Mathematical Biology Assignment 1

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- 1. A boat carries N similar rowers each of whom puts in the same P power to propelling the boat
 - (a) Assuming each rower occupies the same V volume of the boat, show the wetted area of the boat is $A \propto (NV)^{2/3} A$ has units $[L]^2$, NV has units $[L]^3$ since NV is the volume occupied by N rowers

Want to find non-dimensional groupings which work, since the system will have form

$$f(\lambda_1, \lambda_2, \ldots) = 0$$

Where λ_i are non-dimensional groupings of terms. In this case we can generate the non-dimensional grouping

$$\frac{A^3}{(NV)^2}$$

And hence

$$A^3 \propto (NV)^2 \implies A \propto (NV)^{2/3}$$

(b) Assuming that F_{drag} depends on the wetted area of the boat, A, its speed, U, and the density of the water, ρ , show that F_{drag} is proportional to $\rho U^2 A$ and that the rate of energy dissipation due to drag must be proportional to $\rho U^3 A$.

Force has units $[M][L][T]^{-2}$, density $[M][L]^{-3}$, speed $[L][T]^{-1}$, area $[L]^2$ If the LHS is the quantity, and the RHS is the units (I will write F instead of F_{drag})

$$F = \frac{[M][L]}{[T]^2}$$

$$\frac{F}{\rho} = \frac{[M][L][L]^3}{[M][T]^2}$$

$$\frac{F}{\rho} = \frac{[L]^4}{[T]^2}$$

$$\frac{F}{\rho U^2} = \frac{[L]^4[T]^2}{[L]^2[T]^2}$$

$$\frac{F}{\rho U^2} = [L^2]$$

$$\frac{F}{\rho U^2 A} = \frac{[L^2]}{[L]^2} = [1]$$

Hence

$$f\left(\frac{F}{\rho U^2 A}\right) = const \implies F \propto \rho U^2 A$$

And the rate of energy dissipation, has same units as power: dE has units $[M][L]^2[T]^{-3}$ (energy/time)

$$dE = [M][L]^{2}[T]^{-3}$$

$$\frac{dE}{\rho U^{2}A} = \frac{[L]}{[T]}$$

$$\frac{dE}{\rho U^{3}A} = [1]$$

And as before we get

$$f\left(\frac{dE}{\rho U^3 A}\right) = const \implies dE \propto \rho U^3 A$$

(c) Hence show $U \propto N^{1/9} P^{1/3} \rho^{-1/3} V^{-2/9}$ From part (a), $A \propto (NV)^{2/3}$ and the power provided, NP with units $[M][L]^2[T]^{-3}$

$$dE \propto \rho U^3 A$$

$$U \propto \left(\frac{dE}{\rho A}\right)^{1/3}$$

$$U \propto dE^{1/3} \rho^{-1/3} (NV)^{-2/9}$$

But $dE \propto NP$

$$U \propto dE^{1/3} \rho^{-1/3} (NV)^{-2/9}$$

$$U \propto (NP)^{1/3} \rho^{-1/3} (NV)^{-2/9}$$

$$U \propto N^{1/9} P^{1/3} \rho^{-1/3} V^{-2/9}$$

(d) If we assume P, V are both propto body mass, is size an advantage to a rower? A rower will ideally generate the most speed, so it is an advantage if U is bigger. If $P \propto V \propto M$ then we can sub it into the U equation

$$U \propto N^{1/9} P^{1/3} \rho^{-1/3} V^{-2/9}$$

$$U \propto N^{1/9} M^{1/3} \rho^{-1/3} M^{-2/9}$$

$$U \propto N^{1/9} M^{1/9} \rho^{-1/3}$$

Since the power of M is positive, yes it would be an advantage.

2. Investigate the Coriolis effect

Navier-Stokes gives

$$\rho\left(\frac{\partial \mathbf{u}}{\partial t} + 2\mathbf{\Omega} \times \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}\right) = -\nabla p + \mu \nabla^2 \mathbf{u} + \rho(\mathbf{g} - \mathbf{\Omega} \times (\mathbf{\Omega} \times \mathbf{x}))$$

Assuming the origin of the coordinate system is the centre of the Earth. Ω is 2π per 24 hours (or $7.3 \times 10^{-5} s^{-1}$) in the direction of the Earth's axis of rotation. The radius of

the earth is $\approx 6,400km$. Assume the water body is a bathtub with lengthscale $\sim 1m$ and water flows $\sim 1ms^{-1}$. Take density = $1000kg~m^{-3}$ and viscosity $8.9 \times 10^{-4}Pa~s$. Non dimensionalise and determine if the LHS (Coriolis acceleration) is significant (and hence if swirl direction will change depending on which hemisphere you are in)

Where $2\Omega \times \mathbf{u}$ is the Coriolis gravity term.

Let
$$x = L\tilde{x}$$
, $u = U\tilde{u}$, $t = \frac{L}{U}\tilde{t}$, $p = P\tilde{p}$ and $\Omega = \frac{U}{L}\tilde{\Omega}$

$$\rho\left(\frac{\partial\mathbf{u}}{\partial t} + 2\mathbf{\Omega} \times \mathbf{u} + \mathbf{u} \cdot \nabla\mathbf{u}\right) = -\nabla p + \mu \nabla^2 \mathbf{u} + \rho(\mathbf{g} - \mathbf{\Omega} \times (\mathbf{\Omega} \times \mathbf{x}))$$

$$\rho\left(\frac{U^2}{L}\frac{\partial \tilde{\mathbf{u}}}{\partial \tilde{t}} + \frac{U^2}{L}2\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{u}} + \frac{U^2}{L}\tilde{\mathbf{u}} \cdot \nabla\tilde{\mathbf{u}}\right) = -\frac{P}{L}\nabla\tilde{p} + \mu \frac{U}{L^2}\nabla^2\tilde{\mathbf{u}} + \rho(\frac{U^2}{L}\tilde{\mathbf{g}} - \frac{U^2}{L^2}L\tilde{\mathbf{\Omega}} \times (\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{x}}))$$

$$\frac{\partial \tilde{\mathbf{u}}}{\partial \tilde{t}} + 2\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{u}} + \tilde{\mathbf{u}} \cdot \nabla\tilde{\mathbf{u}} = -\frac{P}{U^2\rho}\nabla\tilde{p} + \frac{\mu}{U\rho L}\nabla^2\tilde{\mathbf{u}} + \tilde{\mathbf{g}} - \tilde{\mathbf{\Omega}} \times (\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{x}})$$

$$\frac{\partial \tilde{\mathbf{u}}}{\partial \tilde{t}} + 2\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{u}} + \tilde{\mathbf{u}} \cdot \nabla \tilde{\mathbf{u}} = -\frac{P}{U^2 \rho} \nabla \tilde{p} + \frac{1}{Re} \nabla^2 \tilde{\mathbf{u}} + \tilde{\mathbf{g}} - \tilde{\mathbf{\Omega}} \times (\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{x}})$$

$$Re(\frac{\partial \tilde{\mathbf{u}}}{\partial \tilde{t}} + 2\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{u}} + \tilde{\mathbf{u}} \cdot \nabla \tilde{\mathbf{u}}) = -\frac{P\mu L}{U}\nabla \tilde{p} + \nabla^2 \tilde{\mathbf{u}} + Re(\tilde{\mathbf{g}} - \tilde{\mathbf{\Omega}} \times (\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{x}}))$$

Where $Re = \frac{U\rho L}{\mu}$ If $Re \to 0$ Then the Coriolis effect is negligible, i.e. we get (letting $P = U^2 \rho$)

$$-\nabla \tilde{p} + \nabla^2 \tilde{\mathbf{u}} = 0$$

With no curl terms. If $Re \to \infty$, then the Coriolis effect is not negligible:

$$\frac{\partial \tilde{\mathbf{u}}}{\partial \tilde{t}} + 2\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{u}} + \tilde{\mathbf{u}} \cdot \nabla \tilde{\mathbf{u}} = -\nabla \tilde{p} + \tilde{\mathbf{g}} - \tilde{\mathbf{\Omega}} \times (\tilde{\mathbf{\Omega}} \times \tilde{\mathbf{x}})$$

Where $P = \frac{U}{\mu L}$

Using the given numbers: $U \sim 1$ and $L \sim 1$, $\rho \sim 1000$ and $\mu \sim 8.9 \times 10^{-4}$.

$$Re = \frac{1000}{8.9 \times 10^{-4}} = 8.9 \times 10^{7}$$

Which is quite large. Hence the Coriolis effect is not negligible.

3. Consider the chemical equation

$$mA + nB \stackrel{k_1}{\rightleftharpoons} C$$

(a) Given that the concentration c of C is

$$\frac{dc}{dt} = k_1 a^m b^n - k_{-1} c$$

Write the equations for a, b (the concentrations of A, B) The DEs for a, b are:

$$\frac{da}{dt} = -k_1 a^m b^n + k_{-1} c$$

$$\frac{db}{dt} = -k_1 a^m b^n + k_{-1} c$$

Subject to initial conditions with form $a(0) = a_i$, $b(0) = b_i$ for some a_i, b_i .

(b) Using conservation, eliminate a, and b from the equation for c

$$\frac{d(a+c)}{dt} = 0 \implies a+c = const = a_i$$

$$\frac{d(b+c)}{dt} = 0 \implies b+c = const = b_i$$

$$\frac{dc}{dt} = k_1 a^m b^n - k_{-1} c$$

$$= k_1 (c - a_i)^m (c - b_i)^n - k_{-1} c$$

4. Consider Michaelis-Menten, but relax irreversibility, i.e.

$$E + S \stackrel{\stackrel{k_1}{\longleftarrow}}{\longrightarrow} C \stackrel{\stackrel{k_2}{\longleftarrow}}{\longrightarrow} E + P$$

(a) Write the set of equations for concentrations s, e, c, and p. With ICs

$$s(0) = s_i > 0$$
, $e(0) = e_i = \epsilon s_i > 0$, $c(0) = p(0) = 0$

$$\frac{de}{dt} = -k_1 e s + k_{-1} c + k_2 e p - k_{-2} e p$$

$$\frac{ds}{dt} = -k_1 e s + k_{-1} c$$

$$\frac{dc}{dt} = k_1 e s - k_{-1} e s - k_2 c + k_{-2} e p$$

$$\frac{dp}{dt} = k_2 c - k_{-2} e p$$

With

$$s(0) = s_i > 0$$
, $e(0) = e_i = \epsilon s_i > 0$, $c(0) = p(0) = 0$

(b) Obtain a conservation law and eliminate e from the system

$$\frac{d(e+c)}{dt} = 0 \implies e(t) + c(t) = const = e_i = \epsilon s_i$$

$$\implies e = \epsilon s_i - c$$

Hence the system of equations reduces to

$$\begin{aligned} \frac{ds}{dt} &= -k_1(\epsilon s_i - c)s + k_{-1}c \\ \frac{dc}{dt} &= k_1(\epsilon s_i - c)s - k_{-1}(\epsilon s_i - c)s - k_2c + k_{-2}(\epsilon s_i - c)p \\ \frac{dp}{dt} &= k_2c - k_{-2}(\epsilon s_i - c)p \end{aligned}$$

Let

(c) Nondimensionalise as in lectures with $\epsilon = e_i/s_i \ll 1$. Show the scaled system has 3 dimensionless parameters (give in terms of the original parameters)

$$s = s_i \tilde{s}, \quad c = c_* \tilde{c}, \quad p = p_* \tilde{p}, \quad t = t_* \tilde{t}$$

(Assuming s_i for s is sensible as it is given as the IC) s equation:

$$\frac{s_i}{t_*} \frac{d\tilde{s}}{d\tilde{t}} = -k_1(\epsilon s_i - c_*\tilde{c})s_i\tilde{s} + k_{-1}c_*\tilde{c}$$
$$\frac{d\tilde{s}}{d\tilde{t}} = -t_*k_1(\epsilon s_i - c_*\tilde{c})\tilde{s} + \frac{k_{-1}t_*c_*}{s_i}\tilde{c}$$

c equation

$$\frac{c_*}{t_*} \frac{d\tilde{c}}{d\tilde{t}} = k_1 s_i (\epsilon s_i - c_* \tilde{c}) \tilde{s} - k_{-1} s_i (\epsilon s_i - c_* \tilde{c}) \tilde{s} - k_2 c_* \tilde{c} + k_{-2} (\epsilon s_i - c_* \tilde{c}) p_* \tilde{p}$$

$$\frac{d\tilde{c}}{d\tilde{t}} = k_1 t_* s_i (\frac{\epsilon s_i}{c_*} - \tilde{c}) \tilde{s} - k_{-1} t_* (\frac{\epsilon s_i}{c_*} - \tilde{c}) \tilde{s} - k_2 t_* \tilde{c} + k_{-2} t_* p_* (\frac{\epsilon s_i}{c_*} - \tilde{c}) \tilde{p}$$

p equation

$$\frac{p_*}{t_*} \frac{d\tilde{p}}{d\tilde{t}} = k_2 c_* \tilde{c} - k_{-2} (\epsilon s_i - c_* \tilde{c}) p_* \tilde{p}$$
$$\frac{d\tilde{p}}{d\tilde{t}} = k_2 \frac{t_* c_*}{p_*} \tilde{c} - k_{-2} (\epsilon s_i - c_* \tilde{c}) t_* \tilde{p}$$

Let $c_* = \epsilon s_i$. The system becomes:

$$\begin{split} \frac{d\tilde{s}}{d\tilde{t}} &= -t_* k_1 \epsilon s_i (1-\tilde{c}) \tilde{s} + k_{-1} t_* \epsilon \tilde{c} \\ \frac{d\tilde{c}}{d\tilde{t}} &= k_1 t_* s_i (1-\tilde{c}) \tilde{s} - k_{-1} t_* (1-\tilde{c}) \tilde{s} - k_2 t_* \tilde{c} + k_{-2} t_* p_* (1-\tilde{c}) \tilde{p} \\ \frac{d\tilde{p}}{d\tilde{t}} &= k_2 \frac{t_* c_*}{p_*} \tilde{c} - k_{-2} \epsilon s_i t_* (1-\tilde{c}) \tilde{p} \end{split}$$

Incomplete

(d) Neglect $\mathcal{O}(\epsilon)$ and smaller terms, find the leading order expression for the dimensionless complex concentration, and show that the dimensionless reaction velocity takes form

$$\frac{d\tilde{p}}{d\tilde{t}} = \frac{A_3\tilde{s} - A_1A_2\tilde{p}}{\tilde{s} + A_2\tilde{p} + A_1 + A_3}$$

We have the conservation

$$\frac{d(p+s+c)}{dt} = 0$$

Where A_i are constants Incomplete

(e) Show that to leading order, the steady state of product and substrate concentrations (known as the Haldane relationship) is

$$\frac{\tilde{p}}{\tilde{s}} = \frac{k_1 k_2}{k_{-1} k_{-2}}$$

Incomplete

5. Consider

$$E_1 + S \xrightarrow[k_{-1}]{k_1} C_1 \xrightarrow{k_3} E_1 + P$$

$$E_2 + S \xrightarrow[k_{-2}]{k_2} C_2 \xrightarrow{k_4} E_2 + P$$

(a) Write down the equations for the concentrations of S, E_1, E_2, C_1, C_2, P . Show that there are two conserved quantities and hence reduce the system to 3 equations only containing S, C_1, C_2 .

$$\frac{de_1}{dt} = -k_1 e_1 s + (k_{-1} + k_3) c_1$$

$$\frac{de_2}{dt} = -k_2 e_2 s + (k_{-2} + k_4) c_2$$

$$\frac{dc_1}{dt} = k_1 e_1 s - (k_{-1} + k_3) c_1$$

$$\frac{dc_2}{dt} = k_2 e_2 s - (k_{-2} + k_4) c_2$$

$$\frac{ds}{dt} = -k_1 e_1 s - k_2 e_2 s + k_{-1} c_1 + k_{-2} c_2$$

$$\frac{dp}{dt} = k_3 c_1 + k_4 c_2$$

Clearly, by adding the equations,

$$\frac{d(e_1 + c_1)}{dt} = 0$$

$$\frac{d(e_2 + c_2)}{dt} = 0$$

And the p equation is redundant since

$$\frac{d(c_1+c_2+s+p)}{dt}=0$$

And hence the system can reduce to

$$\frac{dc_1}{dt} = k_1 e_1 s - (k_{-1} + k_3) c_1$$

$$\frac{dc_2}{dt} = k_2 e_2 s - (k_{-2} + k_4) c_2$$

$$\frac{ds}{dt} = -k_1 e_1 s - k_2 e_2 s + k_{-1} c_1 + k_{-2} c_2$$

(b) Assume

$$s(0) = s_i > 0$$
, $e_1(0) = e_2(0) = e_i = \epsilon s_i > 0$

Non-dimensionalise to get a system of form

$$\frac{ds}{dt} = -s(1+\alpha) + c_1(\mu_1 + s) + \alpha c_2(\mu_2 + s)$$

$$\epsilon \frac{dc_1}{dt} = s(1-c_1) - \lambda_1 c_1$$

$$\epsilon \frac{dc_2}{dt} = \alpha \left[s(1-c_2) - \lambda_2 c_2 \right]$$

Defining the parameters in terms of the original dimensionless parameters By using $e_1 = e_i - c_1$ and $e_2 = e_i - c_2$ Let

$$s = s_* \tilde{s}, \quad c_1 = c_1^* \tilde{c}_1, \quad c_2 = c_2^* \tilde{c}_2, \quad t = t^* \tilde{t}$$

$$\begin{split} \frac{ds}{dt} &= -k_1e_1s - k_2e_2s + k_{-1}c_1 + k_{-2}c_2 \\ &= -k_1(e_i - c_1)s - k_2(e_i - c_2)s + k_{-1}c_1 + k_{-2}c_2 \\ &= -k_1e_is + k_1c_1s - k_2e_is + k_2c_2s + k_{-1}c_1 + k_{-2}c_2 \\ &= -s(e_ik_1 + e_ik_2) + c_1(k_{-1} + k_1s) + c_2(k_{-2} + k_2s) \\ &= -se_ik_1(1 + \frac{k_2}{k_1}) + k_1c_1(\frac{k_{-1}}{k_1} + s) + k_2c_2(\frac{k_{-2}}{k_2} + s) \\ \frac{s_*}{t^*} \frac{d\tilde{s}}{d\tilde{t}} &= -s_*\tilde{s}e_ik_1(1 + \frac{k_2}{k_1}) + k_1c_1^*\tilde{c}_1(\frac{k_{-1}}{k_1} + s_*\tilde{s}) + k_2c_2^*\tilde{c}_2(\frac{k_{-2}}{k_2} + s_*\tilde{s}) \\ \frac{d\tilde{s}}{d\tilde{t}} &= -t^*\tilde{s}e_ik_1(1 + \frac{k_2}{k_1}) + t^*k_1c_1^*\tilde{c}_1(\frac{k_{-1}}{k_1s_*} + \tilde{s}) + t^*k_2c_2^*\tilde{c}_2(\frac{k_{-2}}{k_2s_*} + \tilde{s}) \end{split}$$

Letting $t^* = \frac{1}{e_i k_1}$ gives

$$\frac{d\tilde{s}}{d\tilde{t}} = -\tilde{s}(1 + \frac{k_2}{k_1}) + \frac{1}{e_i}c_1^*\tilde{c}_1(\frac{k_{-1}}{k_1s_*} + \tilde{s}) + \frac{1}{e_ik_1}k_2c_2^*\tilde{c}_2(\frac{k_{-2}}{k_2s_*} + \tilde{s})$$

Letting $c_1^* = e_i$, and $\frac{k_2}{k_1} =: \alpha$

$$\frac{d\tilde{s}}{d\tilde{t}} = -\tilde{s}(1+\alpha) + \tilde{c}_1(\frac{k_{-1}}{k_1 s_*} + \tilde{s}) + \frac{1}{e_i}\alpha c_2^* \tilde{c}_2(\frac{k_{-2}}{k_2 s_*} + \tilde{s})$$

Letting $c_2^* = e_i$ gives

$$\frac{d\tilde{s}}{d\tilde{t}} = -\tilde{s}(1+\alpha) + \tilde{c}_1(\frac{k_{-1}}{k_1 s_*} + \tilde{s}) + \alpha \tilde{c}_2(\frac{k_{-2}}{k_2 s_*} + \tilde{s})$$

Considering the c equations:

$$\frac{dc_1}{dt} = k_1 e_1 s - (k_{-1} + k_3) c_1
= k_1 (e_i - c_1) s - (k_{-1} + k_3) c_1
e_i^2 k_1 \frac{d\tilde{c}_1}{d\tilde{t}} = k_1 (e_i - e_i \tilde{c}_1) s_* \tilde{s} - (k_{-1} + k_3) e_i \tilde{c}_1
e_i \frac{d\tilde{c}_1}{d\tilde{t}} = (1 - \tilde{c}_1) s_* \tilde{s} - \frac{(k_{-1} + k_3)}{k_1} \tilde{c}_1
\frac{e_i}{s_*} \frac{d\tilde{c}_1}{d\tilde{t}} = \tilde{s} (1 - \tilde{c}_1) - \frac{(k_{-1} + k_3)}{k_1 s_*} \tilde{c}_1$$

The c_2 equation

$$\begin{split} \frac{dc_2}{dt} &= k_2 e_2 s - (k_{-2} + k_4) c_2 \\ &= k_2 (e_i - c_2) s - (k_{-2} + k_4) c_2 \\ e_i^2 k_1 \frac{d\tilde{c}_2}{d\tilde{t}} &= k_2 (e_i - e_i \tilde{c}_2) s_* \tilde{s} - (k_{-2} + k_4) e_i \tilde{c}_2 \\ e_i \frac{d\tilde{c}_2}{d\tilde{t}} &= \frac{k_2}{k_1} (1 - \tilde{c}_2) s_* \tilde{s} - \frac{(k_{-2} + k_4)}{k_1} \tilde{c}_2 \\ \frac{e_i}{s_*} \frac{d\tilde{c}_2}{d\tilde{t}} &= \alpha \left((1 - \tilde{c}_2) \tilde{s} - \frac{(k_{-2} + k_4)}{k_2 s_*} \tilde{c}_2 \right) \end{split}$$

Using $s_* = s_i$ and $e_i = \epsilon s_i$ gives, for the c equations:

$$\epsilon \frac{d\tilde{c}_1}{d\tilde{t}} = \tilde{s}(1 - \tilde{c}_1) - \frac{(k_{-1} + k_3)}{k_1 s_i} \tilde{c}_1$$

$$\epsilon \frac{d\tilde{c}_2}{d\tilde{t}} = \alpha \left((1 - \tilde{c}_2)\tilde{s} - \frac{(k_{-2} + k_4)}{k_2 s_i} \tilde{c}_2 \right)$$

And letting

$$\lambda_1 = \frac{k_{-1} + k_3}{k_1 s_i}, \quad \lambda_2 = \frac{k_{-2} + k_4}{k_2 s_i}$$

Finally gives (dropping tildes)

$$\epsilon \frac{dc_1}{dt} = s(1 - c_1) - \lambda_1 c_1$$
$$\epsilon \frac{dc_2}{dt} = \alpha \left[s(1 - c_2) - \lambda_2 c_2 \right]$$

Returning to the s equation

$$\frac{d\tilde{s}}{d\tilde{t}} = -\tilde{s}(1+\alpha) + \tilde{c}_1(\frac{k_{-1}}{k_1 s_i} + \tilde{s}) + \alpha \tilde{c}_2(\frac{k_{-2}}{k_2 s_i} + \tilde{s})$$

And letting

$$\mu_1 = \frac{k_{-1}}{k_1 s_i}, \quad \mu_2 = \frac{k_{-2}}{k_2 s_i}$$

Gives (dropping the tildes)

$$\frac{ds}{dt} = -s(1+\alpha) + c_1(\mu_1 + s) + \alpha c_2(\mu_2 + s)$$

I.e. we have the system

$$\frac{ds}{dt} = -s(1+\alpha) + c_1(\mu_1 + s) + \alpha c_2(\mu_2 + s)$$

$$\epsilon \frac{dc_1}{dt} = s(1-c_1) - \lambda_1 c_1$$

$$\epsilon \frac{dc_2}{dt} = \alpha \left[s(1-c_2) - \lambda_2 c_2 \right]$$

Where

$$\alpha = \frac{k_2}{k_1}, \quad \mu_1 = \frac{k_{-1}}{k_1 s_i}, \quad \mu_2 = \frac{k_{-2}}{k_2 s_i}, \quad \lambda_1 = \frac{k_{-1} + k_3}{k_1 s_i}, \quad \lambda_2 = \frac{k_{-2} + k_4}{k_2 s_i}$$

(c) Find leading order solutions for c_1, c_2 and hence s (technology is allowed) To leading order, take perturbation series:

$$c_1 = c_{10} + c_{11}\epsilon + \dots$$

 $c_2 = c_{20} + c_{21}\epsilon + \dots$
 $s = s_0 + s_1\epsilon + \dots$

Where $\epsilon \ll 1$. The leading order system is:

$$\frac{ds_0}{dt} = -s_0(1+\alpha) + c_{10}(\mu_1 + s_0) + \alpha c_{20}(\mu_2 + s_0)$$
$$0 = s_0(1-c_{10}) - \lambda_1 c_{10}$$
$$0 = \alpha \left[s_0(1-c_{20}) - \lambda_2 c_{20} \right]$$

Solve the last two:

$$0 = s_0(1 - c_{10}) - \lambda_1 c_{10}$$
$$s_0 c_{10} + \lambda_1 c_{10} = s_0$$
$$c_{10} = \frac{s_0}{s_0 + \lambda_1}$$

$$0 = s_0(1 - c_{20}) - \lambda_2 c_{20}$$
$$c_{20} = \frac{s_0}{s_0 + \lambda_2}$$

And use in the first equation:

$$\frac{ds_0}{dt} = -s_0(1+\alpha) + c_{10}(\mu_1 + s_0) + \alpha c_{20}(\mu_2 + s_0)$$
$$= -s_0(1+\alpha) + \frac{s_0}{s_0 + \lambda_1}(\mu_1 + s_0) + \alpha \frac{s_0}{s_0 + \lambda_2}(\mu_2 + s_0)$$

$$\int s_0(1+\alpha) - \frac{s_0}{s_0 + \lambda_1}(\mu_1 + s_0) - \alpha \frac{s_0}{s_0 + \lambda_2}(\mu_2 + s_0) ds = \int dt$$

$$\frac{1}{2}s_0^2(1+\alpha) + s_0(\lambda_1 - \mu_1) + s_0\alpha(\lambda_2 - \mu_2) - \alpha\lambda_2\log(\lambda_2 + s_0)(\lambda_2 - \mu_2) - \frac{1}{2}\alpha s_0^2 + \lambda_1\log(\lambda_1 + s_0)(-\lambda_1 + \mu_1) - \frac{1}{2}s_0^2 = k$$

$$s_0(\lambda_1 - \mu_1) + s_0 \alpha(\lambda_2 - \mu_2) - \alpha \lambda_2 \log(\lambda_2 + s_0)(\lambda_2 - \mu_2) + \lambda_1 \log(\lambda_1 + s_0)(-\lambda_1 + \mu_1) = k$$

Where k would be obtained using $s(0) = s_i$. This is an implicit solution in s_0 . Solved the integrals using MATLAB

- 1 syms s lambda1 lambda2 mu1 mu2 a
- $_{2}$ p1 = int(s*(1+a),s)
- $_{3}$ p2 = int(s*(mu1+s)/(s+lambda1),s)
- $_{4}$ p3 = int (a*s*(mu2+s)/(s+lambda2),s)
- (d) Rescale time and find the inner solutions for s, c_1, c_2 Rescale time so that $T = \frac{t}{\epsilon}$

$$\frac{d}{dt} = \frac{\partial T}{\partial t} \frac{\partial}{\partial T} = \frac{1}{\epsilon} \frac{\partial}{\partial T}$$

Giving (to leading order) for the inner solutions:

$$\frac{1}{\epsilon} \frac{ds_0}{dT} = -s_0(1+\alpha) + c_{10}(\mu_1 + s_0) + \alpha c_{20}(\mu_2 + s_0)
\frac{\partial c_1}{\partial T} = s_0(1-c_{10}) - \lambda_1 c_{10}
\frac{\partial c_2}{\partial T} = \alpha \left[s_0(1-c_{20}) - \lambda_2 c_{20} \right]$$

And hence

$$\begin{aligned}
\frac{ds_0}{dT} &= 0\\ \frac{\partial c_1}{\partial T} &= s_0(1 - c_{10}) - \lambda_1 c_{10}\\ \frac{\partial c_2}{\partial T} &= \alpha \left[s_0(1 - c_{20}) - \lambda_2 c_{20} \right]
\end{aligned}$$

Trivially $s_0(T) = s_i$

$$\frac{\partial c_1}{\partial T} = s_0 (1 - c_{10}) - \lambda_1 c_{10}$$

$$\frac{\partial c_1}{\partial T} = s_i (1 - c_{10}) - \lambda_1 c_{10}$$

$$\frac{1}{s_i (1 - c_{10}) - \lambda_1 c_{10}} dc_1 = \int dT$$

Let
$$u = s_i(1 - c_{10}) - \lambda_1 c_{10}$$
, $du = -\lambda_1 - s_i dc_1$

$$\frac{1}{s_i(1-c_{10})-\lambda_1c_{10}}dc_1 = \int dT$$

$$-\frac{1}{s_i+\lambda_1}\int \frac{1}{u}du = T+a$$

$$-\frac{1}{s_i+\lambda_1}\log(u) = T+a$$

$$-\frac{1}{s_i+\lambda_1}\log(s_i(1-c_{10})-\lambda_1c_{10}) = T+a\log(s_i(1-c_{10})-\lambda_1c_{10}) = -T(s_i+\lambda_1)+b$$

$$s_i(1-c_{10})-\lambda_1c_{10} = e^{-T(s_i+\lambda_1)+b}c_{10} = k_1e^{-T(s_i+\lambda_1)} + \frac{s_i}{s_i+\lambda_1}$$

For the inner c_2 equation, the outcome is very similar:

$$\frac{\partial c_2}{\partial T} = \alpha \left[s_i (1 - c_{20}) - \lambda_2 c_{20} \right] \log(s_i (1 - c_{20}) - \lambda_2 c_{20}) = -Tc(s_i + \lambda_2) + a$$

$$c_{20} = k_2 e^{-Tc(s_0 + \lambda_2)} + \frac{s_i}{s_i + \lambda_2}$$

The full solution could be obtained using a matching condition, but this would be difficult since the outer solution for s is implicit.