

# Design of wind turbine systems

## SS 2016

## Tutorial 5

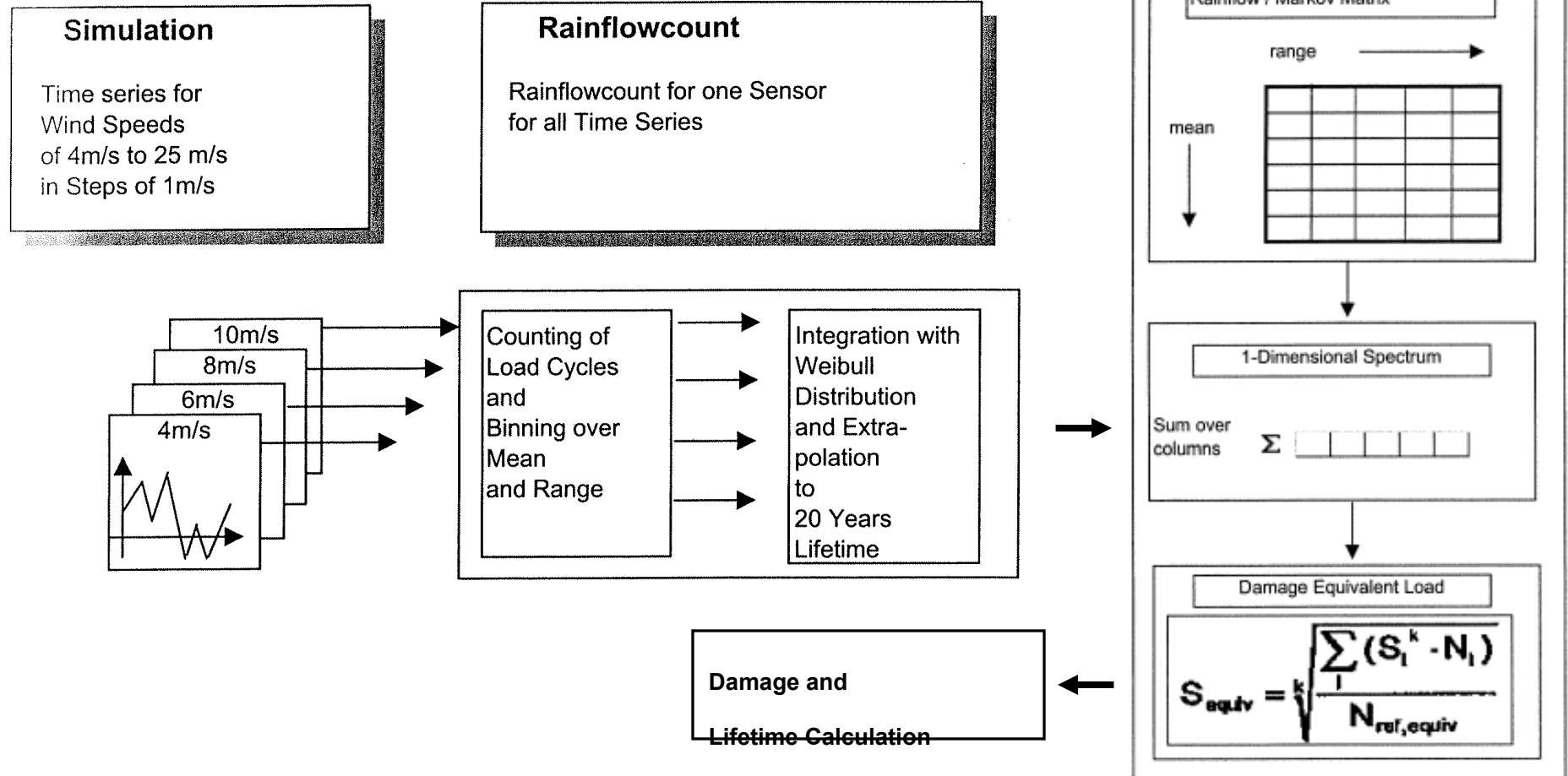
### Loads and components

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*ForWind – Wind Energy Systems*

# Fatigue Analysis - Damage Calculation

## Scheme of Calculation of Load Spectra



# Wöhler curve (I)

- Also known as S-N curve
- Each material has a proper set of curves
- Defines the number of cycles leading to failure for a cyclic loading characterized by
  - a given mean stress  $\sigma_{mi}$
  - a given range  $\sigma_{rj}$
- Curves derived from experimental fatigue test on materials and sections

Material	Wöhler Slope (m)
Steel	4
Cast Iron	5-7
Composites	9-12

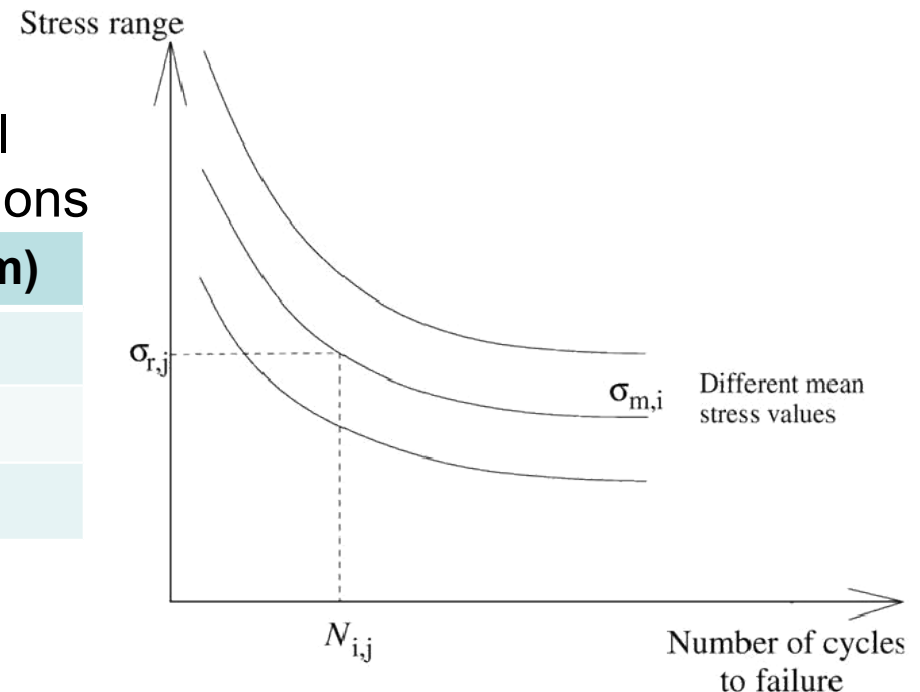


Fig. Hansen 2008

# Wöhler curve (II)

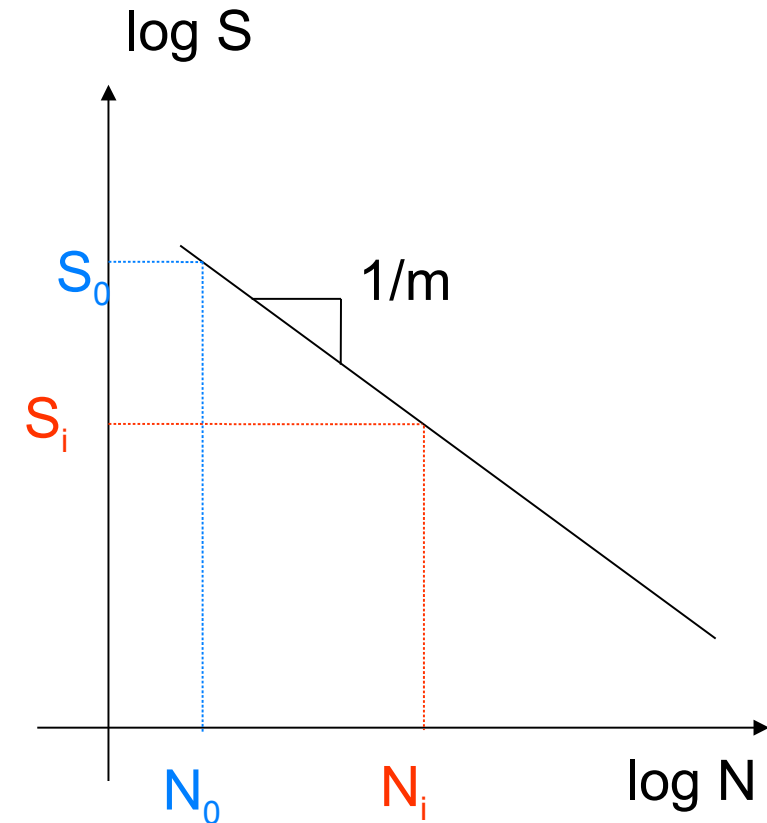
## SN-curve:

- Generally plotted in  $\log(S)$ - $\log(N)$  diagrams
- Assumed  $N_{eq}$  ( $2E+07, 1E+08$  for WTs)
- $S$  = stress amplitude [MPa]
- $N$  = number of cycles
- $m$  = Wöhler slope  $\hat{=}$  typical of the material

$$\log S_0 - \frac{1}{m} \log N_i = \log S_i$$

Equivalent to

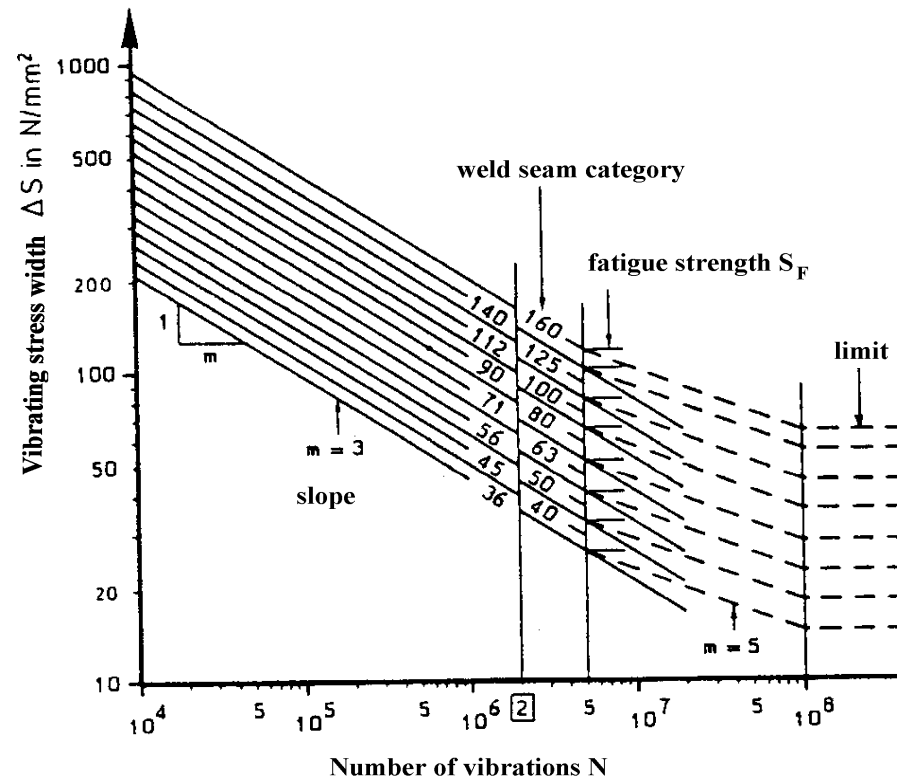
$$N_i = \left( \frac{S_0}{S_i} \right)^m$$

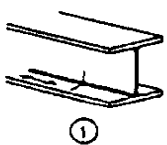
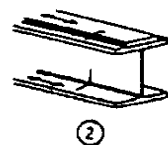
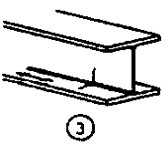
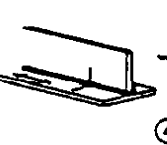
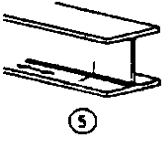
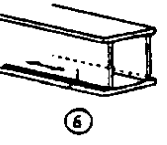
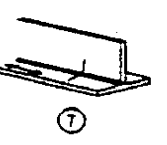
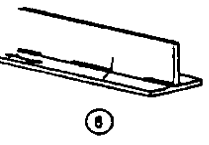
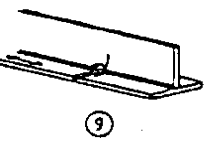


# Wöhler curve (III)

S-N curves, depending on:

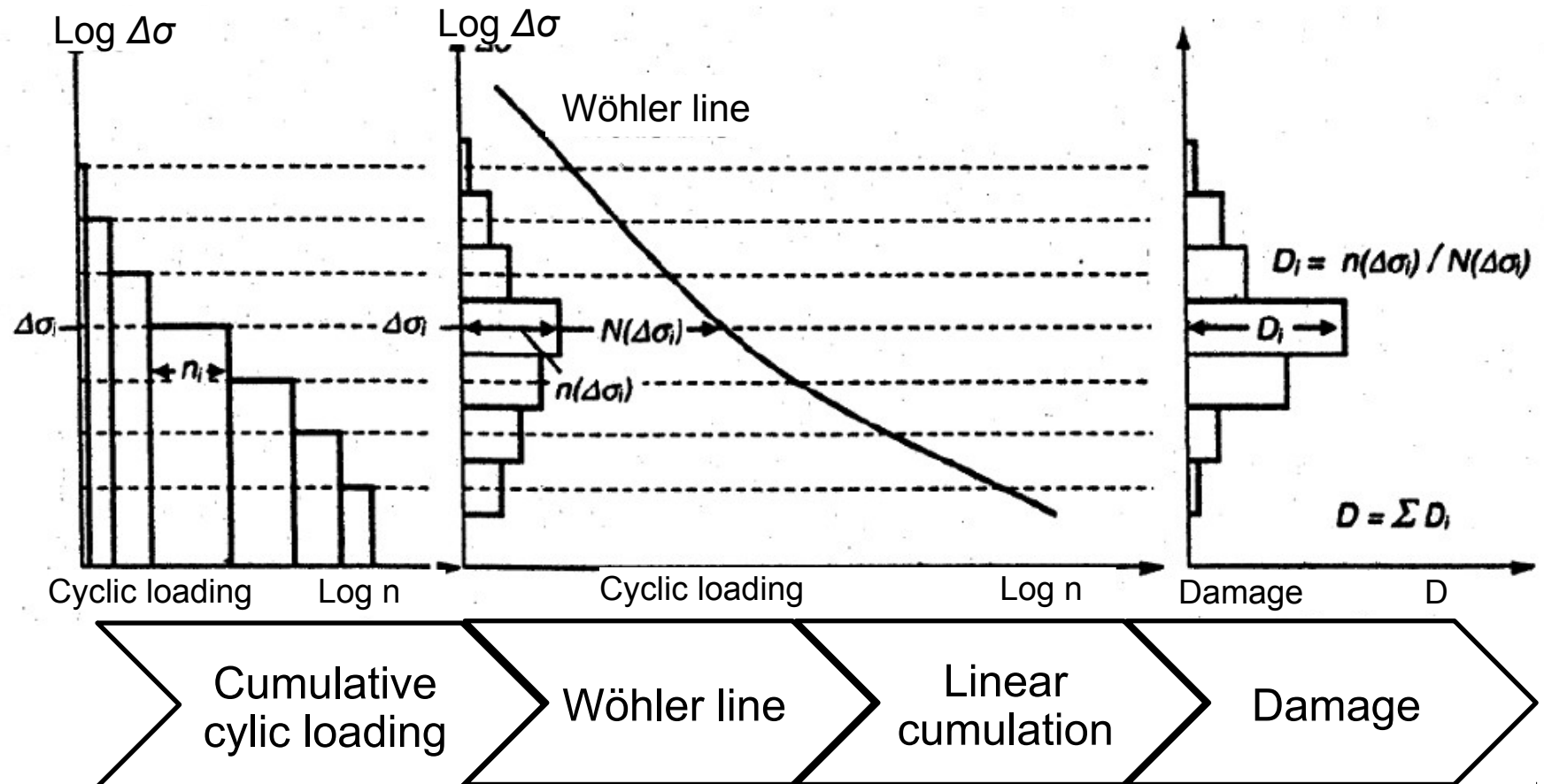
- geometry => notch class, detail category
- size => thickness correction
- environment => inverse slope, knee points



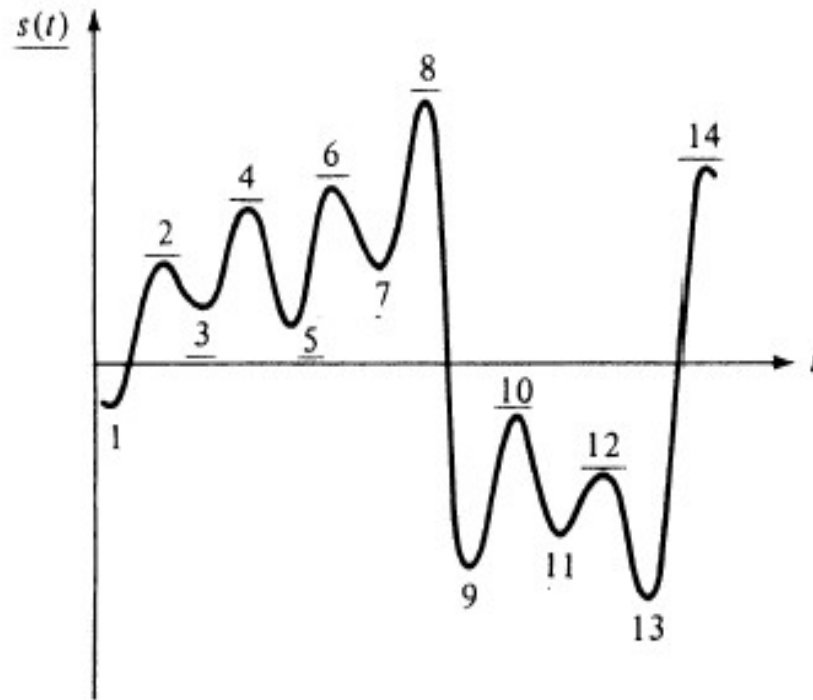
category	weld seam detail
125	 
112	 
100	  
80	
71	

# Linear damage accumulation hypothesis according to Palmgren-Miner (I)

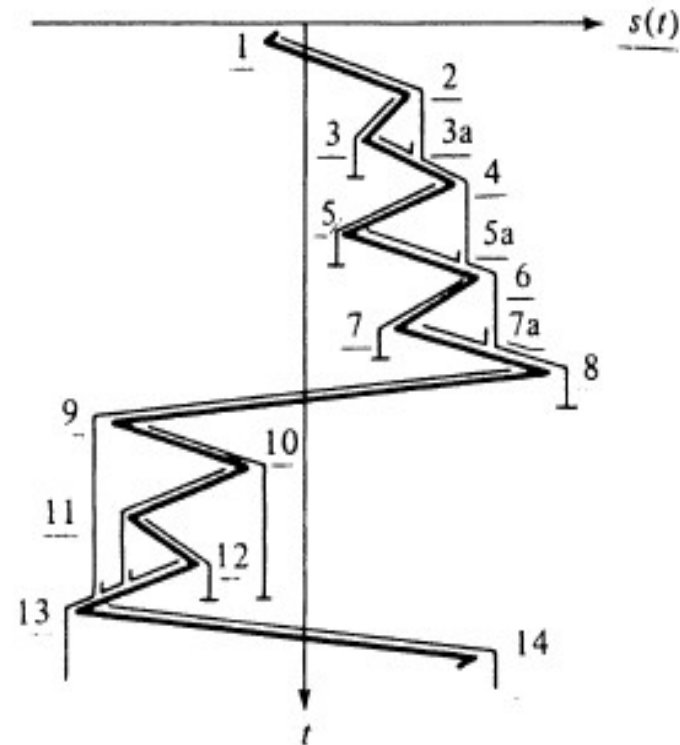
Hypothesis: partial damages  $D_i = n_i / N_i$  can be added **linearly**



# Rainflow Counting



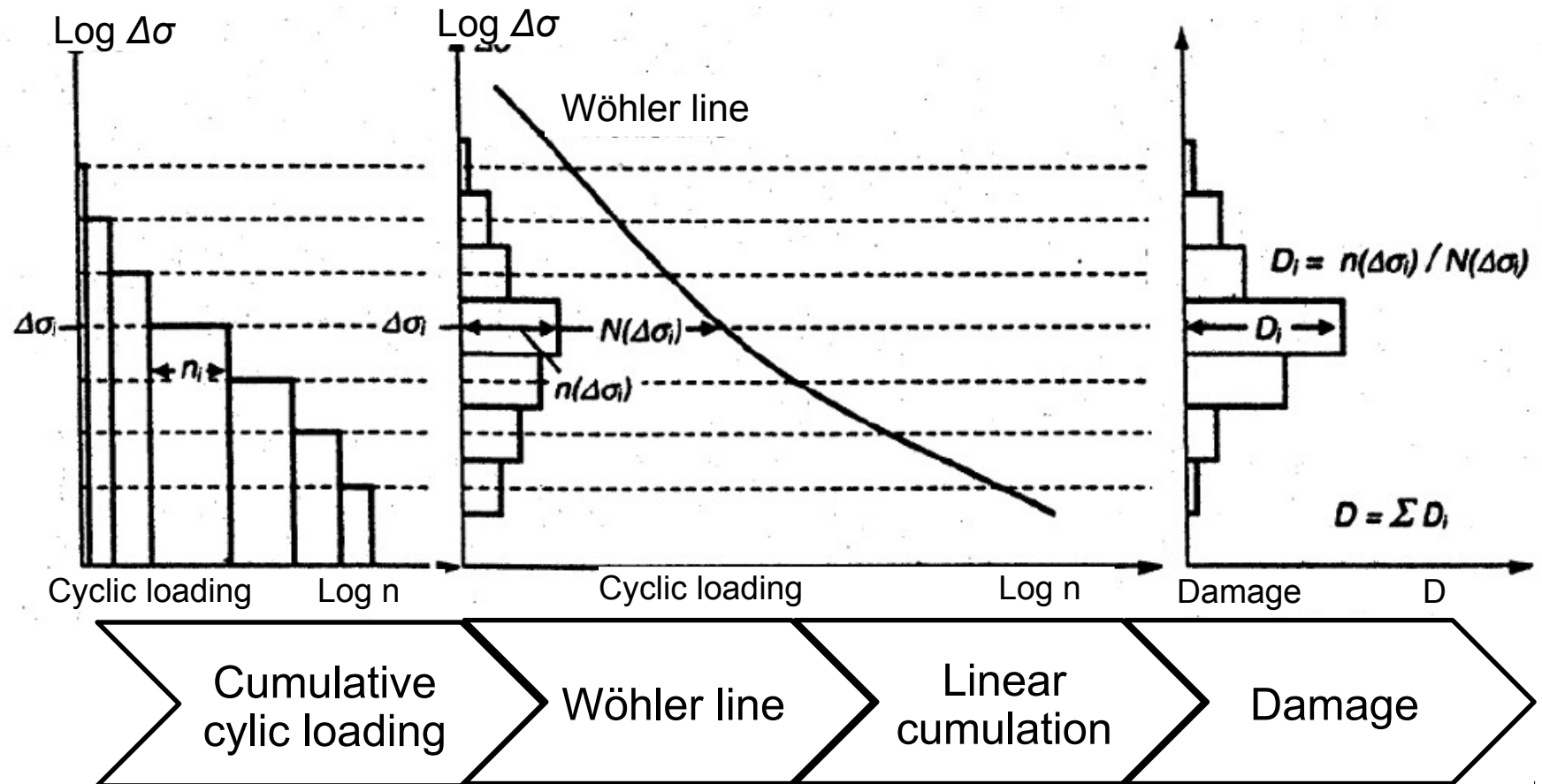
(a)



(b)

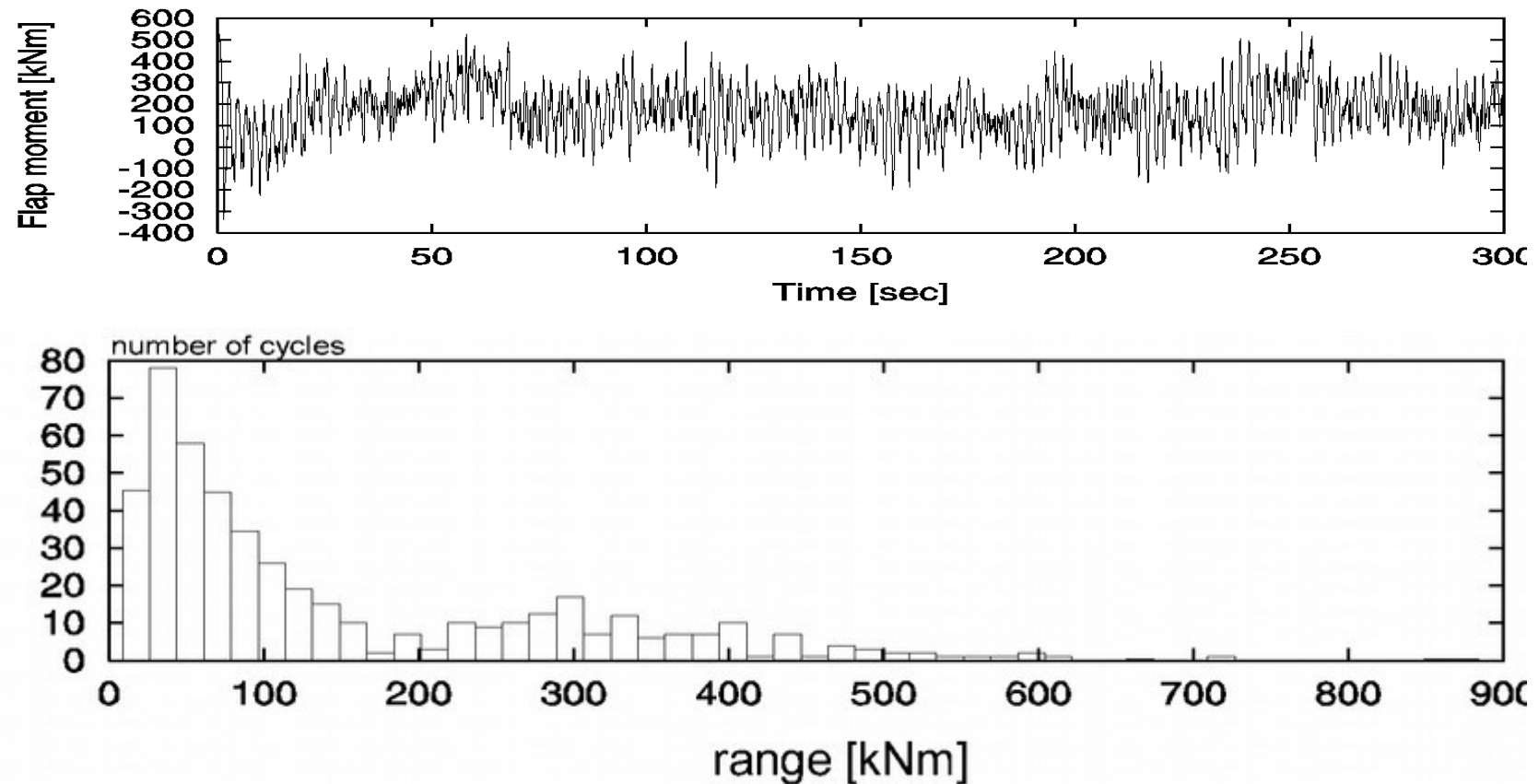
# Linear damage accumulation hypothesis according to Palmgren-Miner (I)

Hypothesis: partial damages  $D_i = n_i / N_i$  can be added **linearly**



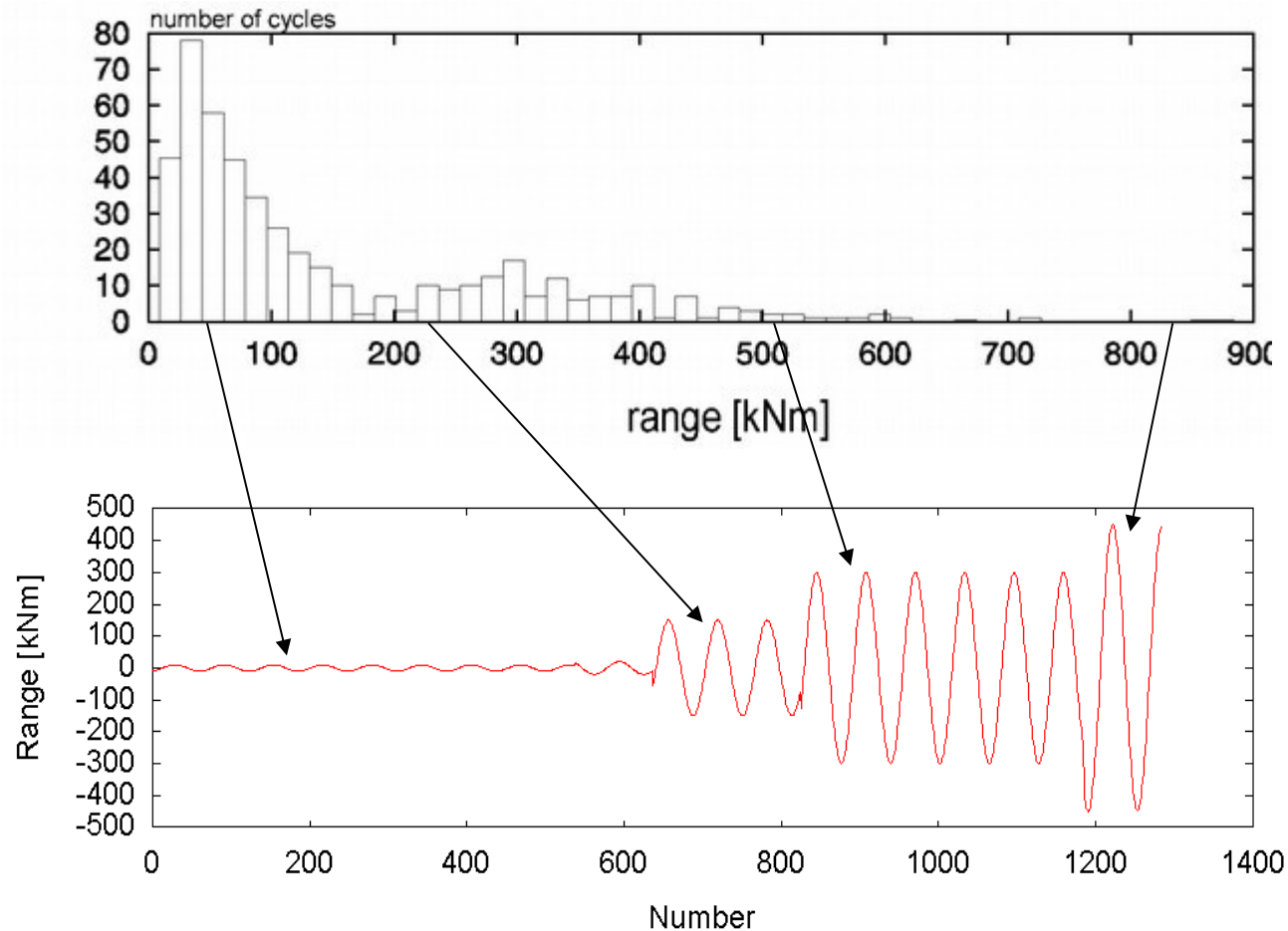


# Rainflow Counting



**Fatigue load spectrum** for ONE load case

# Rainflow Counting = time series rearrangement



## Linear damage accumulation hypothesis according to Palmgren-Miner (II)

$$D = \sum_i \frac{n_i (\Delta \sigma_i)}{N_i (\Delta \sigma_i)}$$

D	damage	$\Delta\sigma_i$	$i^{\text{th}}$ stress range with $n_i$ cycles
$n_i$	number of endured stress cycles	$N_i$	number of endurable stress cycles

- Partial damage contributions  $D_i = n_i / N_i$  are summarized *linearly*
- No influence of load history
- Design criterion  $D \leq D_{\text{design}} \leq 1$ 
  - Wind energy:  
 $D_{\text{design}} = 1$  (safety margin included in design resistance)
  - Offshore technology:  
 $D_{\text{design}} = 0,1 \text{ to } 0,3$  (safety margin considered in design damage)
- Calculated lifetime = design lifetime / damage

# Comparison of fatigue load spectra by means of damage equivalent loads

$$\Delta\sigma_{eq} = \left( \frac{\sum n_j \Delta\sigma_j^m}{N_R} \right)^{1/m}$$

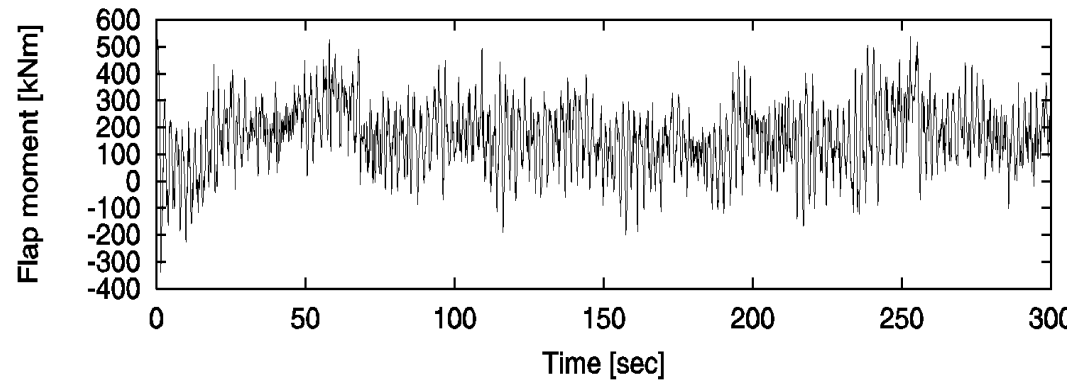
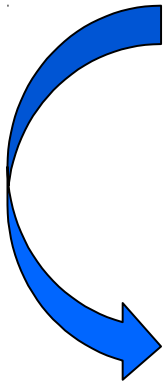
$\Delta\sigma_{eq}$  equivalent stress range

$m$  inverse slope of S - N curve

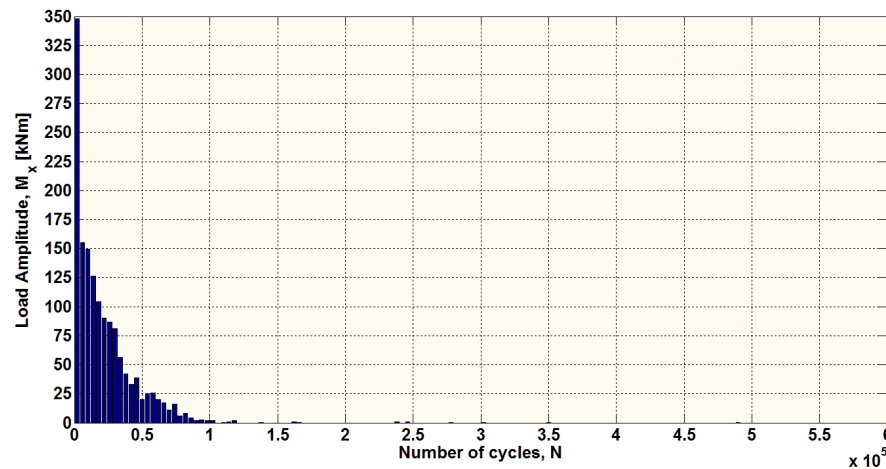
$N_R$  reference number, e.g.  $2 \cdot 10^6$

$\Delta\sigma_j$  j - th stress range with  $n_j$  cycles

# From time series to Equivalent load

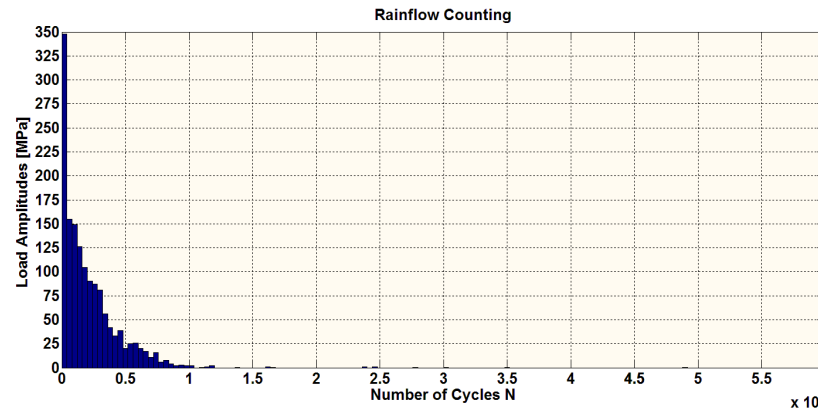


Starting  
Load time  
series

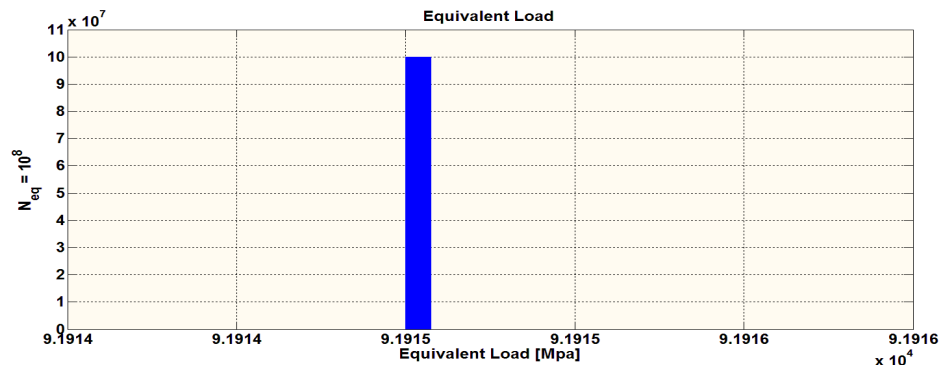


Apply RFC  
to the time  
series

# From time series to Equivalent load

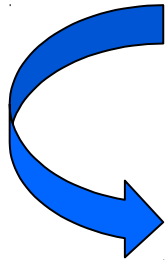


$$\Delta\sigma_{eq} = \left( \frac{\sum n_j \Delta\sigma_j^m}{N_R} \right)^{1/m}$$

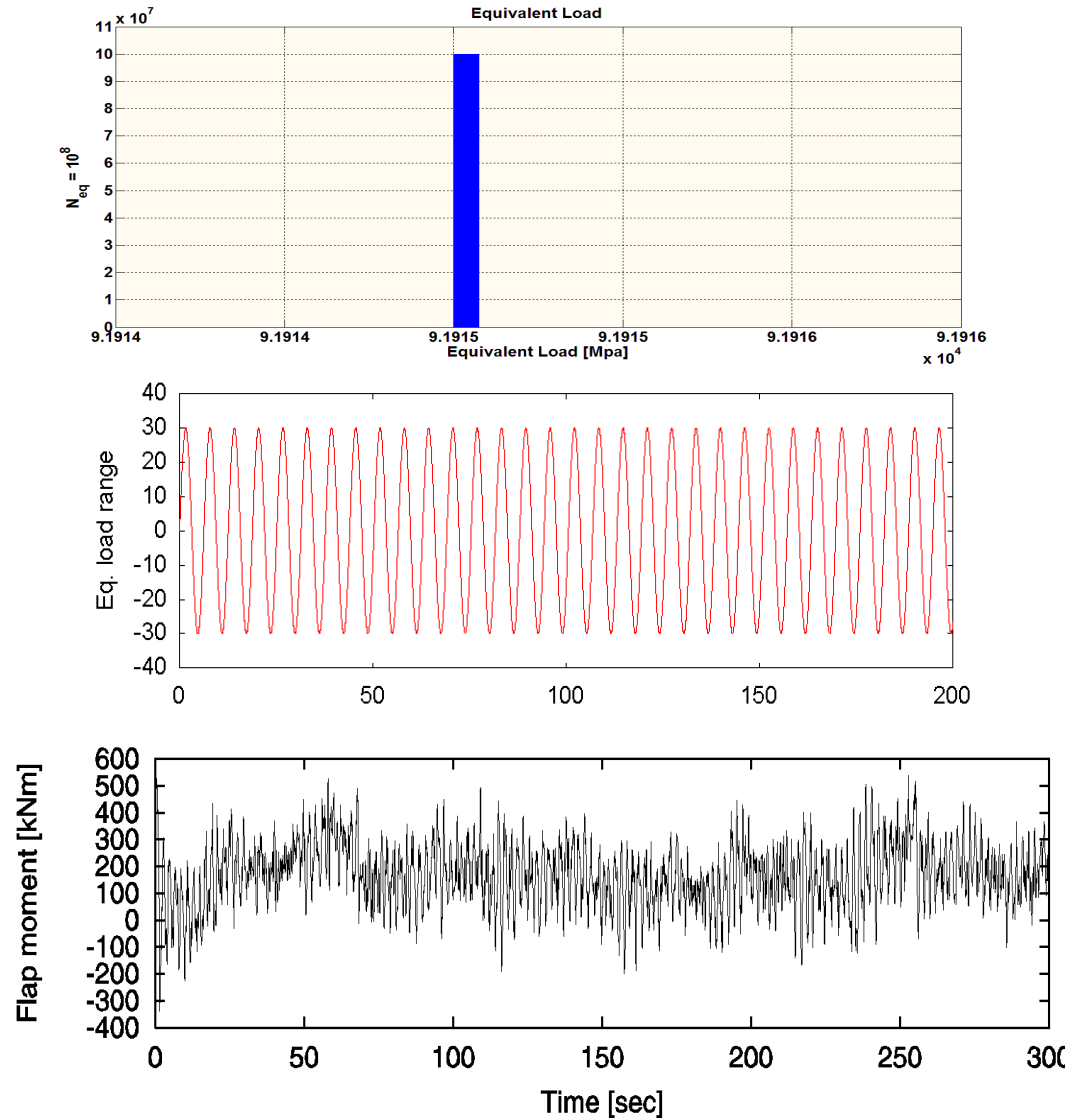


Calculate the equivalent load for a given reference cycle number

# From time series to Equivalent load



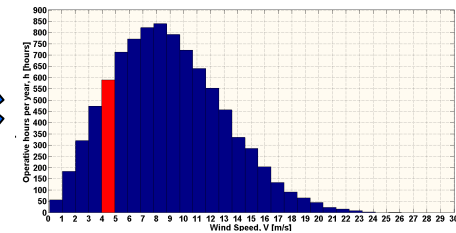
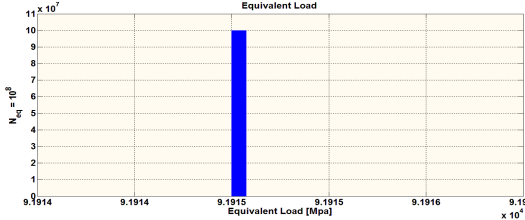
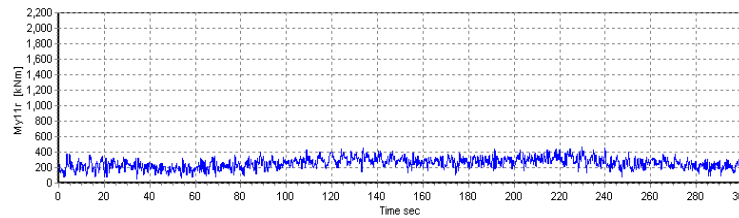
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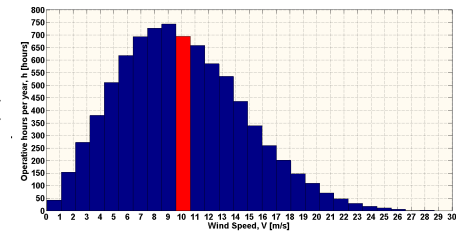
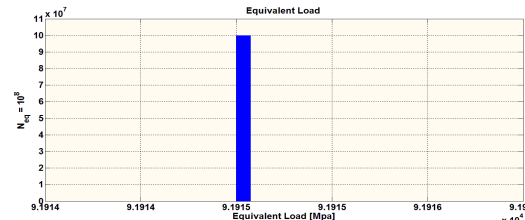
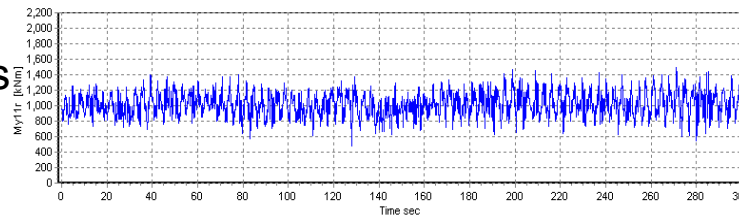
The two time series are equivalent: they produce the same effect on the turbine

# How to use damage equivalent loads

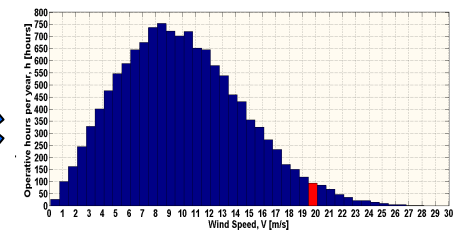
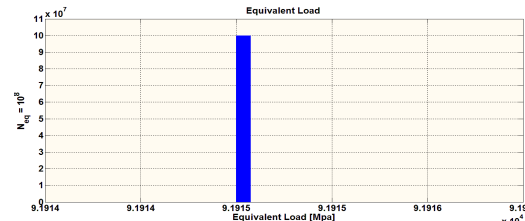
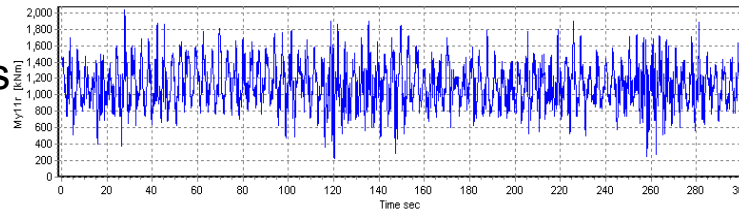
4m/s



10m/s



20m/s



$\Sigma$  all LC's



# Pros and cons of damage-equivalent loads (DELs)

## Pros

- + DELs are proportional to load magnitude of sectional forces
- + while damage is proportional to the 3<sup>rd</sup> to 12<sup>th</sup> power of loading (inverse slope of S-N curve)
- + strength reserve of DELs is nearly proportional to wall thickness reserve of component => simple design optimisation
- + easy comparison of fatigue load spectra with different shape
- + easy dimensioning, when reference number of cycles equals  $2 \cdot 10^6$

## Cons

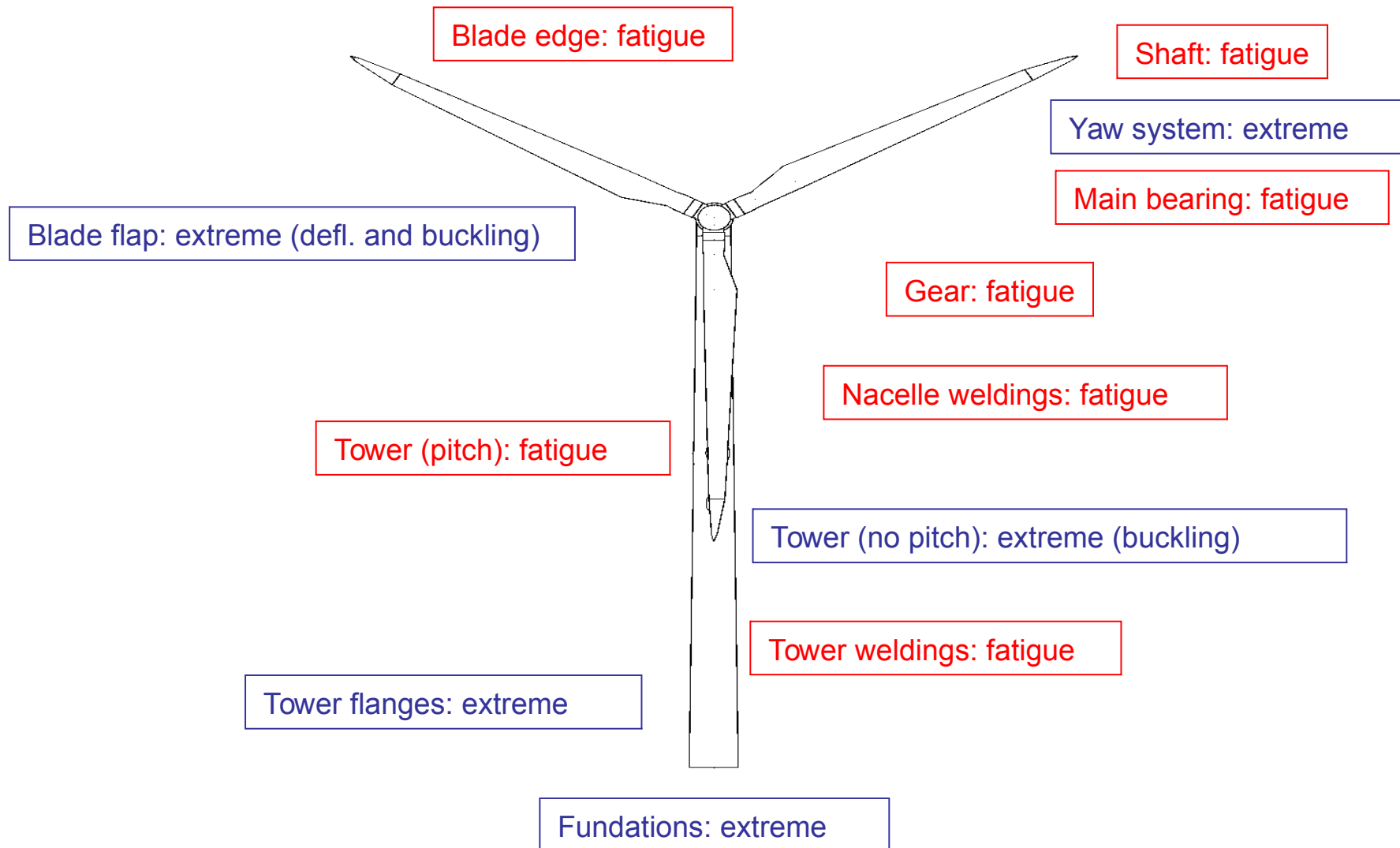
- valid only for S-N curves with constant slope
- conservative with respect to load spectra and time series approach

# Conclusions – Fatigue

## Fatigue analysis of wind turbine response

- Simulation of production at various wind speed bins, start, stops, fault load cases, etc.
- Rainflow-counting of time series and factoring with frequency of occurrence of load cases
  - stress time series at hot spot or
  - sectional forces at cross section or
  - sectional forces at component interface
- S-N curve and Palmgren-Miner hypothesis
- Concept of damage equivalent loads (DEL)  
frequently used for comparison of sectional forces and stresses

# Dominant Loads: Fatigue or Extreme?



# Literature

- [Hau] Erich Hau, Windkraftanlagen. Grundlagen, Technik, Einsatz, Wirtschaftlichkeit. 3. Aufl., 2003, Springer-Verlag; ISBN: 3540574301
- [Burton] T. Burton, et al., Wind Energy Handbook, 2001, Wiley
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- [Hansen] Aerodynamics of wind turbine, 2nd ed., Earthscan, 2008.
- [IEC] IEC 61400-1, ed. 3 2005