

1.8-5 (1-18 in text) Figure P1.8-5 illustrates a fin that is to be used in the evaporator of a space conditioning system for a space-craft.

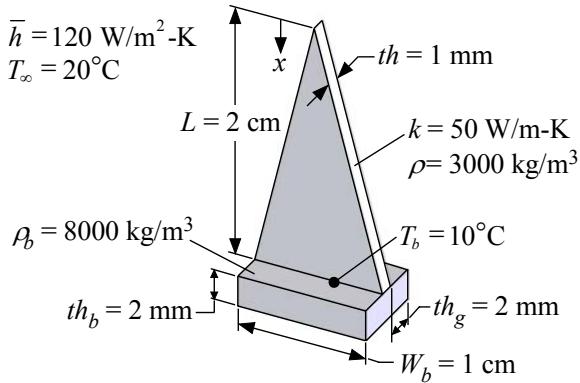


Figure P1.8-5: Fin on an evaporator.

The fin is a plate with a triangular shape. The thickness of the plate is $th = 1 \text{ mm}$ and the width of the fin at the base is $W_b = 1 \text{ cm}$. The length of the fin is $L = 2 \text{ cm}$. The fin material has conductivity $k = 50 \text{ W/m-K}$. The average heat transfer coefficient between the fin surface and the air in the space-craft is $\bar{h} = 120 \text{ W/m}^2\text{-K}$. The air is at $T_\infty = 20^\circ\text{C}$ and the base of the fin is at $T_b = 10^\circ\text{C}$. Assume that the temperature distribution in the fin is 1-D in x . Neglect convection from the edges of the fin.

- Obtain an analytical solution for the temperature distribution in the fin. Plot the temperature as a function of position.
- Calculate the rate of heat transfer to the fin.
- Determine the fin efficiency.

~~The fin has density $\rho = 3000 \text{ kg/m}^3$ and the fin is installed on a base material with thickness $th_b = 2 \text{ mm}$ and density $\rho_b = 8000 \text{ kg/m}^3$. The half-width of the gap between adjacent fins is $th_g = 2 \text{ mm}$. Therefore, the volume of the base material associated with each fin is $th_b W_b (th + 2 th_g)$.~~

- ~~Determine the ratio of the absolute value of the rate of heat transfer to the fin to the total mass of material (fin and base material associated with the fin).~~
- ~~Prepare a contour plot that shows the ratio of the heat transfer to the fin to the total mass of material as a function of the length of the fin (L) and the fin thickness (th).~~
- ~~What is the optimal value of L and th that maximizes the absolute value of the fin heat transfer rate to the mass of material?~~

a) $T(x)$

$$B_i = \frac{\bar{h} W b}{2 k} = \frac{120 \cdot 0.01}{2 \cdot 50} = 0.012 \Rightarrow B_i \ll 1$$

 $th = Wb = 1 \text{ cm}, W = th = 1 \text{ mm}$ $A_s(x) = 2th \frac{x}{L} dx, \text{ convection surface area}$

$$\dot{Q}_{\text{conv}} = 2th \frac{x}{L} dx \bar{h} (T - T_{\infty})$$

$$\dot{Q}_{\text{cond}} = -k th W \frac{x}{L} \frac{dT}{dx}$$

$$0 = \frac{d\dot{Q}_{\text{cond}}}{dx} dx + \dot{Q}_{\text{conv}}$$

$$0 = \frac{d}{dx} \left[-k th W \frac{x}{L} \frac{dT}{dx} \right] dx + 2th \frac{x}{L} dx \bar{h} (T - T_{\infty})$$

$$\frac{d}{dx} \left[x \frac{dT}{dx} \right] dx - \frac{2th \frac{x}{L} \bar{h} L dx}{k th W} T = - \frac{2th \frac{x}{L} \bar{h} L dx}{k + th W} T_{\infty}$$

$$\frac{d}{dx} \left[x \frac{dT}{dx} \right] - 2 \frac{x \bar{h}}{kW} T = -2 \frac{x \bar{h}}{kW} T_{\infty}$$

$$x \frac{d^2 T}{dx^2} + \frac{dT}{dx} - 2 \frac{x \bar{h}}{kW} T = -2 \frac{x \bar{h}}{kW} T_{\infty}$$

$$x \frac{d^2 \theta}{dx^2} + \frac{d\theta}{dx} - x \frac{2 \bar{h}}{kW} \theta = 0, \theta = T - T_{\infty}, \frac{d\theta}{dx} = \frac{dT}{dx}, \frac{d^2 \theta}{dx^2} = \frac{d^2 T}{dx^2}$$

Plugging in to Maple:

$$\theta(x) = C_1 \text{BesselJ}(0, \sqrt{\beta} x) + C_2 \text{BesselY}(0, \sqrt{\beta} x), \beta = \frac{2 \bar{h}}{kW}$$

with β assumed positive

$$\theta(x) = C_1 \text{BesselI}(0, \sqrt{\beta} x) + C_2 \text{BesselK}(0, \sqrt{\beta} x)$$

at $x=0, T < \infty \Rightarrow \theta < \infty \rightarrow C_1 \text{BesselI}(0,0) + C_2 \text{BesselK}(0,0) < \infty$ $\text{BesselK}(0,0) = \infty \Rightarrow C_2 = 0$ at $x=L, \theta = \theta_b = T_b - T_{\infty}$

$$C_1 \text{BesselI}(0, \sqrt{\beta} L) = \theta_b$$

$$C_1 = \frac{\theta_b}{\text{BesselI}(0, \sqrt{\beta} L)}$$

$$\theta(x) = \theta_b \frac{\text{BesselI}(0, \sqrt{\beta} x)}{\text{BesselI}(0, \sqrt{\beta} L)} = \theta_b \frac{\text{BesselI}(0, \sqrt{\frac{2 \bar{h}}{kW}} x)}{\text{BesselI}(0, \sqrt{\frac{2 \bar{h}}{kW}} L)}$$

$$\underline{T(x) = \theta(x) + T_{\infty}}$$

$$\underline{T(x)}$$

b) \dot{Q}_{fin}

$$\dot{Q}_{\text{fin}} = kW th \frac{dT}{dx} \Big|_{x=L} = kW th \frac{d}{dx} \left[\theta_b \frac{\text{BesselI}(0, \sqrt{\beta} x)}{\text{BesselI}(0, \sqrt{\beta} L)} \right]_{x=L}$$

$$\dot{Q}_{\text{fin}} = \frac{kW th \theta_b}{\text{BesselI}(0, \sqrt{\beta} L)} \frac{d}{dx} \left[\text{BesselI}(0, \sqrt{\beta} x) \right]_{x=L}$$

$$\frac{d}{dx} \left[\text{BesselI}(0, \sqrt{\beta} x) \right] = \text{BesselI}'(1, \sqrt{\beta} x) \sqrt{\beta} / x$$

$$\dot{Q}_{\text{fin}} = kW th \theta_b \sqrt{\beta} \frac{\text{BesselI}'(1, \sqrt{\beta} L)}{\text{BesselI}(0, \sqrt{\beta} L)}$$

$$\underline{\dot{Q}_{\text{fin}}}$$

c) η_{fin}

$$\eta_{\text{fin}} = \frac{\dot{Q}_{\text{fin}}}{\bar{h} (2 \cdot \frac{th \cdot L}{2}) \theta_b} = \frac{kW th \theta_b \sqrt{\frac{2 \bar{h}}{kW}} \text{BesselI}(1, \sqrt{\frac{2 \bar{h}}{kW}} L)}{\bar{h} th L \theta_b}$$

$$\eta_{\text{fin}} = \frac{\sqrt{2 \bar{h} L}}{L \sqrt{\bar{h}}} \frac{\text{BesselI}(1, \sqrt{\frac{2 \bar{h}}{kW}} L)}{\text{BesselI}(0, \sqrt{\frac{2 \bar{h}}{kW}} L)}$$

$$\underline{\eta_{\text{fin}}}$$

equations determined here. Evaluated values and plots on next pages