

# FortEPiaNO technical notes

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We present here the main features of our code, **FORTran-Evolved PrimordIAL Neutrino Oscillations** (**FortEPiaNO**) [1]. The code is publicly available at the url [https://bitbucket.org/ahp\\_cosmo/fortepiano\\_public](https://bitbucket.org/ahp_cosmo/fortepiano_public).

## I. EQUATIONS

**FortEPiaNO** can compute oscillations with up to six neutrinos in the early universe. Neutrinos, including the sterile ones, are always treated as ultra-relativistic particles, which is a good approximation if the neutrino masses do not exceed  $\mathcal{O}(\text{a few keV})$ , i.e. neutrinos are still fully relativistic at decoupling. For larger masses, neutrinos may start to become non-relativistic before decoupling, and in that case one should take into account the effect of the mass.

The code computes the evolution of the  $N \times N$  neutrino density matrix [2–5]

$$\varrho(x, y) = \begin{pmatrix} \varrho_{ee} & \varrho_{e\mu} & \varrho_{e\tau} & \varrho_{es_1} & \cdots \\ \varrho_{\mu e} & \varrho_{\mu\mu} & \varrho_{\mu\tau} & \varrho_{\mu s_1} & \\ \varrho_{\tau e} & \varrho_{\tau\mu} & \varrho_{\tau\tau} & \varrho_{\tau s_1} & \\ \varrho_{s_1 e} & \varrho_{s_1\mu} & \varrho_{s_1\tau} & \varrho_{s_1 s_1} & \\ \vdots & & & & \ddots \end{pmatrix}, \quad (1)$$

which is the same for neutrinos and antineutrinos, in terms of the comoving coordinates  $x \equiv m_e a$ ,  $y \equiv p a$ ,  $z \equiv T_\gamma a$  and  $w \equiv T_\nu a$ . The momentum dependence of the density matrix  $\varrho$  is taken into account using a discrete grid of momenta, as described in section IV.

When using  $N$  neutrinos, the mixing matrix is defined as

$$U = R^{(N-1)N} \dots R^{1N} R^{(N-2)(N-1)} \dots R^{1(N-1)} \dots R^{34} R^{24} R^{14} R^{23} R^{13} R^{12}, \quad (2)$$

following and extending the convention presented in Eq. (12) of [6], where each  $R^{ij}$  is a real rotation matrix described by the angle  $\theta_{ij}$ , containing  $\cos \theta_{ij}$  in the diagonal elements  $ii$  and  $jj$ , 1 in the remaining diagonal elements,  $\sin \theta_{ij}$  ( $-\sin \theta_{ij}$ ) in the off-diagonal element  $ij$  ( $ji$ ) and zero otherwise:

$$[R^{ij}]_{rs} = \delta_{rs} + (\cos \theta_{ij} - 1)(\delta_{ri}\delta_{sj} + \delta_{rj}\delta_{si}) + \sin \theta_{ij}(\delta_{ri}\delta_{sj} - \delta_{rj}\delta_{si}). \quad (3)$$

It enters the calculation of the rotated mass matrix  $\mathbb{M}_F = U \mathbb{M} U^\dagger$ , where the diagonal mass matrix is  $\mathbb{M} = \text{diag}(m_1^2, \dots, m_N^2)$ . Other matrices that we need to define are

$$\mathbb{E}_\ell = \text{diag}(\rho_e, \rho_\mu, 0, \dots), \quad \mathbb{P}_\ell = \text{diag}(P_e, P_\mu, 0, \dots), \quad \mathbb{E}_\nu = S_a \frac{1}{\pi^2} \left( \int dy y^3 \varrho \right) S_a \quad \text{with } S_a = \text{diag}(1, 1, 1, 0, \dots), \quad (4)$$

while the interaction matrices used in the collision terms, presented in section II, are

$$G^L = \text{diag}(g_L, \tilde{g}_L, \tilde{g}_L, 0, \dots), \quad G^R = \text{diag}(g_R, g_R, g_R, 0, \dots), \quad (5)$$

where  $g_L = \sin^2 \theta_W + 1/2$ ,  $\tilde{g}_L = \sin^2 \theta_W - 1/2$ ,  $g_R = \sin^2 \theta_W$ , and  $\theta_W$  is the weak mixing angle. It is easy to see from the definitions of Eqs. (56) and (57) that the collision terms vanish when considering the interactions corresponding only to sterile neutrinos. When more than one sterile neutrino is considered, the damping terms between the different sterile neutrinos are therefore set to zero.

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The definitions of comoving energy density and pressure, which can be combined to obtain the comoving entropy density, are written as:

$$\rho_i = g_i \int \frac{dp}{2\pi^2} p^2 E_p \frac{1}{e^{E_p/z} \pm 1}, \quad (6)$$

$$P = g_i \int \frac{dp}{2\pi^2} \frac{p^4}{3E_p} \frac{1}{e^{E_p/z} \pm 1}, \quad (7)$$

$$s = \frac{\rho + P}{z}, \quad (8)$$

where the  $+$  ( $-$ ) applies for fermions (bosons),  $i$  denotes the species, which has  $g_i$  degrees of freedoms,  $p$  is the comoving momentum,  $E_p = \sqrt{p^2 + m_i^2}$ , being  $m_i$  the comoving mass of the particle, and  $z$  must be substituted with  $w$  in the case of neutrinos.

To take into account finite temperature QED (FTQED) corrections [5, 7, 8], we have to modify the total pressure and energy density of the fluid:

$$P = \sum_{i=\gamma, \nu_i, e, \mu} P_i + \delta P(x, z), \quad (9)$$

$$\rho = \sum_{i=\gamma, \nu_i, e, \mu} \rho_i + \delta \rho(x, z), \quad (10)$$

where  $\delta P$  and  $\delta \rho$  are contributions that can be computed using FTQED. It is convenient to define them in terms of the following functions:

$$J_a(r) = \frac{1}{\pi^2} \int_0^\infty du u^a \frac{\exp(\sqrt{u^2 + r^2})}{\left[ \exp(\sqrt{u^2 + r^2}) + 1 \right]^2}, \quad (11)$$

$$K_a(r) = \frac{1}{\pi^2} \int_0^\infty du \frac{u^a}{\sqrt{u^2 + r^2}} \frac{1}{\exp(\sqrt{u^2 + r^2}) + 1}. \quad (12)$$

Let us also define for convenience:

$$\mathcal{N}_p = \frac{2}{e^{E_p/z} + 1}, \quad (13)$$

$$\partial_x \mathcal{N}_p = -\frac{x e^{E_p/z} \mathcal{N}_p^2}{2z E_p}, \quad (14)$$

$$\partial_z \mathcal{N}_p = \frac{e^{E_p/z} E_p \mathcal{N}_p^2}{2z^2}, \quad (15)$$

$$\partial_x \partial_z \mathcal{N}_p = \frac{x e^{E_p/z} \mathcal{N}_p^2}{2z^3} \left( 1 - e^{E_p/z} \mathcal{N}_p + \frac{z}{E_p} \right). \quad (16)$$

The contributions  $\delta P$  and  $\delta \rho$  can be expanded as a series of powers of the electron charge  $e^2 = 4\pi\alpha$ , where  $\alpha$  is the fine structure constant. Taking into account the first orders of the expansion, and using  $r = x/z$ , for the pressure one has [8]

$$\delta P(x, z) = \delta P^{(2)}(x/z) + \delta P^{(2+\ln)}(x, z) + \delta P^{(3)}(x/z) + \dots, \quad (17)$$

$$\delta P^{(2)}(r) = -e^2 z^4 K_2 \left( \frac{1}{6} + \frac{K_2}{2} \right), \quad (18)$$

$$\delta P^{(2+\ln)}(x, z) = \frac{e^2 x^2}{16\pi^4} \iint_0^\infty dy dk \frac{y k}{E_y E_k} \ln \left| \frac{y+k}{y-k} \right| \mathcal{N}_y \mathcal{N}_k, \quad (19)$$

$$\delta P^{(3)}(r) = \frac{2e^3 z^4}{3\pi} \left( K_2 + \frac{r^2}{2} K_0 \right)^{3/2}, \quad (20)$$

while for the energy density the various terms are

$$\delta\rho(x, z) = \delta\rho^{(2)}(x/z) + \delta\rho^{(2+\ln)}(x, z) + \delta\rho^{(3)}(x/z) + \dots, \quad (21)$$

$$\delta\rho^{(2)}(r) = e^2 z^4 \left( \frac{K_2^2}{2} - \frac{K_2 + J_2}{6} - K_2 J_2 \right), \quad (22)$$

$$\delta\rho^{(2+\ln)}(x, z) = \frac{e^2 x^2}{16\pi^4} \iint_0^\infty dy dk \frac{y k}{E_y E_k} \ln \left| \frac{y+k}{y-k} \right| \mathcal{N}_y \left( 2z \partial_z \mathcal{N}_k - \mathcal{N}_k \right), \quad (23)$$

$$\delta\rho^{(3)}(r) = \frac{e^3 z^4}{\pi} \left( K_2 + \frac{r^2}{2} K_0 \right)^{1/2} \left( J_2 + \frac{r^2}{2} J_0 \right). \quad (24)$$

In order to compute the evolution of the neutrino density matrix (1), we have to compute both the derivative of  $\varrho$  (as a function of the momentum) and of the comoving photon temperature  $z$  with respect to our time parameter  $x$ . The differential equations which the code solves are the following [2–5]:

$$\begin{aligned} \frac{d\varrho(y)}{dx} &= \sqrt{\frac{3m_{\text{Pl}}^2}{8\pi\rho}} \left\{ -i \frac{x^2}{m_e^3} \left[ \frac{\mathbb{M}_F}{2y} - \frac{2\sqrt{2}G_F y m_e^6}{x^6} \left( \frac{\mathbb{E}_\ell + \mathbb{P}_\ell}{m_W^2} + \frac{4}{3} \frac{\mathbb{E}_\nu}{m_Z^2} \right), \varrho \right] + \frac{m_e^3}{x^4} \mathcal{I}(\varrho) \right\}, \\ \frac{dz}{dx} &= \frac{\sum_{\ell=e,\mu} \left[ \frac{r_\ell^2}{r} J_2(r_\ell) \right] + G_1(r) - \frac{1}{2\pi^2 z^3} \int_0^\infty dy y^3 \sum_{\alpha=e}^{s_{N_s}} \frac{d\varrho_{\alpha\alpha}}{dx}}{\sum_{\ell=e,\mu} \left[ r_\ell^2 J_2(r_\ell) + J_4(r_\ell) \right] + G_2(r) + \frac{2\pi^2}{15}}, \end{aligned} \quad (25)$$

where  $r_\ell = m_\ell/m_e r$ . The expressions for the  $G_1$  and  $G_2$  functions, which again take into account the FTQED corrections, are written as [5, 8]:

$$G_{1,2}(x, z) = G_{1,2}^{(2)}(x/z) + G_{1,2}^{(2+\ln)}(x, z) + G_{1,2}^{(3)}(x/z) + \dots, \quad (26)$$

$$G_a(r) = \frac{K_2'}{6} - K_2 K_2' + \frac{J_2'}{6} + K_2' J_2 + K_2 J_2', \quad (27)$$

$$G_1^{(2)}(r) = 2\pi\alpha \left[ \frac{1}{r} \left( \frac{K_2}{3} + 2K_2^2 - \frac{J_2}{6} - K_2 J_2 \right) + G_a \right], \quad (28)$$

$$G_2^{(2)}(r) = -8\pi\alpha \left( \frac{K_2}{6} + \frac{J_2}{6} - \frac{1}{2} K_2^2 + K_2 J_2 \right) + 2\pi\alpha r G_a, \quad (29)$$

$$\begin{aligned} G_1^{(2+\ln)}(x, z) &= \frac{e^2 x}{16\pi^4 z^3} \iint_0^\infty dy dk \frac{y k}{E_y E_k} \ln \left| \frac{y+k}{y-k} \right| \left\{ -x \left[ z \left( \partial_x \mathcal{N}_y \partial_z \mathcal{N}_k + \mathcal{N}_y \partial_x \partial_z \mathcal{N}_k \right) - \mathcal{N}_y \partial_x \mathcal{N}_k \right] \right. \\ &\quad \left. - \mathcal{N}_y \mathcal{N}_k - z \mathcal{N}_y \partial_z \mathcal{N}_k + \frac{x^2 (E_y^2 + E_k^2)}{2E_y^2 E_k^2} \left( 2z \mathcal{N}_y \partial_z \mathcal{N}_k - \mathcal{N}_y \mathcal{N}_k \right) \right\}, \end{aligned} \quad (30)$$

$$G_2^{(2+\ln)}(x, z) = \frac{e^2 x^2}{16\pi^4 z^2} \iint_0^\infty dy dk \frac{y k}{E_y E_k} \ln \left| \frac{y+k}{y-k} \right| \partial_z \left( \mathcal{N}_y \partial_z \mathcal{N}_k \right), \quad (31)$$

$$G_b(r) = \sqrt{K_2 + r^2 \frac{K_0}{2}}, \quad (32)$$

$$G_c(r) = \frac{2J_2 + r^2 J_0}{2(2K_2 + r^2 K_0)}, \quad (33)$$

$$G_1^{(3)}(r) = \frac{e^3}{4\pi} G_b \left\{ \frac{1}{r} \left( 2J_2 - 4K_2 \right) - 2J_2' - r^2 J_0' - r \left( 2K_0 + J_0 \right) - G_c \left[ r(K_0 - J_0) + K_2' \right] \right\}, \quad (34)$$

$$G_2^{(3)}(r) = \frac{e^3}{4\pi} G_b \left[ G_c \left( 2J_2 + r^2 J_0 \right) - \frac{2}{r} J_4' - r \left( 3J_2' + r^2 J_0' \right) \right], \quad (35)$$

where the prime denotes derivative with respect to  $r$  and we dropped the explicit dependence on  $r$  in the expressions for the  $G$  functions. For the sake of computational speed, we calculate and store lists for all the terms of Eq. (25) which do not depend on the neutrino density matrix at the initialisation stage, and compute their values through interpolation during the real calculation. The same happens for the energy densities of charged leptons, for which performing an interpolation is much faster than computing an integral. The interpolation, however, can be disabled during compilation (see the **README**), with a  $\lesssim 20\%$  increase of the running time.

In order to estimate the effective comoving neutrino temperature  $w$ , which is not needed for the calculation but useful to understand the final results, we use an equation similar to Eq. (25), but considering only relativistic electrons, i.e. fixing  $r_e = 0$  in the equation.

The finite-temperature electromagnetic corrections are also taken into account in the calculation of the electron mass, used in the collision terms. The contribution to the electron mass, in comoving coordinates, is obtained as [5, 7, 8]:

$$\delta m_e^2(x, y, z) = \frac{2\pi\alpha z^2}{3} + \frac{4\alpha}{\pi} \int_0^\infty dk \frac{k^2}{E_k} \frac{1}{e^{E_k/z} + 1} - \frac{x^2\alpha}{\pi y} \int_0^\infty dk \frac{k}{E_k} \log \left| \frac{y+k}{y-k} \right| \mathcal{N}_k, \quad (36)$$

so that the comoving electron mass must be replaced using  $x^2 \rightarrow x^2 + \delta m_e^2$ . In the calculation of the collision integrals we ignore the log term that depends on  $y$ .

Finally, the effective number of degrees of freedom that the code returns in output is defined as:

$$N_{\text{eff}}^e = \frac{8}{7} \frac{\sum_i \rho_{\nu_i}}{\rho_\gamma} \quad \text{at early times,} \quad (37)$$

$$N_{\text{eff}}^l = \frac{8}{7} \left( \frac{11}{4} \right)^{4/3} \frac{\sum_i \rho_{\nu_i}}{\rho_\gamma} \quad \text{at late times,} \quad (38)$$

being  $\rho_\gamma$  the comoving energy density of photons and  $\rho_{\nu_i}$  the one of the  $i$ -th neutrino.

## II. COLLISION INTEGRALS

The full collision terms are defined by the sum of the contributions from neutrino–electron/positron scattering and  $e^\pm$  annihilation into neutrinos, plus neutrino–neutrino interactions. We neglect other reactions, such as  $\mu^\pm$  annihilation (which only affects at very early temperatures when everything is in equilibrium). We therefore have [2, 23]

$$\mathcal{I}[\varrho(y)] = \frac{G_F^2}{(2\pi)^3 y^2} \mathcal{I}^u, \quad (39)$$

$$\mathcal{I}^u \equiv \mathcal{I}_{\text{sc}}^u + \mathcal{I}_{\text{ann}}^u + \mathcal{I}_{\nu\nu}^u + \mathcal{I}_{\nu\bar{\nu}}^u, \quad (40)$$

$$\mathcal{I}_{\text{sc}}^u = \int dy_2 dy_3 \frac{y_2}{E_2} \frac{y_4}{E_4} \quad (41)$$

$$\left\{ (\Pi_2^s(y, y_4) + \Pi_2^s(y, y_2)) \left[ F_{\text{sc}}^{LL}(\varrho^{(1)}, f_e^{(2)}, \varrho^{(3)}, f_e^{(4)}) + F_{\text{sc}}^{RR}(\varrho^{(1)}, f_e^{(2)}, \varrho^{(3)}, f_e^{(4)}) \right] \right. \\ \left. - 2(x^2 + \delta m_e^2) \Pi_1^s(y, y_3) \left[ F_{\text{sc}}^{RL}(\varrho^{(1)}, f_e^{(2)}, \varrho^{(3)}, f_e^{(4)}) + F_{\text{sc}}^{LR}(\varrho^{(1)}, f_e^{(2)}, \varrho^{(3)}, f_e^{(4)}) \right] \right\},$$

$$\mathcal{I}_{\text{ann}}^u = \int dy_2 dy_4 \frac{y_3}{E_3} \frac{y_4}{E_4} \quad (42)$$

$$\left\{ \Pi_2^a(y, y_4) F_{\text{ann}}^{LL}(\varrho^{(1)}, \varrho^{(2)}, f_e^{(3)}, f_e^{(4)}) + \Pi_2^a(y, y_3) F_{\text{ann}}^{RR}(\varrho^{(1)}, \varrho^{(2)}, f_e^{(3)}, f_e^{(4)}) \right. \\ \left. + (x^2 + \delta m_e^2) \Pi_1^a(y, y_2) \left[ F_{\text{ann}}^{RL}(\varrho^{(1)}, \varrho^{(2)}, f_e^{(3)}, f_e^{(4)}) + F_{\text{ann}}^{LR}(\varrho^{(1)}, \varrho^{(2)}, f_e^{(3)}, f_e^{(4)}) \right] \right\},$$

$$\mathcal{I}_{\nu\nu}^u = \frac{1}{4} \int dy_2 dy_3 \Pi_2^\nu(y, y_2) F_{\nu\nu}(\varrho^{(1)}, \varrho^{(2)}, \varrho^{(3)}, \varrho^{(4)}), \quad (43)$$

$$\mathcal{I}_{\nu\bar{\nu}}^u = \frac{1}{4} \int dy_2 dy_3 \Pi_2^\nu(y, y_4) F_{\nu\bar{\nu}}(\varrho^{(1)}, \varrho^{(2)}, \varrho^{(3)}, \varrho^{(4)}), \quad (44)$$

where  $E_i^2 = \sqrt{x^2 + y_i^2 + \delta m_e^2}$  and

$$\Pi_1^s(y, y_3) = y y_3 D_1 + D_2(y, y_3, y_2, y_4), \quad (45)$$

$$\Pi_1^a(y, y_2) = y y_2 D_1 - D_2(y, y_2, y_3, y_4), \quad (46)$$

$$\Pi_2^s(y, y_2)/2 = y E_2 y_3 E_4 D_1 + D_3 - y E_2 D_2(y_3, y_4, y, y_2) - y_3 E_4 D_2(y, y_2, y_3, y_4), \quad (47)$$

$$\Pi_2^s(y, y_4)/2 = y E_2 y_3 E_4 D_1 + D_3 + E_2 y_3 D_2(y, y_4, y_2, y_3) + y E_4 D_2(y_2, y_3, y, y_4), \quad (48)$$

$$\Pi_2^a(y, y_3)/2 = y y_2 E_3 E_4 D_1 + D_3 + y E_3 D_2(y_2, y_4, y, y_3) + y_2 E_4 D_2(y, y_3, y_2, y_4), \quad (49)$$

$$\Pi_2^a(y, y_4)/2 = y y_2 E_3 E_4 D_1 + D_3 + y_2 E_3 D_2(y, y_4, y_2, y_3) + y E_4 D_2(y_2, y_3, y, y_4), \quad (50)$$

$$\Pi_2^\nu(y, y_2)/2 = y y_2 y_3 y_4 D_1 + D_3 - y y_2 D_2(y_3, y_4, y, y_2) - y_3 y_4 D_2(y, y_2, y_3, y_4), \quad (51)$$

$$\Pi_2^\nu(y, y_4)/2 = y y_2 y_3 y_4 D_1 + D_3 + y_2 y_3 D_2(y, y_4, y_2, y_3) + y y_4 D_2(y_2, y_3, y, y_4), \quad (52)$$

where the functions  $D_i$  have the following definitions [9]:

$$D_1(a, b, c, d) = \frac{16}{\pi} \int_0^\infty \frac{d\lambda}{\lambda^2} \prod_{i=a,b,c,d} \sin(\lambda i), \quad (53)$$

$$D_2(a, b, c, d) = -\frac{16}{\pi} \int_0^\infty \frac{d\lambda}{\lambda^4} \prod_{i=a,b} [\lambda i \cos(\lambda i) - \sin(\lambda i)] \prod_{j=c,d} \sin(\lambda j), \quad (54)$$

$$D_3(a, b, c, d) = \frac{16}{\pi} \int_0^\infty \frac{d\lambda}{\lambda^6} \prod_{i=a,b,c,d} [\lambda i \cos(\lambda i) - \sin(\lambda i)]. \quad (55)$$

The three functions can be written in a more efficient way for the calculation, since they can be solved analytically, see e.g. [10] for the complete expressions.

Finally, the functions that define the phase space factors in the collision terms are [2, 23]:

$$F_{sc}^{ab}(\varrho^{(1)}, f_e^{(2)}, \varrho^{(3)}, f_e^{(4)}) = f_e^{(4)}(1 - f_e^{(2)}) \left[ G^a \varrho^{(3)} G^b (1 - \varrho^{(1)}) + (1 - \varrho^{(1)}) G^b \varrho^{(3)} G^a \right] \\ - f_e^{(2)}(1 - f_e^{(4)}) \left[ \varrho^{(1)} G^b (1 - \varrho^{(3)}) G^a + G^a (1 - \varrho^{(3)}) G^b \varrho^{(1)} \right], \quad (56)$$

$$F_{ann}^{ab}(\varrho^{(1)}, \varrho^{(2)}, f_e^{(3)}, f_e^{(4)}) = f_e^{(3)} f_e^{(4)} \left[ G^a (1 - \varrho^{(2)}) G^b (1 - \varrho^{(1)}) + (1 - \varrho^{(1)}) G^b (1 - \varrho^{(2)}) G^a \right] \\ - (1 - f_e^{(3)})(1 - f_e^{(4)}) \left[ G^a \varrho^{(2)} G^b \varrho^{(1)} + \varrho^{(1)} G^b \varrho^{(2)} G^a \right], \quad (57)$$

$$F_{\nu\nu}(\varrho^{(1)}, \varrho^{(2)}, \varrho^{(3)}, \varrho^{(4)}) = (1 - \varrho^{(1)}) \varrho^{(3)} \left[ (1 - \varrho^{(2)}) \varrho^{(4)} + \text{Tr}(\dots) \right] \\ - \varrho^{(1)} (1 - \varrho^{(3)}) \left[ \varrho^{(2)} (1 - \varrho^{(4)}) + \text{Tr}(\dots) \right] + \text{h.c.} \quad (58)$$

$$F_{\nu\bar{\nu}}(\varrho^{(1)}, \varrho^{(2)}, \varrho^{(3)}, \varrho^{(4)}) = (1 - \varrho^{(1)}) (1 - \varrho^{(2)}) \left[ \varrho^{(4)} \varrho^{(3)} + \text{Tr}(\dots) \right] \\ - \varrho^{(1)} \varrho^{(2)} \left[ (1 - \varrho^{(4)}) (1 - \varrho^{(3)}) + \text{Tr}(\dots) \right] \\ + (1 - \varrho^{(1)}) \varrho^{(3)} \left[ \varrho^{(4)} (1 - \varrho^{(2)}) + \text{Tr}(\dots) \right] \\ - \varrho^{(1)} (1 - \varrho^{(3)}) \left[ (1 - \varrho^{(4)}) \varrho^{(2)} + \text{Tr}(\dots) \right] + \text{h.c.}, \quad (59)$$

where  $\varrho^{(i)} = \varrho(y_i)$  and  $f_e^{(i)} = f_{\text{FD}}(y_i, z)$  represent the momentum distribution function of the various particles, and  $\text{Tr}(\dots)$  denotes the trace of the term immediately before it. The full expression for these functions should take into account the lepton asymmetry and distinguish the momentum distributions of leptons/neutrinos from those of antilepton/antineutrinos. Since we do not include lepton asymmetry, we just report the expressions without the heavier notation required to distinguish the various terms.

Concerning the neutrino-neutrino collision terms [23], there are few more points to be discussed. We can see from Eqs. (58)–(59) that the expressions include up to four products of the neutrino density matrices. With a smart implementation of the integration methods (see sections IV and V), one can use for three of the terms (namely, the ones containing  $y_1$ ,  $y_2$  and  $y_3$ ) the values obtained on the momentum grid. For the fourth occurrence,  $\varrho(y_4)$ , an interpolation is needed. We tested several possibilities, and implemented a scheme that computes the linear interpolation of  $\varrho_{\alpha\alpha}/f_{\text{FD}}$  on the diagonal, and the linear interpolation of  $\varrho_{\alpha\beta}$  ( $\alpha \neq \beta$ ) for the off-diagonal, as it guarantees a better numerical stability (see [23]). Nevertheless, the selection of the momentum grid may have a

strong impact on the results obtained using neutrino–neutrino collision terms, as we will discuss in section VI. We have also verified that the numerical values of  $N_{\text{eff}}$  obtained including the integrals in Eqs. (43)–(44) does not vary significantly if we consider only the diagonal components of  $\varrho$ , or we instead consider the full matrix. The reason is that the off-diagonal terms are typically much smaller than the diagonal ones, so that their combinations are suppressed and give a small contribution to the collision terms. Ignoring the off-diagonal terms, therefore, gives a very precise result with a slightly smaller computational cost. Notice also that the implementation of the neutrino–neutrino collision terms as described here is the first that allows to compute off-diagonal collision terms taking into account the full neutrino density matrix [23].

The code can compute the collision terms according to Eqs. (41)–(44), but the integrals are very expensive. For the non-diagonal terms of the collision matrix we therefore allow the possibility to use damping approximations, in the form

$$\mathcal{I}_{\alpha\beta}^u(\varrho) = -D_{\alpha\beta}\varrho_{\alpha\beta}, \quad (60)$$

for  $\alpha \neq \beta$ . Notice that  $\mathcal{I}_{\alpha\beta}^u(\varrho)$  is the unnormalized term defined in Eq. (40). The expressions for the coefficients  $D_{\alpha\beta}$  depend on the elements considered. In case more than one sterile state is considered, the terms  $D_{s_i s_j}$  are always zero. For the rest of the terms, two possibilities are implemented in the code.

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The second possibility is to implement the coefficients derived in [11], see also [12, 13], which can be written as

$$D_{e\mu}/F = D_{e\tau}/F = 15 + 8 \sin^4 \theta_W, \quad (61)$$

$$D_{\mu\tau}/F = 7 - 4 \sin^2 \theta_W + 8 \sin^4 \theta_W, \quad (62)$$

$$D_{es}/F = 29 + 12 \sin^2 \theta_W + 24 \sin^4 \theta_W, \quad (63)$$

$$D_{\mu s}/F = D_{\tau s}/F = 29 - 12 \sin^2 \theta_W + 24 \sin^4 \theta_W, \quad (64)$$

where  $F = 7\pi^4 z^4 y^3 / 135$  is a common normalisation coefficient.

### III. SOLVER AND INITIAL CONDITIONS

We solve the differential equations with the DLSODA routine from the ODEPACK[14] Fortran package [15, 16]. ODEPACK is a collection of solvers for the initial value problem for systems of ordinary differential equations. It includes methods to deal with stiff and non-stiff systems, and some of the provided subroutines automatically recognise which type of problem they are facing.

The specific solver we use, DLSODA, is a modification of the Double-precision Livermore Solver for Ordinary Differential Equations (DLSODE) which includes an automatic switching between stiff and non-stiff problems of the form  $dy/dt = f(t, y)$ . In the stiff case, it treats the Jacobian matrix  $df/dy$  as either a dense (full) or a banded matrix, and as either user-supplied or internally approximated by difference quotients. It uses Adams methods (predictor-corrector) in the non-stiff case, and Backward Differentiation Formula (BDF) methods (the Gear methods) in the stiff case. The linear systems that arise are solved by direct methods (LU factor/solve). For more details, see the original publications [15, 16].

The initial conditions for DLSODA are defined as follows. The initial time  $x_{\text{in}}$  is an input parameter of the code, and reasonable values would correspond to temperatures between a few hundreds and a few tens of MeV. The initial comoving photon temperature is computed evolving Eq. (25) from even earlier times ( $z_0 = 1$  at  $T_0 = 10 m_\mu$ ,  $x_0 = m_e/T_0$ ) until  $x_{\text{in}}$ . The obtained value  $z_{\text{in}}$  is then considered as the temperature of equilibrium of the entire plasma. Concerning the neutrino density matrix at  $x_{\text{in}}$ , all off-diagonal elements and the diagonal ones for sterile neutrinos are fixed to zero, while the diagonal elements corresponding to active neutrinos are Fermi-Dirac distributions with a temperature  $z_{\text{in}}$ . For typical values that we use in the code, we have  $z_{\text{in}} - 1 = 2.9 \times 10^{-4}$  for  $x_{\text{in}} = 0.001$  (which we use for the 3+1 cases) or  $z_{\text{in}} = 1.098$  for  $x_{\text{in}} = 0.05$  (suitable for the three-neutrino case, see [2]).

### IV. MOMENTUM GRID

In order to follow the evolution of Eq. (1), we discretise its dependence on  $y$  and evolve each of the momentum in  $x$ . One of the most interesting ways to make the code more precise and faster is related to the choice of the  $y_i$ . Discretising the momenta with a linear or logarithmic spacing works, but it is not the most efficient way to generate the grid. Inspired by one of the methods used in CLASS (see [17]), we deeply tested and finally considered a spacing

based on the Gauss-Laguerre (GL) integration method. The crucial point of the calculation is to compute the energy density of neutrinos, given by

$$\rho_\alpha = \frac{1}{\pi^2} \int_0^\infty dy y^3 \varrho_{\alpha\alpha}(y), \quad (65)$$

where  $\varrho_{\alpha\alpha}(y)$  will be close to a Fermi-Dirac distribution and in any case always exponentially suppressed. The Gauss-Laguerre quadrature (see e.g. [18]) is a method that is designed to optimise the solution of integrals of the type

$$I = \int_0^\infty dx y^\alpha e^{-y} f(y) \simeq \sum_i^N w_i^{(\alpha)} f(y_i), \quad (66)$$

where  $f(y)$  is a generic function,  $y_i$  are the  $N$  roots of the Laguerre polynomial  $L_N$  of order  $N$ , and  $w_i$  are relative weights, which are obtained using

$$w_i^{(\alpha)} = \frac{y_i}{(N+1)^2 \left[ L_{N+1}^{(\alpha)}(y_i) \right]^2}. \quad (67)$$

The weights can be computed for example using the `gaulag` routine from [18]. Since our momentum distribution function is not directly proportional to  $e^{-y}$ , we consider  $f(x) = e^y \varrho_{\alpha\alpha}(y)$ , in order to rescale the weights appropriately.

For the simple purpose of integrating the Fermi-Dirac distribution, very few points are typically required. `CLASS`, for example, uses order of ten points for integrating the neutrino distribution. In our case the non-thermal distortions must be computed accurately, and in particular when evolving the thermalisation of a sterile neutrino we need more precision on the small momenta. On the other hand, we do not want to compute the momentum distribution function at very high  $y$ , which gives a very small contribution to the total integral. We therefore use a truncated list of nodes  $y_i$  over which to compute the evolution of  $\varrho$ , selecting only the  $N_y \leq N$  nodes for which  $y_i < 20$ . In this way we can increase the number of points at small  $y$  and the resolution on the thermalisation processes without having to compute a large number of points at high momentum. The number of points we can use is limited by the accuracy of the algorithm that computes the  $w_i$ . For the `gaulag` routine [18], our setup allows to reach  $N_y \sim 50$  when  $N \sim 350$ , when  $y_i < 20$ . This number of momentum nodes is already large enough to reach a precision much better than one per mille on  $N_{\text{eff}}$ , which is the same we could obtain with a linear spacing of the points and  $N_y = 100$  [2]. Since the evaluation of the collision integrals scales as  $N_y^2$  and the number of derivatives in Eq. (25) scales with  $N_y$ , this ensures a significant gain. Unfortunately, since the method used to compute the GL nodes does not allow to increase  $N_y$  arbitrarily, the GL method has limitations when the neutrino-neutrino collision terms are considered. We further comment on these points in the next sections.

## V. NUMERICAL CALCULATION OF 1D AND 2D INTEGRALS

Most of the processing time is spent to compute the collision integrals discussed in section II, which are two-dimensional integrals in the momentum. We compute the integrals using a two-dimensional version of the Gauss-Laguerre method, which has been tested to be precise enough,

$$\int_{x_1}^{x_N} \int_{y_1}^{y_M} dx dy f(x, y) = \sum_{i=1}^N \sum_{j=1}^M w_i w_j f_{ij}. \quad (68)$$

This works under the assumption that  $f(x, y)$  is exponentially suppressed both in  $x$  and  $y$ . Such assumption is valid in our case, as the functions  $F_{ab}$  always contain products of momentum distribution functions, which are typically very close to the Fermi-Dirac. The only exception is the case of the additional neutrino, for which the distribution can be very different from the Fermi-Dirac, but in any case it is always exponentially suppressed, since the lowest momenta are always populated first and its momentum distribution can never exceed the one of standard neutrinos.

When using a linear/logarithmic spacing of points, instead we perform the integrals using a composite two-dimensional Newton-Cotes (NC) formula of order 1 [19]:

$$\int_{x_1}^{x_N} \int_{y_1}^{y_M} dx dy f(x, y) = \sum_{i=1}^{N-1} \sum_{j=1}^{M-1} (x_j - x_i)(y_j - y_i) \left[ \frac{f_{ij} + f_{i+1,j} + f_{i,j+1} + f_{i+1,j+1}}{4} \right], \quad (69)$$

where we used the short notation  $f_{i,j} = f(x_i, y_j)$ , while  $i$  and  $j$  run over the grid of momenta we are using, which contains  $N = M = N_y$  points for each dimension. This avoids us the need to interpolate the density matrix in points outside the momentum grid.

The integrals therefore require  $N_y^2$  evaluations of the integrands at each evaluation: this means that reducing the value of  $N_y$  by a factor of two gives a factor four faster calculation of the integrals. The actual gain in the code is even larger, since the DLSODA algorithm needs to explore less combinations of variations in the  $\varrho_{\alpha\beta}(y_l)$  for the different  $y_l$  in the momentum grid. Our goal is therefore to obtain with a coarse grid a result that is in reasonable agreement with the one obtained using a fine grid.

In order to obtain the maximum speed, we study the accuracy of each function that enters the code in comparison with the analytical results, were they can be obtained. The number of points and the integration methods adopted in all the integrals, for example, have been carefully studied to achieve a reasonable precision with a short computation time. For the two-dimensional integrals, the selected momentum grid fully defines the integration procedure, and the precision is always good when using a reasonable number of points. Depending on the function, we may adopt the Gauss-Laguerre, Newton-Cotes or Romberg integration [20] methods for the one-dimensional integrals. In particular, for the electron and muon energy densities and for most of the functions that enter the calculation of Eq. (25) we use a Gauss-Laguerre method on a dedicated grid of up to 110 points for the most complicated functions. In one single case, the  $K'(r)$  function derived from Eq. (12), the result obtained with the Gauss-Laguerre method did not reach the requested precision and we decided to use a Romberg integration instead. Although this requires a longer computation time, it only affects the initialisation stage, as in the code we interpolate over the pre-computed values. The number of points and the interpolation range have also been studied in order to obtain sufficiently precise results for all the computations required in the code.

## VI. PRECISION OF THE FINAL RESULTS

We have tested our code with the results available in the literature and verified the robustness of our findings against changes in the settings used in the calculations. In particular, we refer to the high-precision results in the three-neutrino case of [2], from which we have adopted most of the equations. Most of the results summarized here are discussed more in details in [1, 23].

Concerning the value of  $N_{\text{eff}}$  that we obtain using only active neutrinos, if we ignore neutrino-neutrino collision terms, we verified that we can reach much better than per mille stability on  $N_{\text{eff}} = 3.044$  using  $N_y \geq 20$  points spaced with the Gauss-Laguerre method, if the tolerance for DLSODA [21] is  $10^{-6}$ . This means that using  $N_y = 50$  instead of  $N_y = 20$  does not significantly alter the result. If we want to consider a linear or logarithmic spacing for the momentum grid, a minimum of 40 grid points must be employed in order to reach the same level of stability. Another possible setting that can give us a faster execution of the code is the precision used for DLSODA. We verified that once the tolerance for DLSODA is smaller than  $10^{-5}$ , the results are already stable at a level much better than per mille (actually closer to the 0.1 per mille) with respect to the most precise case considered here ( $N_y = 50$ , tolerance  $10^{-6}$ ). Using a tolerance of  $10^{-4}$  gives a value of  $N_{\text{eff}}$  which is stable at the level of few per mille, and still better than 1%.

A full calculation of  $N_{\text{eff}}$ , in any case, must be performed taking into account also the neutrino-neutrino collision terms. Including them raises  $N_{\text{eff}}$  by approximately 0.002, depending on the values of the oscillation parameters and the considered momentum grid. Mostly because of the interpolation required to compute  $\varrho(y_4)$  in Eqs. (58)–(59), the numerical uncertainties grow significantly: when a coarse grid is considered, the interpolation is much less precise and the final results are much more instable. As expected, however, the instability decreases when the number of momentum nodes is increased. It is worth noticing that a GL grid tends to give a slightly higher estimation of  $N_{\text{eff}}$  than a grid with linearly spaced momentum nodes, with a difference of  $\sim 0.001$  between the GL case with  $N_y = 50$  and a mixed linear/logarithmic spacing with  $N_y = 100$ , when requiring all the nodes to satisfy  $y_i < 20$ . Since our GL method does not allow to increase arbitrarily the number of nodes when imposing the upper limit on their value, we cannot have a more precise estimate of the effect of the momentum grid, nor to determine at which  $N_y$  the two different momentum grid schemes converge to the same value of  $N_{\text{eff}}$  when requiring a higher precision.

Considering the implementation of the off-diagonal collision terms, we find that the  $N_{\text{eff}}$  output does not change significantly if we use the full integrals or the damping terms, both for neutrino-neutrino and neutrino-electron contributions. The damping formulas are sufficiently good to obtain a very precise result and allow to save a lot of computation time.

If we repeat the same exercise in the 3+1 scheme, using  $\Delta m_{41}^2 = 1.29 \text{ eV}^2$ ,  $|U_{e4}|^2 = 0.012$  [22] and  $|U_{\mu 4}|^2 = |U_{\tau 4}|^2 = 0$ , we find similar conclusions. A tolerance of  $10^{-5}$  gives results very close to those obtained with  $10^{-6}$ , while any larger tolerance gives larger fluctuations depending on  $N_y$ . With  $10^{-4}$ , the precision remains of the order of 0.5%, so it is still safe to compute the value of  $N_{\text{eff}}$  on a grid of active-sterile mixing parameters using this level of precision. With  $N_y = 20$ , a single run takes a few minutes on four cores, and the running time is not significantly affected



by changes in the DLSODA tolerance. When more precision is required, however, the algorithm may have troubles in resolving some of the resonances, and in that case the run can take much longer because of the adaptive nature of the solver.

Another parameter that we tested is the initial value of  $x$ ,  $x_{\text{in}}$ . Apart for fluctuations which are compatible with those obtained varying  $N_y$ , the result is stable against variations in  $5 \times 10^{-4} \leq x_{\text{in}} \leq 5 \times 10^{-2}$ . The largest values of  $x_{\text{in}}$  may be inappropriate for high values of  $\Delta m_{41}^2$ , as it is important for the solver to start the evolution before the sterile state starts to oscillate significantly with the active ones. Smaller values, on the contrary, may create numerical problems in DLSODA due to the very small initial value  $z_{\text{in}} - 1$ , and are never really required for our purposes.

More details on the precision of numerical calculations and the dependence of  $N_{\text{eff}}$  on physical parameters (including Fermi constant, Weinberg angle mass and neutrino mixing parameters) are discussed in [23], considering the three-neutrino case only. In order to study the accuracy of the numerical calculations as functions of the physical parameters, the tolerance for DLSODA has been set to  $10^{-7}$ . Considering variations for the physical parameters in the allowed  $3\sigma$  range (from [24] for the neutrino mixing parameters, from [25] for the weak interaction parameters), we see that the stability of  $N_{\text{eff}}$  is at the  $10^{-4}$  level or better. A similar precision is obtained when changing the way the off-diagonal terms. Altering  $x_{\text{in}}$ , which controls the initial time in the code, only affects  $N_{\text{eff}}$  at the  $10^{-5}$  level. More critical is the dependence on  $N_y$ , which controls the number and the position of the nodes of the momentum grid. Varying  $N_y$  between 25 and 50 only alters the final result at the  $10^{-4}$  level, if neutrino–neutrino collision terms are ignored, but has a much bigger impact if they are considered. In general, variations up to 0.001 can be expected if one includes neutrino–neutrino collisions and changes the momentum grid (using a linear spacing or a GL one for the  $y$  nodes), assuming that a sufficiently high number of nodes is considered ( $N_y \geq 40$  for GL spacing of the nodes,  $N_y \geq 80$  for a linear one).

As a summary, a reasonable estimate of the theoretical and numerical uncertainty on the recommended value obtained considering three active neutrinos,  $N_{\text{eff}} = 3.045$ , is of order  $10^{-3}$ .

## VII. DEFAULTS PARAMETERS

blablabla

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