

# Differential Equations in Geophysical Fluid Dynamics

## XIII. Wind-driven circulation: Stommel wind-driven circulation

Jang-Geun Choi

Center for Ocean Engineering  
University of New Hampshire

Apr, 2025

This seminar is supported by mathematics community EM (maintained by Prof. Gunhee Cho)  
and oceanography community COKOAA.

## Recap

Stommel's wind-driven circulation problem in vorticity equation form is given by

$$\beta \frac{\partial \psi}{\partial x} = \frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s - \frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) \quad (1)$$

Diagram illustrating the components of the equation:

- $\beta \frac{\partial \psi}{\partial x}$ : Planetary  $\beta$ -term (indicated by a blue arrow from the text below)
- $\frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s$ : Wind stress curl (indicated by a red arrow from the text below)
- $-\frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right)$ : Bottom stress curl (indicated by a blue arrow from the text above)

where  $\beta = \partial f / \partial y$  can be approximated to constant ( $f \approx f_0$  if  $y/R \ll 1$ ;  $f$ -plane) or linear polynomial ( $f_0 + \beta_0 y$  if  $y/R < 1$ ;  $\beta$ -plane).

## Recap

Over the  $f$ -plane where  $f \approx f_0$  so  $\beta \approx 0$ , the governing equation can be simplified to

$-(\gamma/h)\nabla \times \vec{u}$ : Bottom stress curl

$$0 = \frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s - \frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) \quad (2)$$

that can be rewritten as  $\nabla \times \vec{u} = (1/(\rho_0 \gamma)) \nabla \times \vec{\tau}^s$  implying curl of ocean current is proportional to the wind stress curl (rotates in same direction).

Note that the momentum equation we used is

Geostrophic

$$i f \vec{u} = -g \frac{\partial \eta}{\partial \vec{n}} + \frac{\vec{\tau}^s}{\rho_0 h} - \frac{\gamma}{h} \vec{u} \quad (3)$$

Surface Ekman

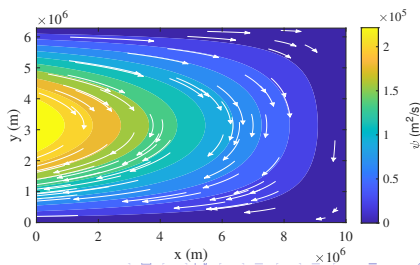
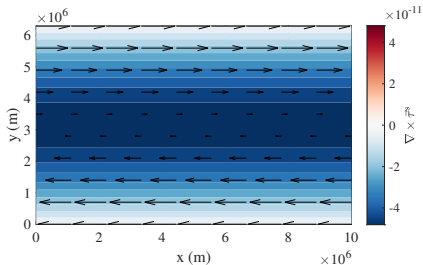
Bottom Ekman

## Recap

Over the  $\beta$ -plane where  $f_0 + \beta_0 y$ , if length scale is large enough to ignore bottom frictional stress curl, the governing equation can be simplified to

$$\beta \frac{\partial \psi}{\partial x} = \frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s - \frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) \quad (4)$$

that is referred to as **Sverdrup balance** (Sverdrup, 1947). This is easy to solve and good enough “interior flow” but can consider only one boundary condition.



# Governing equations

Stommel (1948) discussed

$$\frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) + \beta \frac{\partial \psi}{\partial x} = \frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s \quad (5)$$

with simple forcing (wind stress fields), that idealized wind stress pattern, given by

$$\vec{\tau}^s = (\tau_x^s, \tau_y^s) = (-\tau_0 \cos(\pi y/L_y), 0). \quad (6)$$

So, substituting (6) into (5) yields

$$\boxed{\frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) + \beta \frac{\partial \psi}{\partial x} = -\frac{\tau_0 \pi}{\rho_0 h L_y} \sin(\pi y/L_y)} \quad (7)$$

The boundary conditions are given by

$$\boxed{\psi|_{x=0} = 0, \quad \psi|_{x=L_x} = 0, \quad \psi|_{y=0} = 0, \quad \psi|_{y=L_y} = 0.} \quad (8)$$

# Stommel's wind-driven circulation

Solution to (7) with boundary conditions (8) is given by

$$\psi = \frac{\tau_0 L_y}{\rho_0 \gamma \pi} \left( 1 - \frac{(e^{k^- L_x} - 1)e^{k^+ x} + (1 - e^{k^+ L_x})e^{k^- x}}{e^{k^- L_x} - e^{k^+ L_x}} \right) \quad (9a)$$

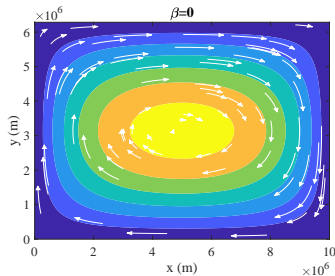
$$k^+ = \frac{-h\beta/\gamma + \sqrt{(h\beta/\gamma)^2 + 4(\pi/L_y)^2}}{2} \quad (9b)$$

$$k^- = \frac{-h\beta/\gamma - \sqrt{(h\beta/\gamma)^2 + 4(\pi/L_y)^2}}{2} \quad (9c)$$

# Stommel's wind-driven circulation

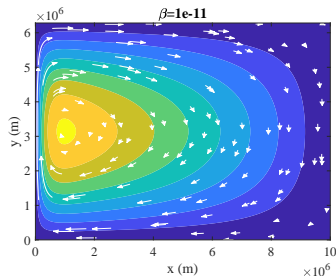
Solution without  $\beta$ -term

$$\frac{\gamma}{h} \nabla^2 \psi = \frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s$$



Solution with  $\beta$ -term

$$\frac{\gamma}{h} \nabla^2 \psi + \beta \frac{\partial \psi}{\partial x} = \frac{1}{\rho_0 h} \nabla \times \vec{\tau}^s$$



Consideration of the  $\beta$ -term tilts the stream function (and sea surface height) westward. This is referred to as “ $\beta$ -effect” yielding western boundary intensification.



# Summary

$$c \frac{\partial \psi}{\partial t} - \beta \frac{\partial \psi}{\partial x} = \frac{\gamma}{h} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right) + \frac{\tau_0 L_y}{\rho_0 \gamma \pi} \sin(\pi y / L_y) \quad (10)$$

1. Note that the governing equation of Stommel's wind-driven circulation problem is the “steady” advection-diffusion equation with forcing term.
2. The planetary  $\beta$ -term plays a role in advecting  $\psi$  toward the negative  $x$ -direction (westward).
3. Due to the  $\beta$ -term, the stream function (sea surface height) becomes asymmetric: steep along the narrow west coast and gentle in the other region. As a result, western boundary (geostrophic) currents are intensified.



# References I

-  Stommel, Henry (1948). "The westward intensification of wind-driven ocean currents". In: *Eos, Transactions American Geophysical Union* 29.2, pp. 202–206.
-  Sverdrup, Harald Ulrich (1947). "Wind-driven currents in a baroclinic ocean; with application to the equatorial currents of the eastern Pacific". In: *Proceedings of the National Academy of Sciences* 33.11, pp. 318–326.