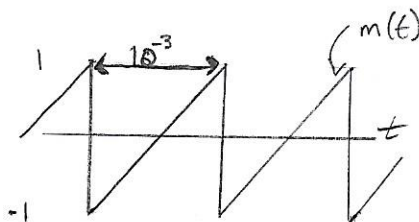


5.1-2) given



- a) Sketch  $\phi_{FM}(t)$  and  $\phi_{PM}(t)$  for  $m(t)$  if  $\omega_c = 2\pi \times 10^6$ ,  $k_F = 2000\pi$ ,  $k_P = \pi/2$   
first need  $m(t)$ , use sawtooth equation

$$m(t) = \frac{2A}{T}t - A = \frac{2(1)}{10^{-3}}t - 1 \Rightarrow m(t) = 2000t - 1$$

and now

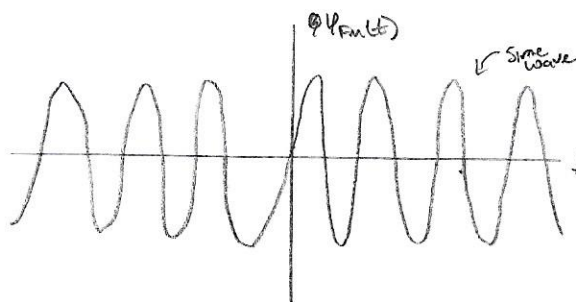
$$\phi_{FM}(t) = A \cos \left[ \underbrace{\omega_c t + k_F \int_0^t m(t) dt}_{\theta} \right]$$

$$\text{and } \omega_i = \frac{d\theta}{dt} \Rightarrow \omega_i = \omega_c + k_F m(t)$$

$$\omega_i = 2\pi \times 10^6 + 2000\pi(2000t - 1) \text{ and changing to } f \Rightarrow f_i = 10^6 + 10^3 m(t)$$

$$f_{i \min} = 0.999 \text{ MHz}$$

$$f_{i \max} = 1.001 \text{ MHz}$$



← carrier frequency switches between the two every half cycle of  $m(t)$

hard to notice difference

and for  $\phi_{PM}(t)$

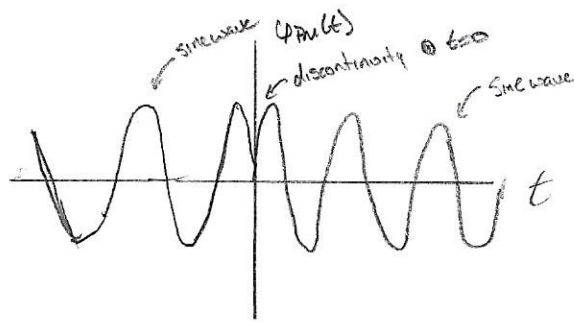
$$\phi_{PM}(t) = A \cos \left[ \underbrace{\omega_c t + k_P m(t)}_{\theta} \right]$$

$$\text{and } \omega_i = \frac{d\theta}{dt} \Rightarrow f_i = 10^6 + \frac{1}{4} \frac{dm(t)}{dt}$$

$$\frac{dm(t)}{dt} = \pm 2000 \Rightarrow f_{i \min} = 0.9995 \text{ MHz} \quad f_{i \max} = 1.0005 \text{ MHz}$$

due to the discontinuities, the PM signal jumps  $\pi$  radians every  $\frac{1}{1000}$  sec

5.1-2)



b)  $\phi_{PLL}(t) = A \cos[\omega_c t + k_p m(t)]$  and  $\omega_i = \omega_c + k_p \dot{m}(t)$

and saw earlier that  $\dot{m}(t) = 2000$ , so plugging in  $\Rightarrow$

$$\omega_i = 2.001\pi \times 10^6$$

The  $m(t)$  signal is increasing the PLL wave's frequency  
the discontinuities lead to the jumps in angle

and because  $k_p(m_p + m_p) = \pi \Rightarrow$  they are always  $\pi$  radians

5.1-4) over  $|t| \leq 1$ ,  $\phi_{FM}(t) = 10 \cos 13,000\pi t$  and  $\omega_c = 10,000\pi$

a. assuming FM signal with  $k_p = 1000$ , find  $m(t)$  over  $|t| \leq 1$

$$\phi_{FM}(t) = A \cos[\omega_c t + k_p m(t)] \text{ and plug in values}$$

$$\phi_{FM}(t) = 10 \cos[10,000\pi t + 1000 m(t)] \text{ and } \phi_{FM}(t) = 10 \cos 13,000\pi t = 10 \cos[10,000\pi + 1000(3\pi t)]$$

$\uparrow$   
 $m(t)$

$$m(t) = 3\pi t$$

b. assuming FM signal with  $k_p = 1000$ , determine  $m(t)$

$$\phi_{FM}(t) = A \cos[\omega_c t + k_p \int_{-\infty}^t m(t) dt] \Rightarrow \int_{-\infty}^t m(t) dt = 3\pi t \Rightarrow m(t) = 3\pi$$

This stays  
the same

$$m(t) = 3\pi$$

5.2-1) a) From the figure,  $m_p = 3V$  and the  $B$  is approximately the value of the 5<sup>th</sup> harmonic frequency  
 $B = 5\left(\frac{1}{T}\right) = 5\left(\frac{1}{0.2 - (-0.05)}\right) \Rightarrow B = 20 \text{ Hz}$

And now use Carson

$$B_{FM} = 2(\Delta f + B) = 2\left[\frac{1}{2\pi} k_p m_p + B\right] = 2\left[\frac{1}{2\pi} \cdot 20\pi \cdot 3 + 20\right] \Rightarrow B_{FM} = 100 \text{ Hz}$$

b)  $B_{PM} = 2(\Delta f + B) = 2\left[\frac{1}{2\pi} k_p m_p + B\right]$  and  $m_p = m(t)_{\max}$

$$m(t) = 60t \Rightarrow m_p = 60$$

$$B_{PM} = 2\left(\frac{1}{2\pi} \cdot \frac{\pi}{2} \cdot 20 + 20\right) \Rightarrow B_{PM} = 70 \text{ Hz}$$

5.2-9) a. Applying Parseval's theorem, show that  $\sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1$

by infinite series  $\sum_{n=-\infty}^{\infty} J_n(\beta) e^{jn\omega t} = e^{j\beta \sin \omega t}$

$$\sum_{n=-\infty}^{\infty} |J_n(\beta)|^2 = \frac{1}{2\pi\omega} \int_{-\pi/\omega}^{\pi/\omega} |e^{j\beta \sin \omega t}|^2 dt = \frac{\omega}{2\pi} \int_{-\pi/\omega}^{\pi/\omega} dt = 1 \Rightarrow \text{real, so}$$

$$|J_n(\beta)|^2 = J_n^2(\beta) \Rightarrow \sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1 \quad \checkmark$$

b.  $J_n(\beta) = \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{j(\beta \sin x - nx)} dx = \frac{1}{2\pi} \int_{-\pi}^{\pi} \cos(\beta \sin x - nx) + j \sin(\beta \sin x - nx) dx$

$$\text{Im}[J_n(\beta)] = \frac{1}{2\pi} \int_{-\pi}^{\pi} \sin(\beta \sin x - nx) dx \Rightarrow \text{Im}[J_n(\beta)] = 0 \quad \text{so } J_n(\beta) = \text{Re}[J_n(\beta)]$$

$$\text{Re}[J_n(\beta)] = \frac{1}{2\pi} \int_{-\pi}^{\pi} \cos(\beta \sin x - nx) dx = \frac{1}{\pi} \int_0^{\pi} \cos(\beta \sin x - nx) dx$$

$$J_n(\beta) = \frac{1}{\pi} \int_0^{\pi} \cos(\beta \sin x + nx) dx = (-1)^n \frac{1}{\pi} \int_0^{\pi} \cos(\beta \sin x - nx) dx \xrightarrow{J_n(\beta)} \Rightarrow$$

$$J_{-n}(\beta) = (-1)^n J_n(\beta)$$

5.3-2) a) Design block diagram of Armstrong FM modulator to generate carrier with  $f_c = 98.1 \text{ MHz}$  and  $\Delta f = 75 \text{ kHz}$

Starting with the generator, need to get the  $\Delta f$  from  $10 \text{ Hz}$  to  $75 \text{ kHz}$

$$\frac{75000}{10} = 7500$$

and with the multipliers, factor out  $\Rightarrow 7500 = 2^2 \cdot 3 \cdot 5^4$   
 $\uparrow \quad \uparrow \quad \uparrow$   
 2 doubler 1 tripler 4 quintupler

but will need to shift frequency too

$$X = \frac{98100000}{100000} = 981 \Rightarrow \frac{981}{7500} \leftarrow \text{ratio to lower carrier frequency}$$

$$f_{\text{signal}} f_{\text{oscillator}} = \frac{981}{7500} f_{\text{carrier}} \Rightarrow f_s = 1.15 f_o \Rightarrow \text{range from } 11.5 \text{ to } 12.6 \text{ MHz}$$

$\uparrow$   
10 to 11 MHz

And in order to reach a frequency in that range

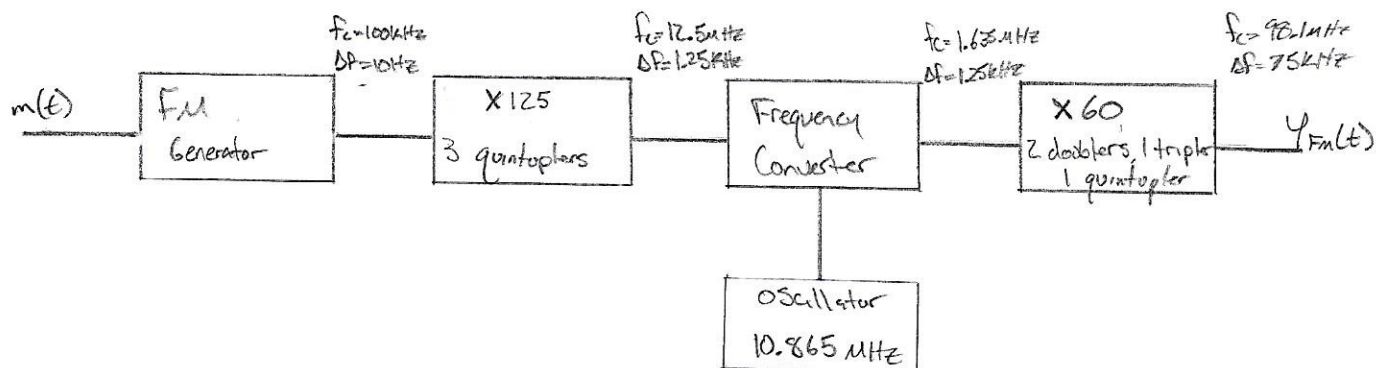
need to look at where to put oscillator with respect to doublers, ...

So what multipliers satisfy that

$$(100,000 \cdot x) \leftarrow \begin{matrix} \uparrow \\ \text{generator frequency} \end{matrix} \begin{matrix} \leftarrow \text{multipliers} \\ \text{something in that range} \\ 11.5 - 12.6 \text{ MHz} \end{matrix} \quad 3 \text{ quintuplers} = 12.5$$

and finally need  $f_o$

$$f_o = \frac{f_s}{1.15} \Rightarrow f_o = 10.865$$





5.3-2) b. Determine the tunable range of the carrier frequency

It is used to lower carrier frequency and <sup>oscillator</sup> 10-11 MHz  $\Rightarrow$  lowest carrier when oscillator 11 MHz

$$f_{c_{\min}} = 60(12.5-11) \text{ MHz} \Rightarrow f_{c_{\min}} = 90 \text{ MHz}$$

and highest carrier with lowest oscillator freq.

$$f_{c_{\max}} = 60(12.5-10) \text{ MHz} \Rightarrow f_{c_{\max}} = 150 \text{ MHz} \Rightarrow$$

The tunable range is 90 to 150 MHz

5.4-4) From small error analysis,  $\Theta_e(s) = \frac{s}{s + AKH(s)} \Theta_i(s)$  where  $\Theta_i(t) = kt^2 \Leftrightarrow \Theta_i(s) = \frac{2k}{s^3}$

$$\Theta_e(s) = \frac{2k}{s^2(s + AKH(s))}$$

$$\text{and to evaluate error } \lim_{t \rightarrow \infty} \Theta_e(t) = \lim_{s \rightarrow 0} s \Theta_e(s) = \lim_{s \rightarrow 0} \frac{2k}{s(s + AKH(s))}$$

for  $H(s) = 1$

$$\lim_{s \rightarrow 0} \frac{2k}{s(s + AK)} = \infty \Rightarrow \lim_{t \rightarrow \infty} \Theta_e(t) = \infty \text{ cannot be tracked}$$

for  $H(s) = \frac{s+a}{s}$

$$\lim_{s \rightarrow 0} \frac{2k}{s(s + AK(\frac{s+a}{s}))} = \lim_{s \rightarrow 0} \frac{2k}{s^2 + AK(s+a)} = \frac{2k}{AKa} \Rightarrow \lim_{t \rightarrow \infty} \Theta_e(t) = \frac{2k}{AKa} \text{ Can be tracked with constant phase error}$$

for  $H(s) = \frac{s^2 + as + b}{s}$

$$\lim_{s \rightarrow 0} \frac{2k}{s(s + AK(\frac{s^2 + as + b}{s}))} = \lim_{s \rightarrow 0} \frac{2ks}{s^3 + AK(s^2 + as + b)} = 0 \Rightarrow \lim_{t \rightarrow \infty} \Theta_e(t) = 0 \text{ Can be tracked with 0 phase error}$$

5.6-1)  $f_c = 1530 \text{ kHz}$  with  $f_{IF} = 455 \text{ kHz}$  so

$$f_{LO} = f_c + f_{IF} = (1530 + 455) \text{ kHz} = 1985 \text{ kHz}$$

but another carrier with

$$f_c' = (1985 + 455) \text{ kHz} = 2440 \text{ kHz} \text{ is also heard because the difference is also } 455 \text{ kHz between new } f_c' \text{ and } f_{LO}$$

This will cause the station to be heard at both  $1530 \text{ kHz}$  and  $2440 \text{ kHz}$

5.6-3) a)  $f_{IF} = 455 \text{ kHz}$  and  $f_c$  can range from  $9.4$  to  $9.9 \text{ MHz}$   $\Rightarrow$

$$f_{LO} = f_c + f_{IF} \Rightarrow f_{LO_{low}} = 9.4 \text{ MHz} + 455 \text{ kHz} = 9.855 \text{ MHz}$$

$$\Rightarrow f_{LO_{high}} = 9.9 \text{ MHz} + 455 \text{ kHz} = 10.355 \text{ MHz}$$

Frequency of the oscillator for this receiver is  
 $9.855 \text{ MHz}$  to  $10.355 \text{ MHz}$

b) In order to receive image station, needs to be separated by  $2f_{IF} = 910 \text{ kHz}$

$$f_{image} = (9.4 \text{ MHz} + 910 \text{ kHz}) \text{ to } (9.9 \text{ MHz} + 910 \text{ kHz})$$

$$= 10.31 \text{ MHz} \text{ to } 10.81 \text{ MHz}$$

$\uparrow$

This is out of the  $9.4 - 9.9 \text{ MHz}$  range and  
 this receiver cannot receive the image station