Management Center Innsbruck

Department of Technology & Life Sciences

Master's program Mechatronics & Smart Technologies



Report

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about

Discrete PID Controller Design for a Buck Converter

from

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Contents

1	Introduction	1
2	Methods	2
3	Results	4
4	Discussion	6
Bi	ibliography	II
Lis	st of Figures	Ш
Lis	st of Tables	IV

Introduction

A discrete Proportional-Integral-Derivative (PID) controller for a $12\,V$ to $5\,V$ Buck-Converter is to be designed and tested using PLECS [1].

The self-imposed charcteristics of the buck converter and the chosen passive components according to [2] are given in Table 1.1 and Table 1.2 respectively.

Parameter	Value
$V_{in,nominal}$	12 V
$V_{in,min}$	8 V
$V_{\sf in,max}$	16 V
V_{out}	5 V
I_{out}	1 A
ΔI_{L} at $V_{in,max}$	400 mA
$f_{\sf sw}$	50 kHz

Table 1.2. Passive components of the Buck-Converter

Component

 \overline{L}

C

R

Value

200 μΗ

50 μF

5Ω

Table 1.1. Buck-Converter Characteristics

A continous controller can be designed according to [3] – for simplicity, the parameters were kept the same for the discrete controller

Parameter	Value
K_D	50LC
K_P	$50\frac{L}{R}$
K_I	50

Table 1.3. PID Controller Parameters

Methods

The PLECS model of the converter includes the following:

- a PID controlled duty cycle
- a noise source for the input voltage
- a variable load

all of which can be selected to be active or inactive as can be seen in Figure 2.1 and Figure 2.2.

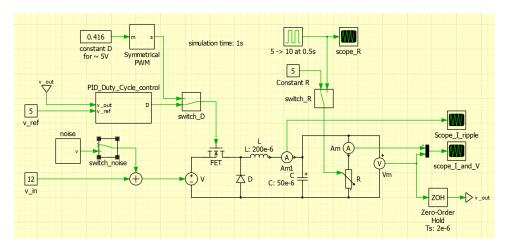
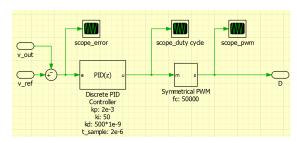
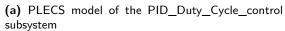


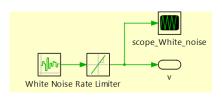
Figure 2.1. PLECS model of the Buck-Converter

The control of the converter was tested under the following conditions and compared to the behaviour of the converter with a fixed duty cycle:

- noise on the input voltage (white noise with a standard deviation of 1 V and a sample time of 50 ms as seen in Figure 2.3)
- a load step from 5Ω to 10Ω at 0.5 s
- startup behaviour







(b) PLECS model of the noise subsystem

Figure 2.2. PLECS model subsystems

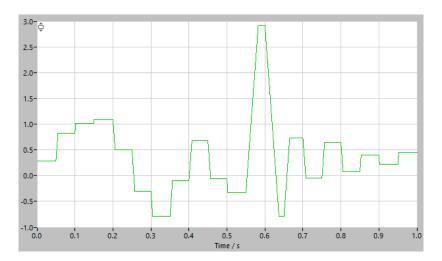


Figure 2.3. White noise with a standard deviation of $1\,\mathrm{V}$ and a sample time of $50\,\mathrm{ms}$

Results

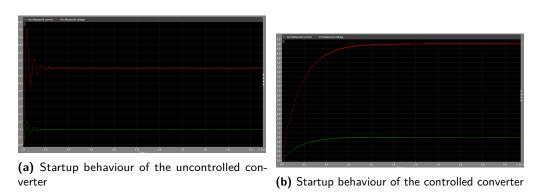
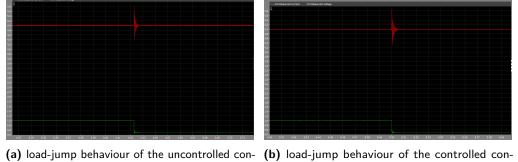


Figure 3.1. Comparison of the startup behaviour of the uncontrolled and controlled converter with current (green) and voltage (red) signals



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Figure 3.2. Comparison of the load-jump behaviour of the uncon-

Figure 3.2. Comparison of the load-jump behaviour of the uncontrolled and controlled converter with current (green) and voltage (red) signals

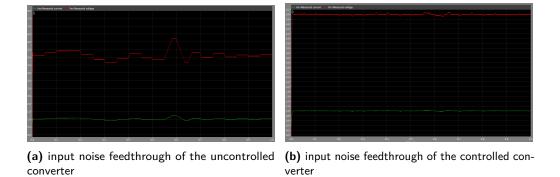


Figure 3.3. Comparison of the input noise feedthrough behaviour of the uncontrolled and controlled converter with current (green) and voltage (red) signals

Discussion

The uncontrolled converter shows a significant overshoot and oscillation before settling to the working point at startup. The controlled converter shows a much smoother startup behaviour, but the settling time is longer than for the uncontrolled converter as shown in Figure 3.1.

The load-jump behaviour of the controlled converter still shows a spike at the load-jump, but quickly settles to the working point as can be seen in Figure 3.2, whereas the uncontrolled converter delivers a higher unwanted constant ouput voltage after the jump.

The input noise feedthrough of the controlled converter is significantly reduced, although not completely eliminated, compared to the uncontrolled converter as can be seen in Figure 3.3.

Overall, the behavioural characteristics of the converter have improved with the addition of the PID-Controller.

Bibliography

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- [3] Ahmad Saudi Samosir, Tole Sutikno, and Luthfiyyatun Mardiyah. "Simple Formula for Designing the PID Controller of a DC-DC Buck Converter". In: International Journal of Power Electronics and Drive Systems (IJPEDS) 14.1 (1 Mar. 1, 2023), pp. 327-336. ISSN: 2722-256X. DOI: 10.11591/ijpeds.v14. i1.pp327-336. URL: https://ijpeds.iaescore.com/index.php/IJPEDS/article/view/22366 (visited on 01/13/2025).

List of Figures

2.1	PLECS model of the Buck-Converter	2
2.2	PLECS model subsystems	3
2.3	White noise with a standard deviation of 1 V and a sample time of	
	50 ms	3
3.1	Comparison of the startup behaviour of the uncontrolled and controlled	
	converter with current (green) and voltage (red) signals	4
3.2	Comparison of the load-jump behaviour of the uncontrolled and	
	controlled converter with current (green) and voltage (red) signals .	4
3.3	Comparison of the input noise feedthrough behaviour of the uncon-	
	trolled and controlled converter with current (green) and voltage (red)	
	signals	5

List of Tables

1.1	Buck-Converter Characteristics	1
1.2	Passive components of the Buck-Converter	1
1.3	PID Controller Parameters	1