# Differential Equations in Geophysical Fluid Dynamics

IV. Generalization of forcing term

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#### Wind-forced linear momentum equation:

$$\frac{\partial \vec{u}}{\partial t} + if\vec{u} = \frac{\vec{\tau}^s}{\rho_0 h} = \frac{\hat{\tau}_0}{\rho_0 h} e^{-iw_0 t}$$

$$\left(\frac{1}{fT}\right) \frac{\partial \vec{u}^*}{\partial t^*} + i\vec{u}^* \text{ where } 1/(fT) \equiv Ro_T$$
is the temporal Rossby number.

Solution to the problem is given by

$$\vec{u} = \frac{\hat{\tau}_0 e^{-iw_0 t}}{\rho_0 hi(f - w_0)}.$$
 (2)

$$\frac{\partial \vec{u}}{\partial t} + if\vec{u} = \frac{\vec{\tau}^s}{\rho_0 h} = \frac{\hat{\tau}_0}{\rho_0 h} e^{-iw_0 t}$$
$$\vec{u} = \frac{\hat{\tau}_0 e^{-iw_0 t}}{\rho_0 h i (f - w_0)}$$

1. case  $w_0 \ll f$  (low frequency or short period forcing)

$$\vec{u} pprox rac{\vec{ au}^s}{i
ho_0 hf} \equiv \vec{u}_e$$
 (3)

that satisfies

$$if ec{u} pprox rac{ec{ au}^s}{
ho_0 h} \ .$$
 (4)

Negligible inertia

$$\frac{\partial \vec{u}}{\partial t} + if\vec{u} = \frac{\vec{\tau}^s}{\rho_0 h} = \frac{\hat{\tau}_0}{\rho_0 h} e^{-iw_0 t}$$
$$\vec{u} = \frac{\hat{\tau}_0 e^{-iw_0 t}}{\rho_0 hi(f - w_0)}$$

2. case  $w_0 \gg f$  (high frequency or long period forcing)

$$\vec{u} \approx \frac{\vec{\tau}^s}{(-iw_0)\rho_0 h} \tag{5}$$

that satisfies

$$\frac{\partial \vec{u}}{\partial t} pprox \frac{\vec{\tau}^s}{\rho_0 h} \,.$$
 (6)

https://www.youtube.com/watch?v=w1UsKanMatM https://www.youtube.com/watch?v=nJphsM4obOk

Negligible Coriolis force

$$\begin{split} \frac{\partial \vec{u}}{\partial t} + i f \vec{u} &= \frac{\vec{\tau}^s}{\rho_0 h} = \frac{\hat{\tau}_0}{\rho_0 h} e^{-ift} \\ \text{As } w_0 \to f, & \vec{u} &= \frac{\hat{\tau}_0 e^{-iw_0 t}}{\rho_0 hi ( \ f - w_0 \ )} \\ \text{magnitude of } \vec{u} \text{ increases!} \end{split}$$

3. case  $w_0 \approx f$  (frequency close to the system's natural frequency)

$$\vec{u} = \frac{\hat{\tau}_0}{\rho_0 h} t e^{-ift} \tag{7}$$

Amplitude linearly increase with time!

that is what we call "resonance".

#### Introduction

Why have so many people used sinusoidal (or monochromatic) forcing?

1. Stommel's (1948) wind driven circulation

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + A \frac{\partial \psi}{\partial x} = B \sin(k_0 y) \tag{8}$$

2. Cushman-Roisin's (2011) upwelling problem

$$\frac{\partial^3 \psi}{\partial t^3} - A \frac{\partial^3 \psi}{\partial t \partial x^2} + B \frac{\partial \psi}{\partial t} = 0, \quad \frac{\partial \psi}{\partial x} \Big|_{x=0} = C \cos(w_0 t) \quad (9)$$

3. Csanady's (1978) steady coastal trapped wave problem

$$-A\frac{\partial \psi}{\partial y} = \frac{\partial^2 \psi}{\partial x^2}, \quad \frac{\partial \psi}{\partial x} \bigg|_{x=0} = B \cos(k_0 y) \tag{10}$$



# Superposition principle:

# Key characteristics of linear differential equations

Problem with additional sinusoidal forcing term

$$\frac{\partial \vec{u}}{\partial t} + \left(if + \frac{\gamma}{h}\right)\vec{u} = \frac{\hat{\tau}_0}{\rho_0 h} e^{-iw_0 t} + \frac{\hat{\tau}_1}{\rho_0 h} e^{-iw_1 t}$$

$$\equiv L[\vec{u}] \text{ where } L = \frac{\partial}{\partial t} + (if + \frac{\gamma}{h})$$
(11)

Superposition principle of linear non-homogeneous differential equation

- 1. Once  $L[u_0] = f_0$  and  $L[u_1] = f_1$ ,  $L[c_0u_0 + c_1u_1] = c_0f_0 + c_1f_1$ .
- 2. Therefore, once  $L[u_0] = f_0$ ,  $L[u_0 + Cu_1] = f_0$  where  $L[u_1] = 0$  (case of  $f_1 = 0$ ).

## Generalization to problem with arbitrary forcing term

Arbitrary function of t (any time series of wind stress)

$$\frac{\partial \vec{u}}{\partial t} + \left(if + \frac{\gamma}{h}\right)\vec{u} = \frac{\vec{\tau}^s(t)}{\rho_0 h} \equiv \frac{1}{\rho_0 h} \sum_{n = -\infty}^{\infty} \hat{\tau}_n e^{-iw_n t}$$
(12)

Note that

$$\hat{\tau}(w) = \mathcal{F}(\vec{\tau}(t)) \tag{13}$$

where  $\mathcal{F}$  indicates Fourier operator. Particular solution to the problem is

$$\vec{u} = \sum_{n=-\infty}^{\infty} \underbrace{\frac{1}{\rho_0 h(i(f-w_n) + \gamma/h)} \hat{\tau}_n e^{-iw_n t}}_{\hat{u}(w_n)}. \tag{14}$$

Fourier series

## Generalization to problem with arbitrary forcing term

Let us consider problem without initial condition ( $\lim_{t\to-\infty} \vec{u} = 0$ )

$$\vec{u} = \frac{1}{\rho_0 h} \sum_{n = -\infty}^{\infty} \frac{1}{(i(f - w_n) + \gamma/h)} \hat{\tau}_n e^{-iw_n t} .$$
 (15)

Corresponding solution (Lentz and Winant, 1986; Austin and Barth, 2002) obtained by the integrating factor is given by

$$\vec{u} = \frac{1}{\rho_0 h} \int_{-\infty}^t g(\tilde{t} - t) \vec{\tau}(\tilde{t}) d\tilde{t} .$$

$$= \frac{1}{\rho_0 h} \int_{-\infty}^t g(\tilde{t} - t) \vec{\tau}(\tilde{t}) d\tilde{t} .$$

$$= \frac{1}{\rho_0 h} \int_{-\infty}^t g(\tilde{t} - t) \vec{\tau}(\tilde{t}) d\tilde{t} .$$

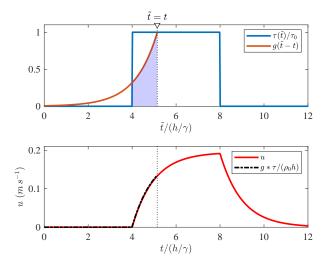
$$= \frac{1}{\rho_0 h} \int_{-\infty}^t g(\tilde{t} - t) \vec{\tau}(\tilde{t}) d\tilde{t} .$$
(16)

where  $g(t^{\star}) = e^{(if + \gamma/h)t^{\star}}$ .

If solution is unique, they must be same. This is end up with "convolution theorem":

$$\hat{g}(w)\hat{\tau}(w) = \mathcal{F}(g(t) * \vec{\tau}(t)) \tag{17}$$

# Generalization to problem with arbitrary forcing term



#### The slab model

Pollard and Millard (1970):

$$\frac{\partial \vec{u}}{\partial t} + if\vec{u} = \frac{\vec{\tau}}{\rho_0 h_1} - \gamma^* \vec{u}$$
 (18)

where  $\gamma^*$  represents linear damping coefficient, that can be determined by calibration.

This is a theoretical model that can still be used for publication (Whitt and Thomas, 2015; Gough et al., 2016; Wang et al., 2019; Zhang et al., 2023)!

#### Summary

$$\frac{\partial \vec{u}}{\partial t} + if\vec{u} = \frac{\vec{\tau}(t)}{\rho_0 h_1} - \gamma^* \vec{u}$$

where  $\vec{\tau}(t)$  is an arbitrary function of t. Solution to the problem is given by

$$\vec{u} = \frac{1}{\rho_0 h} \sum_{n = -\infty}^{\infty} \frac{1}{(i(f - w_n) + \gamma/h)} \hat{\tau}_n e^{-iw_n t}$$

$$= \frac{1}{\rho_0 h} \int_{-\infty}^{t} g(\tilde{t} - t) \vec{\tau}(\tilde{t}) d\tilde{t} .$$
(19)

where  $g(t^\star)=e^{(if+\gamma/h)t^\star}$ . This implies convolution theorem. The contribution of past wind stress to the present current decays exponentially over time by friction term.

#### Assignment

$$\frac{\partial \vec{u}}{\partial t} + if\vec{u} = -g\frac{\partial \eta}{\partial \vec{n}} - \frac{\gamma}{h}\vec{u}$$
 (20a)

$$\vec{u}|_{t=0} = \vec{U}_0$$
 (20b)

$$\frac{d\vec{X}}{dt} = \vec{u} \tag{21}$$

where  $-g\partial\eta/\partial\vec{n}$  is arbitrary constants and  $\vec{X}=X+iY.$  X and Y represent x- and y-position of an object, respectively.

- 1. Solve differential equation (23) for  $\vec{u}$ . What is physical meaning of particular solution component?
- 2. Solve (24) using  $\vec{u}$  from (23) and constant f assumption.

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