Lab 9

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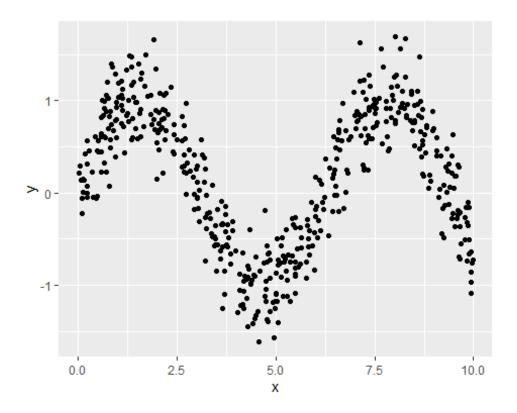
Here we will learn about trees, bagged trees and random forests. You can use the YARF package if it works, otherwise, use the randomForest package (the standard).

Let's take a look at the simulated sine curve data from practice lecture 12. Below is the code for the data generating process:

```
rm(list = ls())
n = 500
sigma = 0.3
x_min = 0
x_max = 10
f_x = function(x){sin(x)}
y_x = function(x, sigma){f_x(x) + rnorm(n, 0, sigma)}
x_train = runif(n, x_min, x_max)
y_train = y_x(x_train, sigma)
```

Plot an example dataset of size 500:

```
pacman::p_load(ggplot2)
ggplot(data.frame(x = x_train, y = y_train)) +
  geom_point(aes(x = x, y = y))
```



Create a test set of size 500 as well

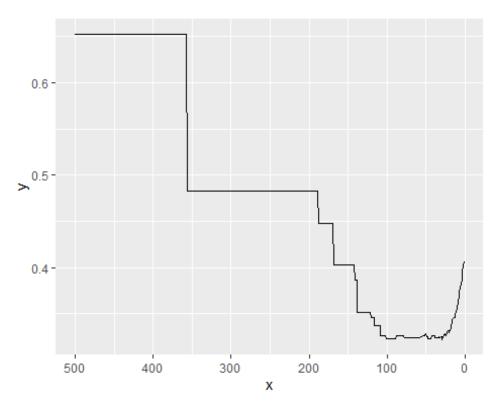
```
x_test = runif(n, x_min, x_max)
y_test = y_x(x_test, sigma)
```

Locate the optimal node size hyperparameter for the regression tree model. I believe you can use randomForest here by setting ntree = 1, replace = FALSE, sampsize = n (mtry is already set to be 1 because there is only one feature) and then you can set nodesize. Plot node size by out of sample SE

```
pacman::p_load(randomForest)
node sizes = 1:n
node_sizes
##
      [1]
             1
                 2
                      3
                               5
                                    6
                                         7
                                                      10
                                                           11
                                                               12
                                                                    13
                                                                         14
                                                                             15
                                                                                  16
                                                                                       17
18
##
    [19]
                          22
                              23
                                   24
                                        25
                                             26
                                                 27
                                                      28
                                                           29
                                                               30
                                                                    31
                                                                         32
                                                                             33
                                                                                  34
                                                                                       35
           19
                20
                     21
36
##
    [37]
                                   42
                                            44
                                                 45
                                                           47
                                                                    49
                                                                         50
                                                                             51
                                                                                  52
                                                                                       53
           37
                38
                     39
                         40
                              41
                                        43
                                                      46
                                                               48
54
##
           55
                56
                     57
                          58
                              59
                                   60
                                        61
                                            62
                                                 63
                                                      64
                                                           65
                                                               66
                                                                    67
                                                                         68
                                                                             69
                                                                                  70
                                                                                       71
    [55]
72
##
                                        79
                                                                                       89
    [73]
           73
                74
                     75
                         76
                              77
                                   78
                                            80
                                                 81
                                                      82
                                                           83
                                                               84
                                                                    85
                                                                         86
                                                                             87
                                                                                  88
90
                                                 99 100 101 102 103 104 105 106 107
##
    [91]
            91
                92
                     93
                         94
                              95
                                   96
                                        97
                                            98
108
```

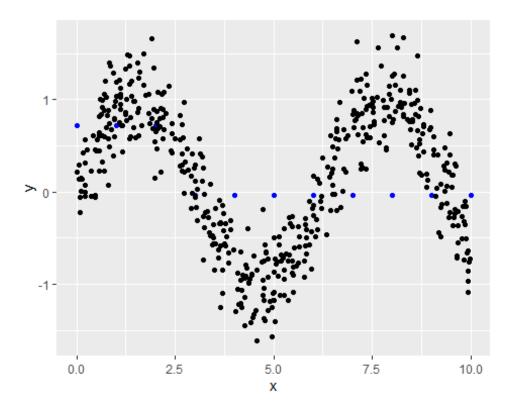
```
## [109] 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125
126
## [127] 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143
144
## [145] 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161
162
## [163] 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179
## [181] 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197
198
## [199] 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215
## [217] 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233
234
## [235] 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251
## [253] 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269
270
## [271] 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287
288
## [289] 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305
## [307] 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323
## [325] 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341
342
## [343] 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359
360
## [361] 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377
## [379] 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395
## [397] 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413
## [415] 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431
432
## [433] 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449
450
## [451] 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467
468
## [469] 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485
486
## [487] 487 488 489 490 491 492 493 494 495 496 497 498 499 500
se_by_node_sizes = array(NA, length(node_sizes))
for (i in 1:length(node sizes)) {
  rf_{mod} = randomForest(x = data.frame(x = x_train), y = y_train, ntree = 1,
replace = FALSE, sampsize = n, nodesize = node_sizes[i])
 y hat test = predict(rf mod, data.frame(x = x test))
 se by node_sizes[i] = sd(y_test - y_hat_test)
```

```
ggplot(data.frame(x = node_sizes, y = se_by_node_sizes)) +
  geom_line(aes(x = x, y = y)) +
  scale_x_reverse()
```



Plot the regression tree model with the optimal node size.

```
rf_mod = randomForest(x = data.frame(x = x_train), y = y_train, ntree = 1,
replace = FALSE, sampsize = n, nodesize = node_sizes[i])
resolution = 1
x_grid = seq(from = x_min, to = x_max, by = resolution)
g_x = predict(rf_mod,data.frame(x = x_grid))
ggplot(data.frame(x = x_grid, y = g_x)) +
    aes(x = x, y = y) +
    geom_point(color = "blue") +
    geom_point( data = data.frame(x = x_train, y = y_train), )
```



Provide the bias-variance decomposition of this DGP fit with this model. It is a lot of code, but it is in the practice lectures. If your three numbers don't add up within two significant digits, increase your resolution.

```
#TO-DO
rm(list = ls())
```

Take a sample of n = 2000 observations from the diamonds data.

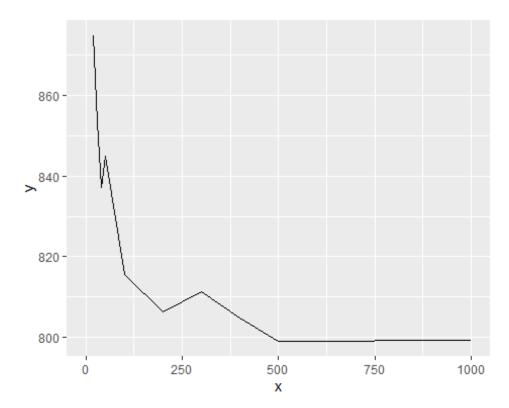
```
pacman::p_load(dplyr)
diamond_samp = diamonds %>%
  sample_n(2000)
```

find the bootstrap s_e for a RF model using 1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000 trees. If you are using the randomForest package, you can calculate oob residuals via e_oob = y_train - rf_mod\$predicted.

```
num_trees = c(1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000)
oob_se_by_num_trees = array(NA, length(num_trees))
for (i in 1:length(num_trees)) {
   rf_mod = randomForest(price ~., data = diamond_samp, ntree = num_trees[i])
   oob_se_by_num_trees[i] = sd(diamond_samp$price - rf_mod$predicted)
}

ggplot(data.frame(x = num_trees, y = oob_se_by_num_trees)) +
```

```
aes(x = x, y = y) +
geom_line()
## Warning: Removed 4 row(s) containing missing values (geom_path).
```

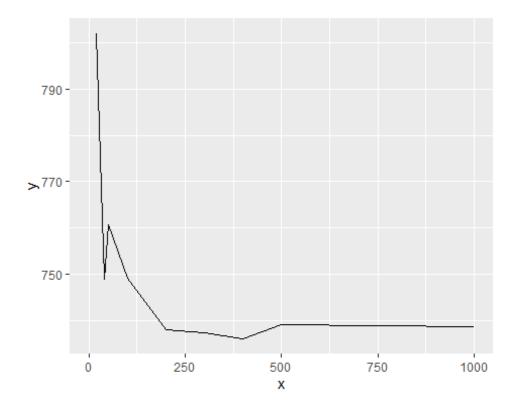


Using the diamonds data, find the bootstrap s_e for a bagged-tree model using 1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000 trees. If you are using the randomForest package, you can create the bagged tree model via setting an argument within the RF constructor function.

```
num_trees = c(1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000)
oob_se_by_num_trees_bag = array(NA, length(num_trees))
for (i in 1:length(num_trees)) {
    rf_mod = randomForest(price ~., data = diamond_samp, ntree = num_trees[i],
    mtry = ncol(diamond_samp) - 1)
    oob_se_by_num_trees_bag[i] = sd(diamond_samp$price - rf_mod$predicted)
}

ggplot(data.frame(x = num_trees, y = oob_se_by_num_trees_bag)) +
    aes(x = x, y = y) +
    geom_line()

## Warning: Removed 4 row(s) containing missing values (geom_path).
```



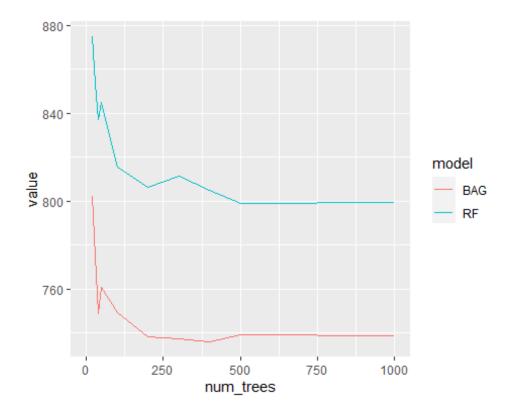
What is the percentage gain / loss in performance of the RF model vs bagged trees model?

```
(oob_se_by_num_trees - oob_se_by_num_trees_bag) / oob_se_by_num_trees_bag *
100

## [1] NA NA NA NA 9.070582 10.096128 11.771930
## [8] 11.068934 8.862912 9.237647 10.041291 9.357293 8.126215 8.223638
```

Plot bootstrap s_e by number of trees for both RF and bagged trees.

```
ggplot(rbind(data.frame(num_trees = num_trees, value = oob_se_by_num_trees,
model = "RF"), data.frame(num_trees = num_trees, value =
oob_se_by_num_trees_bag, model = "BAG"))) +
   geom_line(aes(x= num_trees, y = value, color = model))
## Warning: Removed 8 row(s) containing missing values (geom_path).
```

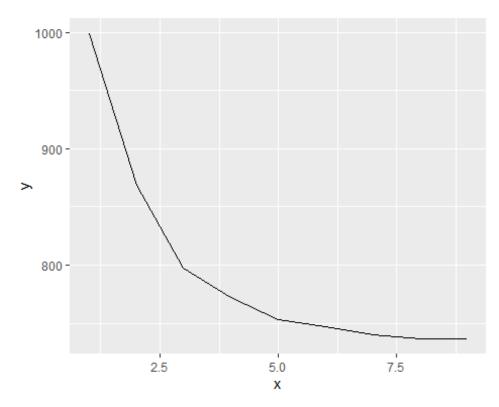


Build RF models for 500 trees using different mtry values: 1, 2, ... the maximum. That maximum will be the number of features assuming that we do not binarize categorical features if you are using randomForest or the number of features assuming binarization of the categorical features if you are using YARF. Calculate bootstrap s_e for all mtry values.

```
mtrys = 1: (ncol(diamond_samp)-1)
oob_se_by_mtrys = array(NA, length(mtrys))
for (i in 1:length(mtrys)) {

    rf_mod = randomForest(price ~., data = diamond_samp, mtry = mtrys[i])
    oob_se_by_mtrys[i] = sd(diamond_samp$price - rf_mod$predicted)
}

ggplot(data.frame(x = mtrys, y = oob_se_by_mtrys)) +
    aes(x = x, y = y) +
    geom_line()
```



```
rm(list = ls())
```

Take a sample of n = 2000 observations from the adult data.

```
pacman::p_load_gh("coatless/ucidata")
data(adult)
adult = na.omit(adult)

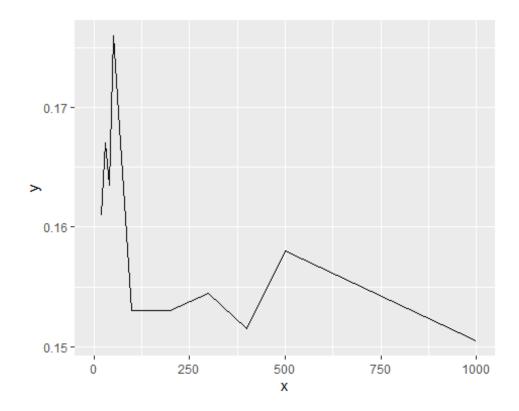
adult_samp = adult %>%
   sample n(2000)
```

Using the adult data, find the bootstrap misclassification error for an RF model using 1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000 trees.

```
num_trees = c(1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000)
oob_se_by_num_trees = array(NA, length(num_trees))
for (i in 1:length(num_trees)) {
   rf_mod = randomForest(income ~., data = adult_samp, ntree = num_trees[i])
   oob_se_by_num_trees[i] = mean(adult_samp$income != rf_mod$predicted)
}

ggplot(data.frame(x = num_trees, y = oob_se_by_num_trees)) +
   aes(x = x, y = y) +
   geom_line()

## Warning: Removed 4 row(s) containing missing values (geom_path).
```



Using the adult data, find the bootstrap misclassification error for a bagged-tree model using 1, 2, 5, 10, 20, 30, 40, 50, 100, 200, 300, 400, 500, 1000 trees.

What is the percentage gain / loss in performance of the RF model vs bagged trees model?

```
# Error when try to knit
#ggplot(rbind(data.frame(num_trees = num_trees, value = oob_se_by_num_trees,
model = "RF"), data.frame(num_trees = num_trees, value =
oob_se_by_num_trees_bag, model = "BAG"))) +
# geom_line(aes(x= num_trees, y = value, color = model))
```

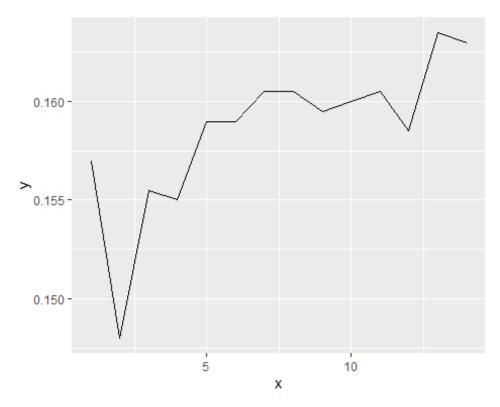
Plot bootstrap misclassification error by number of trees for both RF and bagged trees.

Build RF models for 500 trees using different mtry values: 1, 2, ... the maximum (see above as maximum is defined by the specific RF algorithm implementation).

```
mtrys = 1: (ncol(adult_samp)-1)
oob_se_by_mtrys = array(NA, length(mtrys))
for (i in 1:length(mtrys)) {

    rf_mod = randomForest(income ~., data = adult_samp, mtry = mtrys[i])
    oob_se_by_mtrys[i] = mean(adult_samp$income != rf_mod$predicted)
}

ggplot(data.frame(x = mtrys, y = oob_se_by_mtrys)) +
    aes(x = x, y = y) +
    geom_line()
```



```
rm(list = ls())
```

Write a function random_bagged_ols which takes as its arguments X and y with further arguments num_ols_models defaulted to 100 and mtry defaulted to NULL which then gets set within the function to be 50% of available features. This argument builds an OLS on a bootstrap sample of the data and uses only mtry < p of the available features. The function then returns all the 1m models as a list with size num_ols_models.

```
#num_ols_models = array(NA, 100)
#mtry = 1: ((ncol(adult_samp)-1)/2)
#random_bagged_ols = function(x, y){
```

```
# p = x / y
# for (i in 1: 100) {
#    if(mtry[i] < p){
#        num_ols_models[i] = mtry[i]
#    }
# }
# }</pre>
```

Load up the Boston Housing Data and separate into X and y.

```
pacman::p_load(MASS)
y = Boston$medv
X = Boston[,1:13]
```

Similar to lab 1, write a function that takes a matrix and punches holes (i.e. sets entries equal to NA) randomly with an argument prob missing.

```
punch_hole = function(X,prob_missing){
  n_r = nrow(X)
  n_c = ncol(X)
  M = matrix(rbinom(n_r *n_c, 1, prob_missing), nrow = n_r, ncol = n_c)
  X[M == 1] = NA
  X
}
```

Create a matrix Xmiss which is X but has missingness with probability of 10%.

```
Xmiss = punch_hole(X, 0.10)
Xmiss
##
                   zn indus chas
                                                         dis rad tax ptratio
           crim
                                    nox
                                           rm
                                                age
black
## 1
        0.00632
                 18.0
                      2.31
                               0 0.5380 6.575
                                               65.2
                                                     4.0900
                                                               1 296
                                                                        15.3
396.90
## 2
                               0 0.4690 6.421
        0.02731
                  0.0
                      7.07
                                               78.9
                                                     4.9671
                                                               2 242
                                                                        17.8
396.90
## 3
        0.02729
                               0 0.4690 7.185
                                                               2 242
                  0.0 7.07
                                               61.1 4.9671
                                                                        17.8
392.83
                                     NA 6.998 45.8
                                                                  NA
## 4
             NA
                  0.0
                       2.18
                               0
                                                     6.0622
                                                               3
                                                                        18.7
394.63
## 5
        0.06905
                  0.0
                       2.18
                               0 0.4580 7.147 54.2
                                                          NA
                                                               3 222
                                                                        18.7
396.90
## 6
        0.02985
                  0.0
                       2.18
                               0 0.4580 6.430
                                               58.7
                                                     6.0622
                                                               3 222
                                                                        18.7
394.12
## 7
                               0 0.5240 6.012 66.6
        0.08829
                       7.87
                                                     5.5605
                                                               5 311
                                                                        15.2
                   NA
395.60
                                                              NA 311
## 8
        0.14455
                 12.5 7.87
                               0 0.5240 6.172 96.1
                                                     5.9505
                                                                        15.2
396.90
## 9
             NA
                 12.5
                         NA
                               0 0.5240 5.631 100.0
                                                     6.0821
                                                               5 311
                                                                        15.2
386.63
## 10
        0.17004 12.5 7.87
                               0 0.5240 6.004 85.9 6.5921
                                                               5 311
                                                                        15.2
```

NA ## 11	0 22400	12 5	7 07	0	0 5240	c 277	04.2	6 2467	_	211	15.0
## 11 392.52	0.22489	12.5	7.87	0	0.5240	6.3//	94.3	6.3467	5	311	15.2
## 12 396.90	0.11747	12.5	7.87	0	0.5240	6.009	82.9	6.2267	NA	311	15.2
## 13 390.50	0.09378	12.5	7.87	0	0.5240	5.889	39.0	5.4509	5	NA	15.2
## 14 396.90	0.62976	NA	8.14	0	0.5380	5.949	61.8	4.7075	4	307	21.0
## 15 380.02	0.63796	0.0	8.14	NA	0.5380	6.096	84.5	4.4619	4	307	21.0
## 16 395.62	0.62739	0.0	8.14	0	0.5380	NA	56.5	4.4986	4	307	21.0
## 17 386.85	1.05393	0.0	8.14	NA	0.5380	5.935	29.3	4.4986	4	NA	21.0
## 18 386.75	0.78420	0.0	8.14	0	0.5380	5.990	NA	4.2579	4	307	NA
## 19 288.99	0.80271	0.0	NA	NA	0.5380	5.456	36.6	NA	4	307	21.0
## 20 390.95	NA	0.0	8.14	0	0.5380	5.727	69.5	3.7965	4	307	21.0
## 21 376.57	1.25179	0.0	NA	0	NA	5.570	98.1	3.7979	4	NA	21.0
## 22 392.53	0.85204	0.0	8.14	0	0.5380	5.965	89.2	4.0123	4	307	21.0
## 23 396.90	1.23247	NA	8.14	0	0.5380	6.142	91.7	3.9769	4	307	21.0
## 24 394.54	0.98843	0.0	8.14	0	0.5380	5.813	100.0	4.0952	4	307	21.0
## 25 394.33	0.75026	0.0	8.14	NA	0.5380	5.924	NA	4.3996	4	307	21.0
## 26 303.42	0.84054	0.0	8.14	0	0.5380	5.599	85.7	4.4546	4	307	21.0
## 27 376.88	0.67191	0.0	8.14	0	0.5380	5.813	90.3	NA	4	307	21.0
## 28 306.38	0.95577		8.14	0	0.5380	NA	88.8	4.4534	NA	307	21.0
## 29 387.94	0.77299		8.14	0	0.5380	6.495	94.4	4.4547	4	307	21.0
## 30 380.23	1.00245	0.0	8.14	0	0.5380	6.674	NA	NA	4	307	21.0
## 31 360.17	1.13081	0.0	8.14	0	0.5380	5.713	94.1	4.2330	4	307	21.0
## 32 376.73	NA	0.0	8.14	0	0.5380	6.072	100.0	4.1750	4	307	21.0
## 33 232.60	1.38799	0.0	8.14	0	0.5380	5.950	82.0	3.9900	4	307	21.0
## 34 358.77	NA	0.0	8.14	0	0.5380	5.701	95.0	3.7872	4	307	21.0
## 35	1.61282	0.0	8.14	0	0.5380	6.096	96.9	3.7598	4	NA	21.0

248.31	0.06417	0.0	F 06	0	0 4000	F 022	NIA	2 2602	_	270	10.2
## 36 396.90	0.06417	0.0	5.96	0	0.4990	5.933	NA	3.3603	5	279	19.2
## 37 377.56	0.09744	0.0	5.96	0	0.4990	5.841	61.4	3.3779	5	279	19.2
## 38	0.08014	0.0	5.96	0	0.4990	5.850	41.5	NA	5	279	NA
396.90 ## 39	0.17505	0.0	5.96	0	0.4990	NA	30.2	3.8473	5	NA	19.2
393.43 ## 40	0.02763	NA	2.95	0	0.4280	NA	21.8	5.4011	3	252	18.3
395.63 ## 41	0.03359	75.0	2.95	0	0.4280	7.024	15.8	5.4011	3	252	18.3
395.62 ## 42	NA	0.0	6.91	0	0.4480	6.770	2.9	5.7209	3	233	17.9
385.41 ## 43	0.14150	NA	6.91	0	0.4480	6.169	NA	5.7209	3	233	17.9
383.37 ## 44	0.15936	NA	6.91	0	0.4480	6.211	6.5	5.7209	3	233	17.9
394.46 ## 45	0.12269	0.0	NA	0	0.4480	6.069	40.0	5.7209	NA	233	17.9
389.39 ## 46	0.17142	0.0	6.91	9	0.4480	5.682	33.8	5.1004	3	233	17.9
NA ## 47	0.18836	0.0	6.91		0.4480		33.3	5.1004		233	17.9
396.90	0.10050	0.0	0.51	Ū	0.4400	3.700	33.3	J.1004	,	233	17.5
## 48 392.74	0.22927	0.0	6.91	0	0.4480	6.030	85.5	5.6894	3	NA	17.9
## 49 396.90	0.25387	0.0	6.91	0	0.4480	5.399	95.3	5.8700	3	233	17.9
## 50 396.90	0.21977	0.0	6.91	0	0.4480	5.602	62.0	6.0877	NA	233	17.9
## 51 NA	NA	21.0	5.64	0	0.4390	5.963	45.7	6.8147	4	243	16.8
## 52 393.97	NA	21.0	5.64	0	NA	6.115	63.0	6.8147	4	243	16.8
## 53	NA	NA	5.64	0	0.4390	6.511	21.1	6.8147	4	243	16.8
396.90 ## 54	0.04981	21.0	5.64	0	0.4390	5.998	NA	6.8147	4	243	NA
NA ## 55	NA	75.0	4.00	0	0.4100	5.888	47.6	7.3197	3	469	21.1
396.90 ## 56	0.01311	90.0	NA	0	0.4030	7.249	21.9	8.6966	NA	NA	17.9
395.93 ## 57	0.02055	85.0	0.74	NA	0.4100	6.383	35.7	9.1876	2	313	17.3
NA ## 58	0.01432	100.0	1.32	NA	0.4110	6.816	40.5	8.3248	5	256	15.1
392.90 ## 59	0.15445	25.0	5.13	0	0.4530	6.145	29.2	7.8148	8	NA	19.7
390.68 ## 60	0.10328	25.0	5.13	0	0.4530	5.927	47.2	6.9320	8	284	19.7

396.90			- 40			44			_		
## 61	0.14932	25.0	5.13	0	0.4530	5.741	66.2	7.2254	8	284	NA
395.11 ## 62	0.17171	25.0	5.13	a	0.4530	E 066	02.4	6.8185	0	284	19.7
## 62 378.08	0.1/1/1	25.0	5.15	Ø	0.4550	5.900	93.4	0.0103	0	204	19.7
## 63	0.11027	25.0	5.13	a	0.4530	6.456	67.8	NA	8	284	19.7
NA	0.1102	23.0	3.13	Ū	0.1550	0.150	07.0	1471	Ŭ		13.7
## 64	0.12650	25.0	5.13	0	0.4530	6.762	43.4	7.9809	8	284	19.7
395.58											
## 65	0.01951	17.5	1.38	0	0.4161	7.104	59.5	9.2229	3	216	18.6
393.24											
## 66	0.03584	80.0	3.37	0	0.3980	6.290	17.8	6.6115	4	337	16.1
396.90											
## 67	0.04379	80.0	3.37	0	NA	5.787	NA	6.6115	4	337	16.1
396.90		40 =	- o-	_						2.4-	10.0
## 68	0.05789	12.5	6.07	0	0.4090	5.8/8	21.4	6.4980	NA	345	18.9
396.21	0 13554	12 5	c 07	0	0 4000	F F04	26.0	C 4000	4	245	NA
## 69 396.90	0.13554	12.5	6.07	О	0.4090	5.594	36.8	6.4980	4	345	NA
## 70	0.12816	12.5	6.07	0	NΔ	5.885	33.0	6.4980	1	345	18.9
396.90	0.12010	12.5	0.07	U	IVA.	3.003	23.0	0.4500	7	J - J	10.5
## 71	0.08826	0.0	10.81	NA	0.4130	6.417	6.6	5.2873	4	305	19.2
383.73									-		
## 72	0.15876	NA	10.81	0	NA	NA	17.5	5.2873	4	305	19.2
376.94											
## 73	NA	0.0	10.81	0	0.4130	6.065	7.8	5.2873	4	NA	19.2
390.91											
## 74	0.19539	0.0	10.81	0	0.4130	6.245	6.2	5.2873	4	305	19.2
377.17									_		
## 75	0.07896	0.0	12.83	0	0.4370	6.273	6.0	4.2515	5	398	18.7
394.92	0 00543	0.0	42.02	•	0 4370	c 20c	45.0	4 5026	_	200	40.7
## 76 383.23	0.09512	0.0	12.83	0	0.4370	6.286	45.0	4.5026	5	398	18.7
## 77	0.10153	0.0	NA	a	0.4370	6 270	74.5	4.0522	NΙΛ	398	18.7
373.66	0.10133	0.0	IVA	Ø	0.4370	0.279	74.5	4.0322	IVA	330	10.7
## 78	0.08707	0.0	12.83	0	0.4370	NA	45.8	4.0905	5	398	18.7
386.96				Ū					_		
## 79	0.05646	0.0	12.83	0	0.4370	6.232	53.7	5.0141	5	398	18.7
386.40											
## 80	0.08387	0.0	12.83	NA	0.4370	5.874	36.6	4.5026	5	398	NA
396.06											
## 81	0.04113	NA	NA	0	0.4260	NA	33.5	5.4007	4	281	19.0
396.90											
## 82	0.04462	NA	4.86	0	0.4260	NA	70.4	NA	4	281	19.0
395.63	0.03650	25.0	4 06	•	N1.0	6 202	22.2	NI A	4		10.0
## 83 396.90	0.03659	25.0	4.86	Ø	NA	6.302	32.2	NA	4	NA	19.0
## 84	0.03551	25 0	4.86	a	0.4260	6 167	NA	5.4007	4	NA	19.0
390.64	0.00001	23.0	4.00	ð	0.4200	0.107	INA	J.+00/	4	IVA	17.0
## 85	0.05059	9.9	4.49	a	0.4490	6.389	48.0	4.7794	3	247	18.5
05	0.0000	0.0		J		5.555				,	

396.90									_		10 =
## 86 392.30	0.05735	0.0	4.49	NA	0.4490	6.630	56.1	4.4377	3	247	18.5
## 87	NA	0.0	4.49	a	0.4490	6 015	45.1	4.4272	2	247	18.5
395.99	IVA	0.0	7,72	U	0.4450	0.013	73.1	7.72/2	,	27/	10.5
## 88	0.07151	0.0	4.49	0	NA	6.121	56.8	3.7476	3	247	18.5
395.15											
## 89	0.05660	0.0	3.41	0	0.4890	7.007	86.3	3.4217	2	270	17.8
NA											
## 90	0.05302	0.0	3.41	0	0.4890	7.079	63.1	3.4145	2	270	17.8
396.06											
## 91	0.04684	0.0	3.41	NA	0.4890	6.417	66.1	3.0923	2	NA	17.8
392.18	0 02022	0 0	2 44	•	N. A.	6 405	N1.0	2 0024	_	270	NA
## 92	0.03932	0.0	3.41	0	NA	6.405	NA	3.0921	2	270	NA
393.55 ## 93	0.04203	NΙΛ	15.04	a	0.4640	6 112	53.6	3.6659	1	270	18.2
## 93 395.01	0.04203	NA	15.04	О	0.4640	0.442	55.0	3.0039	4	270	10.2
## 94	0.02875	28 0	15.04	NΔ	0.4640	6 211	28.9	3,6659	4	NA	18.2
NA	0.02075	20.0	13.04	IVA	0.4040	0.211	20.5	3.0033		INA	10.2
## 95	0.04294	28.0	15.04	0	NA	6.249	77.3	3.6150	NA	270	18.2
396.90											
## 96	NA	0.0	2.89	0	0.4450	NA	57.8	3.4952	2	276	18.0
357.98											
## 97	0.11504	0.0	2.89	0	0.4450	NA	69.6	3.4952	2	276	NA
391.83											
## 98	0.12083	0.0	2.89	0	NA	NA	NA	3.4952	2	276	18.0
396.90				_					_		
## 99	0.08187	0.0	2.89	0	0.4450	7.820	NA	NA	2	276	18.0
393.53 ## 100	0.06860	0.0	2.89	a	0.4450	7 116	NA	3.4952	2	276	NA
396.90	0.00000	0.0	2.09	О	0.4450	7.410	IVA	3.4932	2	2/0	INA
## 101	0.14866	0.0	8.56	a	0.5200	6.727	79.9	NA	5	384	20.9
394.76	0.1-000	0.0	0.50	Ū	0.5200	0.727	,,,,	IVA	,	50-	20.5
## 102	0.11432	0.0	8.56	0	0.5200	6.781	71.3	2.8561	5	NA	20.9
395.58											
## 103	0.22876	0.0	8.56	0	0.5200	6.405	85.4	2.7147	5	NA	20.9
70.80											
## 104	0.21161	0.0	NA	0	0.5200	6.137	87.4	2.7147	5	384	NA
394.47											
## 105	0.13960	0.0	8.56	0	0.5200	6.167	90.0	NA	5	384	20.9
392.69	0 12262	0.0	0 56	0	0 5200	г ог1	06.7	2 1000	_	204	20.0
## 106 394.05	0.13262	0.0	8.56	0	0.5200	5.851	96.7	2.1069	5	384	20.9
## 107	0.17120	0.0	8.56	a	0 5200	5 836	01 0	2.2110	5	384	20.9
395.67	0.1/120	0.0	0.50	Ð	0.5200	J.030	21.3	2.2110	ر	J04	20.9
## 108	NA	0.0	8.56	a	0.5200	6.127	NA	2.1224	NΔ	384	20.9
387.69	14/1	3.0	0.50	J	3.3200	3,12,	147 (_,		55.	_0.5
## 109	0.12802	0.0	8.56	0	0.5200	6.474	97.1	2.4329	5	384	20.9
395.24											
## 110	0.26363	0.0	8.56	0	0.5200	6.229	91.2	2.5451	5	384	20.9

391.23 ## 111	0.10793	0.0	8.56	0	0.5200	6 10E	E 1 1	2 7770	_	204	20.9
393.49	0.10/93	0.0	0.50	О	0.5200	0.195	54.4	2.7778	5	384	20.9
## 112 395.59	0.10084	0.0	10.01	0	0.5470	6.715	81.6	2.6775	6	432	17.8
## 113 NA	0.12329	0.0	10.01	0	0.5470	5.913	NA	2.3534	6	432	17.8
## 114 396.90	0.22212	0.0	NA	NA	0.5470	6.092	95.4	2.5480	6	432	17.8
## 115 388.74	0.14231	0.0	10.01	NA	0.5470	6.254	84.2	2.2565	6	432	17.8
## 116 344.91	0.17134	0.0	10.01	0	NA	5.928	88.2	2.4631	6	432	17.8
## 117 393.30	0.13158	0.0	10.01	0	0.5470	6.176	72.5	NA	6	432	NA
## 118 NA	NA	0.0	NA	0	0.5470	6.021	82.6	2.7474	NA	432	17.8
## 119 338.63	0.13058	0.0	10.01	0	0.5470	5.872	NA	NA	NA	432	17.8
## 120	0.14476	0.0	10.01	0	0.5470	5.731	65.2	2.7592	6	432	17.8
391.50 ## 121	0.06899	0.0	25.65	0	0.5810	5.870	69.7	NA	2	188	19.1
389.15 ## 122	NA	NA	25.65	NA	0.5810	6.004	84.1	2.1974	2	188	19.1
377.67 ## 123	0.09299	0.0	25.65	0	0.5810	5.961	92.9	2.0869	2	188	19.1
378.09 ## 124	0.15038	0.0	25.65	0	0.5810	5.856	97.0	NA	2	188	19.1
370.31 ## 125	0.09849	0.0	25.65	0	0.5810	5.879	95.8	NA	2	188	NA
379.38 ## 126	0.16902	0.0	25.65	0	NA	5.986	88.4	1.9929	2	188	19.1
385.02 ## 127	0.38735	0.0	25.65	0	0.5810	5.613	95.6	1.7572	2	188	19.1
359.29 ## 128	0.25915	0.0	21.89	0	0.6240	5.693	NA	1.7883	4	437	21.2
392.11 ## 129	0.32543	NA	21.89	NA	0.6240	6.431	98.8	1.8125	4	437	21.2
396.90 ## 130	0.88125	0.0	21.89	0	0.6240	5.637	94.7	NA	4	437	21.2
396.90 ## 131	0.34006	0.0	21.89	0	0.6240	6.458	98.9	2.1185	4	NA	21.2
395.04 ## 132	1.19294	0.0	21.89	0	0.6240	NA	97.7	NA	4	437	21.2
NA ## 133	0.59005	0.0	21.89	0	0.6240	6.372	NA	2.3274	4	437	21.2
385.76 ## 134	NA		21.89					2.4699		437	21.2
388.69 ## 135	NA		21.89		0.6240					437	21.2

262.76 ## 136												
394.67 ## 137 NA		0 55770	0.0	24 00	•		6 225	00.0	2 4407		427	24 2
## 137 NA 0.0 21.89 NA 0.6240 5.942 93.5 NA 4 437 NA 378.25		0.55//8	0.0	21.89	0	NA	6.335	98.2	2.110/	4	43/	21.2
378.25 ## 138 0.35233 0.0 21.89 0 0.6240 6.454 98.4 1.8498 4 437 21.2 394.08 ## 139 0.24980 0.24980 0.0 21.89 0 0.6240 6.151 97.9 1.6687 4 NA 21.2 396.90 ## 141 0.29090 0.0 21.89 0 0.6240 6.174 93.6 1.6119 4 NA 21.2 388.08 ## 142 338.08 ## 143 332.105 0.0 19.58 1 0.8710 5.408 100.0 1.4394 4 437 NA 396.90 ## 144 NA 0.0 19.58 0 0.8710 5.468 100.0 1.4118 5 403 14.7 396.90 ## 145 2.77974 0.0 19.58 0 0.8710 4.903 97.8 1.3459 NA NA 14.7 396.90 ## 146 2.37934 0.0 19.58 0 0.8710 6.130 100.0 1.4118 5 403 14.7 169.27 ## 148 NA 0.0 19.58 0 0.8710 6.130 100.0 1.5166 5 403 14.7 169.27 ## 148 NA 0.0 19.58 0 0.8710 5.628 100.0 1.5166 5 403 14.7 169.27 ## 149 2.33099 0.0 19.58 0 0.8710 5.628 100.0 1.5166 5 403 14.7 391.71 ## 149 2.33099 0.0 19.58 0 0.8710 5.186 NA 1.5296 5 NA 14.7 3956.99 ## 150 3.73397 0.0 19.58 0 0.8710 5.186 NA 1.5296 5 NA 14.7 391.71 ## 149 2.33099 0.0 19.58 0 0.8710 5.186 NA 1.5296 5 NA 14.7 391.71 ## 150 3.72.80 ## 151 1.65660 0.0 19.58 0 0.8710 5.404 100.0 1.5166 5 403 14.7 372.80 ## 152 1.49632 0.0 19.58 0 0.8710 5.022 NA 1.6180 5 403 14.7 372.80 ## 154 2.14918 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 154 2.14918 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 1.49632 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.41385 NA 19.58 0 0.8710 5.012 NA 1.6180 5 403 14.7 372.80 ## 155 NA 1.479 3.410 1.470 3.410 4.410		NΑ	0 0	21 90	МΛ	0 6240	E 0/12	02 5	NΑ	1	127	NΛ
## 138		INA	0.0	21.05	IVA	0.0240	3.342	33.3	IVA	4	437	IVA
394.08		0 35333	0 0	21 20	a	0 6240	6 151	08 /	1 9/09	1	127	21 2
## 139		0.33233	0.0	21.09	U	0.0240	0.434	30.4	1.0490	4	437	21.2
392.04 ## 140		0 24980	a a	21 89	а	0 6240	5 857	98 2	1 6686	4	437	21 2
## 140		0.24300	0.0	21.05	Ū	0.02-0	3.037	30.2	1.0000		737	21.2
396.90 ## 141		0.54452	NΔ	21.89	9	0.6240	6.151	97.9	1.6687	4	NΔ	21.2
## 141		0.552			·	0.02.0	0.131	2, 12	2,000,	·		
388.08 ## 142		0.29090	0.0	21.89	0	0.6240	6.174	93.6	1.6119	4	NA	21.2
## 142					•				_,,,			
## 143		1.62864	0.0	21.89	0	0.6240	NA	100.0	1.4394	4	437	NA
## 144												
## 144	## 143	3.32105	0.0	19.58	1	0.8710	5.403	100.0	1.3216	5	NA	14.7
## 145	396.90											
## 145	## 144	NA	0.0	19.58	0	0.8710	5.468	100.0	1.4118	5	403	14.7
## 146	396.90											
## 146	## 145	2.77974	0.0	19.58	0	0.8710	4.903	97.8	1.3459	NA	NA	14.7
172.91 ## 147	396.90											
## 147	## 146	2.37934	0.0	19.58	0	0.8710	6.130	100.0	1.4191	NA	403	14.7
## 148	172.91											
## 148	## 147	2.15505	0.0	19.58	0	0.8710	5.628	100.0	1.5166	5	403	14.7
391.71 ## 149	169.27											
## 149		NA	0.0	19.58	0	0.8710	4.926	95.7	1.4608	5	403	14.7
## 150												
## 150		2.33099	0.0	19.58	0	0.8710	5.186	NA	1.5296	5	NA	14.7
## 151 1.65660 0.0 19.58 0 0.8710 6.122 NA 1.6180 5 403 14.7 372.80 ## 152 1.49632 0.0 19.58 0 0.8710 5.404 100.0 1.5916 NA 403 14.7 341.60 ## 153 1.12658 0.0 19.58 1 0.8710 5.012 88.0 NA 5 403 14.7 NA ## 154 2.14918 NA 19.58 0 0.8710 5.709 98.5 1.6232 NA 403 NA 261.95 ## 155 1.41385 NA 19.58 1 NA 6.129 NA 1.7494 5 403 14.7 321.02 ## 156 NA 0.0 19.58 1 0.8710 6.152 82.6 1.7455 5 403 NA 88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89												
## 151 1.65660 0.0 19.58 0 0.8710 6.122 NA 1.6180 5 403 14.7 372.80 ## 152 1.49632 0.0 19.58 0 0.8710 5.404 100.0 1.5916 NA 403 14.7 341.60 ## 153 1.12658 0.0 19.58 1 0.8710 5.012 88.0 NA 5 403 14.7 NA ## 154 2.14918 NA 19.58 0 0.8710 5.709 98.5 1.6232 NA 403 NA 261.95 ## 155 1.41385 NA 19.58 1 NA 6.129 NA 1.7494 5 403 14.7 321.02 ## 156 NA 0.0 19.58 1 0.8710 6.152 82.6 1.7455 5 403 NA 88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		2.73397	0.0	19.58	0	0.8710	5.597	94.9	1.5257	5	403	NA
## 152					_					_		
## 152 1.49632 0.0 19.58 0 0.8710 5.404 100.0 1.5916 NA 403 14.7 341.60 ## 153 1.12658 0.0 19.58 1 0.8710 5.012 88.0 NA 5 403 14.7 NA ## 154 2.14918 NA 19.58 0 0.8710 5.709 98.5 1.6232 NA 403 NA 261.95 ## 155 1.41385 NA 19.58 1 NA 6.129 NA 1.7494 5 403 14.7 321.02 ## 156 NA 0.0 19.58 1 0.8710 6.152 82.6 1.7455 5 403 NA 88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7		1.65660	0.0	19.58	0	0.8710	6.122	NA	1.6180	5	403	14.7
341.60 ## 153		4 40633	0 0	40 50	•	0 0740	- 404	400.0	4 5046		400	44.7
## 153 1.12658 0.0 19.58 1 0.8710 5.012 88.0 NA 5 403 14.7 NA ## 154 2.14918 NA 19.58 0 0.8710 5.709 98.5 1.6232 NA 403 NA 261.95 ## 155 1.41385 NA 19.58 1 NA 6.129 NA 1.7494 5 403 14.7 321.02 ## 156 NA 0.0 19.58 1 0.8710 6.152 82.6 1.7455 5 403 NA 88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		1.49632	0.0	19.58	0	0.8/10	5.404	100.0	1.5916	NA	403	14./
MA ## 154		1 12650	0 0	10 50	1	0 0710	F 013	00 0	NI A	_	402	14 7
## 154 2.14918 NA 19.58 0 0.8710 5.709 98.5 1.6232 NA 403 NA 261.95 ## 155 1.41385 NA 19.58 1 NA 6.129 NA 1.7494 5 403 14.7 321.02 ## 156 NA 0.0 19.58 1 0.8710 6.152 82.6 1.7455 5 403 NA 88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		1.12658	0.0	19.58	Т	0.8/10	5.012	88.0	NA	5	403	14.7
261.95 ## 155		2 1/010	NΙΛ	10 E0	a	0 0710	E 700	00 E	1 6222	NIA	102	NΑ
## 155		2.14918	INA	19.56	О	0.8/10	5.769	90.5	1.0232	IVA	403	INA
321.02 ## 156		1 /1205	NΙΛ	10 50	1	NΙΛ	6 120	NΑ	1 7/0/	_	102	1/1 7
## 156 NA 0.0 19.58 1 0.8710 6.152 82.6 1.7455 5 403 NA 88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		1.41303	IVA	19.30		IVA	0.129	INA	1.7434	ر	403	14.7
88.01 ## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		NΔ	a a	19 58	1	0 8710	6 152	82 6	1 7455	5	103	NΔ
## 157 NA 0.0 19.58 0 0.8710 5.272 94.0 NA 5 403 14.7 88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		IVA	0.0	17.50		3.0710	0.102	02.0	10,400	,	- 05	IVA
88.63 ## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		NΔ	0.0	19.58	a	0.8710	5.272	94.0	NΔ	5	403	14.7
## 158 1.22358 0.0 NA 0 0.6050 6.943 97.4 NA 5 403 14.7 363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		14/1	3.3	12.50	J	3.3, 10	J . L , L	21.0	14/3	,	.55	,
363.43 ## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89		1,22358	0.0	NΑ	0	0.6050	6.943	97.4	NΑ	5	403	14.7
## 159 1.34284 0.0 19.58 0 0.6050 6.066 100.0 1.7573 5 403 14.7 353.89			3.3		J	2.2020		• 1				,
353.89		1.34284	0.0	19.58	0	0.6050	6.066	100.0	1.7573	5	403	14.7
					ĺ							
## 160 1.42502 0.0 19.58 0 0.8710 6.510 100.0 1.7659 5 403 14.7	## 160	1.42502	0.0	19.58	0	0.8710	6.510	100.0	1.7659	5	403	14.7

364.31	1.27346	0.0	19.58	1	0 6050	6 250	02.6	1 7004	5 403	14.7
## 161 338.92	1.2/346	0.0	19.58	1	0.6050	6.250	92.6	1.7984	5 403	14.7
## 162	1.46336	0.0	19.58	0	NA	7.489	90.8	1.9709	5 403	14.7
374.43										
## 163	1.83377	0.0	19.58	1	0.6050	7.802	98.2	2.0407	5 403	14.7
389.61 ## 164	1.51902	a a	19.58	1	0.6050	8 375	93.9	NA	5 403	14.7
388.45	1.31302	0.0	10.00	_	0.0050	0.575	23.2	IVA	J 1 0J	14.7
## 165	2.24236	NA	19.58	0	0.6050	5.854	91.8	2.4220	5 403	14.7
395.11										
## 166	2.92400	0.0	19.58	0	0.6050	6.101	93.0	2.2834	5 403	14.7
240.16 ## 167	2.01019	NΙΛ	19.58	NΙΛ	0.6050	7 020	96.2	2.0459	5 NA	14.7
369.30	2.01019	INA	19.50	INA	0.0050	7.929	90.2	2.0439	5 IVA	14.7
## 168	1.80028	0.0	NA	0	0.6050	5.877	79.2	2.4259	5 403	14.7
227.61										
## 169	2.30040	0.0	19.58	0	0.6050	6.319	96.1	2.1000	5 403	NA
297.09										
## 170	2.44953	0.0	19.58	0	0.6050	6.402	95.2	2.2625	5 403	14.7
330.04 ## 171	1.20742	a a	19.58	a	0.6050	5 875	NA	2.4259	5 403	14.7
292.29	1.20742	0.0	10.00	U	0.0030	3.073	NA.	2.7233	J 1 03	14.7
## 172	2.31390	0.0	19.58	0	0.6050	5.880	97.3	2.3887	5 403	14.7
348.13										
## 173	0.13914	0.0	4.05	0	NA	5.572	88.5	2.5961	5 NA	16.6
396.90	0 00170	0 0	4 05	0	0 5100	NIA	04 1	2 (462	F 20C	16.6
## 174 395.50	0.09178	0.0	4.05	0	0.5100	NA	84.1	2.6463	5 296	16.6
## 175	0.08447	0.0	4.05	0	0.5100	NA	68.7	2.7019	5 296	NA
393.23										
## 176	0.06664	0.0	4.05	0	NA	6.546	NA	3.1323	5 296	16.6
390.96										
## 177	NA	0.0	4.05	0	0.5100	6.020	47.2	NA	5 296	16.6
393.23 ## 178	0.05425	a a	4.05	NΔ	0.5100	6.315	73 4	NA	5 NA	16.6
395.60	0.05425	0.0	7.05	11/-1	3.3100	3.313	, , , , ,	11/7	J 11/A	10.0
## 179	0.06642	0.0	NA	0	0.5100	6.860	74.4	2.9153	5 296	16.6
NA										
## 180	0.05780	0.0	2.46	0	0.4880	6.980	58.4	2.8290	3 193	17.8
396.90	0 06500	0.0	2 40	0	0 4000	7 765	02.2	2 7410	NA 102	17 0
## 181 NA	0.06588	0.0	2.46	Ø	0.4880	7.765	83.3	2.7410	NA 193	17.8
## 182	NA	0.0	2.46	0	0.4880	6.144	62.2	2.5979	NA NA	17.8
396.90			_,.3	J	,					
## 183	0.09103	0.0	NA	0	0.4880	NA	92.2	2.7006	3 193	NA
394.12									_	
## 184	0.10008	0.0	2.46	0	NA	6.563	95.6	2.8470	3 193	17.8
396.90 ## 185	0.08308	0.0	2.46	a	0.4880	5 604	80 S	2.9879	3 193	17.8
ππ 10Э	0.00000	0.0	2.40	Ð	0.4000	3.004	0.00	2.70/3	J 193	17.0

391.00 ## 186	0.06047	0.0	2.46	0	0.4880	C 153	68.8	3.2797	3 193	17.8	
387.11	0.00047	0.0	2.40	Ø	0.4000	0.133	00.0	3.2/9/	3 133	17.0	
## 187 392.63	0.05602	0.0	2.46	0	0.4880	7.831	53.6	3.1992	3 193	17.8	
## 188 393.87	0.07875	45.0	3.44	NA	0.4370	6.782	41.1	3.7886	5 398	NA	
## 189	0.12579	45.0	3.44	0	0.4370	6.556	29.1	4.5667	5 398	15.2	
382.84 ## 190	0.08370	45.0	3.44	0	0.4370	7.185	38.9	4.5667	5 398	15.2	
396.90 ## 191	0.09068	45.0	3.44	0	0.4370	NA	21.5	6.4798	5 398	15.2	
377.68 ## 192	0.06911	45.0	3.44	0	0.4370	6.739	30.8	6.4798	5 NA	NA	
389.71 ## 193	NA	45.0	3.44	NA	0.4370	7.178	26.3	6.4798	5 398	15.2	
390.49			2 22	•					4 045	45.4	
## 194 393.37	0.02187	60.0	2.93	0	0.4010	6.800	9.9	6.2196	1 265	15.6	
## 195 376.70	0.01439	60.0	2.93	0	0.4010	6.604	18.8	6.2196	1 265	15.6	
## 196 394.23	0.01381	80.0	0.46	0	0.4220	7.875	NA	5.6484	4 255	14.4	
## 197 396.90	0.04011	80.0	1.52	0	0.4040	7.287	34.1	7.3090	2 329	12.6	
## 198	0.04666	80.0	1.52	0	0.4040	7.107	36.6	7.3090	2 329	12.6	
354.31 ## 199	0.03768	80.0	NA	0	0.4040	7.274	38.3	7.3090	2 329	12.6	
392.20 ## 200	0.03150	95.0	1.47	0	0.4030	NA	15.3	7.6534	NA 402	17.0	
396.90 ## 201	0.01778	95.0	1.47	0	0.4030	7.135	13.9	7.6534	3 402	17.0	
NA ## 202	0.03445	82.5	2.03	0	NA	6.162	38.4	6.2700	2 348	14.7	
393.77 ## 203	0.02177	82.5	2.03	0	0.4150	7.610	15.7	6.2700	2 348	14.7	
NA ## 204	0.03510				0.4161					14.7	
392.78									4 224		
## 205 390.55	0.02009	95.0	2.68	0	0.4161	8.034	NA	5.1180	4 224	NA	
## 206 396.90	0.13642	0.0	10.59	0	0.4890	5.891	22.3	3.9454	4 277	18.6	
## 207 394.87	0.22969	0.0	10.59	0	0.4890	6.326	52.5	NA	4 277	18.6	
## 208	0.25199	0.0	10.59	0	0.4890	5.783	72.7	4.3549	4 277	18.6	
NA ## 209	0.13587	0.0	10.59	1	0.4890	6.064	NA	4.2392	4 277	18.6	
381.32 ## 210	0.43571	0.0	10.59	1	0.4890	5.344	100.0	3.8750	4 277	18.6	

NA ## 211	0.17446	9 9	10.59	1	0.4890	5 960	92.1	3.8771	4 277	18.6
393.25	0.1/440	0.0	10.33		0.4650	3.900	92.1	3.0//1	4 2//	10.0
## 212 395.24	0.37578	0.0	10.59	1	0.4890	5.404	88.6	3.6650	4 277	18.6
## 213 390.94	0.21719	0.0	10.59	1	0.4890	5.807	53.8	3.6526	4 277	18.6
## 214 385.81	0.14052	NA	10.59	0	0.4890	6.375	32.3	NA	4 277	18.6
## 215 348.93	0.28955	NA	10.59	0	0.4890	5.412	9.8	3.5875	4 277	NA
## 216 393.63	0.19802	0.0	10.59	0	0.4890	6.182	42.4	3.9454	4 NA	18.6
## 217 NA	NA	NA	13.89	1	0.5500	5.888	56.0	NA	5 276	16.4
## 218 392.78	NA	NA	13.89	0	NA	6.642	85.1	3.4211	5 276	16.4
## 219 NA	0.11069	0.0	13.89	1	0.5500	5.951	93.8	2.8893	5 276	16.4
## 220 393.74	0.11425	0.0	13.89	1	0.5500	NA	NA	3.3633	5 276	16.4
## 221 NA	NA	0.0	6.20	1	0.5070	6.951	88.5	2.8617	8 307	NA
## 222 395.24	0.40771	NA	6.20	1	0.5070	6.164	91.3	3.0480	8 307	17.4
## 223 390.39	0.62356	0.0	6.20	1	0.5070	6.879	77.7	3.2721	8 307	17.4
## 224 396.90	0.61470	0.0	6.20	0	0.5070	6.618	80.8	3.2721	8 NA	17.4
## 225 385.05	0.31533	NA	6.20	0	0.5040	8.266	NA	2.8944	NA 307	17.4
## 226 382.00	0.52693	0.0	6.20	0	0.5040	8.725	83.0	NA	8 307	17.4
## 227 387.38	0.38214	0.0	6.20	0	0.5040	8.040	86.5	NA	8 307	17.4
## 228 372.08	0.41238	NA	6.20	0	0.5040	7.163	79.9	3.2157	8 307	17.4
## 229 377.51	0.29819	0.0	6.20	NA	0.5040	7.686	17.0	3.3751	8 307	17.4
## 230 380.34	0.44178	0.0	6.20	0	NA	6.552	21.4	3.3751	8 307	17.4
## 231 378.35	NA	0.0	6.20	0	0.5040	5.981	68.1	3.6715	8 307	17.4
## 232 376.14	0.46296	0.0	6.20	0	0.5040	NA	76.9	3.6715	8 307	17.4
## 233 385.91	0.57529	0.0	6.20	NA	0.5070	8.337	73.3	3.8384	8 307	17.4
## 234 378.95	0.33147	0.0	6.20	0	0.5070	8.247	70.4	3.6519	8 307	17.4
## 235	0.44791	0.0	6.20	1	0.5070	6.726	66.5	3.6519	8 307	17.4

360.20 ## 236	0.33045	0.0	6.20	a	0.5070	NA	NA	3.6519	8 307	17.4
376.75	0.33043	0.0	0.20	Ø	0.5070	INA	IVA	3.0319	0 307	17.4
## 237 388.45	0.52058	0.0	6.20	1	0.5070	NA	76.5	4.1480	8 307	17.4
## 238 390.07	0.51183	0.0	6.20	0	0.5070	7.358	71.6	4.1480	8 307	17.4
## 239 379.41	0.08244	30.0	4.93	0	0.4280	6.481	18.5	6.1899	6 300	16.6
## 240	0.09252	30.0	NA	0	0.4280	6.606	42.2	6.1899	6 300	16.6
383.78 ## 241	0.11329	30.0	4.93	0	NA	6.897	54.3	6.3361	6 300	16.6
391.25 ## 242	0.10612	30.0	4.93	0	0.4280	6.095	65.1	6.3361	6 300	16.6
394.62 ## 243	0.10290	30.0	4.93	NA	0.4280	6.358	52.9	7.0355	NA 300	16.6
NA ## 244	NA	30.0	4.93	0	0.4280	NA	7.8	7.0355	6 NA	16.6
374.71 ## 245	0.20608	22.0	5.86	0	0.4310	5.593	76.5	7.9549	7 330	19.1
372.49 ## 246	0.19133	22.0	5.86	0	NA	5.605	70.2	7.9549	7 330	19.1
389.13 ## 247	0.33983	22.0	5.86	0	0.4310	6.108	34.9	8.0555	7 330	19.1
NA										
## 248 376.14	0.19657	22.0	5.86	0	0.4310	6.226	NA	8.0555	7 330	19.1
## 249 374.71	0.16439	22.0	5.86	0	0.4310	6.433	49.1	7.8265	NA 330	19.1
## 250 NA	NA	22.0	5.86	0	NA	6.718	NA	7.8265	7 330	19.1
## 251 396.28	NA	22.0	5.86	0	0.4310	6.487	13.0	NA	7 330	19.1
## 252	0.21409	22.0	5.86	0	0.4310	6.438	NA	7.3967	7 330	NA
377.07 ## 253	0.08221	22.0	5.86	0	0.4310	6.957	6.8	8.9067	NA 330	19.1
386.09 ## 254	NA	22.0	5.86	0	0.4310	8.259	NA	8.9067	7 330	19.1
396.90 ## 255	0.04819	80.0	3.64	0	0.3920	6.108	32.0	9.2203	1 315	16.4
392.89 ## 256	0.03548	80.0	3.64	0	0.3920	5.876	19.1	9.2203	1 315	16.4
395.18 ## 257	0.01538		3.75					6.3361	3 244	15.9
386.34										
## 258 389.70	0.61154		3.97	0	0.6470				5 264	13.0
## 259 383.29	0.66351	20.0	3.97	0	0.6470	NA	100.0	1.8946	5 264	13.0
	0.65665	NA	3.97	0	0.6470	6.842	NA	2.0107	5 264	13.0

391.93 ## 261	0.54011	20.0	3.97	NA 0.6470 7.20	3 81.8	NA	5 264	13.0
392.80	0.54011	20.0	3.97	NA 0.6470 7.20	01.0	NA	5 204	13.0
## 262 388.37	NA	20.0	3.97	0 NA 7.52	0 89.4	2.1398	5 264	13.0
## 263 NA	0.52014	20.0	3.97	0 0.6470 8.39	8 91.5	2.2885	5 264	13.0
## 264 393.42	0.82526	20.0	3.97	0 NA 7.32	7 94.5	2.0788	5 264	13.0
## 265 387.89	0.55007	20.0	3.97	0 0.6470 7.20	6 91.6	1.9301	5 264	13.0
## 266 NA	0.76162	20.0	3.97	0 0.6470 5.56	0 NA	1.9865	5 264	13.0
## 267 384.07	0.78570	20.0	3.97	0 0.6470 7.01	4 84.6	2.1329	5 264	13.0
## 268 384.54	NA	20.0	3.97	NA 0.5750 8.29	7 67.0	2.4216	5 264	13.0
## 269 390.30	0.54050	20.0	3.97	0 0.5750 7.47	0 52.6	2.8720	5 264	13.0
## 270 391.34	0.09065	20.0	6.96	1 0.4640 5.92	0 61.5	3.9175	3 223	NA
## 271 NA	0.29916	20.0	6.96	0 0.4640 5.85	6 42.1	4.4290	3 NA	18.6
## 272 396.90	0.16211	20.0	6.96	NA 0.4640 6.24	0 16.3	4.4290	3 223	18.6
## 273 394.96	0.11460	20.0	6.96	0 0.4640 6.53	8 58.7	3.9175	3 223	18.6
## 274 NA	0.22188	20.0	6.96	1 0.4640 7.69	1 51.8	4.3665	3 223	18.6
## 275 396.90	0.05644	40.0	6.41	1 0.4470 N	A 32.9	4.0776	4 254	17.6
## 276 396.90	0.09604	40.0	6.41	0 0.4470 6.85	4 42.8	4.2673	4 254	17.6
## 277 NA	0.10469	NA	6.41	NA 0.4470 7.26	7 49.0	4.7872	4 254	17.6
## 278 393.45	0.06127	40.0	6.41	1 0.4470 6.82	6 27.6	4.8628	4 254	17.6
## 279 396.90	0.07978	40.0	6.41	0 0.4470 6.48	2 32.1	4.1403	4 254	17.6
## 280 396.90	0.21038	20.0	3.33	0 0.4429 6.81	2 32.2	4.1007	5 216	14.9
## 281 387.31	NA	20.0	3.33	0 0.4429 7.82	0 64.5	4.6947	5 216	14.9
## 282 392.23	0.03705	20.0	3.33	0 0.4429 6.96	8 37.2	5.2447	5 216	14.9
## 283 NA	0.06129	20.0	3.33	1 0.4429 7.64	5 NA	NA	5 216	14.9
## 284 395.52	0.01501	90.0	1.21	1 0.4010 N	A 24.8	5.8850	1 198	13.6
## 285	0.00906	90.0	2.97	0 0.4000 7.08	8 20.8	7.3073	1 285	15.3

394.72	0.01006	NIA	2 25	0	0 2000	6 453	24 0	7 2072	1 7	00 NA
## 286 NA	0.01096	NA	2.25	0	0.3890	6.453	31.9	7.3073	1 3	00 NA
## 287 341.60	0.01965	80.0	NA	0	0.3850	6.230	31.5	9.0892	1 2	41 18.2
## 288 396.90	0.03871	52.5	NA	0	0.4050	6.209	31.3	7.3172	6 2	93 NA
## 289 396.90	NA	52.5	5.32	NA	0.4050	6.315	45.6	7.3172	6 2	93 16.6
## 290 371.72	0.04297	52.5	5.32	0	NA	6.565	22.9	7.3172	6 2	93 NA
## 291 396.90	0.03502	80.0	4.95	NA	0.4110	6.861	27.9	5.1167	4 2	45 19.2
## 292 396.90	0.07886	NA	4.95	0	0.4110	7.148	27.7	5.1167	4 2	45 19.2
## 293 396.90	NA	80.0	4.95	0	0.4110	6.630	23.4	5.1167	4 2	45 19.2
## 294 396.90	0.08265	0.0	13.92	0	0.4370	6.127	18.4	5.5027	NA 2	89 16.0
## 295 NA	0.08199	0.0	13.92	0	0.4370	6.009	42.3	NA	4 2	89 16.0
## 296 396.90	0.12932	0.0	13.92	0	0.4370	6.678	31.1	5.9604	4 2	89 16.0
## 297 392.85	0.05372	0.0	13.92	0	0.4370	6.549	51.0	5.9604	4 2	89 16.0
## 298 396.90	NA	0.0	13.92	0	NA	5.790	58.0	6.3200	4 2	89 16.0
## 299 368.24	0.06466	70.0	NA	0	0.4000	6.345	20.1	7.8278	5 3	58 14.8
## 300 371.58	0.05561	70.0	2.24	0	0.4000	7.041	10.0	7.8278	5 3	58 14.8
## 301 390.86	0.04417	NA	2.24	0	0.4000	6.871	47.4	7.8278	5 3	58 14.8
## 302 395.75	0.03537	34.0	6.09	0	0.4330	6.590	40.4	5.4917	7 3	29 16.1
## 303 383.61	NA	34.0	6.09	0	0.4330	NA	NA	5.4917	NA 3	29 16.1
## 304 390.43	0.10000	34.0	6.09	0	0.4330	6.982	17.7	5.4917	7 3	29 16.1
## 305 393.68	0.05515	33.0	2.18	0	0.4720	7.236	41.1	4.0220	7	NA 18.4
## 306 NA	0.05479	33.0	2.18	0	0.4720	6.616	58.1	3.3700	7 2	22 18.4
## 307 396.90	0.07503	33.0	2.18	0	NA	7.420	71.9	3.0992	7 2	22 18.4
## 308 NA	NA	33.0	2.18	0	0.4720	6.849	70.3	3.1827	7	NA NA
## 309 396.90	0.49298	0.0	9.90	0	0.5440	6.635	82.5	3.3175	4 3	04 18.4
	0.34940	0.0	9.90	0	0.5440	5.972	76.7	3.1025	4 3	04 18.4

396.24	2 62540	0.0		0.0		4 072	27.0	2 5404	4	204	10.4	
## 311 350.45	2.63548	0.0	NA	9 9	.5440	4.9/3	37.8	2.5194	4	304	18.4	
## 312	0.79041	0.0	NA	a a	.5440	6 122	52.8	2.6403	4	304	NA	
396.90	0.75011	0.0		0 0		0.122	32.0	2.0103	•	50.	100	
## 313	0.26169	0.0	9.90	NA 0	.5440	6.023	90.4	2.8340	4	304	18.4	
396.30												
## 314	0.26938	0.0	9.90	0 0	.5440	6.266	82.8	3.2628	4	304	18.4	
393.39												
## 315	0.36920	0.0	9.90	0 0	.5440	6.567	87.3	3.6023	4	304	NA	
NA	0 25256	0.0	0.00	0.0				2 0450		204	40.4	
## 316	0.25356	0.0	9.90	0 0	.5440	5.705	77.7	3.9450	4	304	18.4	
396.42 ## 317	0.31827	0.0	9.90	0 0	.5440	E 01/	83.2	3.9986	1	304	18.4	
390.70	0.3102/	0.0	9.90	9 6	.5440	5.914	03.2	3.9900	4	304	10.4	
## 318	0.24522	0.0	9.90	a a	.5440	5 782	71.7	4.0317	4	304	18.4	
396.90	0.2-322	0.0	3.30	0 0	7.5440	3.702	, 1.,	4.0317	_	JU-	10.4	
## 319	0.40202	0.0	9.90	0 0	.5440	6.382	NA	3.5325	NA	NA	18.4	
395.21												
## 320	0.47547	0.0	9.90	NA 0	.5440	6.113	58.8	NA	4	304	18.4	
396.23												
## 321	0.16760	0.0	7.38	0 0	.4930	6.426	52.3	4.5404	5	287	19.6	
396.90												
## 322	0.18159	0.0	7.38	NA 0	.4930	6.376	54.3	4.5404	5	287	19.6	
396.90	0 25444	0.0	7 20	0.0	4020	c 0.44		4 7044	_	207	40.6	
## 323	0.35114	0.0	7.38	0 0	.4930	6.041	NA	4.7211	5	287	19.6	
396.90	0 20202	0.0	7 20	0.0	4020	F 700	74.2	4 7211	_	207	10 6	
## 324 391.13	0.28392	0.0	7.38	0 0	.4930	5.708	74.3	4.7211	5	287	19.6	
## 325	0.34109	0.0	7.38	a a	.4930	6 415	40.1	4.7211	5	287	19.6	
396.90	0.54105	0.0	7.30	0 0	7.4230	0.415	40.1	4.7211	,	207	13.0	
## 326	0.19186	0.0	7.38	0	NA	6.431	14.7	5.4159	5	NA	NA	
393.68												
## 327	NA	0.0	7.38	0 0	.4930	NA	28.9	NA	5	287	NA	
396.90												
## 328	0.24103	0.0	7.38	0 0	.4930	6.083	43.7	5.4159	5	287	NA	
396.90												
## 329	0.06617	0.0	3.24	0 0	.4600	5.868	25.8	5.2146	4	NA	16.9	
382.44	0.04704		2 24				4= 0	- 0446	_	420	44.0	
## 330	0.06724	0.0	3.24	0 0	.4600	6.333	17.2	5.2146	4	430	16.9	
375.21 ## 331	0 04544	0.0	2 24	0.0	1600	c 111	22.2	F 0726	4	120	NIA	
## 331	0.04544	0.0	3.24	0 0	.4000	6.144	32.2	5.8736	4	430	NA	
## 332	0.05023	35.0	6.06	a a	1379	5.706	28.4	6.6407	1	304	16.9	
394.02	0.00020	55.0	0.00	0 0	,,,,,	5.700	20.4	0.0407	_	JU4	10.9	
## 333	0.03466	35.0	6.06	0 0	.4379	6.031	23.3	6.6407	1	304	NA	
362.25						,.,,					(
## 334	0.05083	0.0	5.19	NA 0	.5150	6.316	38.1	6.4584	5	224	20.2	
389.71												
## 335	NA	0.0	5.19	0 0	.5150	6.310	38.5	6.4584	5	224	20.2	

NA											
## 336	0.03961	0.0	NA	0	0.5150	6.037	34.5	5.9853	5	224	20.2
396.90	0 02427	0.0	г 10	^	NIA	г осо	46.3	F 2211	_	NIA	20. 2
## 337 396.90	0.03427	0.0	5.19	0	NA	5.869	46.3	5.2311	5	NA	20.2
## 338	0.03041	0.0	5.19	0	NΙΛ	5.895	59.6	NA	_	224	20.2
394.81	0.03041	0.0	3.19	Ø	IVA	3.633	39.0	IVA	ر	224	20.2
## 339	0.03306	0.0	5.19	а	0.5150	6 059	37.3	4.8122	5	224	20.2
396.14	0.03300	0.0	J. 1J	U	0.5150	0.055	37.3	7.0122	,	227	20.2
## 340	0.05497	0.0	5.19	a	0.5150	5.985	45.4	4.8122	5	224	NA
396.90	0.03.13,	0.0	3.12	Ū	0.5250	3.303	.5.				
## 341	0.06151	0.0	5.19	0	0.5150	5.968	58.5	4.8122	5	224	NA
396.90				_					_		
## 342	0.01301	35.0	1.52	0	0.4420	7.241	49.3	7.0379	1	284	15.5
394.74											
## 343	0.02498	0.0	1.89	NA	0.5180	NA	NA	6.2669	1	422	15.9
389.96											
## 344	0.02543	55.0	3.78	0	0.4840	6.696	56.4	5.7321	5	370	17.6
396.90											
## 345	0.03049	NA	3.78	NA	0.4840	6.874	28.1	6.4654	5	370	17.6
387.97											
## 346	0.03113	0.0	4.39	0	NA	6.014	48.5	NA	3	352	18.8
385.64											
## 347	0.06162	0.0	4.39	0	0.4420	5.898	52.3	8.0136	3	352	18.8
364.61									_		
## 348	0.01870	NA	NA	0	0.4290	6.516	27.7	8.5353	4	351	17.9
NA	0.01501			_							4= 0
## 349	0.01501	80.0	2.01	0	NA	6.635	29.7	8.3440	NA	280	17.0
390.94	NΑ	40.0	1 25	0	0 4200	6 020	24 5	0 7021	1	225	10.7
## 350 389.85	NA	40.0	1.25	0	0.4290	6.939	34.5	8.7921	1	335	19.7
## 351	0.06211	40.0	1.25	a	0.4290	6 100	44.4	8.7921	1	335	19.7
396.90	0.00211	40.0	1.23	Ø	0.4230	0.430	44.4	0./321		222	19.7
## 352	0.07950	60.0	1.69	а	0.4110	6 579	35 0	10.7103	МΛ	411	NA
370.78	0.07550	00.0	1.05	U	0.4110	0.575	33.3	10.7103	INA	711	IVA
## 353	0.07244	60.0	1.69	a	0.4110	5.884	18.5	10.7103	NΔ	411	18.3
NA	0.072	00.0	2.03	ŭ	01.110	3.00	2013	201,203			20.3
## 354	0.01709	90.0	2.02	0	NA	6.728	NA	12.1265	5	187	17.0
384.46											
## 355	0.04301	80.0	1.91	0	0.4130	5.663	21.9	10.5857	4	334	22.0
382.80											
## 356	0.10659	80.0	1.91	0	0.4130	5.936	19.5	10.5857	4	334	22.0
376.04											
## 357	8.98296	0.0	18.10	1	0.7700	NA	97.4	2.1222	24	666	20.2
377.73											
## 358	3.84970	0.0	18.10	1	0.7700	6.395	91.0	2.5052	24	666	20.2
## 358 391.34											
## 358 391.34 ## 359	3.84970 5.20177	0.0 0.0						2.50522.7227		666 666	20.2
## 358 391.34		0.0		1	0.7700	6.127	83.4		24	666	

390.74										
## 361	4.54192	0.0	18.10	0	0.7700	NA	88.0	2.5182	24 666	20.2
374.56	2 02604	0.0	10 10	0	0 7700	C 2F1	01 1	2 2055	24 666	20.2
## 362	3.83684	0.0	18.10	0	0.7700	6.251	91.1	2.2955	24 666	20.2
350.65	2 (7022	0 0	NIA	0	0.7700	F 262	06.3	2 1026	24 666	20.2
## 363	3.67822	0.0	NA	9	0.7700	5.362	96.2	2.1036	24 666	20.2
380.79 ## 364	4.22239	0.0	18.10	1	0.7700	E 002	NA	1.9047	24 666	20.2
353.04	4.22239	0.0	10.10		0.7700	5.005	IVA	1.9047	24 000	20.2
## 365	3.47428	0 0	18.10	1	0.7180	NA	82.9	1.9047	24 666	20.2
354.55	3.47420	0.0	10.10		0.7100	IVA	02.9	1.9047	24 000	20.2
## 366	4.55587	a a	18.10	а	0.7180	3 561	87.9	1.6132	24 666	NA
354.70	4.55507	0.0	10.10	U	0.7100	J. JUI	07.5	1.0152	24 000	IVA
## 367	3.69695	9.9	18.10	NΔ	0.7180	4.963	91.4	1.7523	24 666	20.2
316.03	3.03033	0.0	10.10	147 (0.7100	11.505	21.	1.,525	21 000	20.2
	13.52220	0.0	NA	9	0.6310	3.863	100.0	1.5106	24 666	20.2
131.42	13.32220	0.0		·	0.0320	3.003		113100	2. 000	
## 369	4.89822	0.0	NA	0	0.6310	NA	100.0	1.3325	24 666	20.2
375.52				Ū				_,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
## 370	5.66998	0.0	18.10	1	0.6310	6.683	96.8	1.3567	24 666	20.2
375.33										
## 371	NA	0.0	18.10	NA	0.6310	7.016	97.5	1.2024	24 666	20.2
392.05										
## 372	9.23230	0.0	18.10	0	NA	6.216	100.0	1.1691	NA 666	20.2
366.15										
## 373	8.26725	0.0	18.10	1	0.6680	5.875	89.6	1.1296	24 NA	20.2
347.88										
## 374	11.10810	0.0	18.10	0	0.6680	4.906	100.0	1.1742	24 666	NA
396.90										
## 375	18.49820	0.0	18.10	0	0.6680	4.138	100.0	1.1370	24 666	20.2
396.90										
	19.60910	0.0	NA	0	0.6710	7.313	97.9	1.3163	24 666	20.2
396.90										
	15.28800	0.0	18.10	0	0.6710	NA	93.3	1.3449	NA 666	20.2
363.02										
## 378	9.82349	0.0	18.10	0	0.6710	NA	98.8	1.3580	24 666	20.2
NA			10.10	_	0 6740		0.5.0	4 2044		
	23.64820	0.0	18.10	0	0.6710	6.380	96.2	1.3861	24 666	20.2
396.90		0.0	40.40	•	0 6740	6 222	400.0	4 2064	24 666	20.2
## 380	NA	0.0	18.10	0	0.6710	6.223	100.0	1.3861	24 666	20.2
393.74	00 07630	0.0	10 10	0	0 6710	c 0c0	01 0	1 4165	24 666	20.2
	88.97620	0.0	18.10	0	0.6710	6.968	91.9	1.4165	24 666	20.2
396.90	15 07//0	0.0	10 10	0	0 6710	6 545	00 1	1 5100	24 666	20.2
## 382 396.90	15.87440	0.0	18.10	О	0.6710	0.545	99.1	1.5192	24 666	20.2
## 383	9.18702	0.0	18.10	NΙΛ	0.7000	E E26	100 0	1.5804	24 666	20.2
## 383 NA	5.10/02	0.0	10.10	NA	0.7000	٥٠٥٥	100.0	1.5004	24 000	20.2
## 384	7.99248	0 0	18.10	a	0.7000	5 520	100 0	1.5331	24 666	20.2
396.90	7.79240	0.0	10.10	Ð	0.7000	5.520	100.0	1.,,,,,1	Z T 000	20.2
	20.08490	a a	18.10	а	0.7000	4 368	91 2	1.4395	24 NA	20.2
כטכ וווו	20.00770	0.0	10.10	U	3.7000	+.500	71.2	1.4000	4-T IVA	20.2

285.83 ## 386	16.81180	NΑ	18.10	0	0.7000	5.277	98.1	1.4261	24 666	NA	
396.90			10.10	J	0.,000	3.2	3012	11.1201	2. 000		
## 387 396.90	24.39380	0.0	18.10	0	NA	4.652	100.0	1.4672	NA 666	20.2	
## 388	22.59710	0.0	18.10	0	0.7000	5.000	89.5	NA	24 666	20.2	
396.90 ## 389	14.33370	0.0	18.10	0	0.7000	4.880	100.0	1.5895	24 666	20.2	
372.92	0 15174	0.0	10 10	•	0.7000	F 200	00.0	4 7204	24 NA	20.2	
## 390 396.90	8.15174	0.0	18.10	О	0.7000	5.390	98.9	1.7281	24 NA	20.2	
## 391 394.43	6.96215	0.0	18.10	0	0.7000	5.713	97.0	1.9265	24 666	20.2	
## 392	5.29305	NA	NA	0	NA	6.051	82.5	2.1678	24 666	20.2	
NA ## 393	11.57790	9.9	18.10	0	NΔ	5.036	97.0	1.7700	24 666	20.2	
396.90											
## 394 396.90	8.64476	0.0	18.10	0	0.6930	6.193	92.6	1.7912	24 666	20.2	
## 395	13.35980	0.0	18.10	0	0.6930	5.887	NA	1.7821	24 666	NA	
396.90 ## 396	8.71675	0.0	18.10	0	0.6930	6.471	98.8	1.7257	24 666	NA	
391.98 ## 397	5.87205	a a	18.10	а	0.6930	6 405	96.0	NA	24 666	20.2	
396.90	3.07203						30.0	NA.	24 000	20.2	
## 398 393.10	7.67202	NA	18.10	0	0.6930	NA	NA	1.6334	24 666	20.2	
## 399	38.35180	0.0	18.10	0	0.6930	5.453	100.0	1.4896	24 NA	20.2	
NA ## 400	9.91655	0.0	18.10	0	0.6930	5.852	77.8	1.5004	24 666	20.2	
NA	25 04610	0.0	10 10	0	0 6030	F 007	100.0	1 5000	24.666	20. 2	
## 401 396 . 90	25.04610	0.0	18.10	О	0.6930	5.987	100.0	1.5888	24 666	20.2	
## 402 NA	14.23620	0.0	18.10	0	0.6930	NA	100.0	1.5741	24 666	20.2	
## 403	9.59571	0.0	18.10	0	NA	6.404	100.0	1.6390	NA 666	20.2	
376.11 ## 404	24.80170	0.0	NA	0	0.6930	5.349	NA	1.7028	24 666	20.2	
396.90	41.52920	0.0	10 10	α	0 6020	E E21	NΙΛ	1 6074	NA CCC	20. 2	
## 405 329.46	41.52920	0.0	18.10	ь	0.6930	5.531	NA	1.6074	NA 666	20.2	
## 406 384.97	67.92080	0.0	18.10	0	0.6930	5.683	100.0	NA	24 666	NA	
## 407	20.71620	0.0	18.10	0	0.6590	4.138	100.0	1.1781	24 666	20.2	
370.22 ## 408	11.95110	9.9	18.10	а	0.6590	5 608	100.0	1.2852	24 666	20.2	
332.09											
## 409 314.64	7.40389	0.0	18.10	0	NA	5.617	NA	1.4547	NA 666	20.2	
	14.43830	0.0	18.10	0	0.5970	NA	100.0	1.4655	24 666	20.2	

NA ## 411	51.13580	a a	18.10	а	0.5970	5 757	100 0	1.4130	24 666	20.2	
NA	51.15500	0.0	10.10	0	0.3370	3.737	100.0	1.4130	24 000	20.2	
## 412 35.05	14.05070	0.0	18.10	0	0.5970	6.657	100.0	1.5275	24 666	20.2	
	18.81100	0.0	18.10	0	0.5970	4.628	100.0	1.5539	NA 666	NA	
28.79	20 (5500	0.0	10 10	0	0 5070	F 4FF	100.0	1 5004	24 666	20. 2	
## 414 210.97	28.65580	0.0	18.10	О	0.5970	5.155	100.0	1.5894	24 666	20.2	
## 415	NA	NA	18.10	NA	0.6930	4.519	100.0	1.6582	24 NA	20.2	
88.27 ## <i>4</i> 16	18.08460	a a	18.10	a	0.6790	6 131	100 0	1.8347	24 NA	20.2	
27.25	10.00400	0.0	10.10	U	0.0790	0.434	100.0	1.0547	24 NA	20.2	
	10.83420	0.0	18.10	0	0.6790	6.782	90.8	NA	NA 666	20.2	
21.57 ## 418	25.94060	0.0	18.10	0	0.6790	NA	NA	1.6475	24 666	20.2	
127.36											
## 419 16.45	73.53410	0.0	18.10	0	0.6790	5.957	100.0	1.8026	24 666	20.2	
	11.81230	0.0	18.10	0	0.7180	6.824	76.5	1.7940	24 666	20.2	
48.45	11 00710	0.0	10 10	0	0 7400	c 411	100.0	4 0500	24.666	20.2	
## 421 318.75	11.08740	0.0	18.10	0	0.7180	6.411	100.0	1.8589	24 666	20.2	
## 422	7.02259	0.0	18.10	0	0.7180	6.006	95.3	1.8746	24 666	20.2	
319.98 ## <i>4</i> 23	12.04820	a a	18.10	a	0.6140	5 648	NA	1.9512	24 666	20.2	
NA	12.0-020	0.0	10.10	Ū	0.0140	3.040	IVA	1.5512	24 000	20.2	
## 424 2.52	7.05042	0.0	18.10	NA	0.6140	6.103	85.1	2.0218	24 666	20.2	
## 425	8.79212	0.0	18.10	0	0.5840	5.565	70.6	2.0635	24 666	20.2	
3.65											
## 426 7.68	15.86030	0.0	18.10	0	0.6790	5.896	NA	1.9096	NA 666	NA	
## 427	12.24720	NA	18.10	NA	0.5840	5.837	59.7	1.9976	24 666	20.2	
24.65	37.66190	9 9	18.10	a	0.6790	NA	NA	1 8620	24 666	20.2	
## 428 NA	37.00190	0.0	10.10	ð	0.0790	INA	IVA	1.8029	24 000	20.2	
## 429	7.36711	0.0	18.10	0	0.6790	6.193	78.1	NA	NA 666	20.2	
96.73 ## 430	9.33889	0.0	18.10	0	0.6790	6.380	NA	1.9682	24 666	20.2	
60.72											
## 431 83.45	8.49213	0.0	18.10	0	0.5840	NA	86.1	NA	24 666	20.2	
	10.06230	0.0	18.10	0	0.5840	NA	94.3	2.0882	24 666	20.2	
81.33	6 44405	0.0	10 10	0	0 5040	C 425	74.0	2 2004	24 666	20. 2	
## 433 NA	6.44405	0.0	18.10	Ø	0.5840	0.425	/4.8	2.2004	24 666	20.2	
## 434	5.58107	0.0	18.10	0	0.7130	6.436	87.9	2.3158	24 666	20.2	
100.19	13.91340	a a	18.10	a	0.7130	6.202	95 A	2.2222	24 666	20.2	
	10.010 1 0	0.0	10.10	U	3.7130	0.200	22.0	- •	2. 000	20.2	

100.63	44 46040	0.0	10.10	•	0 7400		04.6	2 4247	NA 666	20.2
## 436 109.85	11.16040	0.0	18.10	0	0.7400	6.629	94.6	2.1247	NA 666	20.2
## 437	NA	0.0	18.10	a	0.7400	6.461	93.3	2.0026	24 666	20.2
27.49				Ū		01.02	2010	_,,,,		
## 438	15.17720	0.0	18.10	0	0.7400	6.152	100.0	1.9142	24 666	20.2
9.32										
## 439	NA	0.0	18.10	0	0.7400	5.935	87.9	1.8206	24 666	20.2
68.95	0 20062	NIA	10 10	NIA	0.7400	F 637	02.0	1 0170	24 666	20. 2
## 440 396.90	9.39063	NA	18.10	NA	0.7400	5.62/	93.9	1.8172	24 666	20.2
## 441	NA	a a	18.10	NΔ	0.7400	5 818	NΔ	1.8662	NA 666	20.2
391.45	IVA	0.0	10.10	IVA	0.7400	3.010	IV.	1.0002	NA 000	20.2
## 442	9.72418	0.0	18.10	0	0.7400	6.406	97.2	2.0651	24 666	20.2
385.96										
## 443	NA	0.0	18.10	0	NA	6.219	100.0	2.0048	24 666	20.2
395.69										
## 444	9.96654	0.0	18.10	0	0.7400	6.485	NA	1.9784	24 NA	20.2
386.73 ## 445	NA	0.0	18.10	a	0.7400	E 0E1	06 6	1.8956	24 666	20.2
240.52	IVA	0.0	10.10	О	0.7400	3.634	90.0	1.0930	24 000	20.2
	10.67180	0.0	18.10	0	0.7400	6.459	94.8	1.9879	24 666	20.2
43.06				Ū		01.22				
## 447	6.28807	0.0	18.10	0	0.7400	6.341	96.4	2.0720	24 666	NA
NA										
## 448	9.92485	0.0	18.10	0	0.7400	6.251	96.6	2.1980	24 666	20.2
388.52	0 22000	0.0	10 10	0	0.7130	6 405	00.7	2 2646	24 666	20. 2
## 449 396.90	9.32909	0.0	18.10	0	0.7130	6.185	98.7	2.2616	24 666	20.2
## 450	7.52601	9.9	18.10	0	NΔ	6.417	98.3	2.1850	24 666	20.2
304.21	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.0		Ū		0.127	30.3	_,	2. 000	
## 451	6.71772	0.0	18.10	0	0.7130	6.749	NA	2.3236	24 666	20.2
0.32										
## 452	NA	0.0	18.10	NA	0.7130	6.655	98.2	2.3552	24 666	20.2
355.29	F 00047		40.40	•	0 7430	6 207	04.0	2 2602	24 666	20. 2
## 453	5.09017	0.0	18.10	0	0.7130	6.297	91.8	2.3682	24 666	20.2
385.09 ## 454	8.24809	a a	18.10	a	0 7130	7 393	99.3	2.4527	NA 666	20.2
375.87	0.24007	0.0	10.10	U	0.7130	7.555	JJ.J	2.4321	NA 000	20.2
## 455	9.51363	0.0	18.10	0	0.7130	6.728	94.1	2.4961	24 666	20.2
6.68										
## 456	4.75237	0.0	NA	0	0.7130	6.525	86.5	NA	24 666	20.2
50.92										
## 457	NA	NA	18.10	0	0.7130	5.976	NA	2.5806	24 666	20.2
10.48	0 20050	NIA	10 10	O	0 7120	E 026	90.2	2 7702	24 NA	20. 2
## 458 3.50	8.20058	NA	18.10	О	0.7130	5.930	00.3	2.7792	24 NA	20.2
## 459	7.75223	0.0	18.10	0	0.7130	6.301	83.7	2.7831	24 666	20.2
272.21										- · -
## 460	6.80117	NA	18.10	0	0.7130	6.081	84.4	2.7175	24 NA	20.2

396.90	4 01212	0.0	10 10	0	0.7130	6 701	00.0	2 5075	24 666	20. 2
## 461 255.23	4.81213	0.0	18.10	0	0.7130	6.701	90.0	2.5975	24 666	20.2
## 462	NA	0.0	18.10	0	0.7130	6.376	NA	2.5671	24 666	20.2
391.43										
## 463	6.65492	0.0	18.10	0	0.7130	6.317	83.0	2.7344	24 NA	20.2
NA ## 464	5.82115	9.9	18.10	а	0.7130	6.513	89.9	2.8016	24 666	20.2
393.82	3.02223	0.0	20.20	Ū	01,250	0.525	02.0	2.0020	2. 000	
## 465	7.83932	0.0	18.10	0	0.6550	6.209	65.4	2.9634	24 666	20.2
396.90				_						
## 466 334.40	3.16360	0.0	NA	0	0.6550	5.759	48.2	3.0665	24 666	20.2
## 467	3.77498	0.0	18.10	0	NA	5.952	84.7	2.8715	24 666	20.2
22.01				Ū				_,,,,		
## 468	4.42228	0.0	18.10	0	0.5840	6.003	94.5	2.5403	24 666	20.2
331.29	45 53530	0.0	40.40	•	0 5000		74 0	2 0004	24 666	20.2
## 469 368.74	15.57570	0.0	18.10	0	0.5800	NA	71.0	2.9084	24 666	20.2
	13.07510	0.0	18.10	0	0.5800	5.713	56.7	2.8237	24 666	20.2
396.90										
## 471	4.34879	0.0	18.10	0	0.5800	6.167	84.0	3.0334	24 666	20.2
396.90	4 02044	N1.0	10 10		0 5330	6 220	00.7	2 0002	24 666	20. 2
## 472 395.33	4.03841	NA	18.10	NA	0.5320	6.229	90.7	3.0993	24 666	20.2
## 473	3.56868	0.0	18.10	0	0.5800	6.437	75.0	2.8965	24 666	20.2
393.37										
## 474	4.64689	0.0	NA	0	0.6140	6.980	NA	2.5329	24 666	20.2
374.68	8.05579	0 0	18.10	NΙΛ	0.5840	E 427	95.4	2.4298	24 666	20.2
## 475 352.58	0.055/9	0.0	10.10	INA	0.5840	5.427	95.4	2.4298	24 000	20.2
## 476	NA	0.0	18.10	0	0.5840	6.162	97.4	2.2060	24 666	20.2
302.76										
## 477	4.87141	0.0	18.10	0	0.6140	6.484	93.6	2.3053	24 666	20.2
NA ## 478	15.02340	NΔ	12 10	a	a 614a	5 304	97 3	2.1007	24 666	20.2
349.48	13.02540	IVA	10.10	U	0.0140	J. JU-	27.5	2.1007	24 000	20.2
	10.23300	0.0	18.10	0	0.6140	6.185	96.7	2.1705	24 666	20.2
379.70										
	14.33370	0.0	18.10	0	0.6140	6.229	88.0	1.9512	24 666	20.2
383.32 ## 481	5.82401	9.9	18.10	а	0.5320	6.242	64.7	NA	24 666	20.2
396.90	3.02.01	3.0		J	3.3320	J	01.7	14/1	2. 500	
## 482	5.70818	0.0	18.10	0	0.5320	6.750	NA	3.3317	24 666	20.2
393.07										
## 483 395.28	5.73116	NA	18.10	0	0.5320	7.061	77.0	3.4106	24 666	NA
## 484	2.81838	0.0	18.10	9	0.5320	5.762	40.3	4.0983	24 666	20.2
392.92	0_000	3.0		J						_ • • •
## 485	2.37857	0.0	18.10	0	NA	5.871	41.9	3.7240	24 666	20.2

370.73	2 67267	0.0	10 10	0	0 5030	NIA	F1 0	2 0017	24.666	20. 2	
## 486 388.62	3.67367	0.0	18.10	0	0.5830	NA	51.9	3.9917	24 666	20.2	
## 487	5.69175	0.0	18.10	0	0.5830	6.114	79.8	3.5459	NA 666	20.2	
392.68											
## 488	NA	0.0	18.10	0	NA	5.905	53.2	3.1523	24 666	20.2	
388.22 ## 489	0.15086	a a	27.74	а	0.6090	5 454	92.7	1.8209	4 711	NA	
395.09	0.13000	0.0	2 , •, , ,	Ū	0.0050	J. 1J.	,,,	1.0203	. ,	101	
## 490	0.18337	0.0	27.74	0	0.6090	5.414	98.3	1.7554	4 711	NA	
344.05	0.00746			_				4 0004		00.4	
## 491 318.43	0.20746	0.0	27.74	0	0.6090	5.093	98.0	1.8226	4 711	20.1	
## 492	0.10574	0.0	NA	0	0.6090	5.983	98.8	1.8681	4 711	20.1	
390.11											
## 493	0.11132	0.0	27.74	0	0.6090	5.983	83.5	2.1099	4 711	20.1	
396.90 ## 494	0 17221	0.0	NΙΔ	0	0.5850	F 707	E4 0	2 2017	6 201	10.2	
## 494 396 . 90	0.17331	0.0	NA	О	0.5850	5.707	54.0	2.3817	6 391	19.2	
## 495	0.27957	0.0	9.69	0	NA	NA	42.6	2.3817	6 391	19.2	
396.90											
## 496	0.17899	0.0	9.69	0	NA	5.670	28.8	NA	6 391	19.2	
393.29 ## 497	0.28960	0.0	NA	а	0.5850	5 390	72.9	2.7986	6 391	19.2	
396.90	0.20500	0.0	IVA	Ū	0.3030	3.330	, 2. 3	2.7500	0 331	17.2	
## 498	0.26838	0.0	9.69	0	0.5850	5.794	70.6	2.8927	6 391	19.2	
NA	0 00010		0 - 10	_						10.0	
## 499 NA	0.23912	NA	9.69	0	NA	6.019	65.3	2.4091	NA 391	19.2	
## 500	0.17783	0.0	9.69	0	0.5850	5.569	73.5	2.3999	6 391	19.2	
395.77											
## 501	0.22438	0.0	9.69	0	0.5850	6.027	79.7	2.4982	6 391	19.2	
396.90 ## 502	0.06263	a a	11.93	a	0.5730	6 593	69.1	2.4786	1 273	21.0	
391.99	0.00203	0.0	11.75	U	0.5750	0.555	05.1	2.4700	1 2/3	21.0	
## 503	0.04527	0.0	11.93	0	0.5730	6.120	76.7	2.2875	1 273	21.0	
396.90											
## 504 396.90	NA	NA	11.93	0	0.5730	NA	91.0	2.1675	1 273	21.0	
## 505	0.10959	0.0	11.93	9	0.5730	6.794	NA	2.3889	1 273	NA	
393.45	0.120000	0.0		ŭ	0.3730	01,2.		2.3003	,		
## 506	0.04741	0.0	11.93	0	0.5730	6.030	80.8	2.5050	1 273	21.0	
396.90	1-4-4										
## ## 1	1stat 4.98										
## 2	9.14										
## 3	4.03										
## 4	2.94										
## 5	5.33										
## 6	5.21										

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## 482 7.74
## 483
          NA
## 484 10.42
## 485 13.34
## 486 10.58
## 487 14.98
## 488 11.45
## 489 18.06
## 490 23.97
## 491 29.68
## 492 18.07
## 493
          NA
## 494 12.01
## 495 13.59
## 496 17.60
## 497 21.14
## 498 14.10
## 499 12.92
## 500 15.10
## 501 14.33
## 502
          NA
## 503 9.08
## 504 5.64
## 505
       6.48
## 506 7.88
```

Use a random forest modeling procedure to iteratively fill in the NA's by predicting each feature of X using every other feature of X. You need to start by filling in the holes to use RF. So fill them in with the average of the feature.