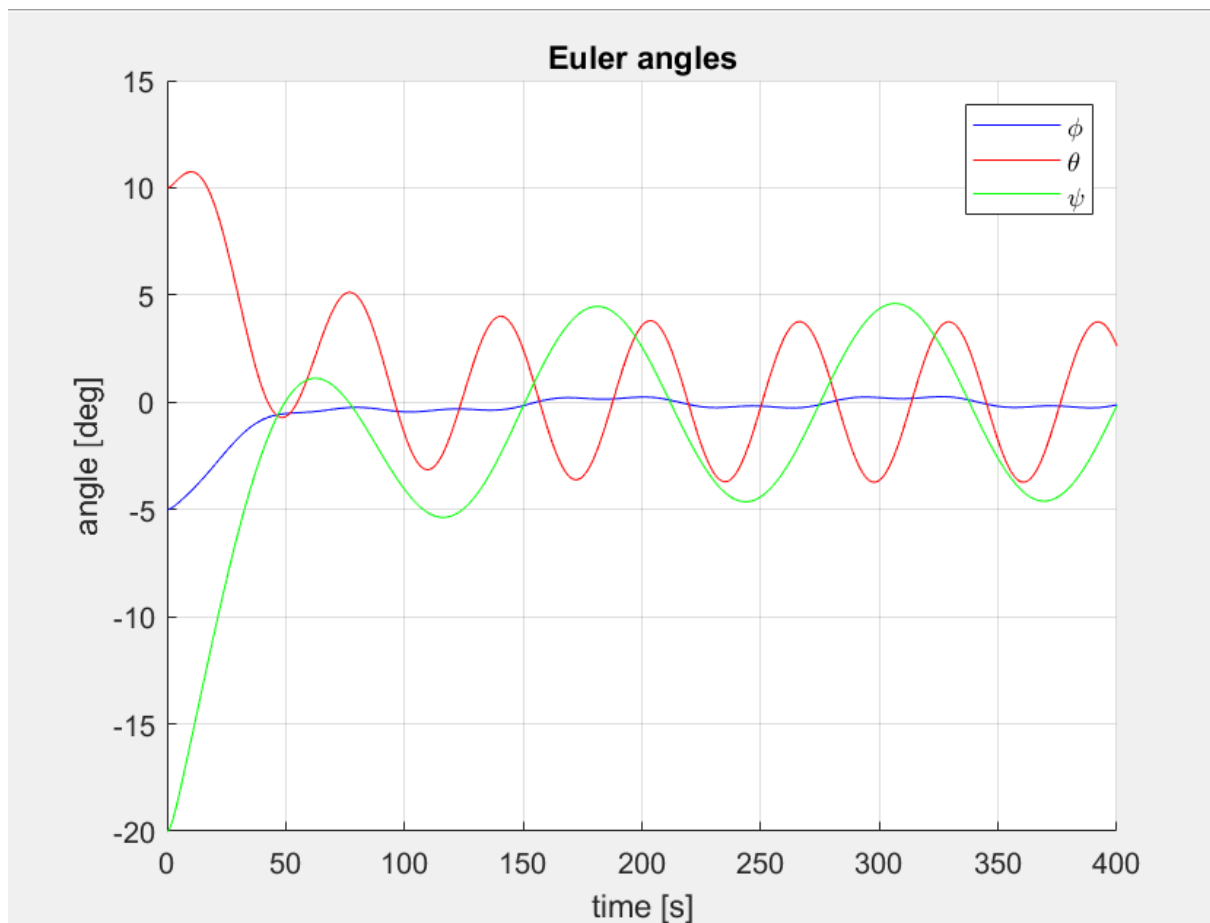
```

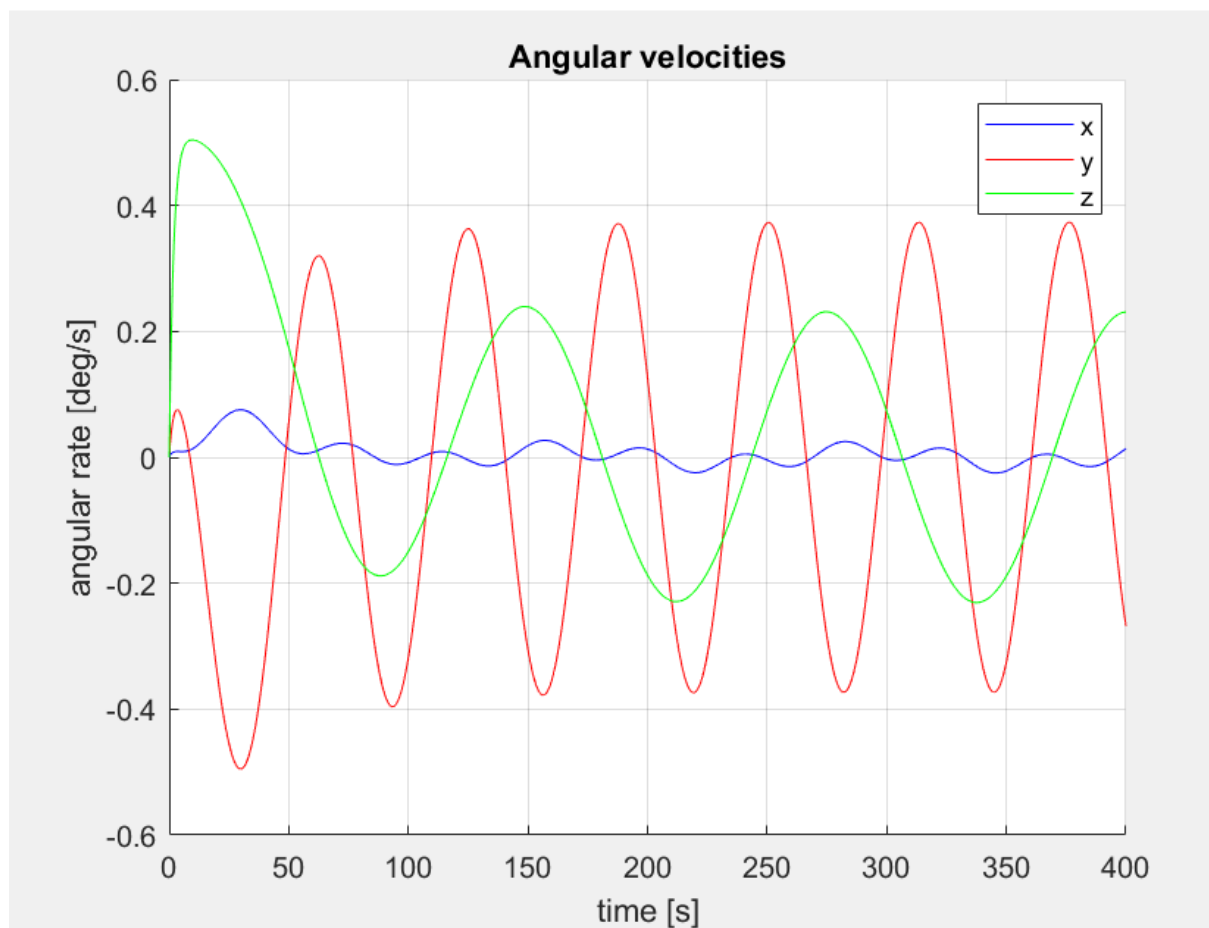
45 - table = zeros(N+1,14);           % memory allocation
46
47 %% FOR-END LOOP
48 - for i = 1:N+1
49 -     t = (i-1)*h;                 % time
50 -     x = [q(2:4)' w']';
51 -     Kp = -kp*eye(3);
52 -     Kd = -kd*eye(3);
53
54 -     K = [Kp, Kd];
55
56 -     tau = K*x;                   % control law
57
58 -     [phi,theta,psi] = q2euler(q); % transform q to Euler angles
59 -     [J,J1,J2] = quatern(q);     % kinematic transformation matrices
60
61 -     q_dot = J2*w;                % quaternion kinematics
62 -     w_dot = I_inv*(Smtrx(I*w)*w + tau); % rigid-body kinetics
63
64 -     table(i,:) = [t q' phi theta psi w' tau']; % store data in table
65
66 -     q = q + h*q_dot;             % Euler integration
67 -     w = w + h*w_dot;
68
69 -     q = q/norm(q);              % unit quaternion normalization
70 - end

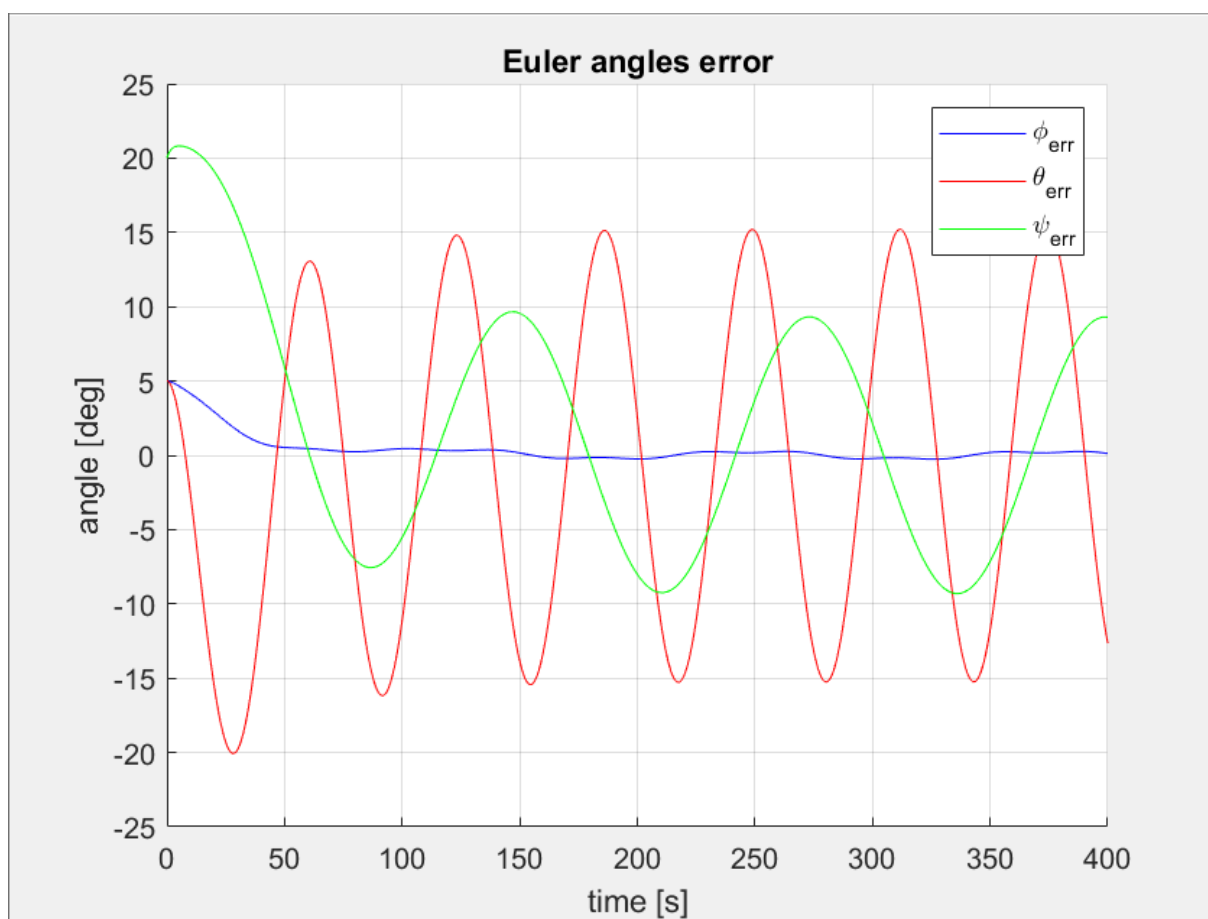
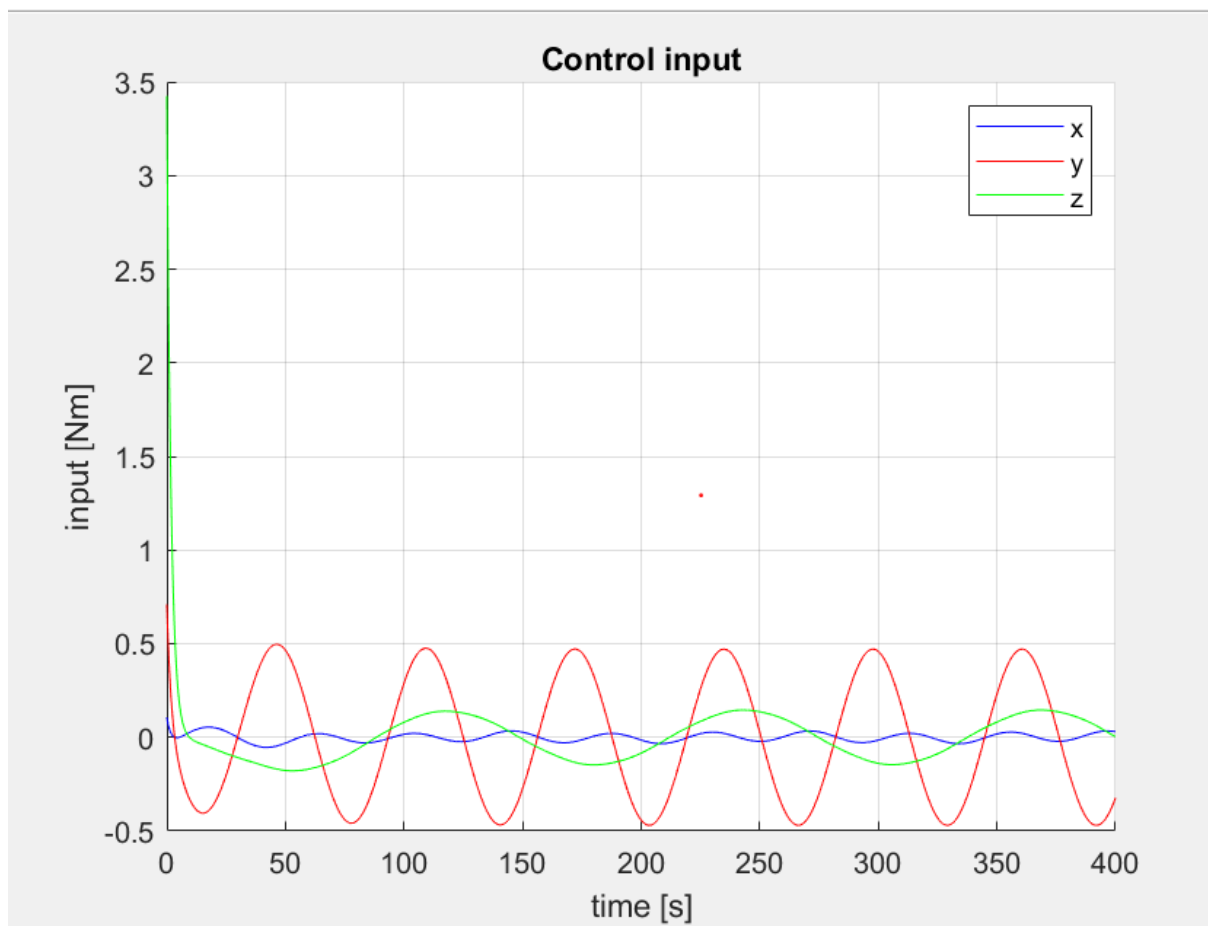
```

The system-response matches our expectations of such a system with a 0-reference. For a non-zero constant reference we would change the feedback-terms in the control-law to be the difference between the reference-state and the current state.

Task 1.5:







Code:

```
22 %% USER INPUTS
23 - addpath(genpath("C:\Users\jacob\Documents\Student\Fartøy\MSS"));
24 - h = 0.1; % sample time (s)
25 - N = 4000; % number of samples. Should be adjusted
26
27 % model parameters
28 - m = 180;
29 - r = 2;
30 - I = m*r^2*eye(3); % inertia matrix
31 - I_inv = inv(I);
32
33 % constants
34 - deg2rad = pi/180;
35 - rad2deg = 180/pi;
36
37 - phi = -5*deg2rad; % initial Euler angles
38 - theta = 10*deg2rad;
39 - psi = -20*deg2rad;
40
41 - q = euler2q(phi,theta,psi); % transform initial Euler angles to q
42
43 - w = [0 0 0]'; % initial angular rates
44
45 - table = zeros(N+1,14); % memory allocation
46
47 - kp = 20; %proportional gain
48 - kd = 400; %derivative gain
49
50 - table_d = zeros(N+1,3);
51
52
53
54 %% FOR-END LOOP
55 - for i = 1:N+1
56 -     t = (i-1)*h; % time
57
58 -     phi_d = 0*deg2rad; %desired phi
59 -     theta_d = 15*cos(0.1*t)*deg2rad; %desired theta
60 -     psi_d = 10*sin(0.05*t)*deg2rad; %desired psi
61
62 -     q_d = euler2q(phi_d,theta_d,psi_d); %desired quaternion
63
64 -     inv_matr = eye(4)*-1; %matrix for inverting the quaternion
65 -     inv_matr(1,1) = 1;
66
```



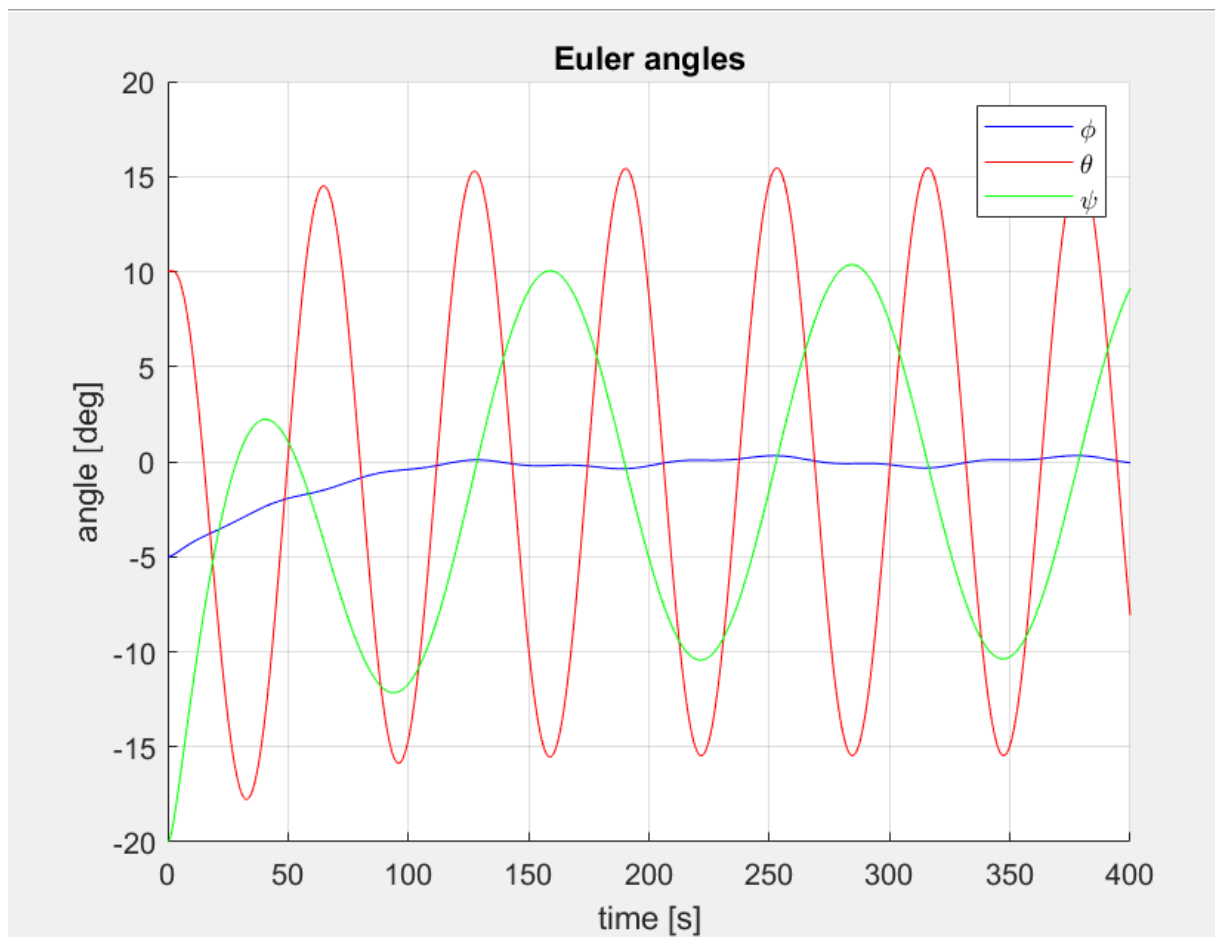
```

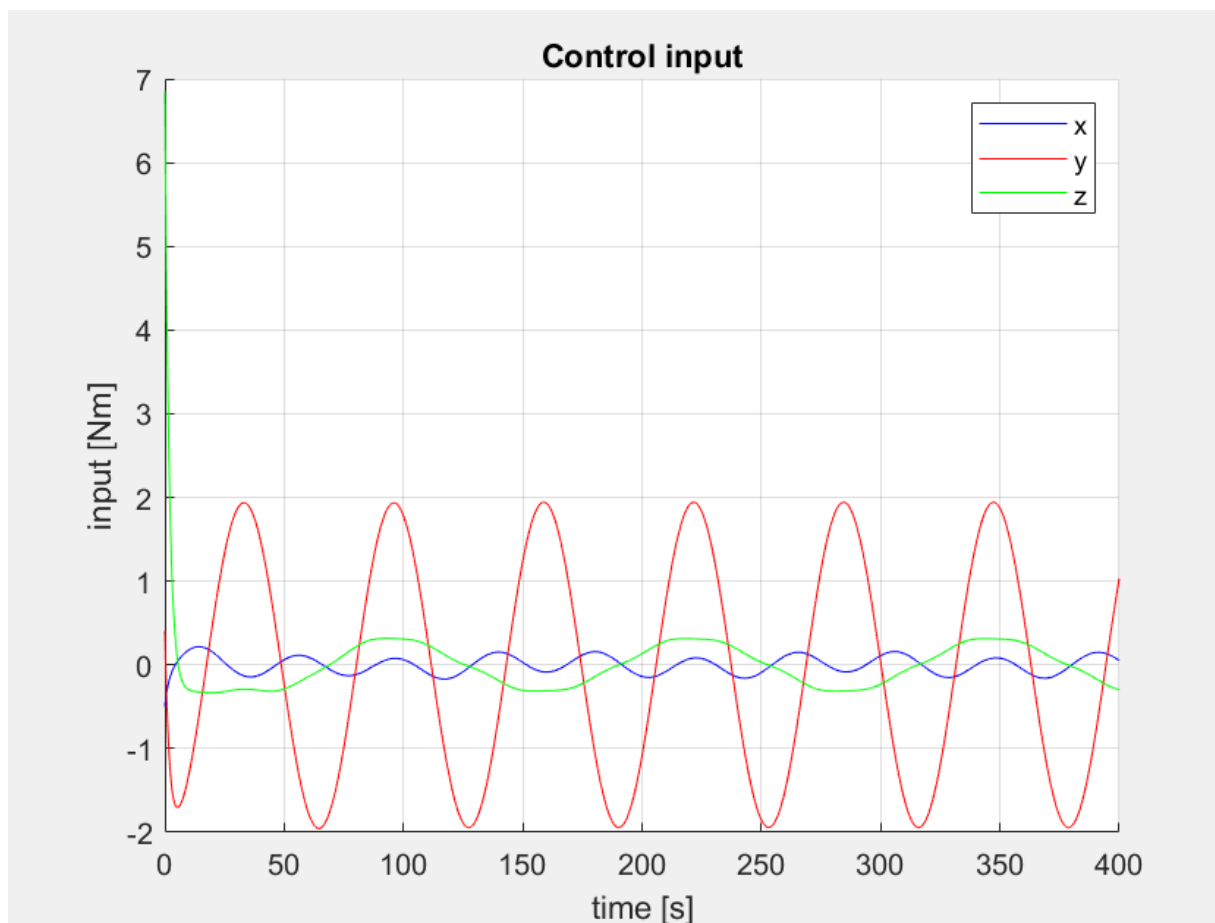
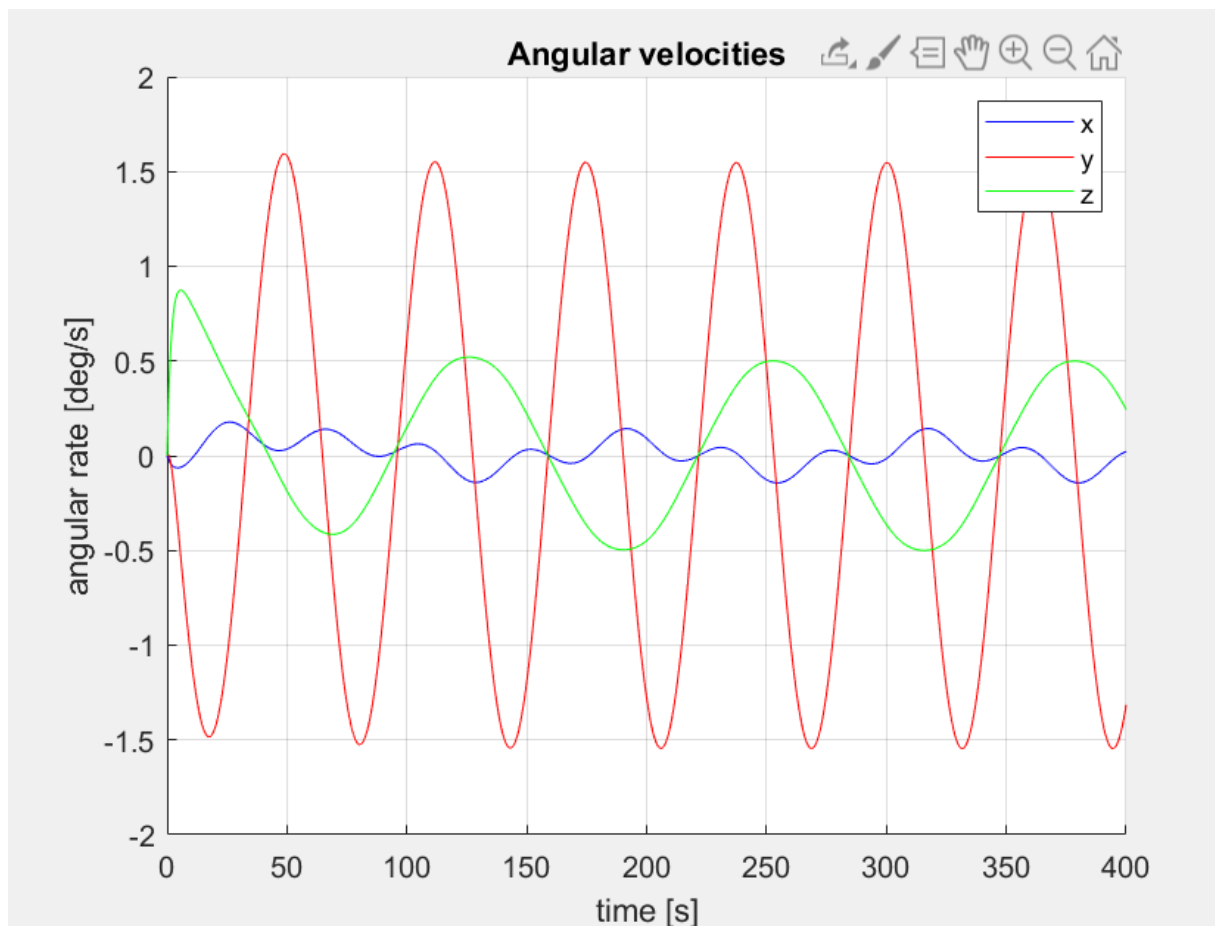
67 - q_d_inv = inv_matr*q_d; %inverting quaternion
68
69
70 - q_err = quatprod(q_d_inv,q); %calculating the error-quaternion
71 - x = [q_err(2:4)' w']';
72 - Kp = -kp*eye(3);
73 - Kd = -kd*eye(3);
74
75 - K = [Kp, Kd];
76
77 - tau = K*x; % control law
78
79 - [phi,theta,psi] = q2euler(q); % transform q to Euler angles
80 - [J,J1,J2] = quatern(q); % kinematic transformation matrices
81
82 - q_dot = J2*w; % quaternion kinematics
83 - w_dot = I_inv*(Smtrx(I*w)*w + tau); % rigid-body kinetics
84
85 - table(i,:) = [t q' phi theta psi w' tau']; % store data in table
86 - table_d(i,:) = [phi_d,theta_d,psi_d];
87
88 - q = q + h*q_dot; % Euler integration
89 - w = w + h*w_dot;
90
91 - q = q/norm(q); % unit quaternion normalization
92 - end
93
94 %% PLOT FIGURES
95 - t = table(:,1);
96 - q = table(:,2:5);
97 - phi = rad2deg*table(:,6);
98 - theta = rad2deg*table(:,7);
99 - psi = rad2deg*table(:,8);
100 - w = rad2deg*table(:,9:11);
101 - tau = table(:,12:14);
102
103 - phi_d = rad2deg*table_d(:,1);
104 - theta_d = rad2deg*table_d(:,2);
105 - psi_d = rad2deg*table_d(:,3);
106
107 - phi_err = phi_d - phi;
108 - theta_err = theta_d - theta;
109 - psi_err = psi_d - psi;

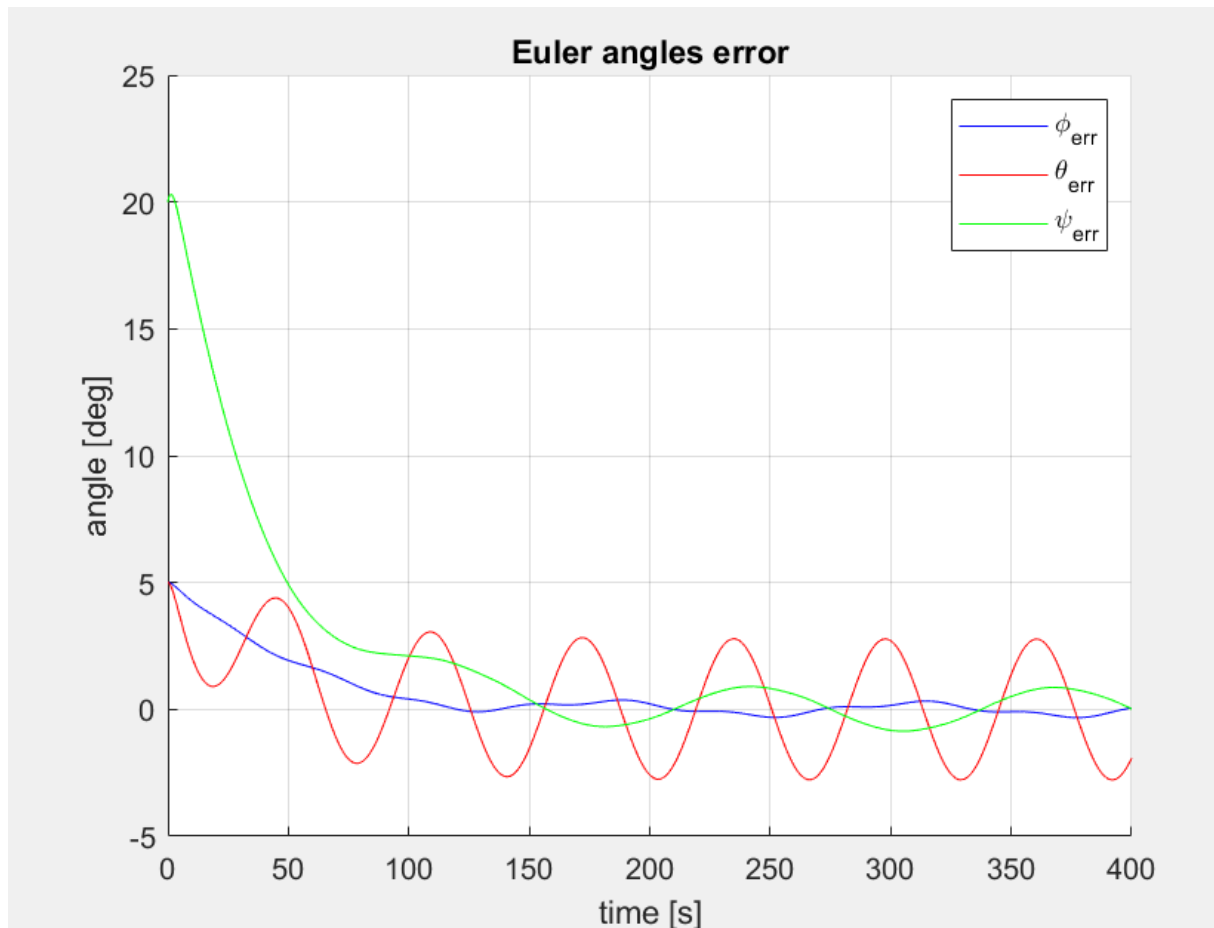
```

The system response is expected. We have no error-state in the omega so the error is quite large. We see the control input also get a sinusoidal shape which makes sense as we are tracking a sinusoidal reference. Since we switched to quaternions we do not get the issue with a singularity at 90 degrees that we would have had from euler angles, but the simulation shows that no state reaches 90 degrees anyways.

Task 1.6:







Code:

```

22 %% USER INPUTS
23 - addpath(genpath("C:\Users\jacob\Documents\Student\Fartøy\MSS"));
24 - h = 0.1; % sample time (s)
25 - N = 4000; % number of samples. Should be adjusted
26
27 % model parameters
28 - m = 180;
29 - r = 2;
30 - I = m*r^2*eye(3); % inertia matrix
31 - I_inv = inv(I);
32
33 % constants
34 - deg2rad = pi/180;
35 - rad2deg = 180/pi;
36
37 - phi = -5*deg2rad; % initial Euler angles
38 - theta = 10*deg2rad;
39 - psi = -20*deg2rad;
40
41 - q = euler2q(phi,theta,psi); % transform initial Euler angles to q
42
43 - w = [0 0 0]'; % initial angular rates
44

```

```

45 - table = zeros(N+1,14);           % memory allocation
46
47 - kp = 20;                         %proportional gain
48 - kd = 400;                       %derivative gain
49
50
51
52
53
54
55
56 %% FOR-END LOOP
57 - for i = 1:N+1
58 -     t = (i-1)*h;                 % time
59
60 -     phi_d = 0*deg2rad;            %desired phi
61 -     theta_d = 15*cos(0.1*t)*deg2rad; %desired theta
62 -     psi_d = 10*sin(0.05*t)*deg2rad; %desired psi
63
64 -     phi_d_dot = 0*deg2rad;        %desired phi_dot
65 -     theta_d_dot = -1.5*sin(0.1*t)*deg2rad; %desired theta_dot
66 -     psi_d_dot = 0.5*cos(0.05*t)*deg2rad; %desired psi_dot
67
68 -     Theta_D = [phi_d_dot, theta_d_dot, psi_d_dot]';
69
70 -     q_d = euler2q(phi_d,theta_d,psi_d); %desired quaternion
71
72 -     inv_matr = eye(4)*-1;         %matrix for inverting the quaternion
73 -     inv_matr(1,1) = 1;
74
75 -     q_d_inv = inv_matr*q_d;       %inverting quaternion
76
77 -     T_inv = [1, 0, -sin(theta);   %T_inv from 2.41 in Fossen
78 -             0, cos(phi), cos(theta)*sin(phi);
79 -             0, -sin(phi), cos(theta)*cos(phi)];
80
81
82 -     w_d = T_inv * Theta_D;        %desired omega
83
84 -     w_err = w-w_d;                %error in omega
85
86
87 -     q_err = quatprod(q_d_inv,q);  %calculating the error-quaternion
88 -     x = [q_err(2:4)' w_err]';
89 -     Kp = -kp*eye(3);
90 -     Kd = -kd*eye(3);

```

```

91
92 - K = [Kp, Kd];
93
94 - tau = K*x;           % control law
95
96 - [phi,theta,psi] = q2euler(q); % transform q to Euler angles
97 - [J,J1,J2] = quatern(q);      % kinematic transformation matrices
98
99 - q_dot = J2*w;              % quaternion kinematics
100 - w_dot = I_inv*(Smtrx(I*w)*w + tau); % rigid-body kinetics
101
102 - table(i,:) = [t q' phi theta psi w' tau']; % store data in table
103
104 - q = q + h*q_dot;           % Euler integration
105 - w = w + h*w_dot;
106
107 - q = q/norm(q);             % unit quaternion normalization
108 - end

```

We see that the tracking-error is much lower now that we included the error-term in the omega. Adding integral action is a bad idea with a time-variant reference because of windup. With some anti-windup law it could perhaps improve the system, but as the system is already really slow, more delay with an integral worsens the system.

Since the reference is time-varying we might consider adding gain-scheduling into the control-law to make the response faster and to further reduce the tracking-error.