## Three Practice Problems for Compressible Flow

11.37 Determine the static pressure to stagnation pressure ratio associated with the following motion in standard air: (a) a runner moving at the rate of 10 mph, (b) a cyclist moving at the rate of 40 mph, (c) a car moving at the rate of 65 mph, (d) an airplane moving at the rate of 500 mph.

With a value of Mach number calculated with

$$Ma = \frac{V}{F}$$
we can calculate
$$\frac{P}{R_0} \text{ with } \frac{P}{R_0} = \left[ \frac{1}{1 + (\frac{1}{K-1})Ma^2} \right]^{\frac{1}{K-1}}$$
(11.59)

For c we use for parts  $a, b$  and c

$$C = \sqrt{RTk} = \sqrt{(1716 \frac{f+1.1b}{5lug.7k})} \frac{(519 R)(1.40)}{(1 \frac{16}{5lug.7k})} = 1117 \frac{f+1}{5}$$
or

$$C = (1117 \frac{f+1}{5}) \frac{(3600 E)}{(3600 E)} = 761.6 \text{ mph}$$
(a) For  $V = 10 \text{ mph}$ 

$$Ma = \frac{10 \text{ mph}}{761.6 \text{ mph}} = 0.0131$$
and
$$P = \sqrt{1 + (\frac{1.4-1}{2})(0.0/31)^2} \sqrt{1.4-1} = \sqrt{1 + (0.2)(0.0/31)^2} = 0.9988$$
(b) For  $V = 40 \text{ mph}$ 

$$Ma = \frac{40 \text{ mph}}{761.6 \text{ mph}} = 0.0525$$
and
$$P = \sqrt{1 + 0.12(0.0525)^2} = 0.998$$
(c) For  $V = 65 \text{ mph}$ 

$$Ma = \frac{65 \text{ mph}}{761.6 \text{ mph}} = 0.0854$$

$$761.6 \text{ mph}$$

$$\frac{1}{762.6 \text{ mph}} = 0.0854$$

$$\frac{3.5}{761.6 \text{ mph}} = 0.0854$$

(d) For airplane we assume a nominal altitude of 30,000 ft.

From Table C. I we note a corresponding temperature of -47.83 F.

Then

$$C = \sqrt{\frac{(716 + 16)}{5 \text{ kig.}^{9} R}} \frac{(47.83 + 460)^{9} R^{3}(1.4)}{(1 \frac{16}{5 \text{ kig.} \frac{47}{52}})}$$

$$c = 995 \frac{ft}{s}$$

$$c = \left(995 \frac{f+}{5}\right) \frac{\left(3600 \frac{5}{hr}\right)}{\left(5280 \frac{f+}{m_i}\right)} = 678 \text{ mph}$$

Then for
$$Ma = \frac{500 \text{ mph}}{678 \text{ mph}} = 0.738$$

$$\frac{P}{P_0} = \left[ \frac{1}{1 + 0.2 (0.739)^2} \right] = 0.696$$

- 11.39 The stagnation pressure and temperature of air flowing past a probe are 120 kPa (abs) and 100 °C, respectively. The air pressure is 80 kPa (abs). Determine the air speed and Mach number considering the flow to be (a) incompressible; (b) compressible.
- (a) Assuming incompressible flow we use Bernoulli's equation (Eq. 3.7) to connect the static and stagnation states and get

$$V = \sqrt{\frac{Z(P_o - P)}{P_o}} \tag{1}$$

With the ideal gas equation of stake (Eq. 1) we obtain

$$P_o = \frac{P_o}{RT_o} \tag{2}$$

and combining Eqs. 1 and 2 we obtain

$$V = \sqrt{\frac{2(P_o - P)RT_o}{P_o}}$$

or

$$V = \sqrt{\frac{2 \left[120 \, \text{kPa}(abs) - 80 \, \text{kPa}(abs)\right] \left(286.9 \, \frac{N.m}{kg.k}\right)^{373k}}{\left[120 \, \text{kPa}(abs)\right] \left(\frac{N}{kg.m}\right)}} = \frac{267 \, \frac{m}{s}}{5}$$

For Mach number we need

$$Ma = \frac{V}{c} = \frac{V}{VRTR}$$
 (3)

To determine T we use the equation of motion (Eq. 11.54) to obtain

$$T = T_o - \frac{V^2(h-1)}{2 kR} = 373K - \frac{(267 \frac{m}{5})^2 (1.4-1)}{2(1.4)(286.9 \frac{N \cdot m}{hg \cdot k})}$$
or  $T = 337.5 \text{ K}$ 

$$Ma = \frac{267 \frac{m}{5}}{\sqrt{\frac{286.9 \frac{N.m}{kg.K}}{\frac{Ng.K}{5}}}} = 0.725$$

(b) For compressible flow

$$\frac{P}{P_0} = \frac{80 \text{ k/a(abs)}}{120 \text{ k/a (abs)}} = 0.67$$

and from Fig. D.1 we read

$$Ma = 0.78$$

Also from Fig. D.1 we read

$$\frac{T}{T_0} = 0.89$$

and thus

$$T = (0.89)(373k) = 332 k$$

Thus,

$$V = Ma \sqrt{RT k} = (0.78) \sqrt{\frac{286.9 \, N.m}{29. \, k}} \sqrt{\frac{332 \, k}{\binom{1.4}{k9. \, \frac{m}{5^2}}}}$$
and

 $V = \frac{285}{5} \frac{m}{5}$ 

11.45 An ideal gas is to flow isentropically from a large tank where the air is maintained at a temperature and pressure of 59 °F and 80 psia to standard atmospheric discharge conditions. Describe in general terms the kind of duct involved and determine the duct exit Mach number and velocity in ft/s if the gas is air.

To determine the duct exit Mach number, Maexit, we use Eq. 11.59 or for air, Fig. D.1. Thus,

$$Ma_{exit} = \sqrt{\frac{1}{\binom{P_{exit}}{P_{e}}}} \frac{k-1}{k} - 1 \sqrt{\frac{2}{k-1}}$$

$$(1)$$

To determine exit velocity, Vexit, we use

$$V_{exit} = (Ma_{exit}) C_{exit} = Ma_{exit} \sqrt{RT_{exit}} k$$
 (3)

$$T_{exit} = \frac{T_o}{1 + \left(\frac{k-1}{2}\right) M_{a_{exit}}^2}$$
(4)

$$T_{exit} = T_o \left( \frac{T_{exit}}{T_o} \text{ value from Fig. D.1 for } M_{q_{exit}} \right)$$
 (5)

$$\frac{P_{\text{exi}}t}{P_{\text{o}}} = \frac{14.7 \, psi_{\text{a}}}{80 \, psi_{\text{a}}} = 0.1838$$

and thus from Fig. D.1, the corresponding values are

and 
$$\frac{Ma_{0x)t} = \frac{1.8}{1.8}}{\frac{T_{0x}t}{T_{0}}} = 0.62$$

(con't)

Then with Eq. 5 we obtain

and with Eq. 3 we conclude that
$$V_{\text{exit}} = (1.8) \sqrt{\frac{(17/6 + 1/6)}{5/49. ^{\circ}R} \frac{(322 ^{\circ}R)(1.4)}{(\frac{1}{5/49. ^{\circ}R})}} = \frac{1580}{5} \frac{ft}{5}$$

A converging-diverging nossle is required because the exit flow is supersonic.